

**SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE
PORTSMOUTH, NEW HAMPSHIRE**

**CONFERENCE ROOM A
CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE**

*Members of the public also have the option to join the meeting over Zoom
(See below for more details)**

2:00 PM

August 1, 2023

AGENDA

I. APPROVAL OF MINUTES

- A. Approval of minutes from the July 5, 2023 Site Plan Review Technical Advisory Committee Meeting.

II. NEW BUSINESS

- A. The request of **Clyde Logue (Owner)**, for property located at **27 Shaw Road** requesting Lot line Relocation and Subdivision as follows: Tax Map 223 Lot 18 decreasing from 34,205 square feet and 230 feet of frontage to 20, 1999 square feet and 129 feet of frontage; Map 223 Lot 18-1 decreasing from 23,149 square feet and 127 feet of frontage to 21, 241 square feet and 101 feet of frontage; and creation of a new lot with a lot area of 15,812 square feet and 101 feet of frontage. Said property is located on Assessor Map 223 Lot 18 and lies within the Single Residence B (SRB) District. (LU-23-102)
- B. The request of **Lonza Biologics (Owner)**, for property located at **101 International Drive** requesting to amend the Master Plan to reduce the overall square footage to 800,000 square feet in three buildings and reduce the height of building #1 from 3 stories to 1 story. Amended site plan approval for Phase 2 which includes fit-up of Building #1 and the utility building, construction of a temporary surface parking lot and gravel area for construction trailers, parking, and laydown area. Said property is located on Assessor Map 305 Lot 6 and lies within the Airport Business Commercial (ABC) District. (LU-23-108)
- C. The request of **Banfield Realty LLC (Owner)**, for property located at **375 Banfield Road** Preliminary and Final Subdivision approval to subdivide one lot into two lots to create the following: Proposed Lot 1 with 6.65 acres of lot area and 354 feet of street frontage and Proposed Lot 2 with 7.96 acres of lot area and 200 feet of street frontage. Said property is located on Assessor Map 266 Lot 7 and lies within the Industrial (I) District. (LU-23-107)

- D.** The request of **JKM Realty LLC (Owner)**, for property located at **700 Peverly Hill Road** requesting Site Plan Approval for construction of a 3,385 square foot addition to an existing commercial building with associated site improvements. Said property is located on Assessor Map 252 Lot 2-10 and lies within the Industrial (I) District. (LU-23-109)

III. OTHER BUSINESS

IV. ADJOURNMENT

https://us06web.zoom.us/webinar/register/WN_qmpQ3vBzSDiXAJumbMT74Q

**SITE PLAN REVIEW TECHNICAL ADVISORY COMMITTEE
PORTSMOUTH, NEW HAMPSHIRE**

**CONFERENCE ROOM A
CITY HALL, MUNICIPAL COMPLEX, 1 JUNKINS AVENUE**

2:00 PM

July 5, 2023

MINUTES

MEMBERS PRESENT:

Peter Stith, Chairperson, Planning Manager; David Desfosses, Construction Technician Supervisor; Patrick Howe, Deputy Fire Chief; Shanti Wolph, Chief Building Inspector; Peter Britz, Planning & Sustainability Director; Zachary Cronin, Assistant City Engineer, Eric Eby, Parking and Transportation Engineer; Mike Maloney; Deputy Police Chief

MEMBERS ABSENT:

ADDITIONAL

STAFF PRESENT:

Stefanie Casella, Planner II; Kate Homet, Associate Environmental Planner

[4:26] Chairman Stith called the meeting to order at 2:00 p.m.

I. APPROVAL OF MINUTES

- A. Approval of minutes from the June 6, 2023 Site Plan Review Technical Advisory Committee Meeting.

[4:45] P. Howe made a motion to approve the minutes as presented. Z. Cronin seconded the motion. The motion passed unanimously with P. Britz abstaining from the vote.

II. NEW BUSINESS

- A. The request of **Aviation Avenue Group LLC (Applicant)**, for property located at **80 Rochester Avenue (100 New Hampshire Avenue)** requesting Amended Site Plan Approval for construction of a 101,200 sq. ft. footprint including 4,700 sq. ft. of office space and associated site improvements consisting of parking, loading docks, underground utilities, landscaping, lighting, and a stormwater management system.

Said property is located on Assessor Map 308 Lot 1 and lies within the Pease Industrial (PI) District. (LU-22-210)

SPEAKING TO THE APPLICATION

[5:35] Neil Hansen (Tighe & Bond), Joe Geoghegan and Eben Tormey (Tidemark), John Bosen (Attorney) and Mike Mates (PDA) came to present this application. The applicants are requesting an amended site plan approval due to the applicant having a confirmed tenant to lease the previously approved space. The new tenant requires 101,000 s.f. building with thirty loading bays in the rear and sixty eight parking spaces on the south end of the site. They are proposing access for passenger vehicles to New Hampshire Avenue and access for trucks onto Rochester Avenue. They are proposing similar stormwater treatment to what was previously approved along with utilities with amended landscaping plans and photometric plans.

Staff comments from the Department of Public Works were addressed and plans were amended for the stormwater which were then sent to Underwood Engineering for a third-party review last week. This review is still in process.

[8:14] Mr. Hansen went on to review and respond to the list of staff comments.

1. *Drainage and stormwater plans will require third party review.*

These have been sent to Underwood.

2. *All work in the right of way and all utility work will require third party inspection.*

These have been sent to Underwood.

3. *Trailer storage stall length must meet trailer length. Move and widen the adjacent driveway so vehicles do not enter the parking lot into trailer storage.*

The length of the trailer storage has increased to 55 ft for 53 ft trailers. An emergency connection has been realigned for fire trucks to drive straight through the site if needed.

4. *In the trailer storage area, increase distance from curb to back of sidewalk to 12'.*

They have pulled that area back and increased the distance to 20 ft.

5. *Change curbing at back of trailer storage from sloped to vertical curbing.*

Noted on the details.

6. *In right of way, use DOT spec 609.01 for vertical granite curb.*

Noted on the details.

7. *In right of way, change sidewalk detail to:*
 - a. *Remove ¾" smooth dowel bar from Expansion Joint B.*
 - b. *Remove rebar from Construction Joint.*
 - c. *Remove sealant from Control Joint A.*
 - d. *30 days after concrete sidewalk sets use siloxane concrete sealer.*

These revisions have been done as requested.

8. *Remove "STOP" lettering behind stop bars at stop signs.*

These have been removed.

9. *Remove truck restriction signage.*

A previous review from the PDA's peer reviewer, VHB, had requested this and they have left it in but are open to discuss the change.

10. *Explain truck access and egress plan.*

See site note #20. Incoming deliveries will access the site from Lee Street via Aviation Avenue and the truck turning exhibit has been revised to show this. They anticipate four large tractor trailers delivering to the site per day, with up to thirty smaller box truck trips to the site per day. This number of vehicle trips is significantly reduced from the previously approved proposal.

11. *Move NH Ave driveway to Newfields Street and line it up to the driveway across the street.*

Applicants asked for additional feedback on this comment, asking for clarification as they felt their proposed alignment was better for fire truck access. E. Eby noted that the proximity to the nearby intersection is quite close. Mr. Hansen noted that there is only a five-foot difference between the Newfields Street driveway and what the applicants are proposing, which is not a significant difference.

12. *Show truck access route leading to Lee Street.*

This has been added to the plan.

13. *Widen truck access driveway to accommodate tractor trailer turning movements.*

A dimension has been added to the plans on Lee Street to show this.

14. *Move PSMH-02 out of the truck access driveway.*

The building connection to sewer manhole one has been shown and sewer manhole two has been removed. D. Desfosses noted that they wanted sewer manhole two to be added back in because

they do not opposing flows going into each other and to move it fifteen feet away so it is not located in the driveway. This will be revised.

15. Show detail for connection of new sewer main to existing sewer main. Fernco connection with paver under pipe for support.

This detail has been added to sheet 506.

16. Show the drainage connection locations of all proposed catch basins.

This has been added to the drainage plans.

17. Replace entire connection of PCB-26 to PDMH-07.

This has been added.

18. Show invert in drain manhole detail similar to sewer manhole detail.

This has been revised.

19. All tapping sleeves must be stainless steel.

This has been added to utility note 10.

20. Domestic and fire services may need to be spaced farther apart. DPW to confirm at time of water connection application.

They acknowledge this and will revise if needed.

21. In the right of way, all electrical primary voltage conduit must be concrete encased.

This has been revised.

22. In electrical conduit detail, fix the leader for the buried cable safety ribbon to point to the cable safety ribbon.

This has been revised.

23. Move trees out of the snow storage area.

This has been addressed.

24. Move trees so they are not on top of the stormwater treatment devices.

This has been addressed.

25. *Move trees out from behind the trailer storage area, or move them so they are in between the parking stalls so as to not get hit by trailers.*

This has been addressed.

26. *Fix typo on "Proposed Emergenc(y) Access Gate" on sheet 102.2.*

This has been fixed.

27. *Colored site plan and other plan sets do not match. Discrepancies include the number of trailer storage spaces, number of parking spaces, and location of emergency access gate.*

This has been updated.

28. *How will the current proposed operations be different from the previously approved advanced manufacturing facility's operations?*

This new proposed facility will be a logistics center with home delivery, this is different because now only a handful of large trucks will be on site with a majority of the trips being done by small box trucks.

29. *Please consider utilizing solar for the roof of this project*

They cannot commit to anything at this time but will look into it.

PUBLIC HEARING

[39:27] Chairman Stith opened up the public hearing portion of this application.

[39:37] Bob Dion, chairman of the Greenland NH Planning Board, came to speak on this application. Mr. Dion asked for clarification on the orientation of the plans and asked to see a map showing exactly where the proposed site was in relation to the rest of Pease, which was provided. He asked for clarification on whether the trucks would be driving by the golf course which they confirmed would occur. He noted that during the work week, there is significant traffic in Greenland and he wanted to know how the proposal would impact traffic on Route 33.

[44:16] Mr. Hansen responded that daily trips would be approximately 288 and the majority of their trips would be during off-peak hours, with approximately five trucks coming into the site during peak hours.

[52:50] Chairman Stith closed the public comment portion of the hearing.

DISCUSSION AND DECISION OF THE BOARD

[53:19] E. Eby asked if the revised plans had been uploaded. Chairman Stith responded that they were available on ViewPoint.

[53:32] D. Desfosses noted that they needed to make a few revisions and that their third party review would have to be in before the Planning Board submission deadline (July 26 for August 17 meeting).

[55:47] D. Desfosses noted that as long as they get the third party response by the first week of August then the Department of Public Works (DPW) should have enough time to review.

[56:28] D. Desfosses made a motion to move this application forward with the conditions that DPW reviews the third party stormwater report and that all other revisions are made based on the comments. P. Howe seconded the motion.

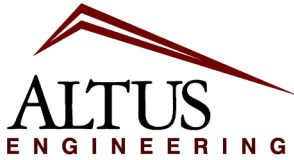
[58:10] The motion passed unanimously.

III. ADJOURNMENT

The meeting adjourned at 2:53 p.m.

Respectfully submitted,

Kate E. Homet
Secretary for the Technical Advisory Committee



**Civil
Site Planning
Environmental
Engineering**

133 Court Street
Portsmouth, NH
03801-4413

July 10, 2023

Peter Britz, Planning and Sustainability Director
City of Portsmouth Municipal Complex
1 Junkins Avenue
Portsmouth, New Hampshire 03801

**Re: Application for Lot Line Adjustment Subdivision Approval
Assessor's Map 223, Lots 18 and 18-1
27 Shaw Road and Walker Bungalow Road
Altus Project No. 5279**

Dear Peter,

On behalf of the Mary Duff (Bonnie) Kastel and Clyde Logue, Altus Engineering respectfully submits an application for Lot Line Adjustment and Subdivision. Bonnie and Clyde intended to complete a lot line adjustment with Lot 18-1 to create frontage on Walker Bungalow Road for the potential of a driveway to the proposed new lot created primarily from Lot 18.

An existing drainage easement that bisects Lot 18 will be relocated along the eastern boundary of the new lot to minimize the potential for impacts to the development area.

It is our intention to fully address the stormwater management required for the new lot so that we can incorporate appropriate measures to ensure that there are no downgradient impacts to abutting properties.

Enclosed please find the following items for consideration at the August 1st TAC Meeting:

- Letter of Authorization
- Subdivision Application Checklist
- Lot Line Adjustment and Subdivision Plans (JBE)
- Stormwater Management Plans (Altus)
- Drainage narrative

Please call or email me directly should you have any questions or need any additional information.

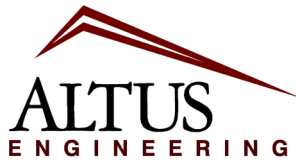
Sincerely,

A handwritten signature in black ink, appearing to read "B. Logue", written over a light blue horizontal line.

wde/5279.00 cvr ltr.docx

Enclosures

eCopy: Bonnie and Clyde Logue
Joe Coronati, JBE



Civil
Site Planning
Environmental
Engineering

133 Court Street
Portsmouth, NH
03801-4413

**Revised Drainage Summary
For
27 Shaw Road
Portsmouth, NH**

Project Description

Bonnie and Clyde are owners of property identified as Assessor’s Map 223, Lot 18 & 18-1, located at 27 Shaw Road. They intended to complete a lot line adjustment with Lot 18-1 to create frontage on Walker Bungalow Road for a driveway to the proposed new lot created primarily from Lot 18.

Site conditions on Lot 18 will remain unchanged except for the removal of 319 square feet of paved driveway, thereby reducing the lot’s runoff. The grass underdrain soil filter (GUSF) on Lot 18-1 was reshaped to accommodate the revised lot configuration. The GUSF a larger infiltration bottom area and storage capacity than previously approved, thereby providing additional stormwater treatment and reducing runoff to the City’s closed drainage system.

It is our intention to fully address the stormwater management required for the new lot, so that we can incorporate appropriate measures to ensure that there are no downgradient impacts to abutting properties.

Drainage Analysis

A complete summary of the drainage model will be provided upon request. The following table compares pre- and post-development peak rates for the 2, 10, 25, and 50-year storm events associated with Lot 18-1 only:

Stormwater Modeling Summary Peak Q (cfs) for Type III 24-Hour Storm Events

*Rainfall Intensities Reflect 15% Increase per AoT	2-Yr Storm (3.69 inch)	10-Yr Storm (5.60 inch)	25-Yr Storm (7.10 inch)	50-Yr Storm (8.50 inch)
POA #1				
Pre	0.65	1.32	1.87	2.39
Post	0.06	0.59	1.36	2.18
Change	-0.59	-0.73	-0.51	-0.21

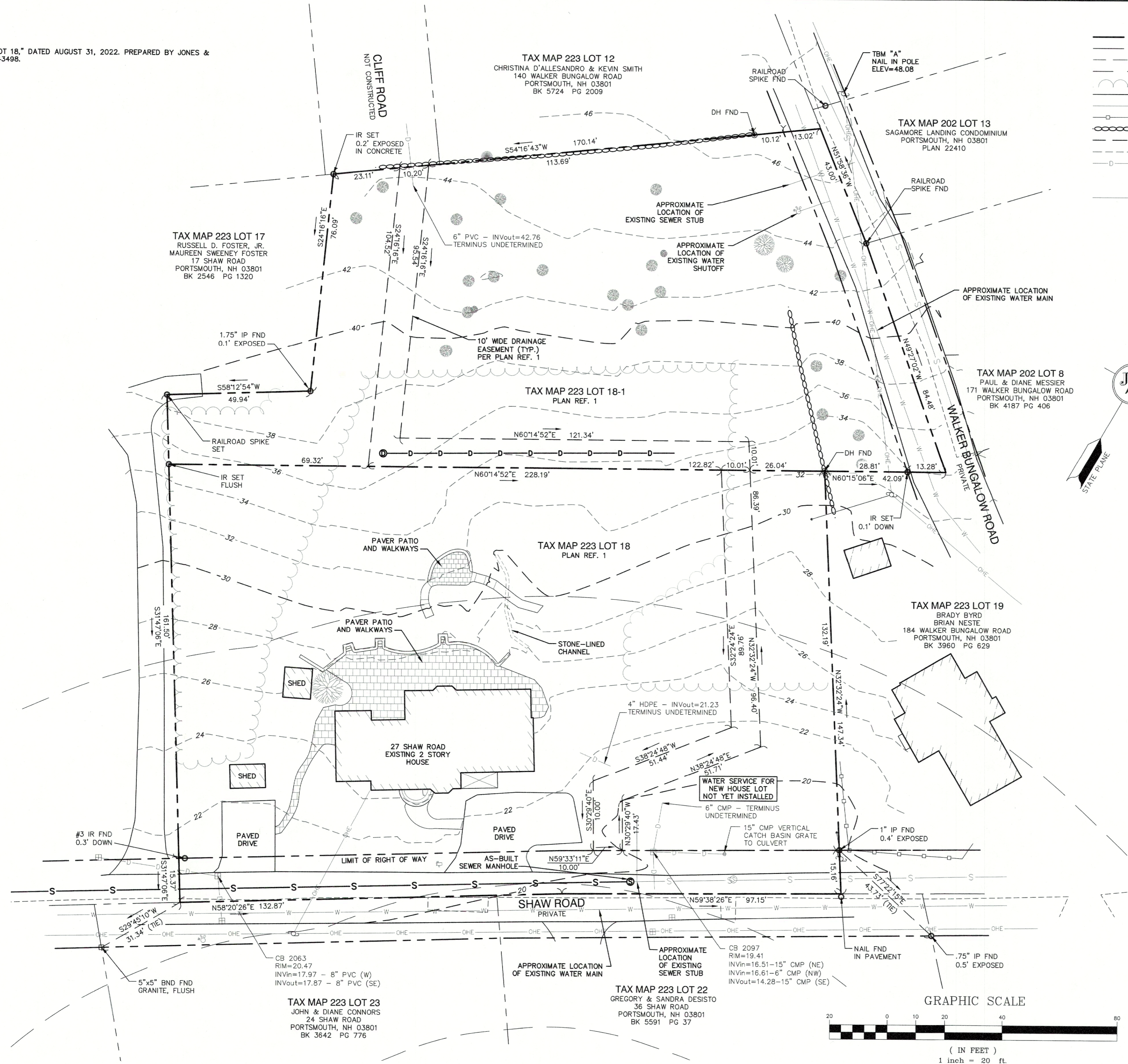
Conclusion

This proposed residential development off Shaw Road in Portsmouth, NH will have minimal adverse effect on abutting properties and infrastructure as a result of stormwater runoff or siltation. Post-construction peak rates of runoff from the site will be lower than the existing conditions for all analyzed storm events. The new stormwater management system will also provide appropriate treatment of runoff from the proposed impervious area. Appropriate steps will be taken to properly mitigate erosion and sedimentation using temporary and permanent Best Management Practices for sediment and erosion control, including vegetated swales and a raingarden.

5279.05 SWM.narrative.docx

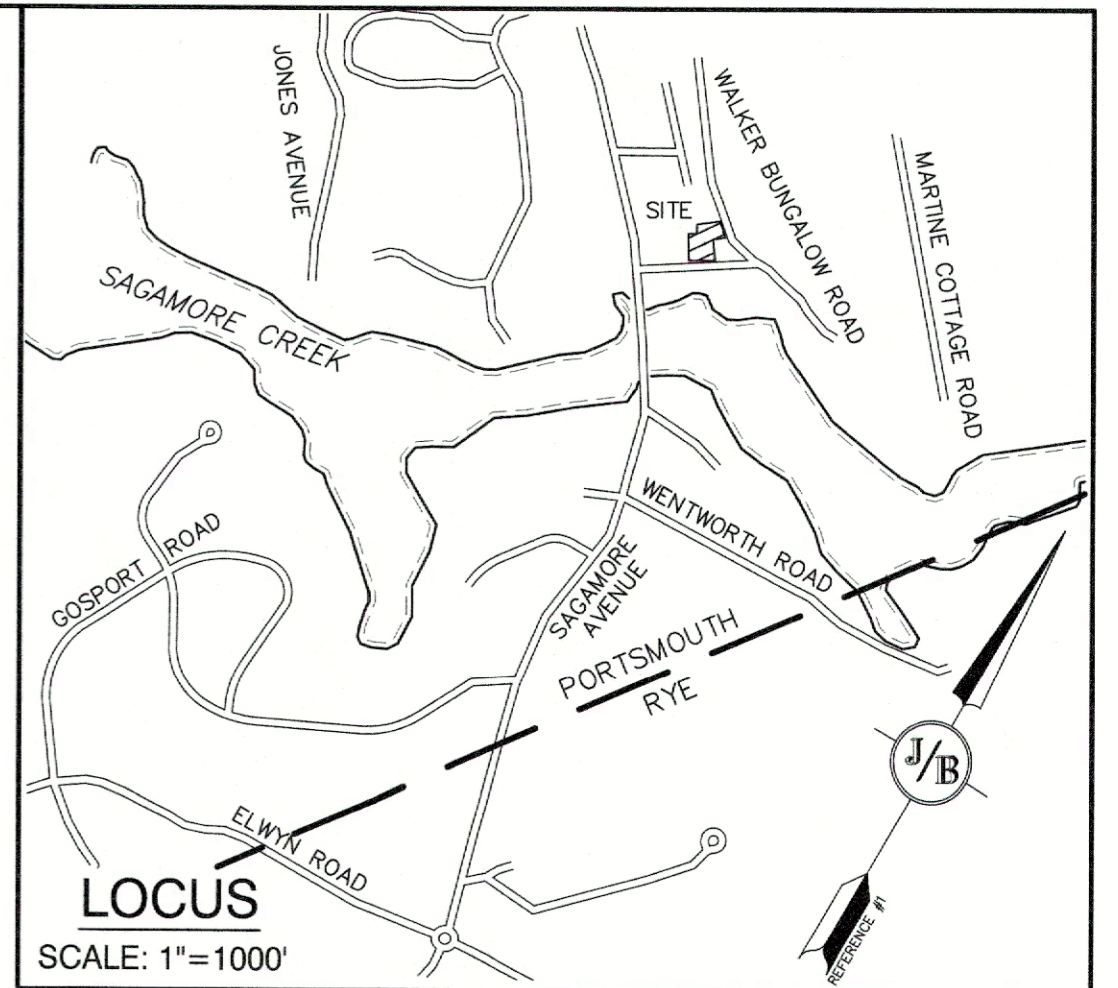
PLAN REFERENCES:

1. "SUBDIVISION PLAN, TAX MAP 223 LOT 18," DATED AUGUST 31, 2022. PREPARED BY JONES & BEACH ENGINEERS, INC. R.C.R.D. D-43498.



LEGEND

- PROPERTY LINE
- - - ABUTTER PROPERTY LINE
- - - BUILDING SETBACK
- - - SURVEY TIE LINES
- - - TREE LINE
- - - EDGE OF PAVEMENT
- - - OVERHEAD ELECTRIC LINES
- - - FENCE
- - - STONE WALL
- - - MAJOR CONTOUR
- - - MINOR CONTOUR
- - - DRAIN LINE
- - - CATCH BASIN
- - - DRAIN MANHOLE
- - - WATER LINE
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- - - UTILITY POLE
- - - GUY WIRE ANCHOR
- - - ELECTRIC METER

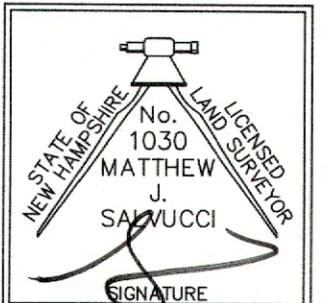


NOTES:

1. THE INTENT OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS OF LOT 18 DEPICTED ON PORTSMOUTH TAX MAP 223.
2. ZONING DISTRICT: SINGLE RESIDENCE B
LOT AREA MINIMUM = 15,000 SF
LOT FRONTAGE MINIMUM = 100'
BUILDING SETBACKS (MINIMUM):
FRONT SETBACK = 30'
SIDE SETBACK = 10'
REAR SETBACK = 30'
WETLAND SETBACK = 100'; LIMITED CUT 50'. (NO WETLANDS OBSERVED)
MAX. BUILDING HEIGHT = 35'
3. THE UTILITY LOCATIONS SHOWN HEREON WERE DETERMINED BY OBSERVED ABOVE GROUND EVIDENCE AND SHOULD BE CONSIDERED APPROXIMATE IN LOCATION ONLY. LOCATION, DEPTH, SIZE, TYPE, EXISTENCE OR NONEXISTENCE OF UNDERGROUND UTILITIES AND/OR UNDERGROUND STORAGE TANKS WAS NOT VERIFIED BY THIS SURVEY. ALL CONTRACTORS SHOULD NOTIFY IN WRITING ALL UTILITY COMPANIES AND GOVERNMENT AGENCIES PRIOR TO ANY EXCAVATION WORK OR CALL DIG-SAFE AT 1-888-DIG-SAFE.
4. THE SUBJECT PARCEL IS NOT LOCATED WITHIN AN AREA HAVING A ZONE DESIGNATION BY THE FEDERAL EMERGENCY MANAGEMENT AGENCY (FEMA), ON FLOOD INSURANCE RATE MAP NO. 33015C0286F, WITH EFFECTIVE DATE OF JANUARY 29, 2021.
5. BASIS OF BEARING: HORIZONTAL - NAD83 NH STATE PLANE.
VERTICAL - NAVD88.
6. CERTAIN DATA HEREON MAY VARY FROM RECORDED DATA DUE TO DIFFERENCES IN DECLINATION, ORIENTATION, AND METHODS OF MEASUREMENT.
7. ALL BOOK AND PAGE NUMBERS REFER TO THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
8. THE TAX MAP AND LOT NUMBERS ARE BASED ON THE CITY OF PORTSMOUTH TAX RECORDS AND ARE SUBJECT TO CHANGE.
9. RESEARCH WAS PERFORMED AT THE CITY OF PORTSMOUTH ASSESSOR'S OFFICE AND PLANNING OFFICE, AND THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
10. THIS SURVEY IS NOT A CERTIFICATION TO OWNERSHIP OR TITLE OF LANDS SHOWN. OWNERSHIP AND ENCUMBRANCES ARE MATTERS OF TITLE EXAMINATION NOT OF A BOUNDARY SURVEY. THE INTENT OF THIS PLAN IS TO RETRACE THE BOUNDARY LINES OF DEEDS REFERENCED HEREON. OWNERSHIP OF ADJOINING PROPERTIES IS ACCORDING TO ASSESSOR'S RECORDS. THIS PLAN MAY OR MAY NOT INDICATE ALL ENCUMBRANCES EXPRESSED, IMPLIED OR PRESCRIPTIVE.
11. ANY USE OF THIS PLAN AND OR ACCOMPANYING DESCRIPTIONS SHOULD BE DONE WITH LEGAL COUNSEL, TO BE CERTAIN THAT TITLES ARE CLEAR, THAT INFORMATION IS CURRENT, AND THAT ANY NECESSARY CERTIFICATES ARE IN PLACE FOR A PARTICULAR CONVEYANCE, OR OTHER USES.
12. NO WETLANDS WERE OBSERVED ON THE SUBJECT PREMISES.
13. SURVEY TIE LINES SHOWN HEREON ARE NOT BOUNDARY LINES. THEY SHOULD ONLY BE USED TO LOCATE THE PARCEL SURVEYED FROM THE FOUND MONUMENTS SHOWN AND LOCATED BY THIS SURVEY.
14. SHAW ROAD AND WALKER BUNGALOW ROAD ARE PRIVATE WAYS. RECORD DEEDS AND PLANS INDICATE A RIGHT OF WAY WIDTH OF THIRTY FEET FOR SHAW ROAD. NO WIDTH IS INDICATED FOR WALKER BUNGALOW ROAD. THE BOUNDARY LINE OF THE SUBJECT PARCEL HAS BEEN HELD AS THE CENTER OF SAID WAYS.

CERTIFICATION:

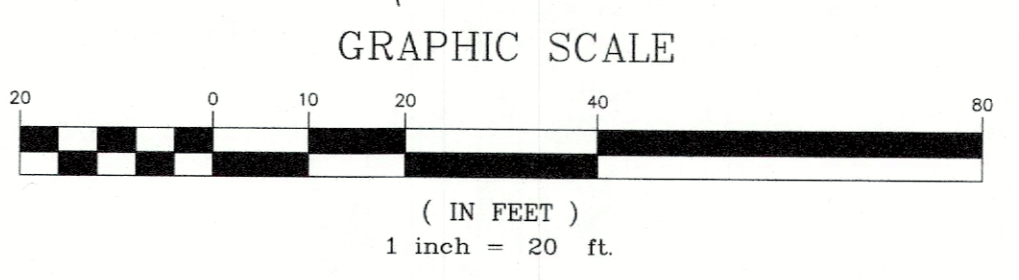
PURSUANT TO RSA 676:18-III AND RSA 672:14
I CERTIFY THAT THIS SURVEY PLAT IS NOT A SUBDIVISION PURSUANT TO THIS TITLE AND THAT THE LINES OF STREETS AND WAYS SHOWN ARE THOSE OF PUBLIC OR PRIVATE STREETS OR WAYS ALREADY ESTABLISHED AND THAT NO NEW WAYS ARE SHOWN.
I CERTIFY THAT THIS PLAT WAS PREPARED UNDER MY DIRECT SUPERVISION, THAT IT IS THE RESULT OF A FIELD SURVEY BY THIS OFFICE AND HAS AN UNADJUSTED LINEAR ERROR OF CLOSURE THAT EXCEEDS BOTH THE MINIMUM OF 1:10,000 AS DEFINED IN SECTION 503.04 OF THE NEW HAMPSHIRE CODE OF ADMINISTRATIVE RULES AND THE MINIMUM OF 1:15,000 AS DEFINED IN SECTION 4.2 OF THE N.H.L.S.A. ETHICS AND STANDARDS.
THIS SURVEY CONFORMS TO A CATEGORY 1 CONDITION 1 SURVEY AS DEFINED IN SECTION 4.1 OF THE N.H.L.S.A. ETHICS AND STANDARDS.



MATTHEW J. SALVUCCI, LLS 1030
ON BEHALF OF JONES & BEACH ENGINEERS, INC.

7/5/23
DATE:

TOTAL LOT AREA
57,354 SQ. FT.
1.32 ACRES



Design: JAC	Draft: MJS	Date: 11/18/21
Checked: JAC	Scale: 1"=20'	Project No.: 21222
Drawing Name: 21222-PLAN.dwg		
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.		

REV.	DATE	REVISION	BY
9	6/14/23	UPDATED EXISTING DRAINAGE	DJM
8	6/6/23	UPDATED EXISTING CONDITIONS PLAN	DJM
7	5/26/23	AMENDED SUBDIVISION PLAN	DJM
6	6/23/22	REMOVED HOLDING TANK	DJM
5	6/2/22	ADDED DRAINAGE EASEMENTS	MJS

J/B Jones & Beach Engineers, Inc.
Civil Engineering Services
85 Portsmouth Ave. PO Box 219 Stratham, NH 03885
603-772-4746
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM




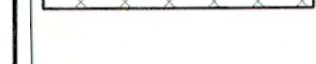
Plan Name:	EXISTING CONDITIONS PLAN
Project:	PROPOSED SUBDIVISION 27 SHAW ROAD, PORTSMOUTH, NH
Owner of Record:	CLYDE LOGUE & MARY DUFF KASTEL 27 SHAW RD., PORTSMOUTH, NH 03801 BK 6455 PG 1068

DRAWING No.	C1
SHEET 1 OF 2	
JBE PROJECT NO. 21222	









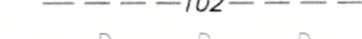




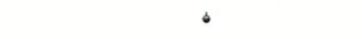





PLAN REFERENCES:

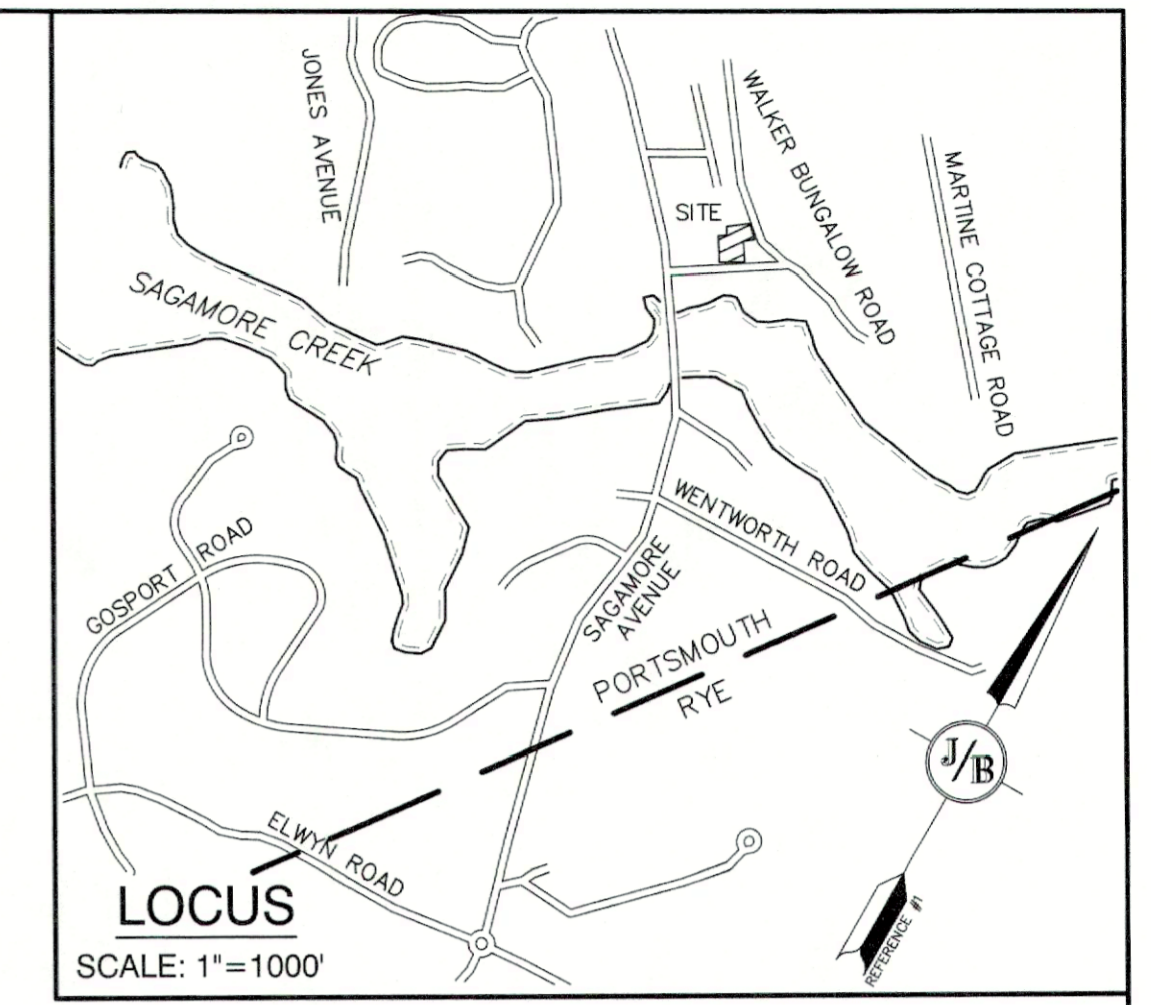
- "SUBDIVISION PLAN, TAX MAP 223 LOT 18," DATED AUGUST 31, 2022. PREPARED BY JONES & BEACH ENGINEERS, INC. R.C.R.D. D-43498.

EASEMENT CHANGES

-  EXISTING EASEMENT ON LOT 18-1 TO REMAIN
-  EXISTING EASEMENT ON LOT 18-1 TO BE REDEEDED TO LOT 18-0-1
-  EXISTING EASEMENT TO BE RELOCATED ON LOT 18-0-1
-  PROPOSED RELOCATED EASEMENT ON LOT 18-0-1

LEGEND

-  EXISTING PROPERTY LINE
-  PROPOSED PROPERTY LINE
-  ABUTTER PROPERTY LINE
-  BUILDING SETBACK
-  SURVEY TIE LINES
-  TREE LINE
-  EDGE OF PAVEMENT
-  OVERHEAD ELECTRIC LINES
-  STONE WALL
-  MAJOR CONTOUR
-  MINOR CONTOUR
-  DRAIN LINE
-  CATCH BASIN
-  DRAIN MANHOLE
-  WATER LINE
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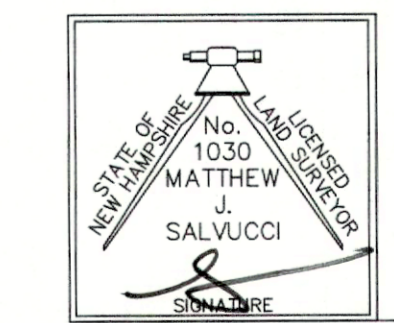


NOTES:

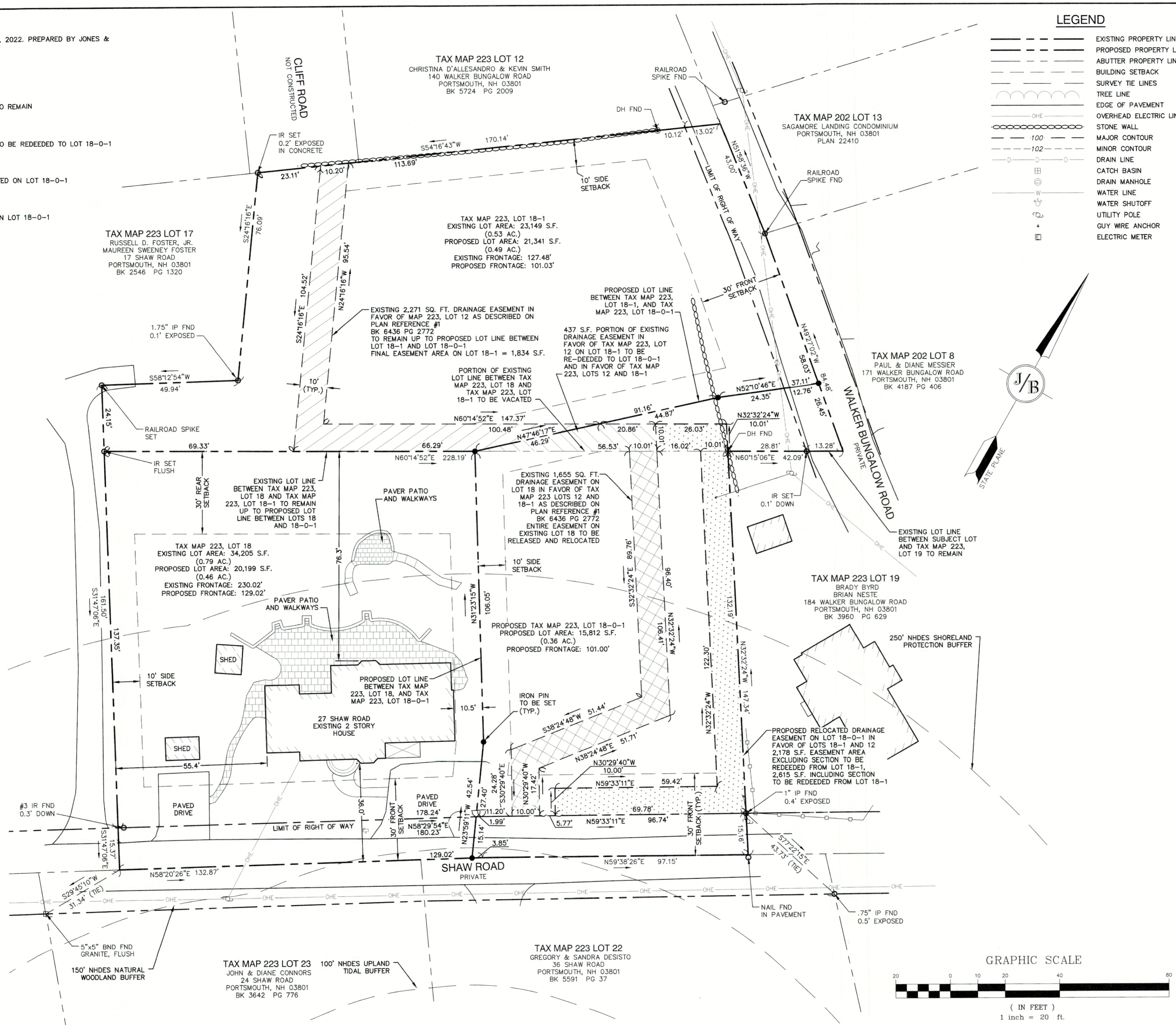
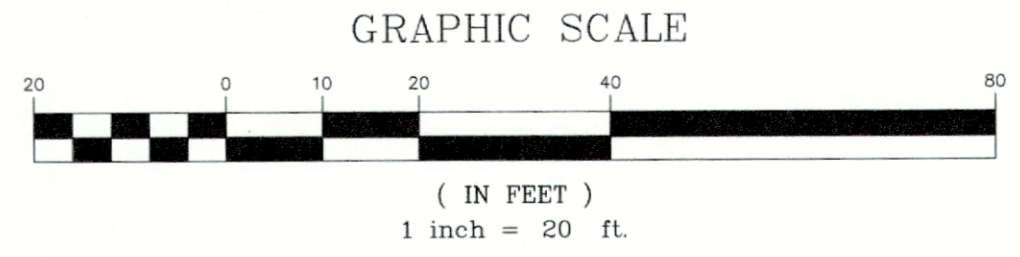
- THE INTENT OF THIS PLAN IS TO ADJUST THE LOT LINE BETWEEN LOTS 18 AND 18-1 AS DEPICTED ON PORTSMOUTH TAX MAP 223, AND THEN SUBDIVIDE LOT 18. EACH WILL BE SERVICED BY CITY WATER AND SEWER.
- ZONING DISTRICT: SINGLE RESIDENCE B
LOT AREA MINIMUM = 15,000 SF
LOT FRONTAGE MINIMUM = 100'
BUILDING SETBACKS (MINIMUM):
FRONT SETBACK = 30'
SIDE SETBACK = 30'
REAR SETBACK = 30'
WETLAND SETBACK = 100', LIMITED CUT 50'. (NO WETLANDS OBSERVED)
MAX. BUILDING HEIGHT = 35'
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- CERTAIN DATA HEREON MAY VARY FROM RECORDED DATA DUE TO DIFFERENCES IN DECLINATION, ORIENTATION, AND METHODS OF MEASUREMENT.
- ALL BOOK AND PAGE NUMBERS REFER TO THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
- THE TAX MAP AND LOT NUMBERS ARE BASED ON THE CITY OF PORTSMOUTH TAX RECORDS AND ARE SUBJECT TO CHANGE.
- RESEARCH WAS PERFORMED AT THE CITY OF PORTSMOUTH ASSESSOR'S OFFICE AND PLANNING OFFICE, AND THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
- THIS SURVEY IS NOT A CERTIFICATION TO OWNERSHIP OR TITLE OF LANDS SHOWN. OWNERSHIP AND ENCUMBRANCES ARE MATTERS OF TITLE EXAMINATION NOT OF A BOUNDARY SURVEY. THE INTENT OF THIS PLAN IS TO REINSTATE THE BOUNDARY LINES OF DEEDS REFERENCED HEREON. OWNERSHIP OF ADJOINING PROPERTIES IS ACCORDING TO ASSESSOR'S RECORDS. THIS PLAN MAY OR MAY NOT INDICATE ALL ENCUMBRANCES EXPRESSED, IMPLIED OR PRESCRIPTIVE.
- ANY USE OF THIS PLAN AND OR ACCOMPANYING DESCRIPTIONS SHOULD BE DONE WITH LEGAL COUNSEL, TO BE CERTAIN THAT TITLES ARE CLEAR, THAT INFORMATION IS CURRENT, AND THAT ANY NECESSARY CERTIFICATES ARE IN PLACE FOR A PARTICULAR CONVEYANCE, OR OTHER USES.
- NO WETLANDS WERE OBSERVED ON THE SUBJECT PREMISES.
- SURVEY TIE LINES SHOWN HEREON ARE NOT BOUNDARY LINES. THEY SHOULD ONLY BE USED TO LOCATE THE PARCEL SURVEYED FROM THE FOUND MONUMENTS SHOWN AND LOCATED BY THIS SURVEY.
- SHAW ROAD AND WALKER BUNGALOW ROAD ARE PRIVATE WAYS. RECORD DEEDS AND PLANS INDICATE A RIGHT OF WAY WIDTH OF THIRTY FEET FOR SHAW ROAD. NO WIDTH IS INDICATED FOR WALKER BUNGALOW ROAD. THE BOUNDARY LINE OF THE SUBJECT PARCEL HAS BEEN HELD AS THE CENTER OF SAID WAYS.
- PORTION OF EXISTING DRAINAGE EASEMENT ON LOT 18-1 IS TO REMAIN OR BE REDEEDED TO LOT 18-0-1 AS APPROPRIATE PER LOCATION OF PROPOSED PROPERTY LINE. PORTION OF EXISTING DRAINAGE EASEMENT ON LOT 18 AS INDICATED ON PLAN REFERENCE #1 IS TO BE RELEASED AND NEW DEED FOR EASEMENT ON LOT 18-0-1 IS TO BE RECORDED.

CERTIFICATION:

PURSUANT TO RSA 676:18-III AND RSA 672:14
I CERTIFY THAT THIS PLAN WAS PREPARED UNDER MY DIRECT SUPERVISION, THAT IT IS THE RESULT OF A FIELD SURVEY BY THIS OFFICE AND HAS AN UNADJUSTED LINEAR ERROR OF CLOSURE THAT EXCEEDS BOTH THE MINIMUM OF 1:10,000 AS DEFINED IN SECTION 503.04 OF THE NEW HAMPSHIRE CODE OF ADMINISTRATIVE RULES AND THE MINIMUM OF 1:15,000 AS DEFINED IN SECTION 4.2 OF THE N.H.L.S.A. ETHICS AND STANDARDS.
THIS SURVEY CONFORMS TO A CATEGORY 1 CONDITION 1 SURVEY AS DEFINED IN SECTION 4.1 OF THE N.H.L.S.A. ETHICS AND STANDARDS.



MATTHEW J. SALVUCCI, LLS 1030
ON BEHALF OF JONES & BEACH ENGINEERS, INC. DATE: 7/5/23



TOTAL LOT AREA
57,354 SQ. FT.
1.32 ACRES

APPROVED - PORTSMOUTH, NH
PLANNING BOARD

DATE:

REV.	DATE	REVISION	BY
9	6/14/23	UPDATED EXISTING DRAINAGE	DJM
8	6/6/23	UPDATED EXISTING CONDITIONS PLAN	DJM
7	5/26/23	AMENDED SUBDIVISION PLAN	DJM
6	6/23/22	REMOVED HOLDING TANK	DJM
5	6/2/22	ADDED DRAINAGE EASEMENTS	MJS

Designed and Produced in NH
J/B Jones & Beach Engineers, Inc.
Civil Engineering Services
85 Portsmouth Ave. PO Box 219 Stratham, NH 03885
603-772-4746
FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name: **AMENDED SUBDIVISION AND LOT LINE ADJUSTMENT PLAN**
TAX MAP 223, LOTS 18 & 18-1
Project: **PROPOSED SUBDIVISION**
27 SHAW ROAD, PORTSMOUTH, NH
Owner of Record: **CLYDE LOGUE & MARY DUFF KASTEL**
27 SHAW RD., PORTSMOUTH, NH 03801 BK 6455 PG 1068

DRAWING No.
A1
SHEET 2 OF 2
JBE PROJECT NO. 21222

Design: JAC Draft: MJS Date: 11/18/21
Checked: JAC Scale: 1"=20' Project No.: 21222
Drawing Name: 21222-PLAN.dwg
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

GRADING AND DRAINAGE NOTES

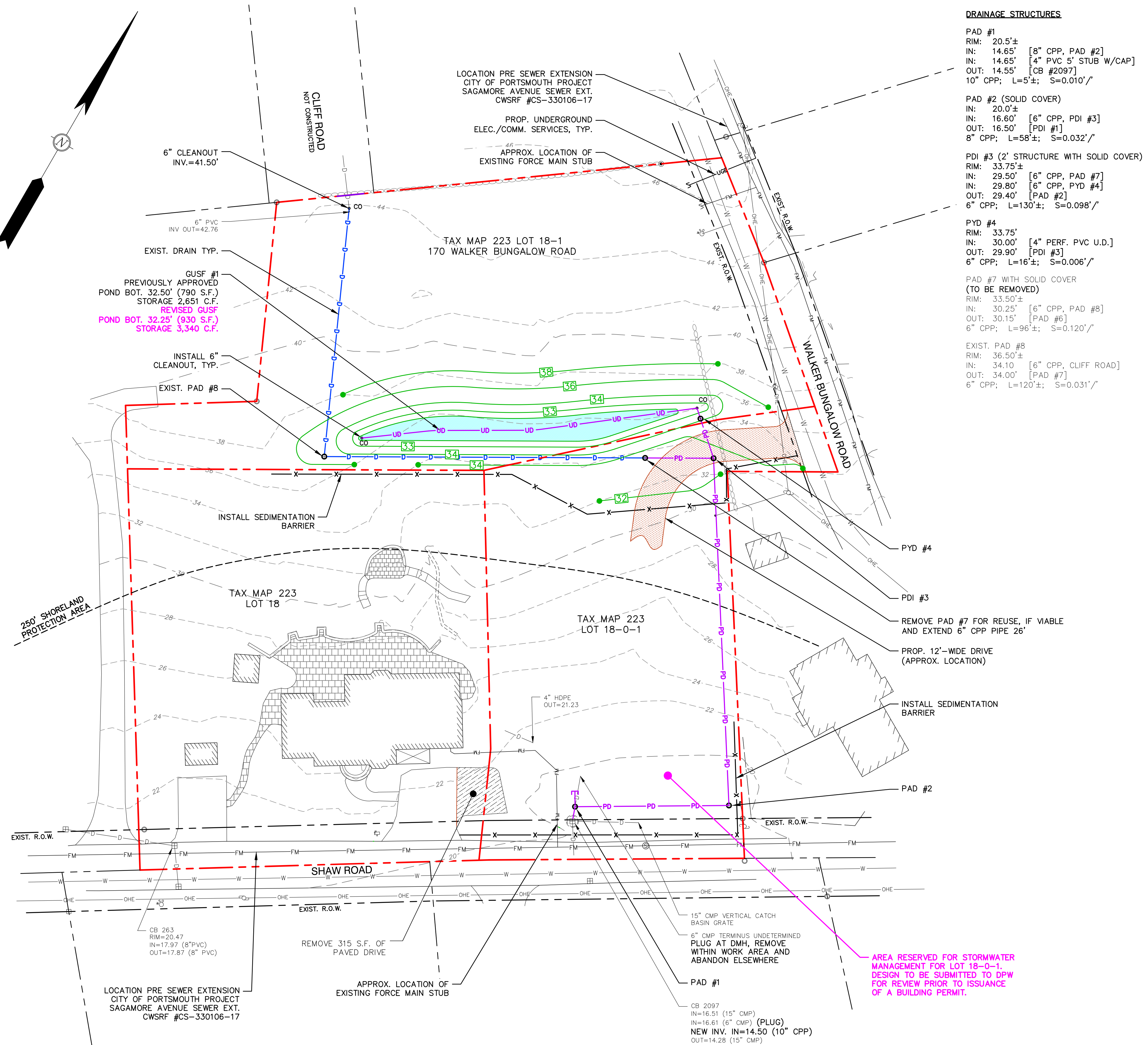
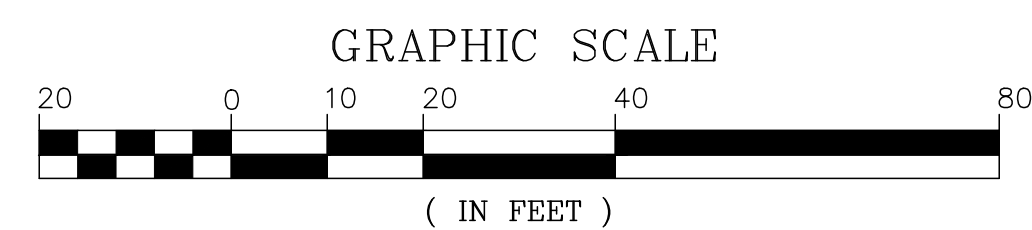
- DO NOT BEGIN CONSTRUCTION UNTIL ALL STATE AND LOCAL PERMITS HAVE BEEN APPLIED FOR AND RECEIVED.
- CONTRACTOR SHALL OBTAIN A "DIGSAFE" NUMBER AT LEAST 72 HOURS PRIOR TO COMMENCING CONSTRUCTION.
- ALL CONSTRUCTION SHALL MEET THE MINIMUM CONSTRUCTION STANDARDS OF THE CITY OF PORTSMOUTH AND NHDOT STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, LATEST EDITION. THE MORE STRINGENT SPECIFICATION SHALL GOVERN.
- ALL BENCHMARKS AND TOPOGRAPHY SHALL BE FIELD VERIFIED BY THE CONTRACTOR PRIOR TO INITIATING CONSTRUCTION.
- UNLESS OTHERWISE AGREED IN WRITING, THE CONTRACTOR SHALL BE RESPONSIBLE FOR ESTABLISHING AND MAINTAINING TEMPORARY BENCHMARKS (TBM) AND PERFORMING ALL CONSTRUCTION SURVEY LAYOUT.
- PROTECTION OF SUBGRADE: THE CONTRACTOR SHALL BE REQUIRED TO MAINTAIN STABLE, DEWATERED SUBGRADES FOR FOUNDATIONS, PAVEMENT AREAS, UTILITY TRENCHES, AND OTHER AREAS DURING CONSTRUCTION. SUBGRADE DISTURBANCE MAY BE INFLUENCED BY EXCAVATION METHODS, MOISTURE, PRECIPITATION, GROUNDWATER CONTROL, AND CONSTRUCTION ACTIVITIES. THE CONTRACTOR SHALL TAKE PRECAUTIONS TO PREVENT SUBGRADE DISTURBANCE. SUCH PRECAUTIONS MAY INCLUDE DIVERTING STORMWATER RUNOFF AWAY FROM CONSTRUCTION AREAS, REDUCING TRAFFIC IN SENSITIVE AREAS, AND MAINTAINING AN EFFECTIVE DEWATERING PROGRAM. SOILS EXHIBITING HEAVING OR INSTABILITY SHALL BE OVER EXCAVATED TO MORE COMPETENT BEARING SOIL AND REPLACED WITH FREE DRAINING STRUCTURAL FILL. IF THE EARTHWORK IS PERFORMED DURING FREEZING WEATHER, EXPOSED SUBGRADES ARE SUSCEPTIBLE TO FROST. NO FILL OR UTILITIES SHALL BE PLACED ON FROZEN GROUND. THIS WILL LIKELY REQUIRE REMOVAL OF A FROZEN SOIL CRUST AT THE COMMENCEMENT OF EACH DAY'S OPERATIONS. THE FINAL SUBGRADE ELEVATION WOULD ALSO REQUIRE AN APPROPRIATE DEGREE OF INSULATION AGAINST FREEZING.
- IF SUITABLE, EXCAVATED MATERIALS SHALL BE PLACED AS FILL WITHIN UPLAND AREAS ONLY AND SHALL NOT BE PLACED WITHIN WETLANDS. PLACEMENT OF BORROW MATERIALS SHALL BE PERFORMED IN A MANNER THAT PREVENTS LONG TERM DIFFERENTIAL SETTLEMENT. EXCESSIVELY WET MATERIALS SHALL BE STOCKPILED AND ALLOWED TO DRAIN BEFORE PLACEMENT. FROZEN MATERIAL SHALL NOT BE USED FOR CONSTRUCTION.
- IN ORDER TO PROVIDE VISUAL CLARITY ON THE PLANS, DRAINAGE AND OTHER UTILITY STRUCTURES MAY NOT BE DRAWN TO SCALE. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROPER SIZING AND LOCATION OF ALL STRUCTURES AND IS DIRECTED TO RESOLVE ANY POTENTIAL DISCREPANCY WITH THE ENGINEER PRIOR TO CONSTRUCTION.
- GRASS UNDERDRAIN SOIL FILTER (GUSF) IS SIZED BASED ON AN ESTIMATED 6,000 S.F. IMPERVIOUS AREA FOR LOT 18-1.
- DRIP EDGES WILL BE UTILIZED AROUND PROPOSED HOUSES AS PART OF STORMWATER MANAGEMENT.

UTILITY NOTES

- ALL EXISTING UTILITIES SHOWN ARE PER PLAN REFERENCE #1. LOCATIONS AND COMPLETENESS ARE NOT GUARANTEED BY ENGINEER OR OWNER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO VERIFY ALL EXISTING UTILITIES PRIOR TO BEGINNING ANY CONSTRUCTION ACTIVITIES.
- SITE WILL BE SERVED BY MUNICIPAL WATER & SEWER.
- COORDINATE ALL WATER LINE CONSTRUCTION ACTIVITIES WITH PORTSMOUTH PUBLIC WORKS.
- COORDINATE ALL SEWER LINE CONSTRUCTION ACTIVITIES WITH PORTSMOUTH PUBLIC WORKS AND CITY OF PORTSMOUTH SEWER EXTENSION PROJECT.

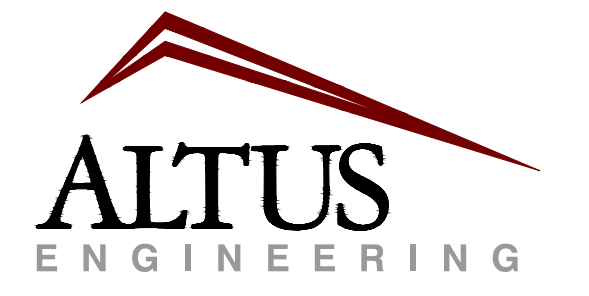
PLAN REFERENCE

- SHEET C1, "EXISTING CONDITIONS PLAN", DATED JULY 5, 2023, PREPARED JONES & BEACH ENGINEERS, INC.
- SHEET A1, "AMENDED SUBDIVISION AND LOT LINE ADJUSTMENT, TAX MAP 223, LOTS 18 & 18-1", DATED JULY 5, 2023, PREPARED JONES & BEACH ENGINEERS, INC.

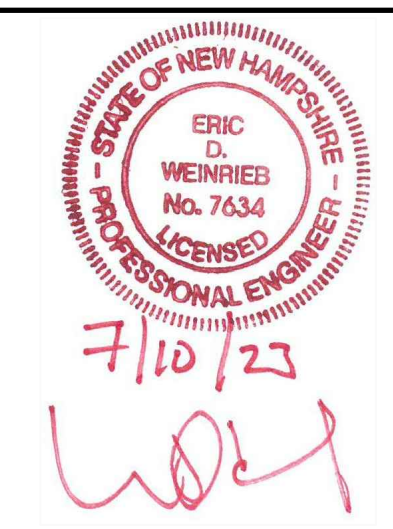


DRAINAGE STRUCTURES

- PAD #1**
 RIM: 20.5'±
 IN: 14.65' [8" CPP, PAD #2]
 IN: 14.65' [4" PVC 5' STUB W/CAP]
 OUT: 14.55' [CB #2097]
 10" CPP; L=5'±; S=0.010'/'
- PAD #2 (SOLID COVER)**
 RIM: 20.0'±
 IN: 16.60' [6" CPP, PDI #3]
 OUT: 16.50' [PDI #1]
 8" CPP; L=58'±; S=0.032'/'
- PDI #3 (2' STRUCTURE WITH SOLID COVER)**
 RIM: 33.75'±
 IN: 29.50' [6" CPP, PAD #7]
 IN: 29.80' [6" CPP, PYD #4]
 OUT: 29.40' [PAD #2]
 6" CPP; L=130'±; S=0.098'/'
- PYD #4**
 RIM: 33.75'
 IN: 20.0'±
 OUT: 29.90' [PDI #3]
 6" CPP; L=16'±; S=0.006'/'
- PAD #7 WITH SOLID COVER (TO BE REMOVED)**
 RIM: 33.50'±
 IN: 30.25' [6" CPP, PAD #8]
 OUT: 30.15' [PAD #6]
 6" CPP; L=96'±; S=0.120'/'
- EXIST. PAD #8**
 RIM: 36.50'±
 IN: 34.10 [6" CPP, CLIFF ROAD]
 OUT: 34.00' [PAD #7]
 6" CPP; L=120'±; S=0.031'/'



133 Court Street Portsmouth, NH 03801
 (603) 433-2335 www.altus-eng.com



NOT FOR CONSTRUCTION
 ISSUED FOR: APPROVAL
 ISSUE DATE: JULY 10, 2023

NO.	DESCRIPTION	BY	DATE
0	INITIAL SUBMISSION	EDW	08/03/22
1	ADD GUSF, LLA	EDW	10/04/22
2	RE-ALIGN DRAINAGE	EDW	07/10/23

DRAWN BY: RMB
 APPROVED BY: EDW
 DRAWING FILE: 5279SITE-LOT2.DWG

SCALE:
 (22"x34") 1" = 20'
 (11"x17") 1" = 40'

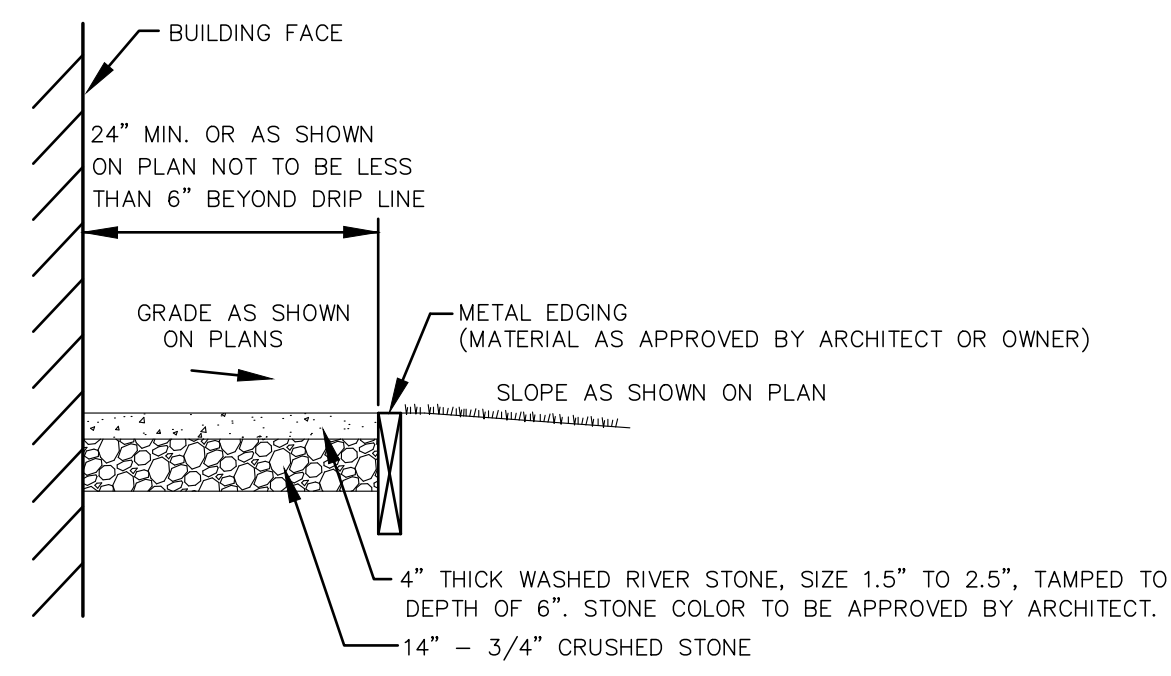
OWNER/APPLICANT:
 BONNIE AND CLYDE LOGUE
 27 SHAW ROAD
 PORTSMOUTH, NH 03801

PROJECT:
 RESIDENTIAL DEVELOPMENT
 TAX MAP 223, LOTS 18 & 18-1
 27 SHAW ROAD
 PORTSMOUTH, NH

TITLE:
 STORMWATER MANAGEMENT PLAN

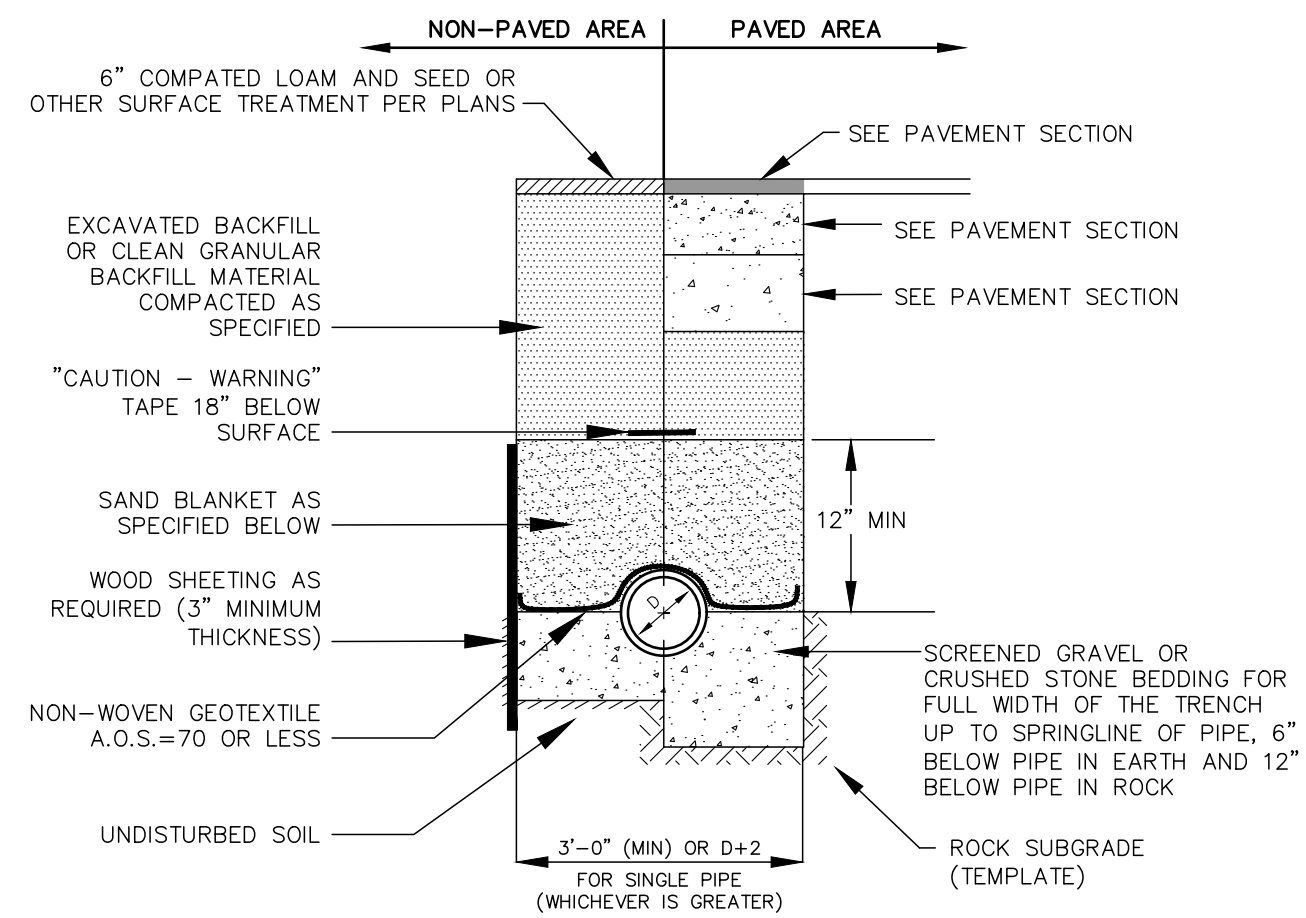
SHEET NUMBER:
 C - 1

P-5279



DRIP EDGE DETAIL

NOT TO SCALE

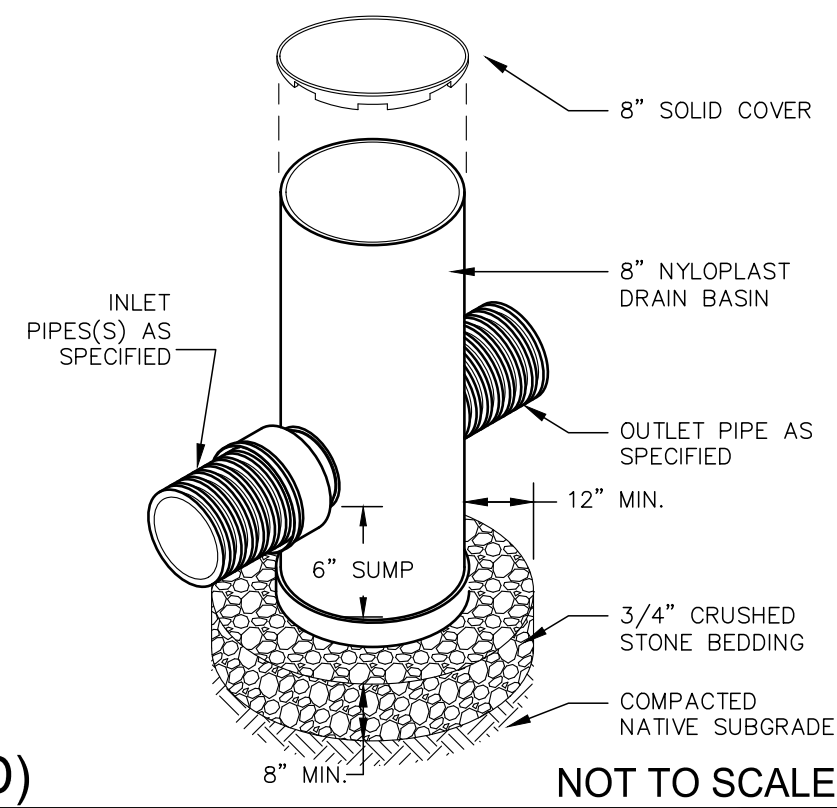


AREA DRAIN (PAD)

NOT TO SCALE

NOTES:

- FRAMES AND GRATES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
- DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN AND DETAILS.
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE, N-12HP AND PVC SEWER.
- INLINE DRAIN TO BE PVC, DIAMETER AS SPECIFIED AND AS MANUFACTURED BY ADS OR APPROVED EQUAL.
- THE CONTRACTOR SHALL INSTALL THE DRAIN BASIN PER THE MANUFACTURER'S RECOMMENDATIONS AND AS SHOWN ON THE DRAWINGS.
- FOR INSTALLATION IN PEDESTRIAN AND LANDSCAPE AREAS ONLY.



NOTES:

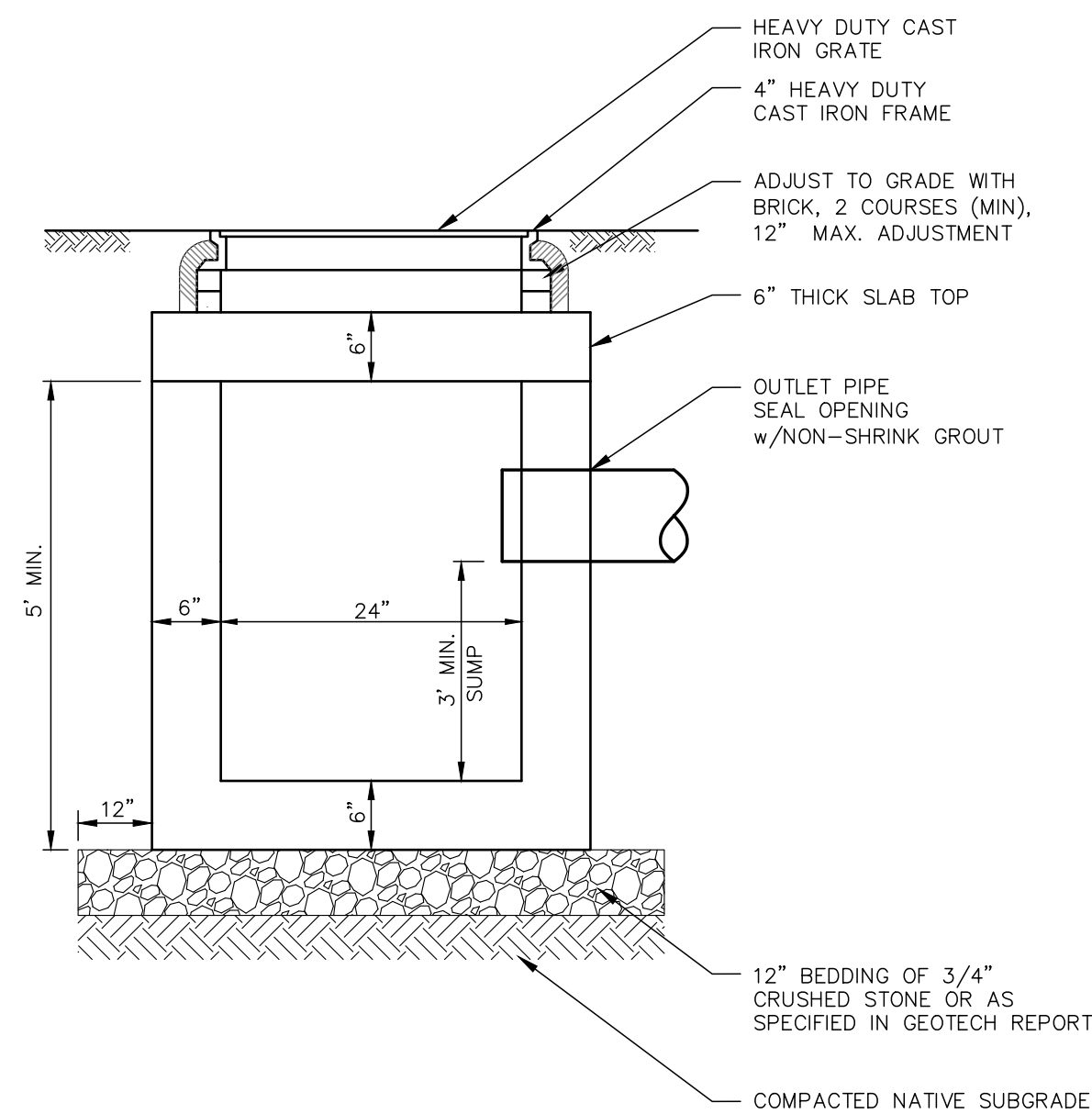
- BACKFILL MATERIAL BELOW PAVED OR CONCRETE AREAS, BEDDING MATERIAL, AND SAND BLANKET SHALL BE COMPACTED TO NOT LESS THAN 95% OF AASHTO T 99, METHOD C. SUITABLE BACKFILL MATERIAL BELOW LDAM AREAS SHALL BE COMPACTED TO NOT LESS THAN 90% OF AASHTO T 99, METHOD C.
- INSULATE GRAVITY SEWER AND FORCEMAINS WHERE THERE IS LESS THAN 5'-0" OF COVER WITH 2" THICK CLOSED CELL RIGID BOARD INSULATION, 18" ON EACH SIDE OF PIPE.
- MAINTAIN 12" MINIMUM HORIZONTAL SEPARATION AND WIDEN TRENCH ACCORDINGLY IF MULTIPLE PIPES ARE IN TRENCH.

SAND BLANKET/BARRIER		SCREENED GRAVEL OR CRUSHED STONE BEDDING*	
SIEVE SIZE	% FINER BY WEIGHT	SIEVE SIZE	% PASSING BY WEIGHT
1/2"	90 - 100	1"	100
200	0 - 15	3/4"	90 - 100
		3/8"	20 - 55
		# 4	0 - 10
		# 8	0 - 5

* EQUIVALENT TO STANDARD STONE SIZE #67 - SECTION 703 OF NHDOT STANDARD SPECIFICATIONS

DRAINAGE TRENCH

NOT TO SCALE



NOTES:

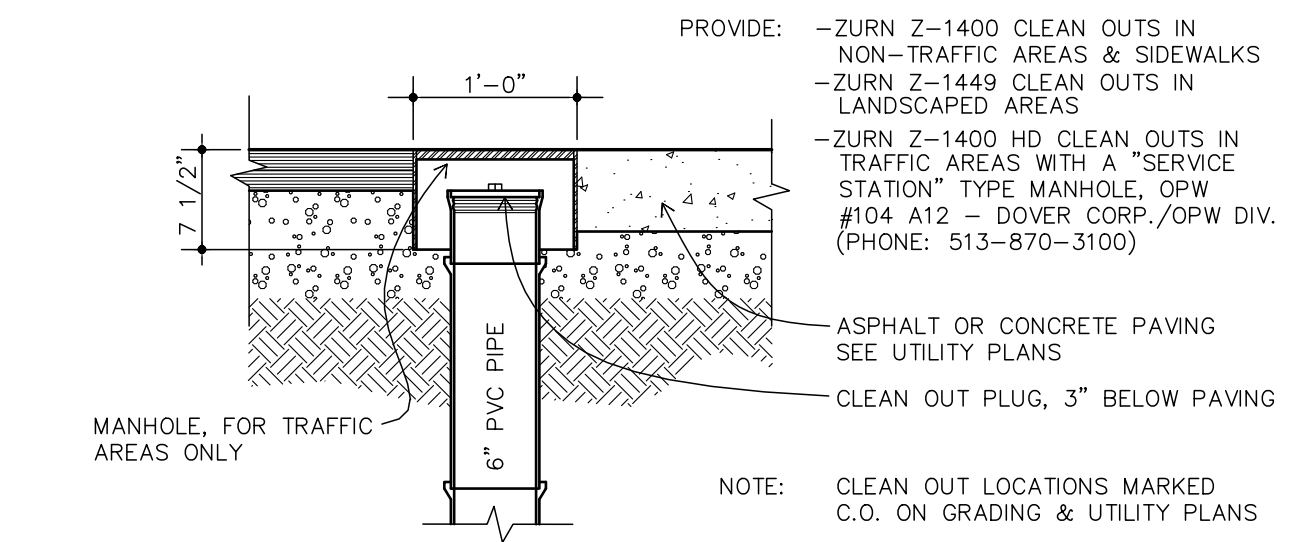
- STRUCTURE SHALL TO ACCOMMODATE HEAVY DUTY 24" SQ. C.I. FRAME AND GRATE.
- "24" SQUARE AREA DRAIN" AVAILABLE FROM PHOENIX PRECAST PRODUCTS (800-639-2199) OR APPROVED EQUAL.
- CONCRETE: 4,000 PSI AFTER 28 DAYS
- STRUCTURE SHALL BE STEEL REINFORCED MEET OR EXCEED H-20 LOADING.
- SEAL ALL TONGUE AND GROOVE JOINTS w/BUTYL RUBBER JOINT COMPOUND.

PDI #3 (2' STRUCTURE)

NOT TO SCALE

CLEANOUT DETAIL

NOT TO SCALE



NOTES:

- WHEN CONTRACTOR EXCAVATES RAIN GARDEN AREA TO SUBGRADE, DESIGN ENGINEER SHALL PERFORM SUBSURFACE EVALUATION PRIOR TO THE PLACEMENT OF ANY SELECT MATERIAL OR OTHER BACKFILL.
- SOIL FILTER MEDIA SHALL EITHER OPTION A OR OPTION B AT CONTRACTOR'S DISCRETION.
- DO NOT PLACE RAINGARDEN INTO SERVICE UNTIL IT HAS BEEN PLANTED AND ITS CONTRIBUTING AREAS STABILIZED.
- DO NOT DISCHARGE SEDIMENT-LADEN WATERS FROM CONSTRUCTION ACTIVITIES TO THE RAINGARDEN DURING ANY STAGE OF CONSTRUCTION.
- DO NOT TRAFFIC EXPOSED SURFACES OF RAINGARDEN WITH CONSTRUCTION EQUIPMENT. IF FEASIBLE, PERFORM EXCAVATION ACTIVITIES WITH EQUIPMENT POSITIONED OUTSIDE THE LIMITS OF THE BASIN.

MAINTENANCE REQUIREMENTS

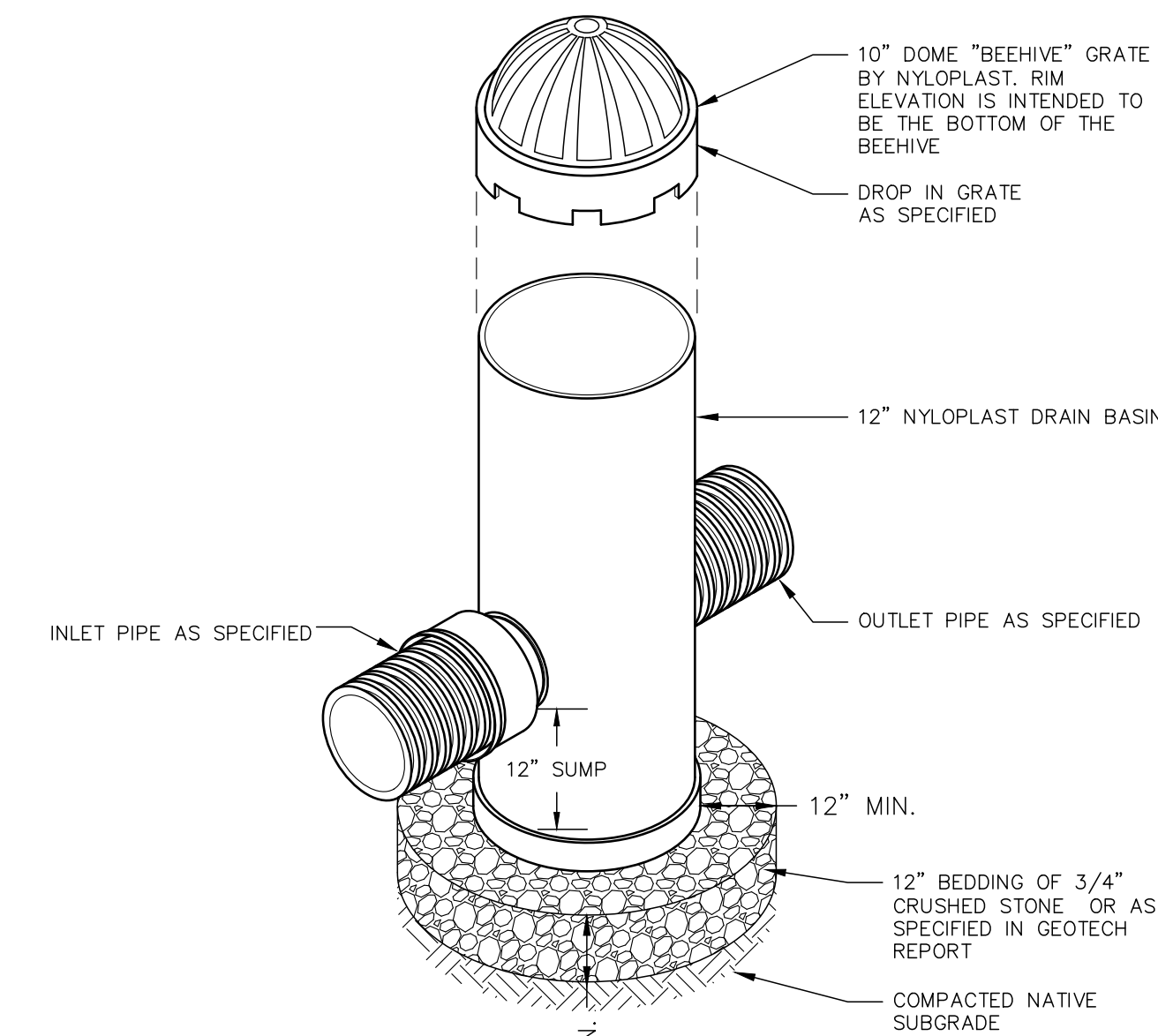
- SYSTEMS SHOULD BE INSPECTED AT LEAST TWICE ANNUALLY, AND FOLLOWING ANY RAINFALL EXCEEDING 2.5 INCHES IN A 24-HOUR PERIOD, WITH MAINTENANCE OR REHABILITATION CONDUCTED AS A WARRANTED BY SUCH INSPECTION.
- PRETREATMENT MEASURES SHOULD BE INSPECTED AT LEAST TWICE ANNUALLY, AND CLEANED OF ACCUMULATED SEDIMENT AS WARRANTED BY INSPECTION, BUT NO LESS THAN ONCE ANNUALLY.
- AT LEAST ONCE ANNUALLY, SYSTEM SHOULD BE INSPECTED FOR DRAWDOWN TIME. IF BIORETENTION SYSTEM DOES NOT DRAIN WITHIN 72-HOURS FOLLOWING A RAINFALL EVENT, THEN A QUALIFIED PROFESSIONAL SHOULD ASSESS THE CONDITION OF THE FACILITY TO DETERMINE MEASURES REQUIRED TO RESTORE FILTRATION FUNCTION OR INFILTRATION FUNCTION (AS APPLICABLE), INCLUDING BUT NOT LIMITED TO REMOVAL OF ACCUMULATED SEDIMENTS OR RECONSTRUCTION OF THE FILTER MEDIA.
- VEGETATION SHOULD BE INSPECTED AT LEAST ANNUALLY, AND MAINTAINED IN HEALTHY CONDITION, INCLUDING, PRUNING, REMOVAL, AND REPLACEMENT OF DEAD OR DISEASED VEGETATION, AND REMOVAL OF INVASIVE SPECIES.

DESIGN REFERENCES

- UNH STORMWATER CENTER
- EPA (1999A)
- NEW HAMPSHIRE STORMWATER MANAGEMENT MANUAL, VOLUME 2, DECEMBER 2008 AS AMENDED.

TYPICAL GRASSED UNDERDRAIN SOIL FILTER

NOT TO SCALE

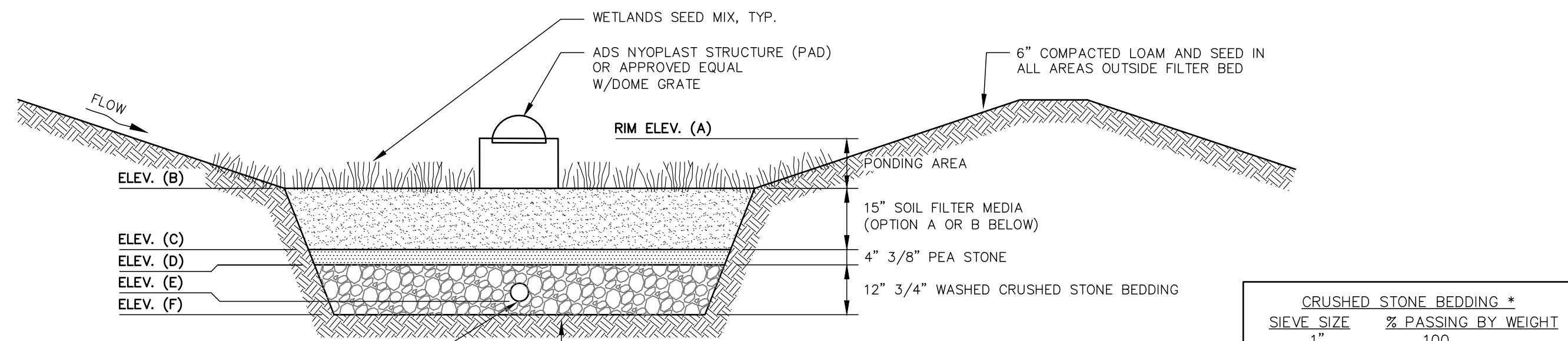


NOTES:

- FRAMES AND GRATES SHALL BE PEDESTRIAN-RATED DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
- DRAIN BASIN TO BE CUSTOM MANUFACTURED ACCORDING TO PLAN AND DETAILS.
- DRAINAGE CONNECTION STUB JOINT TIGHTNESS SHALL CONFORM TO ASTM D3212 FOR CORRUGATED HDPE, N-12HP AND PVC SEWER.
- INLINE DRAIN TO BE PVC DIAMETER AS SPECIFIED AND AS MANUFACTURED BY ADS OR APPROVED EQUAL.
- THE CONTRACTOR SHALL INSTALL THE DRAIN BASIN PER THE MANUFACTURER'S RECOMMENDATIONS AND AS SHOWN ON THE DRAWINGS.
- INLET AND OUTLET GEOMETRY MAY NOT BE SYMMETRICAL. ALL INLETS AND OUTLET LOCATIONS SHALL CONFORM TO THE LINES AND ANGLES SHOWN ON THE PLANS.

YARD DRAIN (PYD)

NOT TO SCALE

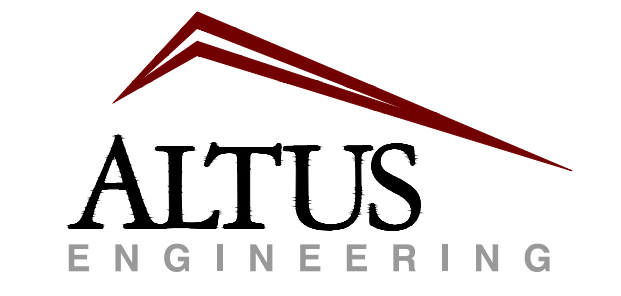


ELEV.	GUSE 1
A	33.75
B	32.25
C	31.00
D	30.67
E	30.00
F	29.67

CRUSHED STONE BEDDING *	
SIEVE SIZE	% PASSING BY WEIGHT
1"	100
3/4"	90 - 100
3/8"	20 - 55
# 4	0 - 10
# 8	0 - 5

* EQUIVALENT TO STANDARD STONE SIZE #67 - SECTION 703 OF NHDOT STANDARD SPECIFICATIONS

FILTER MEDIA MIXTURES			
Component Material	Percent of Mixture by Volume	Gradation of material	
		Sieve No.	Percent by Weight Passing Standard Sieve
Filter Media Option A			
ASTM C-33 concrete sand	50 to 55		
Loamy sand topsoil, with fines as indicated	20 to 30	200	15 to 25
Moderately fine shredded bark or wood fiber mulch, with fines as indicated	20 to 30	200	< 5
Filter Media Option B			
Moderately fine shredded bark or wood fiber mulch, with fines as indicated	20 to 30	200	< 5
		10	85 to 100
		20	70 to 100
Loamy coarse sand	70 to 80	60	15 to 40
		200	8 to 15



133 Court Street
(603) 433-2335
Portsmouth, NH 03801
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NOT FOR CONSTRUCTION

ISSUED FOR: APPROVAL

ISSUE DATE: JULY 10, 2023

NO.	DESCRIPTION	BY	DATE
0	REVIEW	EDW	08/03/22
1	RE-ALIGN DRAINAGE	EDW	07/10/23

DRAWN BY: RMB

APPROVED BY: EDW

DRAWING FILE: 5279SITE.DWG

SCALE: NOT TO SCALE

OWNER/APPLICANT: BONNIE AND CLYDE LOGUE

27 SHAW ROAD
PORTSMOUTH, NH 03801

PROJECT: RESIDENTIAL DEVELOPMENT

TAX MAP 223, LOTS 18 & 18-1
27 SHAW ROAD
PORTSMOUTH, NH

TITLE: DETAIL SHEET

SHEET NUMBER: C - 3

STORMWATER INSPECTION AND MAINTENANCE MANUAL

Bonnie and Clyde Logue Assessor's Map 223, Lot 18

OWNER AT TIME OF SUBDIVISION APPROVAL:

Bonnie and Clyde Logue
27 Shaw Road
Portsmouth, NH 03801

Proper inspection, maintenance, and repair are key elements in maintaining a successful stormwater management program on a developed property. Routine inspections ensure permit compliance and reduce the potential for deterioration of infrastructure or reduced water quality. The following responsible parties shall be in charge of managing the stormwater facilities:

RESPONSIBLE PARTIES:

Owner: Bonnie and Clyde Logue (603) 479-3981
Name Company Phone

Inspection: Bonnie and Clyde Logue (603) 479-3981
Name Company Phone

Maintenance: Bonnie and Clyde Logue (603) 479-3981
Name Company Phone

NOTES:

Inspection and maintenance responsibilities shall transfer to any future property owner(s).

This manual shall be updated as needed to reflect any changes related to any transfer of ownership and/or any delegation of inspection and maintenance responsibilities to another entity

INFILTRATION PONDS

Function – Infiltration ponds allow for the infiltration and treatment of stormwater runoff.

Maintenance

- Inspect annually and after significant rainfall events.
- If an infiltration-based practice does not completely drain within 72-hours following a rainfall event, then a qualified professional shall be retained to assess the condition of the facility to determine measures required to restore its filtration and/or infiltration function(s), including but not limited to removal of accumulated sediments and/or replacement or reconstruction of the structure.
- Remove any obstructions, litter and accumulated sediment or debris as warranted but no less than once a year.
- Mowing of any grassed area in or adjacent to a raingarden, including its berm, shall be performed at least twice per year (when areas are not inundated) to keep the vegetation in vigorous condition. The cut grass shall be removed to prevent the decaying organic litter from clogging the filter media or choking other vegetation.
- Select vegetation should be maintained in healthy condition. This may include pruning, removal and replacement of dead or diseased vegetation.
- Remove any hard wood growth from pond areas, including side slopes and berms.

STONE DRIP EDGE

Function – Drip edge accepts runoff from a peaked roof without gutter, allowing runoff to be detained at the drip line and filtered through the foundation backfill. The detention and filtration reduces the potential for runoff to the public drainage system, helps reduce flooding and minimizes the amount of pollutants flowing from the roof into a storm drain.

Maintenance

- Keep area free of vegetation and organic litter.

LANDSCAPED AREAS – ORGANIC FERTILIZER MANAGEMENT

Function – All fertilizer used on site shall be certified organic. Organic fertilizer management involves controlling the rate, timing and method of organic fertilizer application so that the nutrients are taken up by the plants thereby reducing the chance of polluting the surface and ground waters. Organic fertilizer management can be effective in reducing the amounts of phosphorus and nitrogen in runoff from landscaped areas, particularly lawns.

Maintenance

- Have the soil tested by your landscaper or local Soil Conservation Service for nutrient requirements and follow the recommendations.
- Do not apply organic fertilizer to frozen ground.
- Clean up any organic fertilizer spills.
- Do not allow organic fertilizer to be broadcast into water bodies.
- When organically fertilizing a lawn, water thoroughly, but do not create a situation where water runs off the surface of the lawn.



City of Portsmouth, New Hampshire

Subdivision Application Checklist

This subdivision application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. A pre-application conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all subdivision review requirements. Please refer to the Subdivision review regulations for full details.

Applicant Responsibilities (Section III.C): Applicable fees are due upon application submittal along with required number of copies of the Preliminary or final plat and supporting documents and studies. Please consult with Planning staff for submittal requirements.

Owner: Clyde Logue & Mary Duff Kastel Date Submitted: 7/5/23

Applicant: Same

Phone Number: 603-479-3981 E-mail: clyde3@gmail.com

Site Address 1: 27 Shaw Road Map: 223 Lot: 18

Site Address 2: Walker Bungalow Road Map: 223 Lot: 18 -1

Application Requirements			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested
<input checked="" type="checkbox"/>	Completed Application form. (III.C.2-3)	Supplemental material	N/A
<input checked="" type="checkbox"/>	All application documents, plans, supporting documentation and other materials provided in digital Portable Document Format (PDF) on compact disc, DVD or flash drive. (III.C.4)	Supplemental materials	N/A

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Name and address of record owner, any option holders, descriptive name of subdivision, engineer and/or surveyor or name of person who prepared the plat. (Section IV.1/V.1)	Plan title blocks (both sheets)	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	<p>Preliminary Plat Names and addresses of all adjoining property owners. (Section IV.2)</p> <p>Final Plat Names and addresses of all abutting property owners, locations of buildings within one hundred (100) feet of the parcel, and any new house numbers within the subdivision. (Section V.2)</p>	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	North point, date, and bar scale. (Section IV.3/V3)	Required on all Plan Sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	Zoning classification and minimum yard dimensions required. (Section IV.4/V.4)	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	<p>Preliminary Plat Scale (not to be smaller than one hundred (100) feet = 1 inch) and location map (at a scale of 1" = 1000'). (Section IV.5)</p> <p>Final Plat Scale (not to be smaller than 1"=100'), Location map (at a scale of 1"=1,000') showing the property being subdivided and its relation to the surrounding area within a radius of 2,000 feet. Said location map shall delineate all streets and other major physical features that my either affect or be affected by the proposed development. (Section V.5)</p>	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	Location and approximate dimensions of all existing and proposed property lines including the entire area proposed to be subdivided, the areas of proposed lots, and any adjacent parcels in the same ownership. (Section IV.6)	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Dimensions and areas of all lots and any and all property to be dedicated or reserved for schools, parks, playgrounds, or other public purpose. Dimensions shall include radii and length of all arcs and calculated bearing for all straight lines. (Section V.6/ IV.7)	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	Location, names, and present widths of all adjacent streets, with a designation as to whether public or private and approximate location of existing utilities to be used. Curbs and sidewalks shall be shown. (Section IV.8/V.7)	both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Location of significant physical features, including bodies of water, watercourses, wetlands, railroads, important vegetation, stone walls and soils types that may influence the design of the subdivision. (Section IV.9/V.8)	Both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Preliminary Plat Proposed locations, widths and other dimensions of all new streets and utilities, including water mains, storm and sanitary sewer mains, catch basins and culverts, street lights, fire hydrants, sewerage pump stations, etc. (Section IV.10) Final Plat Proposed locations and profiles of all proposed streets and utilities, including water mains, storm and sanitary sewer mains, catchbasins and culverts, together with typical cross sections. Profiles shall be drawn to a horizontal scale of 1"=50' and a vertical scale of 1"=5', showing existing centerline grade, existing left and right sideline grades, and proposed centerline grade. (Section V.9)	no new streets or utilities proposed	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	When required by the Board, the plat shall be accompanied by profiles of proposed street grades, including extensions for a reasonable distance beyond the subject land; also grades and sizes of proposed utilities. (Section IV.10)	No new streets are proposed	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Base flood elevation (BFE) for subdivisions involving greater than five (5) acres or fifty (50) lots. (Section IV.11)	Note 4 both sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	For subdivisions of five (5) lots or more, or at the discretion of the Board otherwise, the preliminary plat shall show contours at intervals no greater than two (2) feet. Contours shall be shown in dotted lines for existing natural surface and in solid lines for proposed final grade, together with the final grade elevations shown in figures at all lot corners. If existing grades are not to be changed, then the contours in these areas shall be solid lines. (Section IV.12/ V.12)	Existing topography not required but provided. No alteration of contours proposed.	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Dates and permit numbers of all necessary permits from governmental agencies from which approval is required by Federal or State law. (Section V.10)	No state permitting required for subdivision. NHDES Shoreland Permit required for	<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	For subdivisions involving greater than five (5) acres or fifty (50) lots, the final plat shall show hazard zones and shall include elevation data for flood hazard zones. (Section V.11)	Not required. Provided. See note 4, both sheets.	<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Location of all permanent monuments. (Section V.12)	Sheet A1	<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

General Requirements¹

<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/>	1. Basic Requirements: (VI.1) a. Conformity to Official Plan or Map b. Hazards c. Relation to Topography d. Planned Unit Development	Sheet A1 PUD not proposed	
<input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input checked="" type="checkbox"/> <input type="checkbox"/>	2. Lots: (VI.2) a. Lot Arrangement b. Lot sizes c. Commercial and Industrial Lots	Meets zoning, sheet A1 Residential development not commercial or industrial	
<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>	3. Streets: (VI.3) a. Relation to adjoining Street System b. Street Rights-of-Way c. Access d. Parallel Service Roads e. Street Intersection Angles f. Merging Streets g. Street Deflections and Vertical Alignment h. Marginal Access Streets i. Cul-de-Sacs j. Rounding Street Corners k. Street Name Signs l. Street Names m. Block Lengths n. Block Widths o. Grade of Streets p. Grass Strips	Not applicable - no streets proposed	
<input checked="" type="checkbox"/>	4. Curbing: (VI.4)	not applicable	
<input checked="" type="checkbox"/>	5. Driveways: (VI.5)	to be submitted with lot development.	
<input checked="" type="checkbox"/>	6. Drainage Improvements: (VI.6)	to be submitted with lot development	
<input checked="" type="checkbox"/>	7. Municipal Water Service: (VI.7)	in street	
<input checked="" type="checkbox"/>	8. Municipal Sewer Service: (VI.8)	stub provided	
<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>	9. Installation of Utilities: (VI.9) a. All Districts b. Indicator Tape	No new utility extensions proposed.	
<input checked="" type="checkbox"/>	10. On-Site Water Supply: (VI.10)	NA	
<input checked="" type="checkbox"/>	11. On-Site Sewage Disposal Systems: (VI.11)	NA	
<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>	12. Open Space: (VI.12) a. Natural Features b. Buffer Strips c. Parks d. Tree Planting	NA	
<input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/>	13. Flood Hazard Areas: (VI.13) a. Permits b. Minimization of Flood Damage c. Elevation and Flood-Proofing Records d. Alteration of Watercourses	NA	
<input type="checkbox"/>	14. Erosion and Sedimentation Control (VI.14)		

<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input checked="" type="checkbox"/>	15. Easements (VI.15) a. Utilities <input type="checkbox"/> b. Drainage <input checked="" type="checkbox"/>	on sheet A1	
<input checked="" type="checkbox"/>	16. Monuments: (VI.16)	Sheet A1	
<input checked="" type="checkbox"/>	17. Benchmarks: (VI.17)	Utility Pole sheet C1, top center	
<input checked="" type="checkbox"/>	18. House Numbers (VI.18)	to be provided	

Design Standards			
	Required Items for Submittal	Indicate compliance and/or provide explanation as to alternative design	Waiver Requested
<input checked="" type="checkbox"/>	1. Streets have been designed according to the design standards required under Section (VII.1). a. Clearing b. Excavation c. Rough Grade and Preparation of Sub-Grade d. Base Course e. Street Paving f. Side Slopes g. Approval Specifications h. Curbing i. Sidewalks j. Inspection and Methods	NA	
<input checked="" type="checkbox"/>	2. Storm water Sewers and Other Drainage Appurtenances have been designed according to the design standards required under Section (VII.2). a. Design b. Standards of Construction	NA	
<input checked="" type="checkbox"/>	3. Sanitary Sewers have been designed according to the design standards required under Section (VII.3). a. Design b. Lift Stations c. Materials d. Construction Standards	NA	
<input checked="" type="checkbox"/>	4. Water Mains and Fire Hydrants have been designed according to the design standards required under Section (VII.4). a. Connections to Lots b. Design and Construction c. Materials d. Notification Prior to Construction	NA	

Applicant's/Representative's Signature: *Ric D. Weinreb, PE* Date: 7/5/23

¹ See City of Portsmouth, NH Subdivision Rules and Regulations for details.
Subdivision Application Checklist/January 2018

Letter of Authorization

I, Clyde Logue & Mary Duff Kastel, hereby authorize Altus Engineering, LLC of Portsmouth, NH to represent us in all matters concerning the engineering and related permitting of improvements to the property located at 27 Shaw Road and Walker Bungalow Road in Portsmouth, NH on Assessors Map 223, Lots 18 and 18-1. This authorization shall include any signatures required for Federal, State and Municipal permit applications.

Signature



Mary Duff Kastel

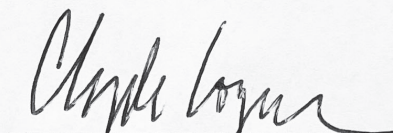
July 7, 2023
Date

Witness

Clyde Logue
Print Name

July 7, 2023
Date

Signature



Clyde Logue

July 7, 2023
Date

Witness

Mary Kastel
Print Name

July 7, 2023
Date

L0700-026
July 17, 2023

Mr. Peter Britz, Director of Planning & Sustainability
City of Portsmouth Planning & Sustainability Department
1 Junkins Avenue
Portsmouth NH, 03801

Re: **Lonza Biologics – Proposed Industrial Development
Amended Site Plan Review Application**

Dear Peter:

On behalf of Lonza Biologics, Inc. (Lonza), we are pleased to submit one (1) set of hard copies and one electronic file (.pdf) of the following information to support a request to the Planning Board for a recommendation for approval to the Pease Development Authority (PDA) for Amended Site Plan Review for a proposed industrial development located at 36, 46, 52, 70 and 80 Corporate Drive on Pease International Tradeport:

- PDA Application for Site Review, dated June 16, 2023;
- Site Plan Set, last revised July 17, 2023;
- Drainage Analysis, last revised July 17, 2023;
- Operations & Maintenance Manual, last revised July 17, 2023;
- Traffic Impact Study, last revised July 17, 2023;
- PB Stipulations of Approval Letter, dated June 16, 2023;
- Wastewater Correspondence Letter by DTC Lawyers, dated February 14, 2023;
- Architectural Renderings;
- Amended Site Review Application fee check, \$800.00

PROJECT SUMMARY

Background

The proposed project will expand Lonza's facility to support its growing product development services to the pharmaceutical and biologic industries. The project was granted Site Plan approval on January 17, 2019, and amended by administrative approvals on September 27, 2019, and January 27, 2023, with seven (7) Conditions Subsequent. Per Condition Subsequent 2.8 the Planning Board's recommended approval applied only to Phases 1A and 1B. Subsequent phases of development shall require submission of updated plans and supporting documents and noticed public hearings with the City's Technical Advisory Committee and Planning Board for amended site plan approval.

Currently Phase 1A construction is nearing completion, and Phase 1B work will be breaking ground in mid-July. Accordingly, this amended site review application is submitted to allow Lonza to proceed to Phase 2 of the project which includes the fit up of Building #1 and the construction of a temporary surface parking lot to support the employees of Building #1.



Existing Condition

The project is located on the vacant portion of Lonza's 46-acre parcel, referred to as the Iron Parcel, that once consisted of military housing and streets for Pease Air Force Base. The houses and roads were removed in the mid to late 1990's as part of the Civil Redevelopment Plan for Pease after the closure of the Air Force Base. The Iron Parcel was merged with Lonza's original parcel at 101 International Drive as part of the 2019 subdivision approval.

The existing 101 International Drive facility is approximately 800,000 SF in gross floor area and includes approximately 900 employees. Site work is ongoing on the Iron Parcel for the final completion of Phase 1A and the commencement of Phase 1B. The following summarizes the work completed during Phase 1A and to be completed during Phase 1B:

Phase 1A

- Daylighting of Hodgson Brook on the Iron Parcel
- Removal of the existing Hodgson Brook culvert
- Construction of the sidewalk and landscaping along Corporate Drive
- Completion of Soils Management Plan

Phase 1B

- Construction of building #1 shell
- Construction site improvements for building #1 such as drive aisles, fire lanes, utilities, lighting, sidewalks and stormwater management including Gravel Wetland #1
- Construction of the utility building shell
- Temporary gravel area for construction trailers, parking and laydown in approximate location of Proposed Building #3
- Intermittent grading between stream and Building #1
- Temporary sedimentation basins at locations of Gravel Wetland #2 and Rain Garden #1

Amended Site Plan

The total master plan build-out of the proposed industrial development is depicted in the enclosed Site Plan set. The master plan includes three (3) new buildings totaling approximately 800,000 square feet of gross floor area, a central utility building, and a new parking garage. The full master plan build-out has the potential to create approximately 800 new jobs. The project's site improvements consist of drive aisles, sidewalks, fire lanes, utilities, lighting and landscaping. The site improvements will consist of new stormwater management systems that include two (2) gravel wetlands and one (1) rain garden. The project has already received Alteration of Terrain Permit from the New Hampshire Department of Environmental Services (NHDES) for the the stormwater management design.

This master plan will be constructed in phases. Full-buildout will take several years and must be completed in phases as Lonza identifies clients and fits out the buildings to meet their needs. At this time Lonza is seeking a recommendation for approval from the Planning Board for Phase 2 of the development which is included in the Site Plan set that was enclosed with this letter, along with the amended master plan. The following summarizes the work to be completed during Phase 2:

Phase 2

- Final fit-up of Building #1
- Final fit-up of Utility Building
- Construction of the temporary surface parking lot

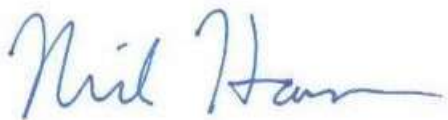


- Temporary gravel area for construction trailers, parking and laydown in approximate location of Proposed Building #2

We respectfully request to be placed on the Technical Advisory Committee (TAC) meeting agenda for July 5, 2023. If you have any questions or need any additional information, please contact Neil Hansen by phone at (603) 294-9213 or by email at nahansen@tighebond.com.

Sincerely,

TIGHE & BOND, INC.



Neil A. Hansen, PE
Project Manager



Patrick M. Crimmins, PE
Vice President

Copy: Lonza Biologics (via email)
Pease Development Authority

J:\L\L0700 Lonza Biologics Expansion was 1576F\026_Project Albacore\Report_Evaluations\Applications\City of
Portsmouth\20230717 TAC Submission\L0700-026 TAC Cover Letter.docx

L0700-026
July 17, 2023

Mr. Peter Britz, Director of Planning & Sustainability
City of Portsmouth Planning & Sustainability Department
1 Junkins Avenue
Portsmouth NH, 03801

Re: **Lonza Biologics – Proposed Industrial Development
Site Plan Review Permit – Stipulations of Approval, Conditions Subsequent**

Dear Peter:

On behalf of Lonza, we are pleased to submit Amended Site Plans and Drainage Analysis for the above referenced project. The project was granted Site Plan approval on January 17, 2019, and amended by administrative approvals on September 27, 2019 and January 27, 2023, with seven (7) Conditions Subsequent. The enclosed Site Plans, Drainage Analysis, and Traffic Impact Study have been revised to address these Conditions, and the following is an update on the status of those conditions:

2.5 *PDA staff and Board may review and address any outstanding issues raised by the third party peer review and have the third party peer reviewer do a final review of the plans prior to construction. Any revisions to drainage plans and reports which may result should be provided to the City's Planning Department.*

Prior to the commencement of Phase 1A construction coordination was completed between the applicant and the peer reviewer. Additional administrative and amended approvals were also granted by the PDA and PDA Board in January 2023 for Phase 1B construction to commence.

2.6 *Applicant shall not proceed to Phase 2 until the project has been issued an approved application for water service(s) associated with the expansion.*

The applicant acknowledges that an application for water service will be required prior to commencing Phase 2 construction.

2.7 *The applicant shall not proceed to Phase 2 until the project has been issued an Industrial User Permit by the City for the increased wastewater flows and loads associated with the expansion.*

The applicant acknowledges that an approved application for an Industrial User Permit by the City will be required prior to commencing Phase 2 construction. The applicants expected development on the Iron Parcel for the foreseeable future will not necessitate additional capacity for increased wastewater flows beyond its existing permits. This has been previously communicated to the City in the enclosed letter from DTC Lawyers dated February 14, 2023.

2.8 The Planning Board's recommended approval applies only to Phase 1A and Phase 1B as depicted on the approved site and grading plans. Any changes to said plans, as well as subsequent phases of development shall require submission of updated plans and supporting documents and noticed public hearings with the City's Technical Advisory Committee and Planning Board for amended site plan approval.

Acknowledged.

2.9 For the purpose of this site plan approval, the term "active and substantial development or building" shall mean the construction of the stream restoration and associated site improvements included in Phase 1(A). The term "substantial completion of the improvements as shown on the subdivision plat or site plan" shall mean the completion of all site improvements depicted in Phase 1(B), to include drive aisles, fire lanes, utilities, lighting, sidewalks, stormwater management, as well as the construction of a temporary gravel area for construction trailers, parking and laydown in the approximate location of proposed building #3, intermittent grading between stream and building #1 and temporary sedimentation basins at locations of gravel wetland #2 and rain garden #1, and construction of the shell of building #1, but not final fit-out of building #1.

Acknowledged.

2.10 For subsequent phases of development (beyond Phase 1A and Phase 1B), applicant shall update the Traffic Analysis to include the following intersections:

- Gosling Road/ Spaulding Turnpike Intersection
- International Drive/Corporate Drive/Manchester Square Intersection
- International Drive/Pease Blvd Intersection
- New Hampshire Ave/International Dr./Corporate Dr./Durham St. Intersection
- Corporate Drive/Grafton Drive Intersection
- NH 33/ Grafton Drive Intersection

The Traffic Impact Study has been updated to include the requested additional intersections, as well as for the updated size of building #1. The updated Traffic Study is enclosed as part of this submission.

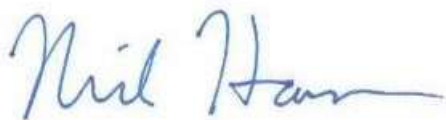
2.11 Applicant shall verify how fertilizer will be applied as part of the stream restoration.

Fertilizer was not used as part of the construction of the stream.

If you have any questions or need any additional information, please contact Neil Hansen by phone at (603) 294-9213 or by email at nahansen@tighebond.com.

Sincerely,

TIGHE & BOND, INC.



Neil A. Hansen, PE
Project Manager



Patrick M. Crimmins, PE
Vice President

Copy: Lonza Biologics Inc. (via email)
Pease Development Authority





CELEBRATING OVER 35 YEARS OF SERVICE TO OUR CLIENTS

LIZABETH M. MACDONALD
JOHN J. RATIGAN
DENISE A. POULOS
ROBERT M. DEROSIER
CHRISTOPHER L. BOLDT
SHARON CUDDY SOMERS
DOUGLAS M. MANSFIELD
KATHERINE B. MILLER
CHRISTOPHER T. HILSON
HEIDI J. BARRETT-KITCHEN
JUSTIN L. PASAY
ERIC A. MAHER
CHRISTOPHER D. HAWKINS
BRENDAN A. O'DONNELL
ELAINA L. HOEPPNER
WILLIAM K. WARREN

RETIRED
MICHAEL J. DONAHUE
CHARLES F. TUCKER
ROBERT D. CIANDELLA
NICHOLAS R. AESCHLIMAN

14 February 2023

Via email: smwoodland@cityofportsmouth.com
and U.S. Mail

Suzanne M. Woodland, Esquire
Deputy City Manager/Deputy City Attorney
City of Portsmouth
City Hall
1 Junkins Avenue
Portsmouth, NH 03801

Re: Pease Wastewater Treatment Facility Improvements Design Effort

Dear Suzanne:

This letter follows the productive meeting between representatives of Lonza Biologics, Inc. ("Lonza") and representatives of the City of Portsmouth and its Public Works and Engineering Departments on Monday, 6 February, and responds to your letter dated 13 December 2022, all of which pertain to the City's anticipated Pease Wastewater Treatment Facility ("PWWTF") improvement project. We understand that the City is in the process of working with AECOM Engineering ("AECOM") to determine the central purpose of that project as one rooted in addressing infrastructure obsolescence and reliability issues at the PWWTF, and potentially one which also incorporates improvements to account for increased demand for capacity by Lonza associated with development of the Iron Parcel, which is now a part of Lonza's leased property at 101 International Drive (the "Iron Parcel").

Executive Summary

Lonza is excited to inform you that it is finalizing a pending growing collaboration with a customer that, if and when completed, will require manufacturing space that Lonza intends to provide in Building 1 of its approved site plan for the Iron Parcel, thus advancing Lonza's long-standing investment in Portsmouth and the state of New Hampshire. However, based on Lonza's progressing sustainability initiatives as well as the unique requirements of the customer, Lonza anticipates being able to stay within the parameters of its existing water and wastewater permits. As a result, Lonza's current development plans for the Iron Parcel do not justify capital planning or budgeting for infrastructure improvements to the PWWTF to accommodate additional capacity demand by Lonza, at this time.

DONAHUE, TUCKER & CIANDELLA, PLLC
16 Acadia Lane, P.O. Box 630, Exeter, NH 03833
111 Maplewood Avenue, Suite D, Portsmouth, NH 03801
Towle House, Unit 2, 164 NH Route 25, Meredith, NH 03253
83 Clinton Street, Concord, NH 03301

Lonza looks forward to beginning construction of the shell of Building 1 on the Iron Parcel and to beginning the local review process for the fit-up and occupation of that building with the City's staff, Technical Review Committee and Planning Board in the near future.

Analysis

By way of brief background, in 2019, Lonza obtained land use permitting approvals to facilitate the phased construction of three industrial buildings and related site improvements on the Iron Parcel (the "Iron Parcel Approvals" or the "Iron Parcel Project" or the "Project"). More specifically, as originally approved, the phased development contemplated proposed building #1 with a 132,000 sf footprint ("Building 1"), proposed building #2 with a 150,000 sf footprint, and proposed building #3 with a 62,000 sf footprint. Over the subsequent years, Lonza obtained successive extensions of the Iron Parcel Approvals and a renewed Conditional Use Permit approval, all of which approvals are now vested by virtue of certain site work Lonza has performed at the Iron Parcel to include, among other things, the "day-lighting" and restoration of Hodgson Brook which resulted in approximately 42,500 sf of wetland creation.

While Lonza worked to vest its Iron Parcel Approvals to preserve its ability to develop the Iron Parcel, it was also expanding its investment in Lonza's existing facility. Specifically, in an effort to enhance its mammalian drug substance manufacturing capabilities in both Visp, Switzerland and Portsmouth, Lonza fit-up formerly unoccupied space in the existing building at Lonza's Portsmouth facility to support late-phase clinical and commercial development and manufacturing of pharmaceuticals, which initiative will help address increasing market demand for small to mid-scale mammalian-derived biologics (the "Lynx Project"). Lonza's investment in the Lynx Project includes state-of-the-art technologies in perfusion, purification and automation and is projected, once fully operational, to create 250 new jobs.

Additionally, over the last few years, Lonza has been focused on improving its existing operations at the Portsmouth facility and on establishing and implementing new sustainability initiatives, and continues to do so within the context of water reuse efforts, all to decrease its operational footprint and water usage.

Lonza greatly appreciates all of the efforts made by the City, and other regulatory agencies, over the last several years regarding the recently issued National Pollutant Discharge Elimination System Permit (the "NPDES Permit"). With the finalization of the NPDES Permit and the corresponding appeal, Lonza is happy to share with the City news that Lonza recently began working with a customer who has an immediate need for manufacturing space which Lonza intends to accommodate in Building 1 of the Iron Parcel Project (the "Customer"). Towards that end, last month, Lonza obtained minor site plan amendment approvals from the Pease Development Authority's Board of Directors ("PDA") for several minor changes to the Iron Parcel Project's site plan that are required to accommodate the Customer. Should Lonza finalize a deal with the Customer, these approvals will clear the way for Lonza to begin construction of the shell of Building 1 and associated site improvements on the Iron Parcel. Further, these minor site plan amendments from the PDA clear the path for Lonza to initiate the City of Portsmouth's review, through its City Staff, the Technical Review Committee and

ultimately the Planning Board, of Phase II of the Project, which pertains to the fit-up and eventual occupation of Building 1 by the Customer (“Phase II”). Lonza anticipates that should it finalize a deal with the Customer and obtain the necessary land use permits, the new operation on the Iron Parcel will create many additional jobs, further cementing Lonza’s continuing investment in Portsmouth, in New Hampshire, and in the surrounding region.

As the City is well-aware, part of the Phase II review and approval process requires a review of the anticipated water and wastewater needs and the implications of same on Lonza’s existing water and wastewater permits. Fortunately, and as we discussed at our meeting on 6 February, based on Lonza’s progressing sustainability initiatives and the unique requirements of the Customer, Lonza anticipates being able to work within the parameters of its existing permits such that no increased wastewater flows are anticipated at this time. Lonza looks forward to discussing this issue further with the City’s Public Works and Engineering Departments.

Finally, as currently contemplated, Lonza’s expected development on the Iron Parcel for the foreseeable future will not necessitate additional capacity for increased wastewater flows beyond its existing permits. Accordingly, the City does not need to, and should not, incorporate expansion improvements by Lonza within its capital improvement budgeting and planning for the PWWTF project, which it is currently undertaking with AECOM.

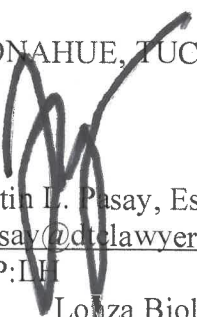
Conclusion

Lonza continues to appreciate the collaboration with and support from the City of Portsmouth which it has enjoyed over the years and Lonza looks forward to advancing its investment in Portsmouth through the development of the Iron Parcel as summarized in this letter.

Thank you very much for your time, and please do not hesitate to reach out to me with comments or questions that you may have.

Yours truly,

DONAHUE, TUCKER & CIANDELLA, PLLC



Justin L. Pasay, Esq.
jpasay@dtclawyers.com
JLP:DH

cc: Lonza Biologics, Inc.
Pease Development Authority
Tighe & Bond

Pease Development Authority
 55 International Drive, Portsmouth, NH 03801, (603) 433-6088



Application for Site Review

For PDA Use Only			
Date Submitted: _____	Municipal Review: _____	Fee: _____	
Application Complete: _____	Date Forwarded: _____	Paid: _____	Check #: _____

Applicant Information

Applicant: Lonza Biologics, Inc.	Agent: Tighe & Bond, Inc.
Address: 101 International Drive Portsmouth, NH 03801	Address: 177 Corporate Drive Portsmouth, NH 03801
Business Phone: 603-570-3625	Business Phone: 603-433-8818
Mobile Phone: _____	Mobile Phone: _____
Fax: _____	Fax: _____

Site Information

Portsmouth Tax Map: 305	Lot #: 006	Zone: Airport, Business, Commercial
Site Address / Location : 101 International Drive, Portsmouth, NH 03801		
Site Address / Location :		Area of On-site Wetlands: 4,087 SF

Activity Information

Change of Use: Yes [] No [X]	Existing Use: <u>Office/Research/Manufacturing</u>
	Proposed Use: <u>Office/Research/Manufacturing</u>

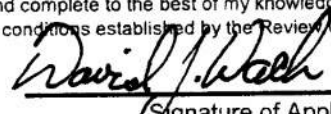
Description of Project:

The total master plan build-out of the proposed industrial development is depicted in the enclosed Site Plan set. The master plan includes three (3) new buildings totaling approximately 800,000 square feet of gross floor area, a central utility building, and a new parking garage. Phase 1A construction is nearing completion, and Phase 1B work will be breaking ground in early July. Accordingly, this amended site review application is submitted to allow Lonza to proceed to Phase 2 of the project which includes the fit up of Building #1 and the construction of a temporary surface parking lot to support the employees of Building #1. Per a condition of approval subsequent phases beyond 1A & 1B require submission of updated plans and supporting documents.

All above information shall be shown on a site plan submitted with this application. Provide 3 full size hard copies and one PDF copy of all application materials as well as one half-size set of drawings to PDA. Applicant shall supply additional copies as may be required by applicable municipality. Refer to Chapter 400 of PDA land Use Controls for additional information.

Certification

I hereby certify under the penalties of perjury that the foregoing information and accompanying plans, documents, and supporting data are true and complete to the best of my knowledge. I hereby apply for Site Review and acknowledge I will comply with all regulations and any conditions established by the Review Committee(s) and PDA Board in the development and construction of this project.



 (Signature of Applicant)

 Date

DAVID J. WACH

 Printed Name

N:\Engineer\ ApplicationforSiteReview.xlsx

PROPOSED INDUSTRIAL DEVELOPMENT

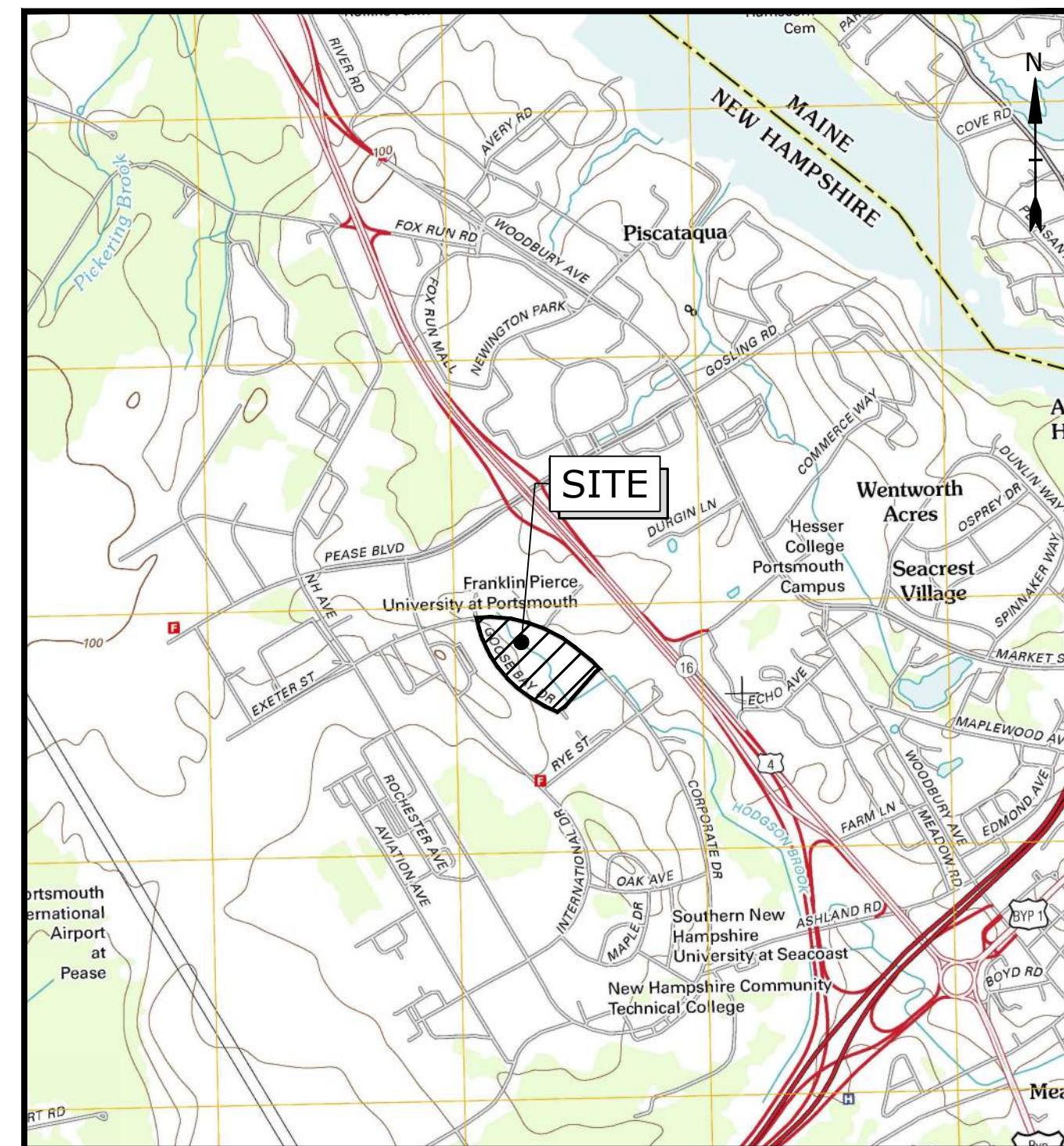
70 & 80 CORPORATE DRIVE PORTSMOUTH, NEW HAMPSHIRE

PROJECT NO: L-0700-13

APRIL 3, 2018

LAST REVISED: JULY 17, 2023

PLAN SET INDEX		
SHEET TITLE	# OF SHEETS	LAST REVISED
COVER SHEET	1	7/17/2023
SHEET INDEX	1	7/17/2023
EXISTING CONDITIONS & SUBDIVISION PLANS COVER SHEET	1	11/2/2021
EXISTING CONDITIONS & SUBDIVISION PLANS	6	11/2/2021
MASTER PLAN COVER SHEET	1	7/17/2023
MASTER PLAN SET	19	7/17/2023
PHASE 1B COVER SHEET	1	7/17/2023
PHASE 1B PLAN SET	27	7/17/2023
DETAILS COVER SHEET	1	7/17/2023
EROSION CONTROL NOTES & DETAILS SHEETS	12	7/17/2023



LOCATION MAP
SCALE: 1" = 2,000'

LESSOR: PEASE DEVELOPMENT AUTHORITY
55 INTERNATIONAL DRIVE
PORTSMOUTH, NEW HAMPSHIRE 03801

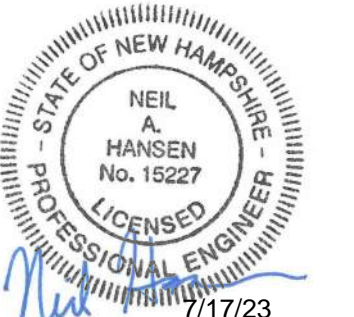
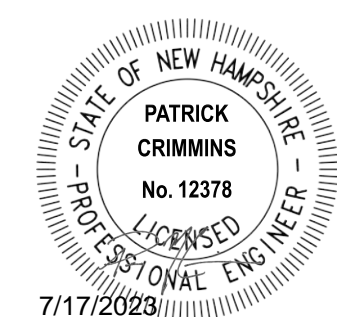
APPLICANT/OWNER: LONZA BIOLOGICS
101 INTERNATIONAL DRIVE
PORTSMOUTH, NH 03801

CIVIL ENGINEER: **Tighe&Bond**
177 CORPORATE DRIVE
PORTSMOUTH, NEW HAMPSHIRE 03801

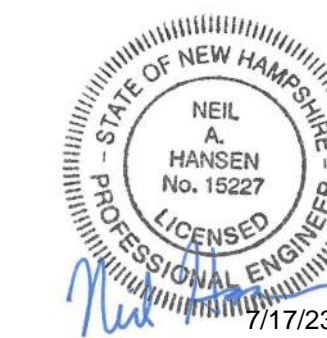
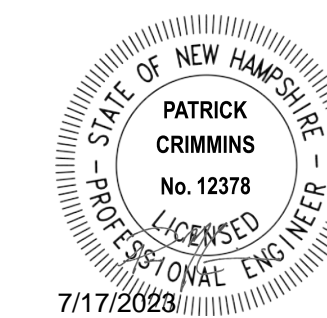
SURVEYOR: DOUCET SURVEY, INC.
102 KENT PLACE
NEWMARKET, NEW HAMPSHIRE 03857

WETLAND SCIENTIST: GOVE ENVIRONMENTAL SERVICES, INC.
8 CONTINENTAL DRIVE, UNIT H
EXETER, NEW HAMPSHIRE 03833

LIST OF PERMITS		
LOCAL	STATUS	DATE
SITE PLAN REVIEW PERMIT	APPROVED	1/17/2019
AMENDED SITE PLAN REVIEW PERMIT	PENDING	
STATE		
NHDES - ALTERATION OF TERRAIN PERMIT	ISSUED: AOT-1498	10/02/2018
NHDES - WETLANDS PERMIT	ISSUED: #2018-01731	12/21/2018
FEDERAL		
PHASE 1A - EPA - NPDES CGP	ISSUED: NHR1001EU	2/24/2022
PHASE 1B - EPA - NPDES CGP	PENDING:NHR1001SK	
	PENDING:NHR1001SL	



**TAC SUBMISSION
COMPLETE SET 70 SHEETS**



EXISTING CONDITIONS & SUBDIVISION PLANS SHEET INDEX		
SHEET NO.	SHEET TITLE	LAST REVISED
	COVER SHEET	11/2/2021
1 of 4	EXISTING CONDITIONS PLAN	08/16/2018
2 of 4	EXISTING CONDITIONS PLAN	08/16/2018
3 of 4	EXISTING CONDITIONS PLAN	08/16/2018
4 of 4	EXISTING CONDITIONS PLAN	08/16/2018
1 of 2	SUBDIVISION PLAN	11/2/2021
2 of 2	SUBDIVISION PLAN	11/2/2021

PHASE 2 PLAN SET SHEET INDEX		
SHEET NO.	SHEET TITLE	LAST REVISED
	PHASE 2 PLAN SET COVER SHEET	7/17/2023
C-161	PHASE 2 DEMOLITION PLAN	7/17/2023
C-162	PHASE 2 DEMOLITION PLAN	7/17/2023
C-163	PHASE 2 DEMOLITION PLAN	7/17/2023
C-163.1	PHASE 2 PRE-CONSTRUCTION LAYOUT PLAN	7/17/2023
C-164	PHASE 2 OVERALL SITE PLAN	7/17/2023
C-165	PHASE 2 SITE PLAN	7/17/2023
C-166	PHASE 2 SITE PLAN	7/17/2023
C-167	PHASE 2 SITE PLAN	7/17/2023
C-168	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-169	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-170	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-171	PHASE 2 UTILITIES PLAN	7/17/2023
C-172	PHASE 2 UTILITIES PLAN	7/17/2023
C-173	PHASE 2 UTILITIES PLAN	7/17/2023
C-174	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-175	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-176	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-177	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-178	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-179	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
A-1110	GROUND FLOOR PLAN - BL1	6/2/2023
A-2001	OVERALL BUILDINGS ELEVATIONS	6/2/2023
A-2002	BUILDING ELEVATIONS - BL1	6/2/2023
A-2003	BUILDING ELEVATIONS - BL1	6/2/2023
A310-000	REFERENCE GROUND FLOOR PLAN -CUB	6/2/2023
A500-000	BUILDING ELEVATIONS (N-S) - CUB	6/2/2023
A500-001	BUILDING ELEVATIONS (E-W) - CUB	6/2/2023

DETAILS SHEET INDEX		
SHEET NO.	SHEET TITLE	LAST REVISED
	DETAILS COVER SHEET	7/17/2023
C-501	EROSION CONTROL NOTES & DETAILS SHEET	7/17/2023
C-502	DETAILS SHEET	7/17/2023
C-503	DETAILS SHEET	7/17/2023
C-504	DETAILS SHEET	7/17/2023
C-505	DETAILS SHEET	7/17/2023
C-506	DETAILS SHEET	7/17/2023
C-507	DETAILS SHEET	7/17/2023
C-508	DETAILS SHEET	7/17/2023
C-509	DETAILS SHEET	7/17/2023
C-510	DETAILS SHEET	7/17/2023
C-511	DETAILS SHEET	7/17/2023
C-512	DETAILS SHEET	7/17/2023

MASTER PLAN SET SHEET INDEX		
SHEET NO.	SHEET TITLE	LAST REVISED
	MASTER PLAN SET COVER SHEET	7/17/2023
C-101	DEMOLITION PLAN	7/17/2023
C-102	DEMOLITION PLAN	7/17/2023
C-103	DEMOLITION PLAN	7/17/2023
C-104	OVERALL SITE PLAN	7/17/2023
C-105	SITE PLAN	7/17/2023
C-106	SITE PLAN	7/17/2023
C-107	SITE PLAN	7/17/2023
C-108	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-109	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-110	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-111	UTILITIES PLAN	7/17/2023
C-112	UTILITIES PLAN	7/17/2023
C-113	UTILITIES PLAN	7/17/2023
C-114	LANDSCAPE PLAN	7/17/2023
C-115	LANDSCAPE PLAN	7/17/2023
C-116	LANDSCAPE PLAN	7/17/2023
C-117	PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-118	PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-119	PHOTOMETRIC LIGHTING PLAN	7/17/2023

Proposed Industrial Development

Lonza Biologics

Portsmouth,
New Hampshire

L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

MARK	DATE	DESCRIPTION
PROJECT NO:	L-0700-013	
DATE:	04/03/2018	
FILE:	L-0700-026-C-COVR.dwg	
DRAWN BY:	CJK	
CHECKED:	NAH	
APPROVED:	PMC	

SHEET INDEX

SCALE: AS SHOWN

C-100

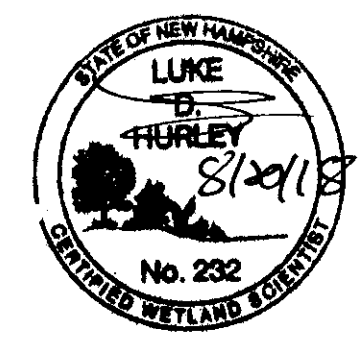
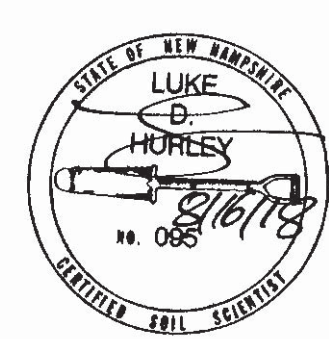
EXISTING CONDITIONS & SUBDIVISION PLANS

APRIL 3, 2018

REVISED: NOVEMBER 2, 2021

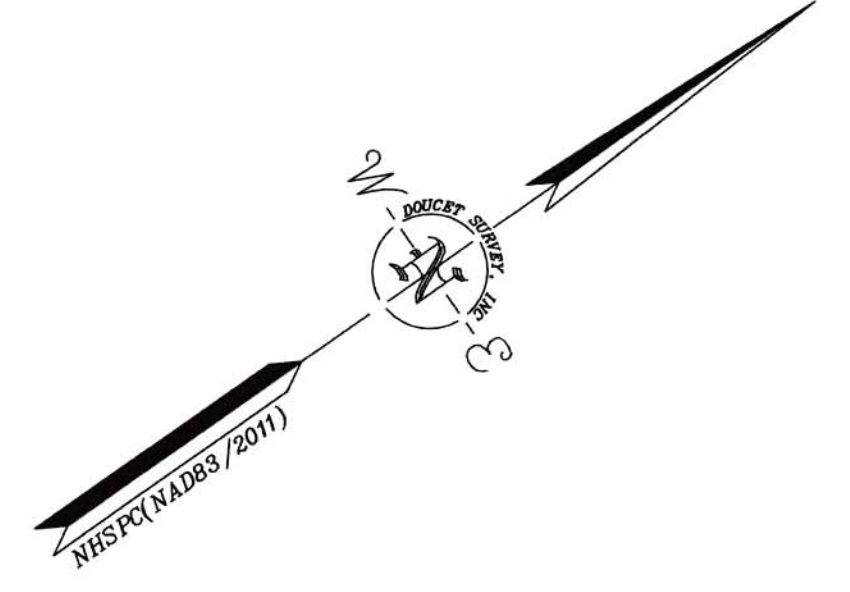
LIST OF DRAWINGS		
SHEET NO.	SHEET TITLE	LAST REVISED
	COVER SHEET	11/2/2021
1 of 4	EXISTING CONDITIONS PLAN	11/2/2021
2 of 4	EXISTING CONDITIONS PLAN	08/16/2018
3 of 4	EXISTING CONDITIONS PLAN	08/16/2018
4 of 4	EXISTING CONDITIONS PLAN	08/16/2018
1 of 2	SUBDIVISION PLAN	11/2/2021
2 of 2	SUBDIVISION PLAN	11/2/2021

SOIL IDENTIFICATION LEGEND	
SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHENTS URBAN LAND, >25 PERCENT SLOPES



TAX MAP 303, LOT 2-1
OPROCK PORTSMOUTH INTL FEE LLC
C/O OCEAN PROPERTIES LTD
1000 MARKET ST SUITE 300
PORTSMOUTH, NH 03801
R.C.R.D. BOOK 4831, PAGE 2677

TAX MAP 303, LOT 2-2
RESPORT LLC
1000 MARKET ST BLDG 1 STE 300
PORTSMOUTH, NH 03801



TAX MAP 305, LOT 7
PEASE DEVELOPMENT AUTHORITY
55 INTERNATIONAL DRIVE
PORTSMOUTH, NEW HAMPSHIRE 03801

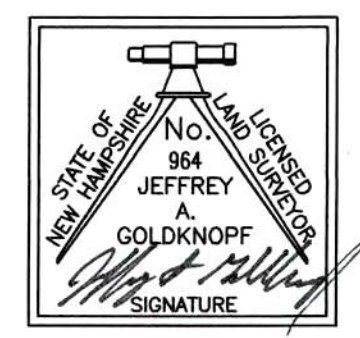
TAX MAP 305, LOT 7-1
UNIVERSITY SYSTEM OF NEW HAMPSHIRE
COLLEGE FOR LIFELONG LEARNING
51 INTERNATIONAL DRIVE
PORTSMOUTH, NH 03801

TAX MAP 305, LOT 7-1
CITY OF PORTSMOUTH
1 JUNKINS AVE
PORTSMOUTH, NH 03801

TAX MAP 303, LOT 3
RED HOOK BREWERY INC
C/O WIDMER BROTHERS BREWING CO
929 NORTH RUSSELL ST.
PORTLAND, OR 97227

TAX MAP 305, LOT 6
LONZA BIOLOGICS INC
101 INTERNATIONAL DRIVE
PORTSMOUTH, NH 03801

305-1
443,578 Sq. Ft.
10.18 Acres



PURSUANT TO RSA 676:18, III:
I CERTIFY THAT THIS SURVEY PLAT IS NOT A SUBDIVISION PURSUANT TO THIS TITLE AND THAT THE LINES OF STREETS AND WAYS SHOWN ARE THOSE OF PUBLIC OR PRIVATE STREETS OR WAYS ALREADY ESTABLISHED AND THAT NO NEW WAYS ARE SHOWN.

I CERTIFY THAT THIS SURVEY AND PLAN WERE PREPARED BY ME OR BY THOSE UNDER MY DIRECT SUPERVISION AND FALLS UNDER THE URBAN SURVEY CLASSIFICATION OF THE NH CODE OF ADMINISTRATIVE RULES OF THE BOARD OF LICENSURE FOR LAND SURVEYORS. I CERTIFY THAT THIS SURVEY WAS MADE ON THE GROUND AND IS CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. RANDOM TRAVERSE SURVEY BY TOTAL STATION, WITH A PRECISION GREATER THAN 1:15,000."

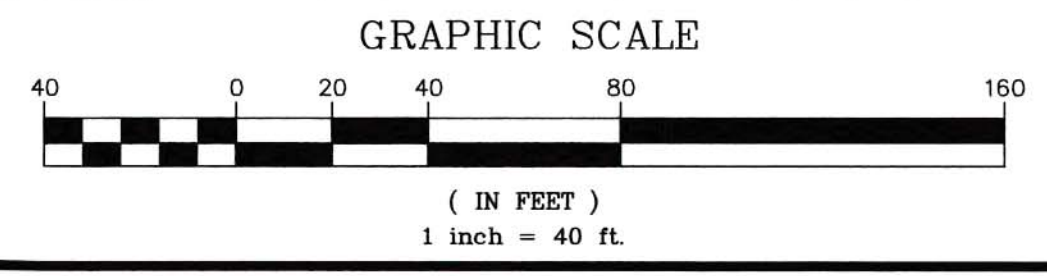
Jeffrey A. Goldknopf L.L.S. #964
8-16-18 DATE

THE CERTIFICATIONS SHOWN HEREON ARE INTENDED TO MEET REGISTRY OF DEED REQUIREMENTS AND ARE NOT A CERTIFICATION TO TITLE OR OWNERSHIP OF PROPERTY SHOWN. OWNERS OF ADJOINING PROPERTIES ARE ACCORDING TO CURRENT TOWN ASSESSORS RECORDS.

**EXISTING CONDITIONS PLAN
FOR
TIGHE & BOND AND LONZA
LAND OF
PEASE DEVELOPMENT AUTHORITY
(TAX MAP 305, LOTS 1 & 2)
GOOSE BAY DRIVE & CORPORATE DRIVE
PORTSMOUTH, NEW HAMPSHIRE**

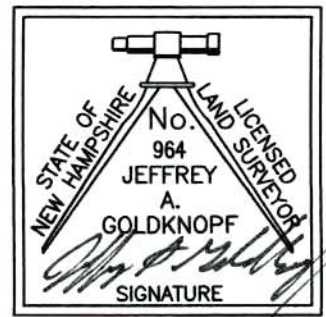
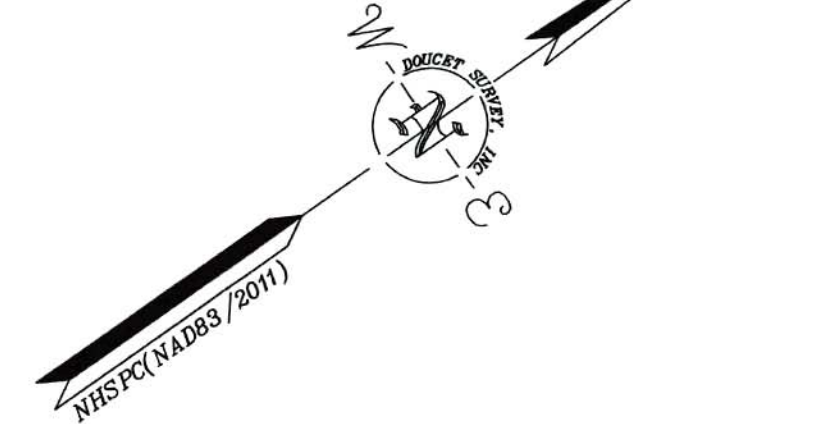
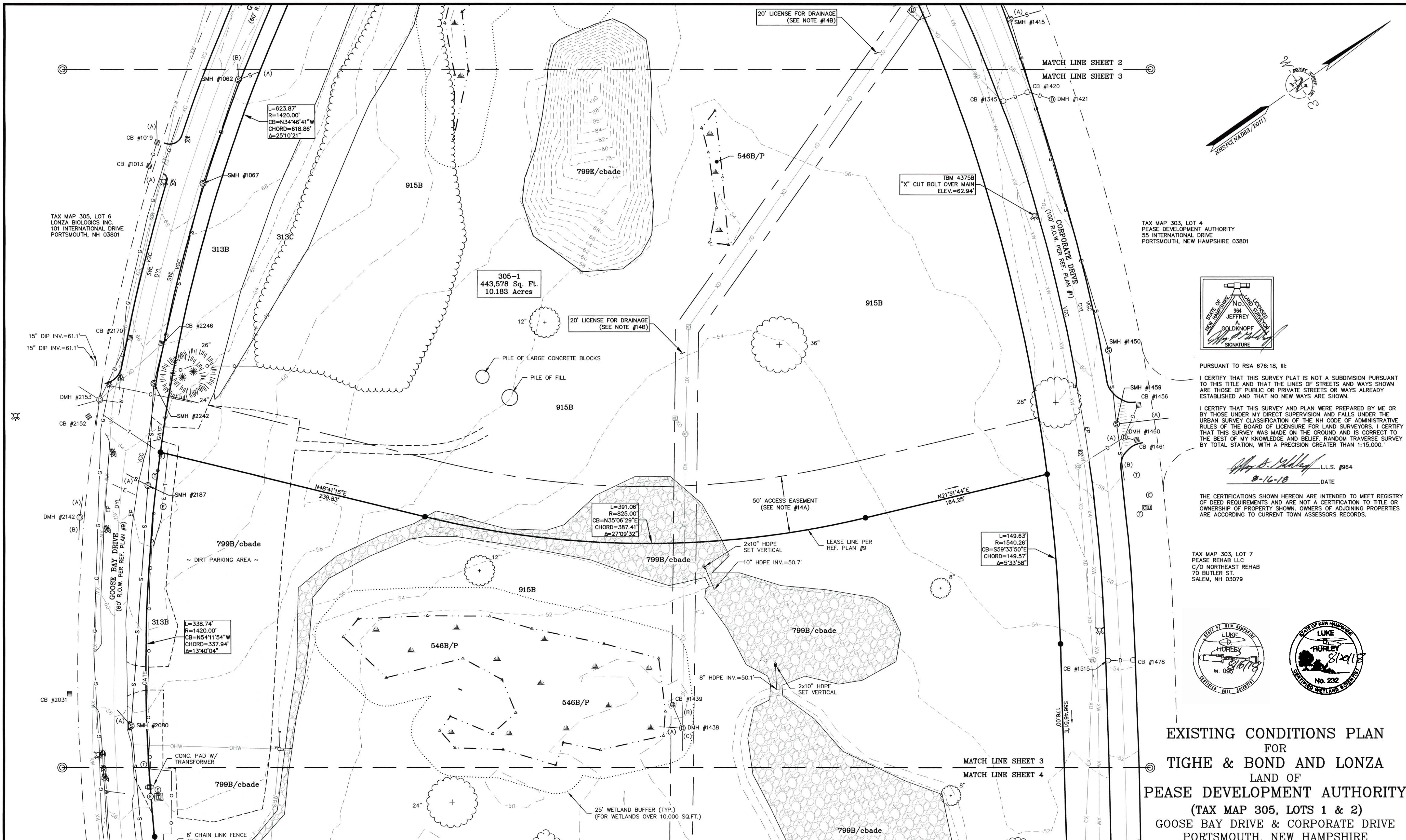
NO.	DATE	DESCRIPTION	BY
2	8/16/18	MOD. DRAINAGE	J.A.G.
		MOD. SOIL TYPES PER G.E.S.	
1	8/3/16	GENERAL EDITS AND ADDED WETLANDS BUFFER	J.A.G.

NOTE:
ALL ELECTRIC, GAS, TEL, WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION. THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 1-888-DIG-SAFE.



DRAWN BY:	K.C.W.	DATE:	DEC. 23, 2015
CHECKED BY:	J.A.G.	DRAWING NO.:	4375A
JOB NO.:	4375	SHEET	2 OF 4

DOUCET SURVEY
Serving Your Professional Surveying & Mapping Needs
102 Kent Place, Newmarket, NH 03857 (603) 859-8560
10 Steer Street (Riverview Suite) Kennebunk, ME (207) 502-7005
http://www.doucetsurvey.com

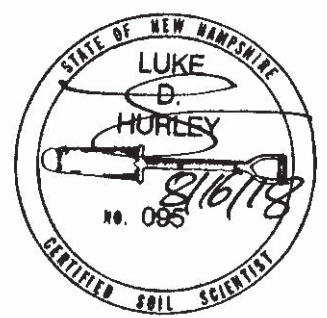


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Luke D. Hurley L.L.S. #964
 8-16-18 DATE

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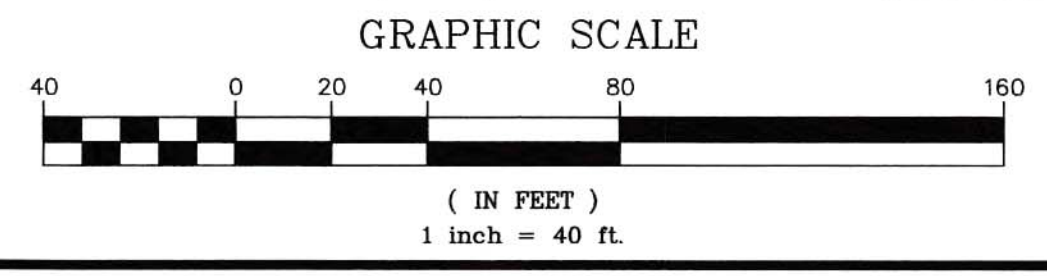
TAX MAP 303, LOT 7
 PEASE REHAB LLC
 C/O NORTHEAST REHAB
 70 BUTLER ST.
 SALEM, NH 03079



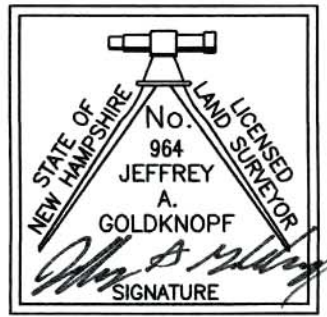
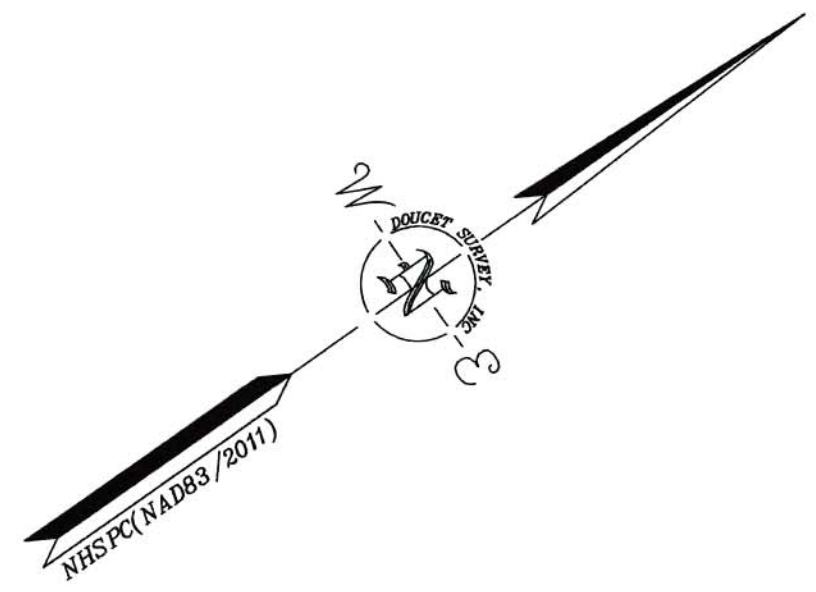
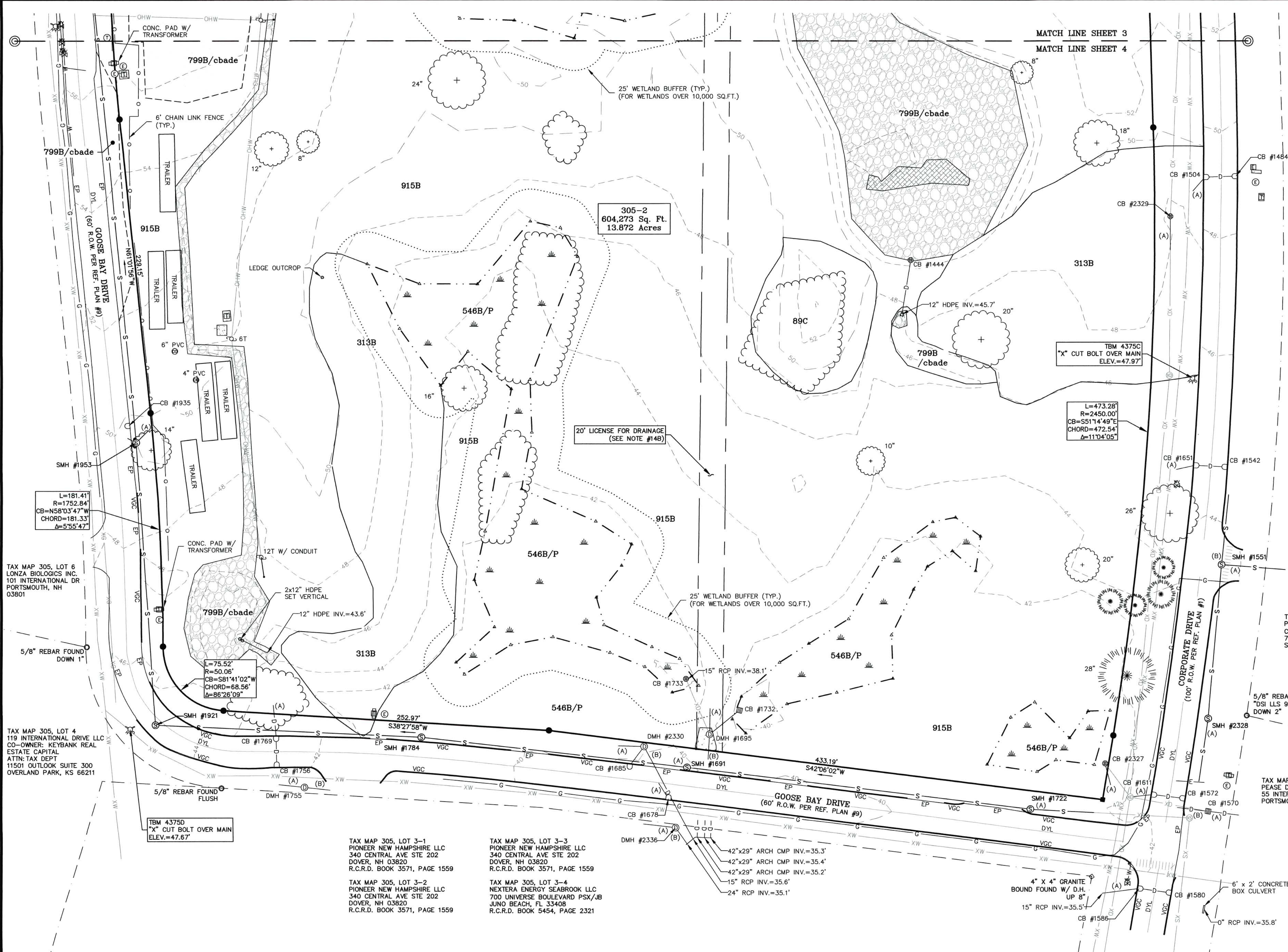
EXISTING CONDITIONS PLAN
 FOR
TIGHE & BOND AND LONZA
 LAND OF
PEASE DEVELOPMENT AUTHORITY
 (TAX MAP 305, LOTS 1 & 2)
 GOOSE BAY DRIVE & CORPORATE DRIVE
 PORTSMOUTH, NEW HAMPSHIRE

NO.	DATE	DESCRIPTION	BY
2	8/16/18	MOD. DRAINAGE	J.A.G.
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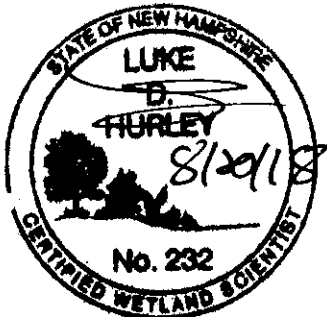
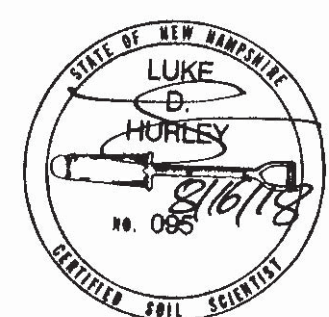
DRAWN BY:	K.C.W.	DATE:	DEC. 23, 2015
CHECKED BY:	J.A.G.	DRAWING NO.:	4375A
JOB NO.:	4375	SHEET	3 OF 4



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Jeffrey A. Goldknopf L.L.S. #964
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TAX MAP 303, LOT 7
 PEASE REHAB LLC
 C/O NORTHEAST REHAB
 70 BUTLER ST.
 SALEM, NH 03079

5/8" REBAR FOUND W/
 "DSI ILLS 937" CAP,
 DOWN 2"

TAX MAP 303, LOT 8
 PEASE DEVELOPMENT AUTHORITY
 55 INTERNATIONAL DRIVE
 PORTSMOUTH, NEW HAMPSHIRE 03801

**EXISTING CONDITIONS PLAN
 FOR
 TIGHE & BOND AND LONZA
 LAND OF
 PEASE DEVELOPMENT AUTHORITY
 (TAX MAP 305, LOTS 1 & 2)
 GOOSE BAY DRIVE & CORPORATE DRIVE
 PORTSMOUTH, NEW HAMPSHIRE**

TAX MAP 305, LOT 6
 LONZA BIOLOGICS INC.
 101 INTERNATIONAL DR
 PORTSMOUTH, NH
 03801

TAX MAP 305, LOT 4
 119 INTERNATIONAL DRIVE LLC
 CO-OWNER: KEYBANK REAL
 ESTATE CAPITAL
 ATTN: TAX DEPT.
 11501 OUTLOOK SUITE 300
 OVERLAND PARK, KS 66211

TAX MAP 305, LOT 3-1
 PIONEER NEW HAMPSHIRE LLC
 340 CENTRAL AVE STE 202
 DOVER, NH 03820
 R.C.R.D. BOOK 3571, PAGE 1559

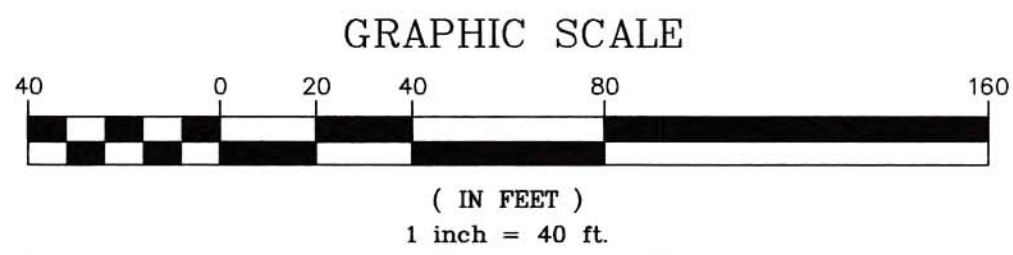
TAX MAP 305, LOT 3-3
 PIONEER NEW HAMPSHIRE LLC
 340 CENTRAL AVE STE 202
 DOVER, NH 03820
 R.C.R.D. BOOK 3571, PAGE 1559

TAX MAP 305, LOT 3-2
 PIONEER NEW HAMPSHIRE LLC
 340 CENTRAL AVE STE 202
 DOVER, NH 03820
 R.C.R.D. BOOK 3571, PAGE 1559

TAX MAP 305, LOT 3-4
 NEXTERA ENERGY SEABROOK LLC
 700 UNIVERSE BOULEVARD PSX/JB
 JUNO BEACH, FL 33408
 R.C.R.D. BOOK 5454, PAGE 2321

NO.	DATE	DESCRIPTION	BY
2	8/16/18	MOD. DRAINAGE	J.A.G.
1	8/3/16	MOD. SOIL TYPES PER G.E.S. GENERAL EDITS AND ADDED WETLANDS BUFFER	J.A.G.

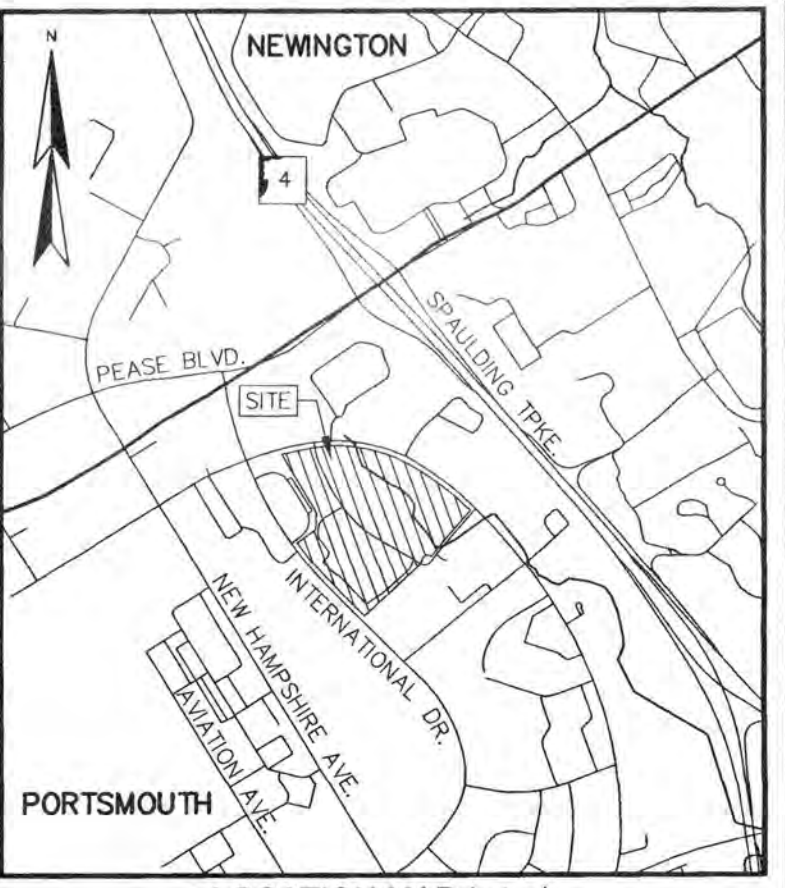
NOTE:
 ALL ELECTRIC, GAS, TEL, WATER, SEWER AND DRAIN SERVICES ARE SHOWN IN SCHEMATIC FASHION. THEIR LOCATIONS ARE NOT PRECISE OR NECESSARILY ACCURATE. NO WORK WHATSOEVER SHALL BE UNDERTAKEN ON THIS SITE USING THIS PLAN TO LOCATE THE ABOVE SERVICES. CONSULT WITH THE PROPER AUTHORITIES CONCERNED WITH THE SUBJECT SERVICE LOCATIONS FOR INFORMATION REGARDING SUCH. CALL DIG-SAFE AT 1-888-DIG-SAFE.



DRAWN BY:	K.C.W.	DATE:	DEC. 23, 2015
CHECKED BY:	J.A.G.	DRAWING NO.:	4375A
JOB NO.:	4375	SHEET	4 OF 4

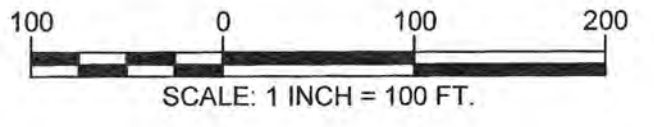
DOUCET SURVEY
 Serving Your Professional Surveying & Mapping Needs
 102 Kent Place, Newmarket, NH 03857 (603) 659-8560
 10 Shore Street (Overview Side) Kennebunk, ME (207) 502-7005
<http://www.doucetsurvey.com>

Carolyn Seay



LOCATION MAP (n.t.s.)

- LEGEND**
- LEASE LINE
 - - - PROPOSED LEASE LINE
 - - - PROPOSED EASEMENT/LICENSE
 - - - LEASE/ROW/EASEMENT/LICENSE LINE TO BE ABANDONED
 - - - APPROXIMATE ABUTTERS LOT LINE
 - - - EASEMENT LINE
 - TAX MAP 305, LOT 3-4
 - DRILL HOLE FOUND
 - IRON PIPE/ROD FOUND
 - TYP. TYPICAL
 - GRAN. GRANITE
 - CONC. CONCRETE
 - BND. FND. BOUND FOUND
 - D.H.F. DRILL HOLE FOUND
 - I.P.F. IRON PIPE FOUND
 - 4"x4" GRANITE BOUND SET FLUSH (10/28/2021)
 - 5/8" REBAR W/ ID CAP SET FLUSH (10/28/2021)

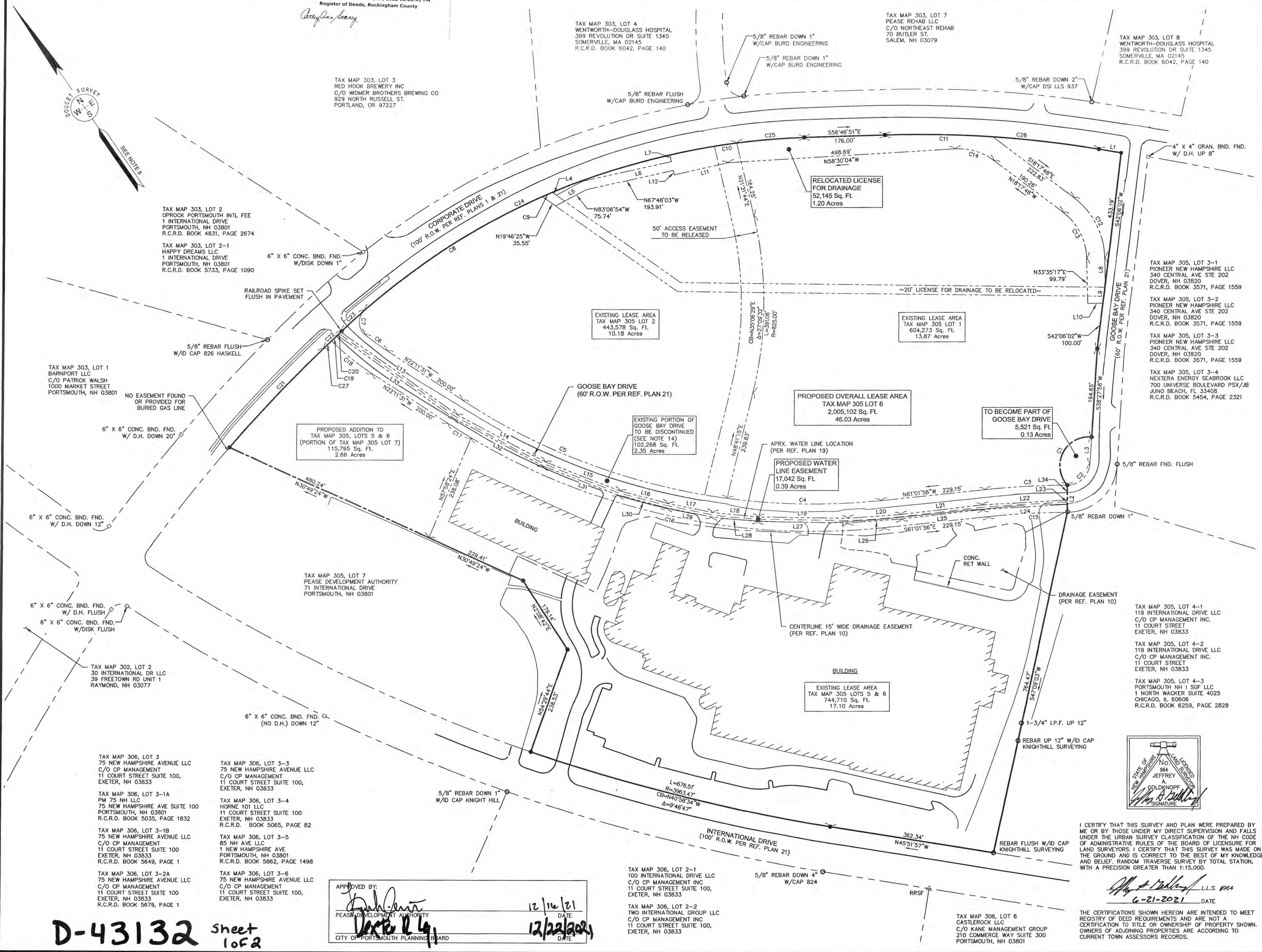


SUBDIVISION PLAN
 LAND OF
 PEASE DEVELOPMENT AUTHORITY
 LEASED TO
 LONZA BIOLOGICS, INC.
 OF
 TAX MAP 305 LOTS 1, 2, 5, 6, & 7
 AND
 GOOSE BAY DRIVE
 INTERNATIONAL DRIVE - CORPORATE DRIVE
 GOOSE BAY DRIVE
 PORTSMOUTH, NEW HAMPSHIRE

NO.	DATE	DESCRIPTION	BY
1	11/02/21	ADDED MONUMENTS SET	J.A.G.

DRAWN BY:	W.D.C.	DATE:	JUNE 21, 2021
CHECKED BY:	J.A.G.	DRAWING NO.:	6228B
JOB NO.:	6228	SHEET	1 OF 2

DOUCET SURVEYS
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APPROVED BY:
[Signature]
 PEASE DEVELOPMENT AUTHORITY
 CITY OF PORTSMOUTH PLANNING BOARD
 DATE: 12/16/21
 DATE: 12/22/21

I CERTIFY THAT THIS SURVEY AND PLAN WERE PREPARED BY ME OR BY THOSE UNDER MY DIRECT SUPERVISION AND FALLS UNDER THE URBAN SURVEY CLASSIFICATION OF THE NH CODE OF ADMINISTRATIVE RULES OF THE BOARD OF LICENSURE FOR LAND SURVEYORS. I CERTIFY THAT THIS SURVEY WAS MADE ON THE GROUND AND IS CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF. RANDOM TRAVERSE SURVEY BY TOTAL STATION, WITH A PRECISION GREATER THAN 1:15,000.

[Signature] L.L.S. #964
 6-21-2021 DATE

THE CERTIFICATIONS SHOWN HEREON ARE INTENDED TO MEET REGISTRY OF DEED REQUIREMENTS AND ARE NOT A CERTIFICATION TO TITLE OR OWNERSHIP OF PROPERTY SHOWN. OWNERS OF ADJOINING PROPERTIES ARE ACCORDING TO CURRENT TOWN ASSESSORS RECORDS.

D-43132 Sheet 1 of 2

FILE NAME: \\P:\PROJECTS\2021\01\18\SUBDIVISION PLAN (SHEET 1) PLOTTED: Tuesday, December 14, 2021 - 4:01 PM

PLAN NUMBER 43132 SHEET 001.PTR - 6/29/2023 - 16:33

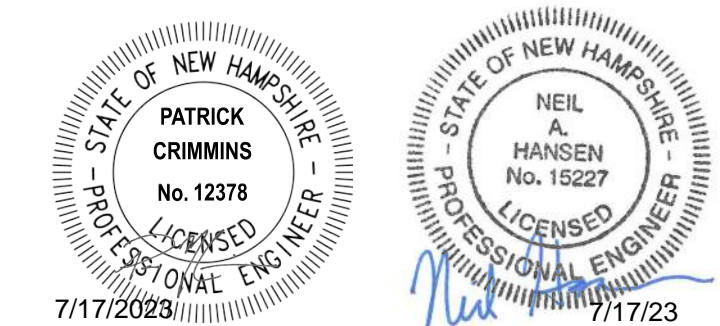
MASTER PLAN SET

APRIL 3, 2018

REVISED: JULY 17, 2023



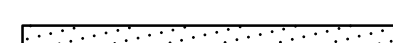
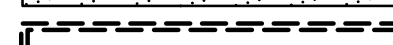


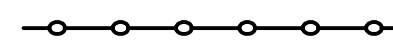








LIST OF DRAWINGS		
SHEET NO.	SHEET TITLE	LAST REVISED
	MASTER PLAN SET COVER SHEET	7/17/2023
C-101	DEMOLITION PLAN	7/17/2023
C-102	DEMOLITION PLAN	7/17/2023
C-103	DEMOLITION PLAN	7/17/2023
C-104	OVERALL SITE PLAN	7/17/2023
C-105	SITE PLAN	7/17/2023
C-106	SITE PLAN	7/17/2023
C-107	SITE PLAN	7/17/2023
C-108	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-109	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-110	GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-111	UTILITIES PLAN	7/17/2023
C-112	UTILITIES PLAN	7/17/2023
C-113	UTILITIES PLAN	7/17/2023
C-114	LANDSCAPE PLAN	7/17/2023
C-115	LANDSCAPE PLAN	7/17/2023
C-116	LANDSCAPE PLAN	7/17/2023
C-117	PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-118	PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-119	PHOTOMETRIC LIGHTING PLAN	7/17/2023

Last Save Date: July 12, 2023 4:31 PM By: CKRZCUIK
Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
P&E File Location: J:\U0700 Lenze Biologics Expansion.was 1276P.026 - Project Abstract\Drawings\AutoCAD\0700-026-C-CORR.dwg Layout Tab: MASTER.CS



COMPLETE SET 20 SHEETS

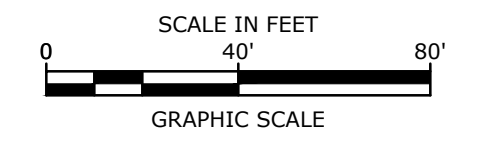
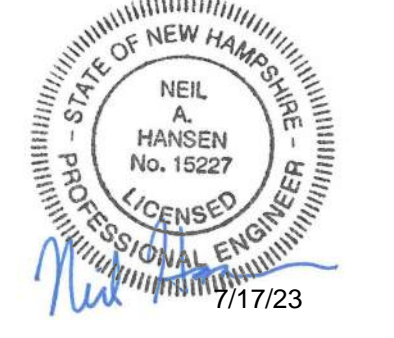
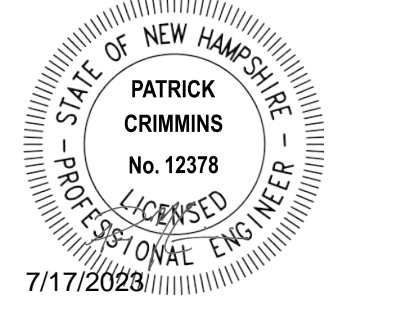
LEGEND

-  APPROXIMATE LIMIT OF PROPOSED SAW CUT
-  LIMIT OF WORK
-  TREELINE TO BE REMOVED
-  APPROXIMATE LIMIT OF PAVEMENT TO BE REMOVED
-  LOCATION OF PROPOSED BUILDING
-  PROPOSED CONSTRUCTION ENTRANCE
-  PROPOSED SILT SOCK
-  PROPOSED TEMPORARY SNOW FENCE
-  PROPOSED TREE PROTECTION
-  PROPOSED INLET PROTECTION BARRIER
-  TBR TO BE REMOVED
-  BLDG TO BE REMOVED
-  TYP TYPICAL
-  COORD COORDINATE
-  CONST CONSTRUCT

DEMOLITION NOTES:

1. THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES AND RELOCATE EXISTING UTILITIES REQUIRED TO COMPLETE THE WORK.
2. THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES. CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
3. ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES EXCEPT AS SPECIFIED IN NOTE #25.
4. COORDINATE REMOVAL, RELOCATION, DISPOSAL OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY.
5. ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO MATCH ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
6. SAW CUT AND REMOVE PAVEMENT ONE (1) FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN ALL AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO REMAIN.
7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL OF THE PERMIT APPROVALS.
8. THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR NECESSARY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION.
9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEMOLITION AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK, EXCEPT FOR WORK NOTED TO BE COMPLETED BY OTHERS AND AS SPECIFIED IN NOTE #25.
10. UTILITIES SHALL BE TERMINATED AT THE MAIN LINE PER UTILITY COMPANY AND THE CITY OF PORTSMOUTH STANDARDS. THE CONTRACTOR SHALL REMOVE ALL ABANDONED UTILITIES LOCATED WITHIN THE LIMITS OF WORK.
11. CONTRACTOR SHALL VERIFY ORIGIN OF ALL DRAINS AND UTILITIES PRIOR TO REMOVAL/TERMINATION TO DETERMINE IF DRAINS OR UTILITY IS ACTIVE, AND SERVICES ANY ON OR OFF-SITE STRUCTURE TO REMAIN. THE CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY SUCH UTILITY FOUND AND SHALL MAINTAIN THESE UTILITIES UNTIL PERMANENT SOLUTION IS IN PLACE.
12. PAVEMENT REMOVAL LIMITS ARE SHOWN FOR CONTRACTOR'S CONVENIENCE. ADDITIONAL PAVEMENT REMOVAL MAY BE REQUIRED DEPENDING ON THE CONTRACTOR'S OPERATION. CONTRACTOR TO VERIFY FULL LIMITS OF PAVEMENT REMOVAL PRIOR TO BID.
13. THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE PADS, UTILITIES AND PAVEMENT WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ITEMS TO BE REMOVED INCLUDE BUT ARE NOT LIMITED TO: CONCRETE, PAVEMENT, CURBS, LIGHTING, MANHOLES, CATCH BASINS, UNDER GROUND PIPING, POLES, STAIRS, SIGNS, FENCES, RAMPS, WALLS, BOLLARDS, BUILDING SLABS, FOUNDATION, TREES AND LANDSCAPING.
14. COORDINATE ALL WORK WITHIN THE PUBLIC RIGHT OF WAYS WITH THE CITY OF PORTSMOUTH AND PEASE DEVELOPMENT AUTHORITY.
15. REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL STUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF SITE IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL LAWS AND REGULATIONS.
16. CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED BY THE CONTRACTOR, THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO REPLACE DISTURBED MONUMENTS.
17. PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS/CURB INLETS WITHIN CONSTRUCTION LIMITS AS WELL AS CATCH BASINS/CURB INLETS THAT MAY RECEIVE RUNOFF FROM CONSTRUCTION ACTIVITIES. INLET PROTECTION BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE "HIGH FLOW SILT SACK" BY ACF ENVIRONMENTAL OR EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN EVENT OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED OR SEDIMENT HAS ACCUMULATED TO 1/3 THE DESIGN DEPTH OF THE BARRIER.
18. THE CONTRACTOR SHALL PHASE DEMOLITION AND CONSTRUCTION AS REQUIRED TO PROVIDE CONTINUOUS SERVICE TO EXISTING BUSINESSES THROUGHOUT THE CONSTRUCTION PERIOD. EXISTING BUSINESS SERVICES INCLUDE, BUT ARE NOT LIMITED TO ELECTRICAL, COMMUNICATION, FIRE PROTECTION, DOMESTIC WATER AND SEWER SERVICES. TEMPORARY SERVICES, IF REQUIRED, SHALL COMPLY WITH ALL FEDERAL, STATE, LOCAL AND UTILITY COMPANY STANDARDS. CONTRACTOR SHALL PROVIDE DETAILED CONSTRUCTION SCHEDULE TO OWNER PRIOR TO ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
19. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
20. THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
21. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL UTILITIES TO BE REMOVED AND PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN.
22. THE CONTRACTOR SHALL ACQUIRE A PDA DIG PERMIT BEFORE ANY EARTH DISTURBANCE CAN TAKE PLACE. ALLOW 7 CALENDAR DAYS FOR PROCESSING.
23. ALL MONITORING WELLS WITHIN LIMIT OF WORK SHALL BE PROTECTED DURING CONSTRUCTION. IF ANY MONITORING WELL NEEDS TO BE REMOVED OR ADJUSTED THIS WORK SHALL BE COORDINATED WITH THE PEASE DEVELOPMENT AUTHORITY.
24. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS PRIOR TO CONSTRUCTION.
25. ALL EXCESS SOIL RESULTING FROM THE CONSTRUCTION SHALL REMAIN ON SITE. COORDINATE WITH OWNER AND PEASE DEVELOPMENT AUTHORITY ON FINAL LOCATION OF EXCESS MATERIALS.
26. BEFORE ANY DEWATERING IS PERFORMED, COORDINATION BETWEEN THE OWNER, CONTRACTOR, PDA, NHDES AND THE AIR FORCE IS REQUIRED TO DETERMINE PROPER PROCEDURES AND PERMITTING REQUIRED. AT A MINIMUM A NHDES TEMPORARY DISCHARGE PERMIT IS REQUIRED.

Tighe & Bond



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission
MARK	DATE	DESCRIPTION

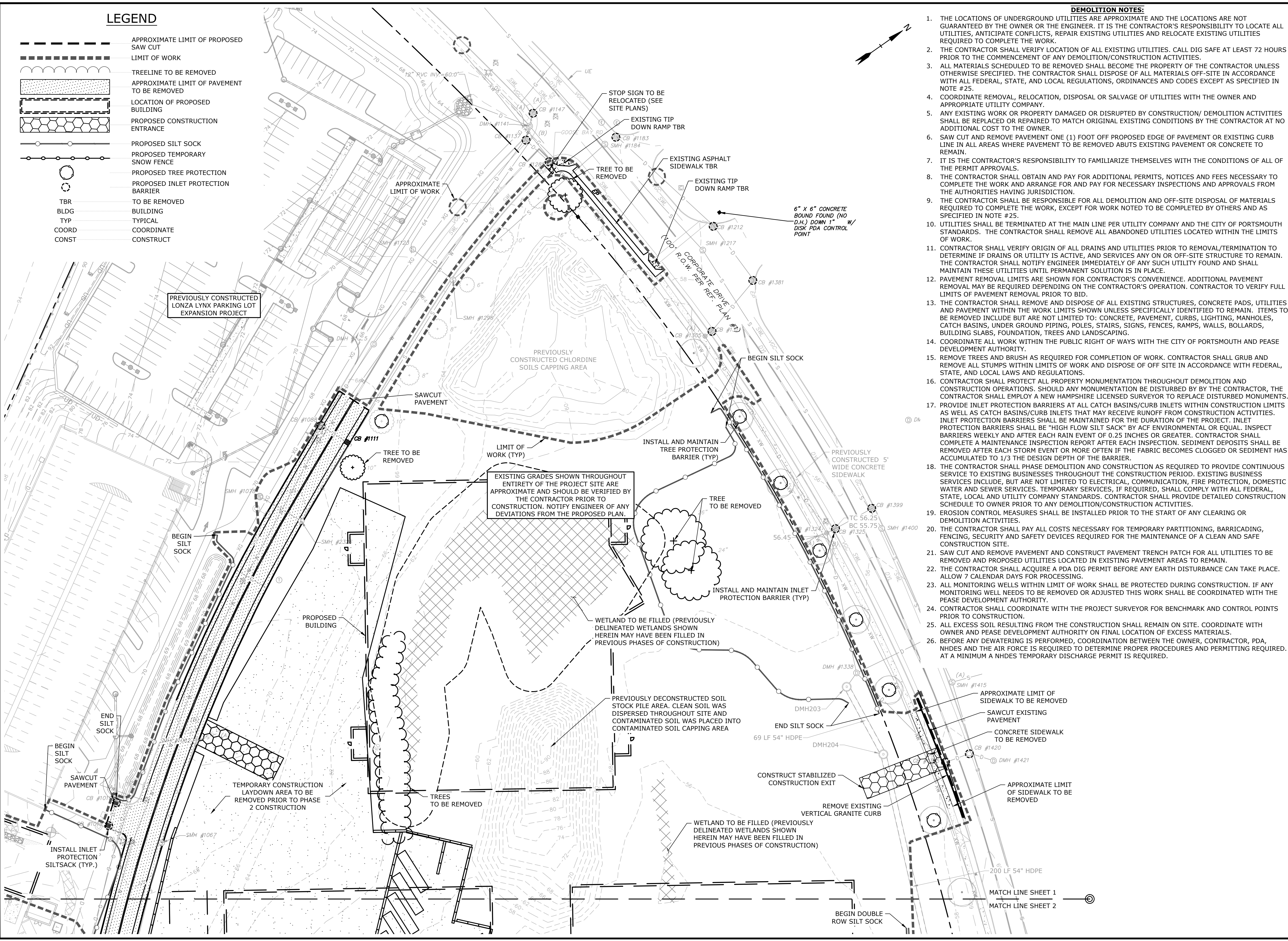
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DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

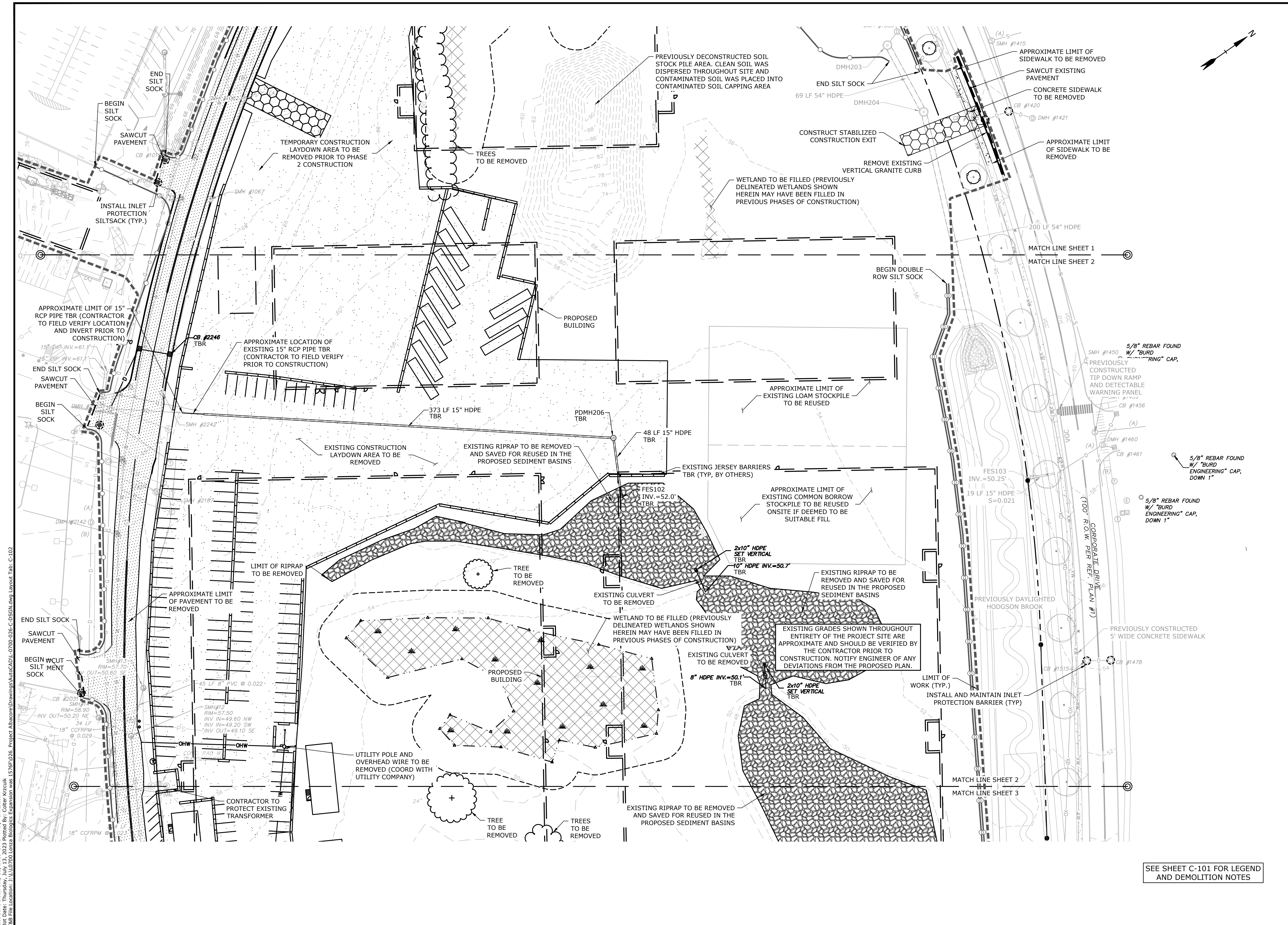
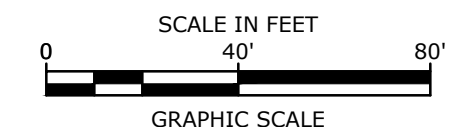
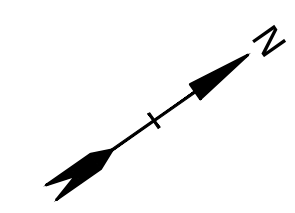
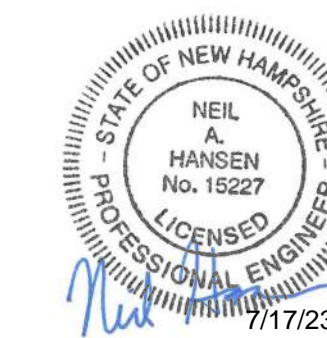
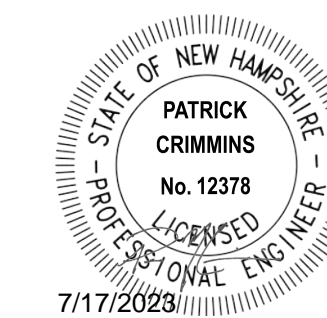
DEMOLITION PLAN

SCALE: AS SHOWN

C-101

Last Save Date: July 13, 2023 3:42 PM BY: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuk
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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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CHECKED:	NAH
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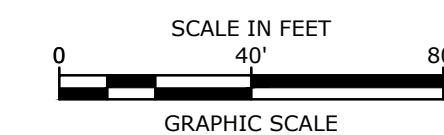
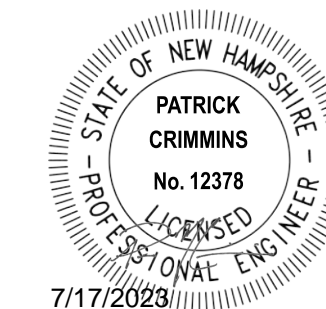
DEMOLITION PLAN

SCALE: AS SHOWN

C-102

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SEE SHEET C-101 FOR LEGEND AND DEMOLITION NOTES



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

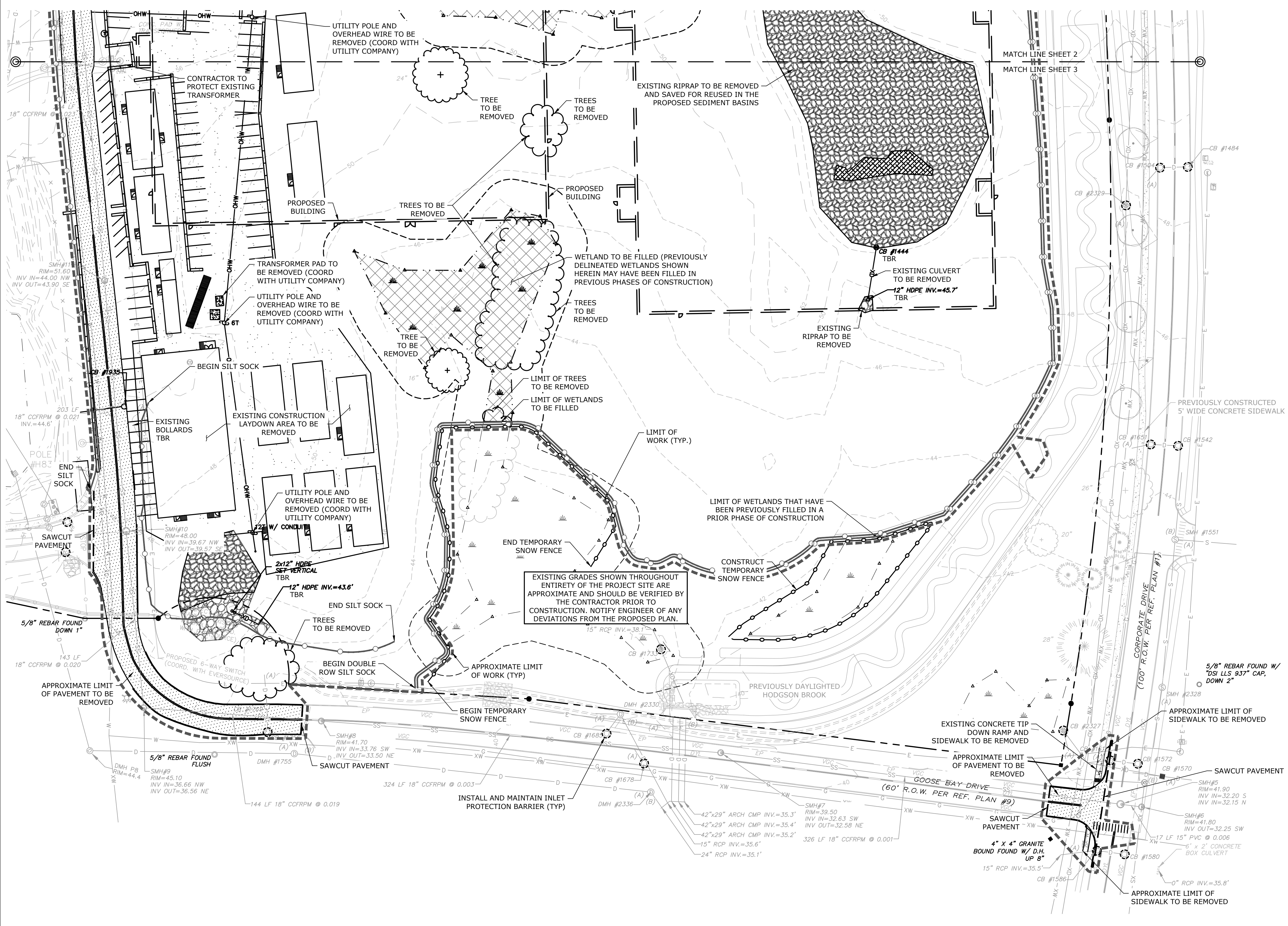
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K	5/5/2023	Phase 1B Issued for Bid
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PROJECT NO:	L-0700-013
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DRAWN BY:	CIK
CHECKED:	NAH
APPROVED:	PMC

DEMOLITION PLAN

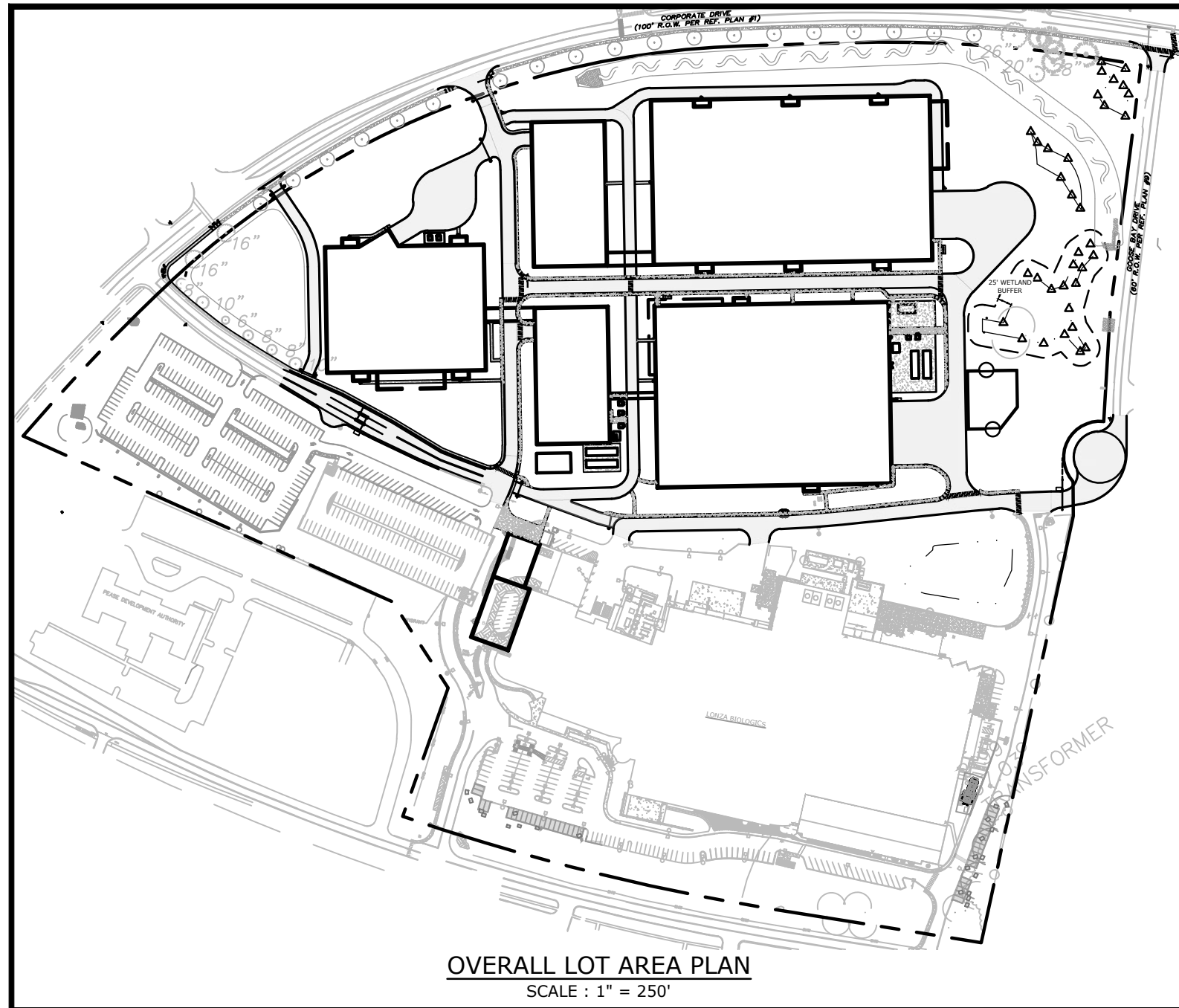
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C-103



SEE SHEET C-101 FOR LEGEND AND DEMOLITION NOTES

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 P&E File Location: J:\U0700 Lonza Biologics Expansion.was 15758.026 Project Abstract: Drawings\AutoCAD\U-0700-026-C-DSGN.dwg Layout Tab: C-103



OVERALL LOT AREA PLAN
SCALE: 1" = 250'

SITE DATA

LOCATION: TAX MAP 305, LOTS 1 & 2
70 & 80 CORPORATE DRIVE
PORTSMOUTH, NH

TAX MAP 305, LOT 6
101 INTERNATIONAL DRIVE
PORTSMOUTH, NH

ZONING DISTRICT: AIRPORT, BUSINESS & COMMERCIAL (ABC)

DIMENSIONAL REQUIREMENTS:

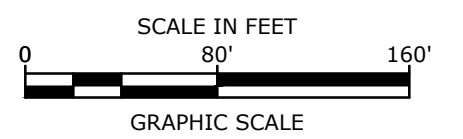
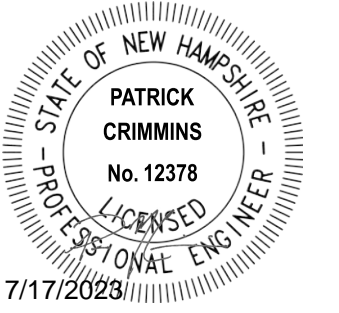
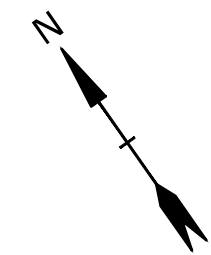
	REQUIRED	PROVIDED
MINIMUM LOT AREA:	5 AC	43.4± AC
MINIMUM STREET FRONTAGE:	200 FT	1,038 FT
MINIMUM FRONT YARD SETBACK:	70 FT	70 FT
SIDE SETBACK:	30 FT	30 FT
REAR SETBACK:	50 FT	51 FT
MINIMUM OPEN SPACE:	25 %	43.3± %

MAXIMUM STRUCTURE HEIGHT SHALL NOT EXCEED FAA CRITERIA.

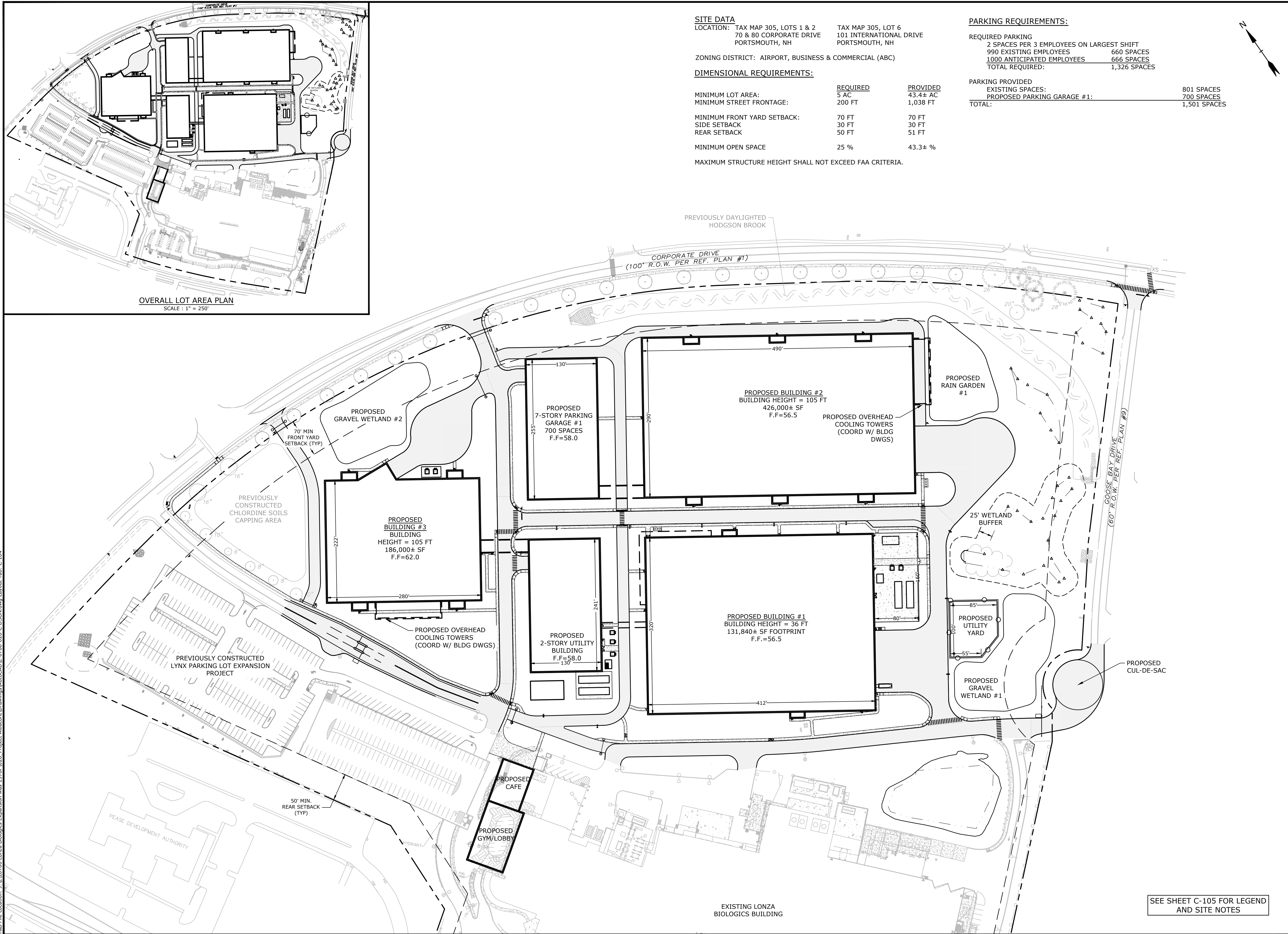
PARKING REQUIREMENTS:

REQUIRED PARKING
2 SPACES PER 3 EMPLOYEES ON LARGEST SHIFT
990 EXISTING EMPLOYEES 660 SPACES
1000 ANTICIPATED EMPLOYEES 666 SPACES
TOTAL REQUIRED: 1,326 SPACES

PARKING PROVIDED
EXISTING SPACES: 801 SPACES
PROPOSED PARKING GARAGE #1: 700 SPACES
TOTAL: 1,501 SPACES



Last Save Date: July 14, 2023 11:10 AM By: CKRCKUIK
 Plot Date: Monday, July 17, 2023 Plotted By: Colter Krzculik
 P&E File Location: J:\110702 Lonza Biologics Expansion.was 12762.026 Project Abstract\Drawings\AutoCAD\11-0702-026-C-DSGN.dwg Layout Tab: C-104



Proposed Industrial Development

Lonza Biologics

Portsmouth,
New Hampshire

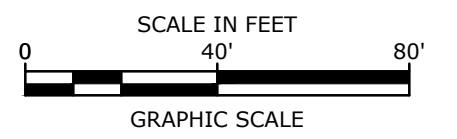
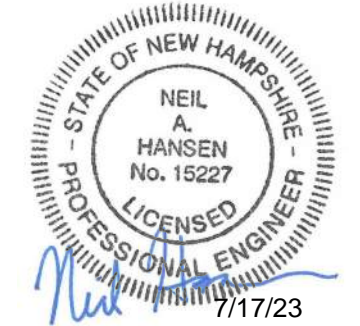
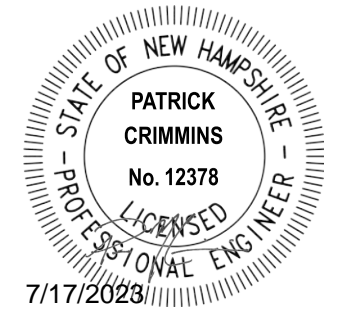
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DRAWN BY:	CJK
CHECKED BY:	NAH
APPROVED BY:	PMC

MASTER SITE PLAN

SCALE: AS SHOWN

SEE SHEET C-105 FOR LEGEND AND SITE NOTES



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
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F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

SITE PLAN

SCALE: AS SHOWN

C-105

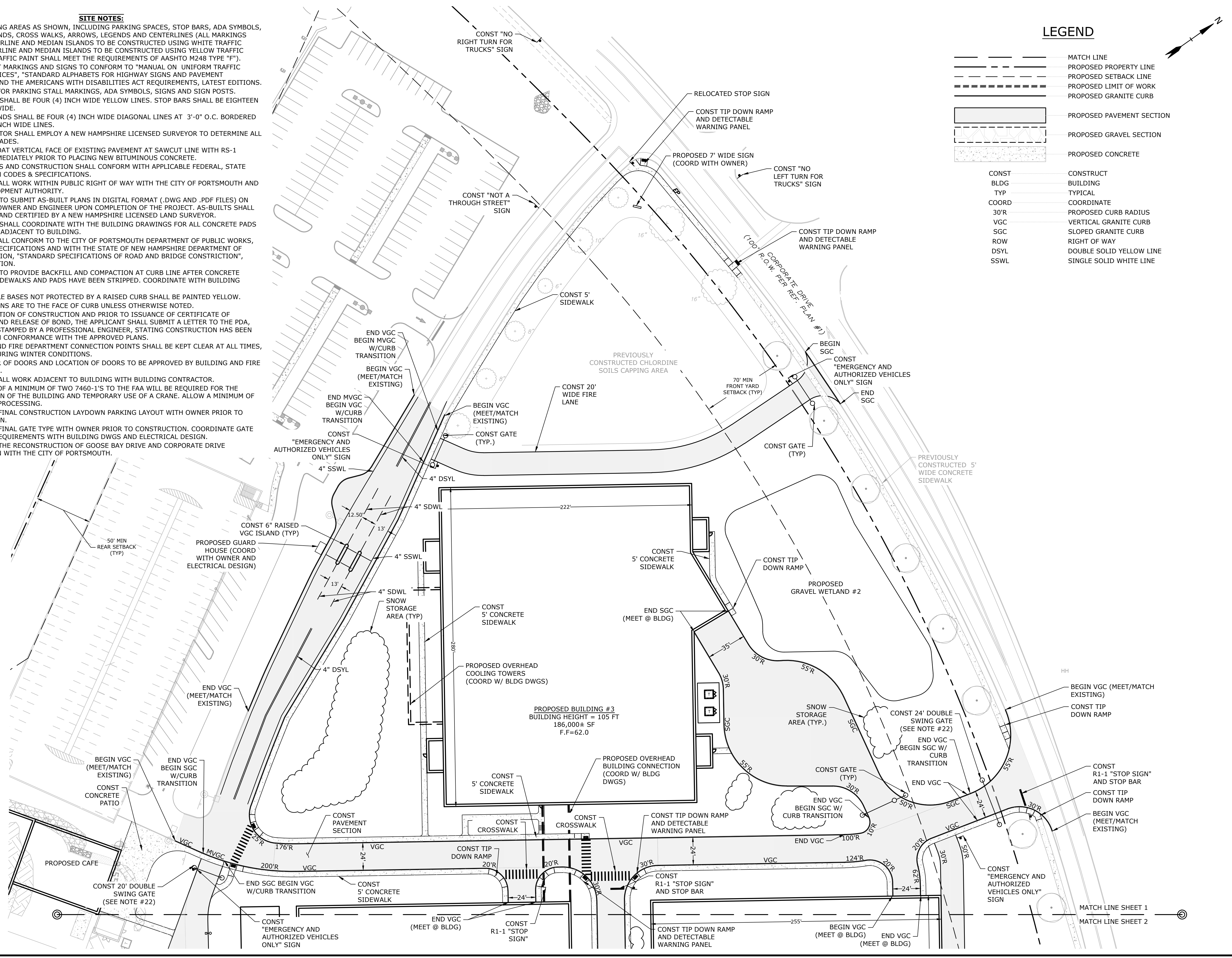
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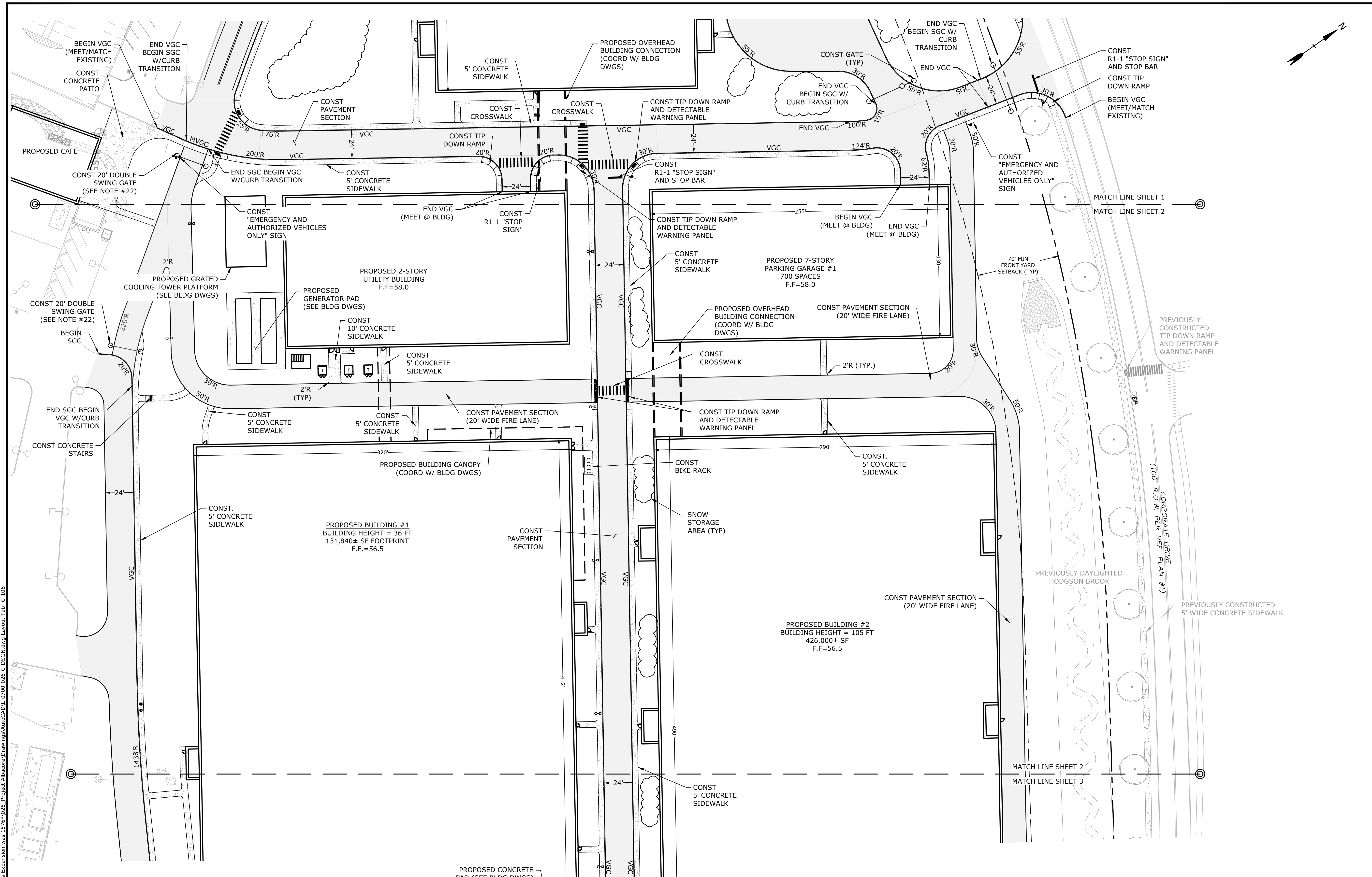
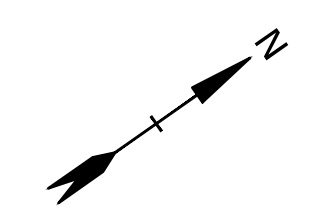
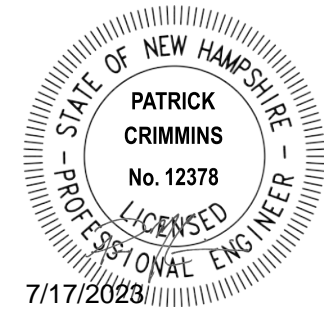
1. STRIPE PARKING AREAS AS SHOWN, INCLUDING PARKING SPACES, STOP BARS, ADA SYMBOLS, PAINTED ISLANDS, CROSS WALKS, ARROWS, LEGENDS AND CENTERLINES (ALL MARKINGS EXCEPT CENTERLINE AND MEDIAN ISLANDS TO BE CONSTRUCTED USING WHITE TRAFFIC PAINT. CENTERLINE AND MEDIAN ISLANDS TO BE CONSTRUCTED USING YELLOW TRAFFIC PAINT. ALL TRAFFIC PAINT SHALL MEET THE REQUIREMENTS OF AASHTO M248 TYPE "F").
2. ALL PAVEMENT MARKINGS AND SIGNS TO CONFORM TO "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES", "STANDARD ALPHABETS FOR HIGHWAY SIGNS AND PAVEMENT MARKINGS", AND THE AMERICANS WITH DISABILITIES ACT REQUIREMENTS, LATEST EDITIONS.
3. SEE DETAILS FOR PARKING STALL MARKINGS, ADA SYMBOLS, SIGNS AND SIGN POSTS.
4. CENTERLINES SHALL BE FOUR (4) INCH WIDE YELLOW LINES. STOP BARS SHALL BE EIGHTEEN (18) INCHES WIDE.
5. PAINTED ISLANDS SHALL BE FOUR (4) INCH WIDE DIAGONAL LINES AT 3'-0" O.C. BORDERED BY FOUR (4) INCH WIDE LINES.
6. THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO DETERMINE ALL LINES AND GRADES.
7. CLEAN AND COAT VERTICAL FACE OF EXISTING PAVEMENT AT SAWCUT LINE WITH RS-1 EMULSION IMMEDIATELY PRIOR TO PLACING NEW BITUMINOUS CONCRETE.
8. ALL MATERIALS AND CONSTRUCTION SHALL CONFORM WITH APPLICABLE FEDERAL, STATE AND/OR TOWN CODES & SPECIFICATIONS.
9. COORDINATE ALL WORK WITHIN PUBLIC RIGHT OF WAY WITH THE CITY OF PORTSMOUTH AND PEASE DEVELOPMENT AUTHORITY.
10. CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
11. CONTRACTOR SHALL COORDINATE WITH THE BUILDING DRAWINGS FOR ALL CONCRETE PADS & SIDEWALKS ADJACENT TO BUILDING.
12. ALL WORK SHALL CONFORM TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS, STANDARD SPECIFICATIONS AND WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, "STANDARD SPECIFICATIONS OF ROAD AND BRIDGE CONSTRUCTION", CURRENT EDITION.
13. CONTRACTOR TO PROVIDE BACKFILL AND COMPACTION AT CURB LINE AFTER CONCRETE FORMS FOR SIDEWALKS AND PADS HAVE BEEN STRIPPED. COORDINATE WITH BUILDING CONTRACTOR.
14. ALL LIGHT POLE BASES NOT PROTECTED BY A RAISED CURB SHALL BE PAINTED YELLOW.
15. ALL DIMENSIONS ARE TO THE FACE OF CURB UNLESS OTHERWISE NOTED.
16. UPON COMPLETION OF CONSTRUCTION AND PRIOR TO ISSUANCE OF CERTIFICATE OF OCCUPANCY AND RELEASE OF BOND, THE APPLICANT SHALL SUBMIT A LETTER TO THE PDA, SIGNED AND STAMPED BY A PROFESSIONAL ENGINEER, STATING CONSTRUCTION HAS BEEN COMPLETED IN CONFORMANCE WITH THE APPROVED PLANS.
17. FIRE LANES AND FIRE DEPARTMENT CONNECTION POINTS SHALL BE KEPT CLEAR AT ALL TIMES, INCLUDING DURING WINTER CONDITIONS.
18. FINAL NUMBER OF DOORS AND LOCATION OF DOORS TO BE APPROVED BY BUILDING AND FIRE DEPARTMENTS.
19. COORDINATE ALL WORK ADJACENT TO BUILDING WITH BUILDING CONTRACTOR.
20. SUBMISSION OF A MINIMUM OF TWO 7460-1'S TO THE FAA WILL BE REQUIRED FOR THE CONSTRUCTION OF THE BUILDING AND TEMPORARY USE OF A CRANE. ALLOW A MINIMUM OF 45 DAYS FOR PROCESSING.
21. COORDINATE FINAL CONSTRUCTION LAYDOWN PARKING LAYOUT WITH OWNER PRIOR TO CONSTRUCTION.
22. COORDINATE FINAL GATE TYPE WITH OWNER PRIOR TO CONSTRUCTION. COORDINATE GATE ELECTRICAL REQUIREMENTS WITH BUILDING DWGS AND ELECTRICAL DESIGN.
23. COORDINATE THE RECONSTRUCTION OF GOOSE BAY DRIVE AND CORPORATE DRIVE INTERSECTION WITH THE CITY OF PORTSMOUTH.

LEGEND

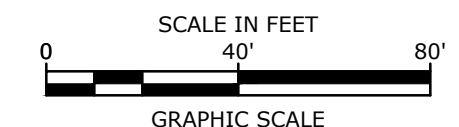
- MATCH LINE
- - - - PROPOSED PROPERTY LINE
- - - - PROPOSED SETBACK LINE
- - - - PROPOSED LIMIT OF WORK
- - - - PROPOSED GRANITE CURB
- [Pattern] PROPOSED PAVEMENT SECTION
- [Pattern] PROPOSED GRAVEL SECTION
- [Pattern] PROPOSED CONCRETE
- CONST --- CONSTRUCT
- BLDG --- BUILDING
- TYP --- TYPICAL
- COORD --- COORDINATE
- 30'R --- PROPOSED CURB RADIUS
- VGC --- VERTICAL GRANITE CURB
- SGC --- SLOPED GRANITE CURB
- ROW --- RIGHT OF WAY
- DSYL --- DOUBLE SOLID YELLOW LINE
- SSWL --- SINGLE SOLID WHITE LINE

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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
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MATCH LINE SHEET 1
MATCH LINE SHEET 2



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

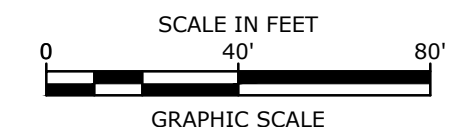
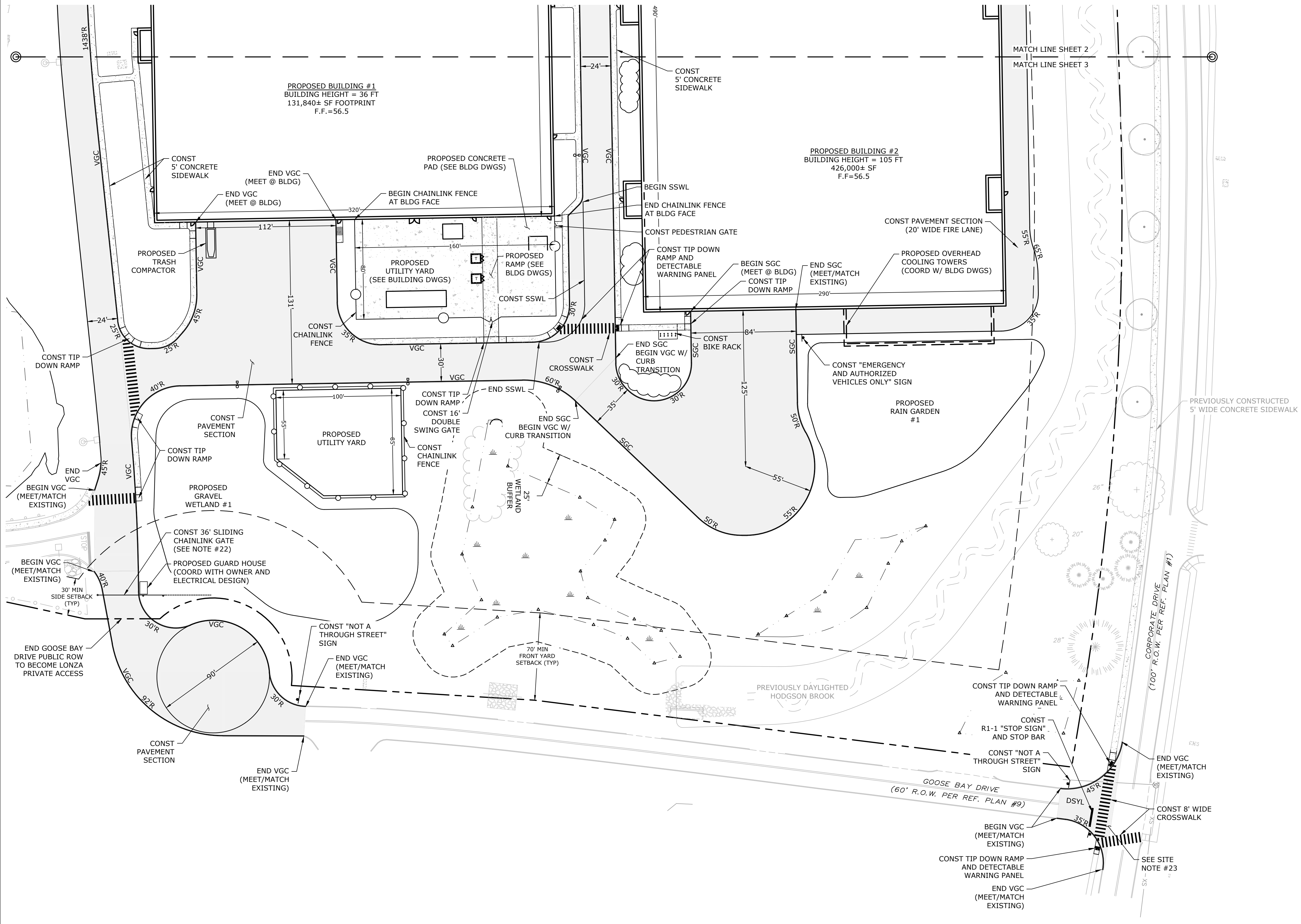
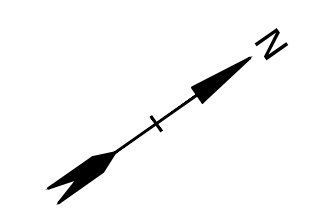
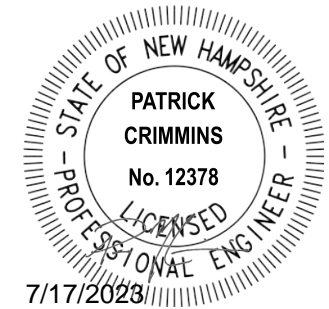
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DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

SEE SHEET C-105 FOR LEGEND AND SITE NOTES

SITE PLAN
SCALE: AS SHOWN
C-106

Last Save Date: July 13, 2023 3:42 PM By: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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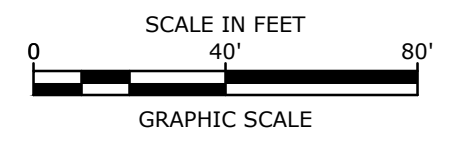
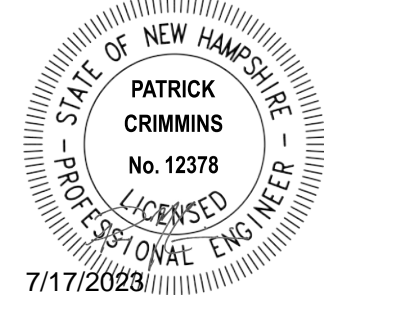
SITE PLAN

SCALE: AS SHOWN

C-107

SEE SHEET C-105 FOR LEGEND AND SITE NOTES

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Proposed Industrial Development
Lonza Biologics

Portsmouth, New Hampshire

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APPROVED:	PMC

GRADING, DRAINAGE & EROSION CONTROL PLAN

SCALE: AS SHOWN

GRADING AND DRAINAGE NOTES:

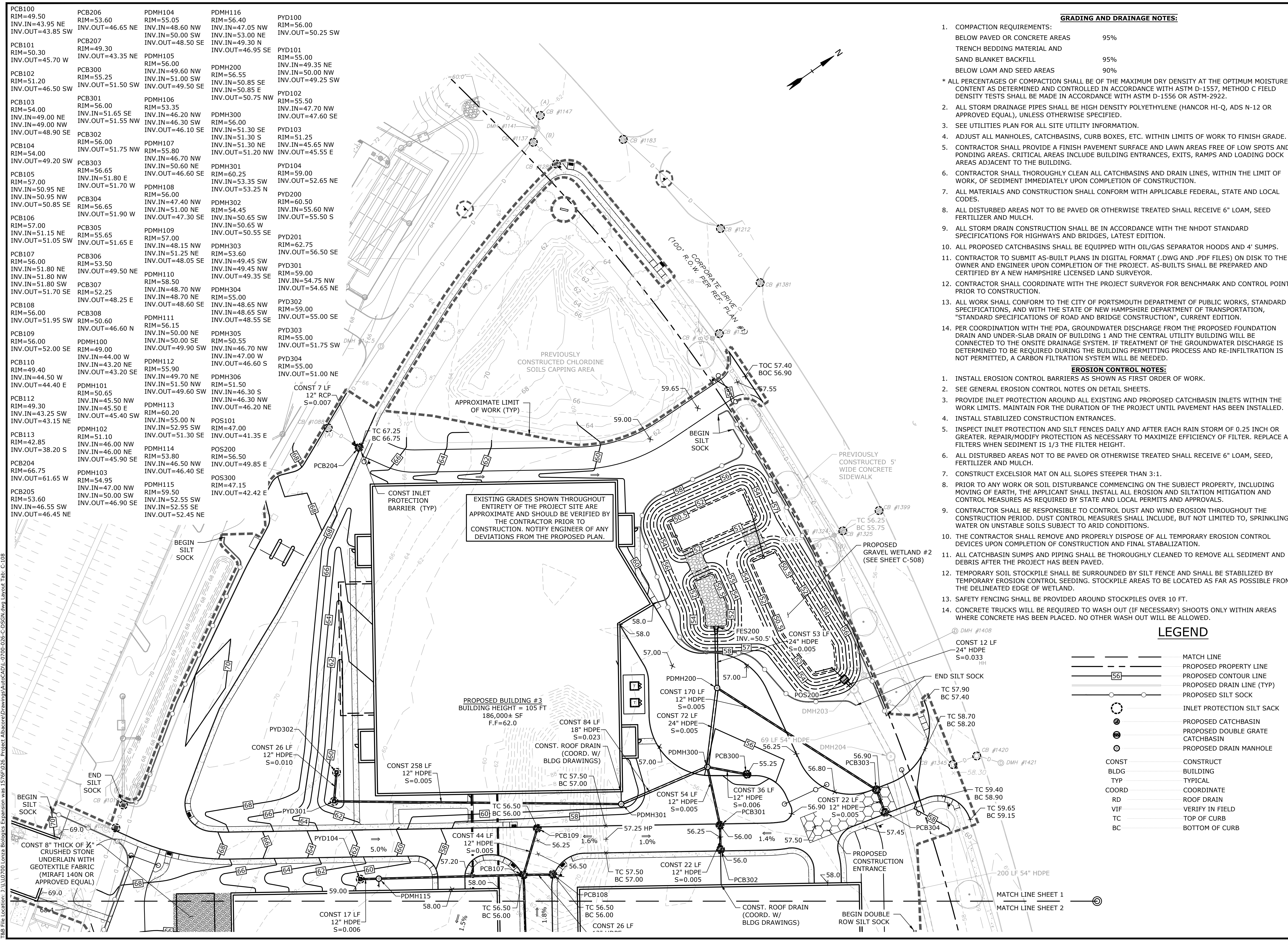
1. COMPACTION REQUIREMENTS:
BELOW PAVED OR CONCRETE AREAS 95%
TRENCH BEDDING MATERIAL AND SAND BLANKET BACKFILL 95%
BELOW LOAM AND SEED AREAS 90%
* ALL PERCENTAGES OF COMPACTION SHALL BE OF THE MAXIMUM DRY DENSITY AT THE OPTIMUM MOISTURE CONTENT AS DETERMINED AND CONTROLLED IN ACCORDANCE WITH ASTM D-1557, METHOD C FIELD DENSITY TESTS SHALL BE MADE IN ACCORDANCE WITH ASTM D-1556 OR ASTM-2922.
2. ALL STORM DRAINAGE PIPES SHALL BE HIGH DENSITY POLYETHYLENE (HANCOR HI-Q, ADS N-12 OR APPROVED EQUAL), UNLESS OTHERWISE SPECIFIED.
3. SEE UTILITIES PLAN FOR ALL SITE UTILITY INFORMATION.
4. ADJUST ALL MANHOLES, CATCHBASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE.
5. CONTRACTOR SHALL PROVIDE A FINISH PAVEMENT SURFACE AND LAWN AREAS FREE OF LOW SPOTS AND PONDING AREAS. CRITICAL AREAS INCLUDE BUILDING ENTRANCES, EXITS, RAMPS AND LOADING DOCK AREAS ADJACENT TO THE BUILDING.
6. CONTRACTOR SHALL THOROUGHLY CLEAN ALL CATCHBASINS AND DRAIN LINES, WITHIN THE LIMIT OF WORK, OF SEDIMENT IMMEDIATELY UPON COMPLETION OF CONSTRUCTION.
7. ALL MATERIALS AND CONSTRUCTION SHALL CONFORM WITH APPLICABLE FEDERAL, STATE AND LOCAL CODES.
8. ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED SHALL RECEIVE 6" LOAM, SEED FERTILIZER AND MULCH.
9. ALL STORM DRAIN CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE NHDOT STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES, LATEST EDITION.
10. ALL PROPOSED CATCHBASINS SHALL BE EQUIPPED WITH OIL/GAS SEPARATOR HOODS AND 4' SUMPS.
11. CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
12. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS PRIOR TO CONSTRUCTION.
13. ALL WORK SHALL CONFORM TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS, STANDARD SPECIFICATIONS, AND WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, "STANDARD SPECIFICATIONS OF ROAD AND BRIDGE CONSTRUCTION", CURRENT EDITION.
14. PER COORDINATION WITH THE PDA, GROUNDWATER DISCHARGE FROM THE PROPOSED FOUNDATION DRAIN AND UNDER-SLAB DRAIN OF BUILDING 1 AND THE CENTRAL UTILITY BUILDING WILL BE CONNECTED TO THE ONSITE DRAINAGE SYSTEM. IF TREATMENT OF THE GROUNDWATER DISCHARGE IS DETERMINED TO BE REQUIRED DURING THE BUILDING PERMITTING PROCESS AND RE-INFILTRATION IS NOT PERMITTED, A CARBON FILTRATION SYSTEM WILL BE NEEDED.

EROSION CONTROL NOTES:

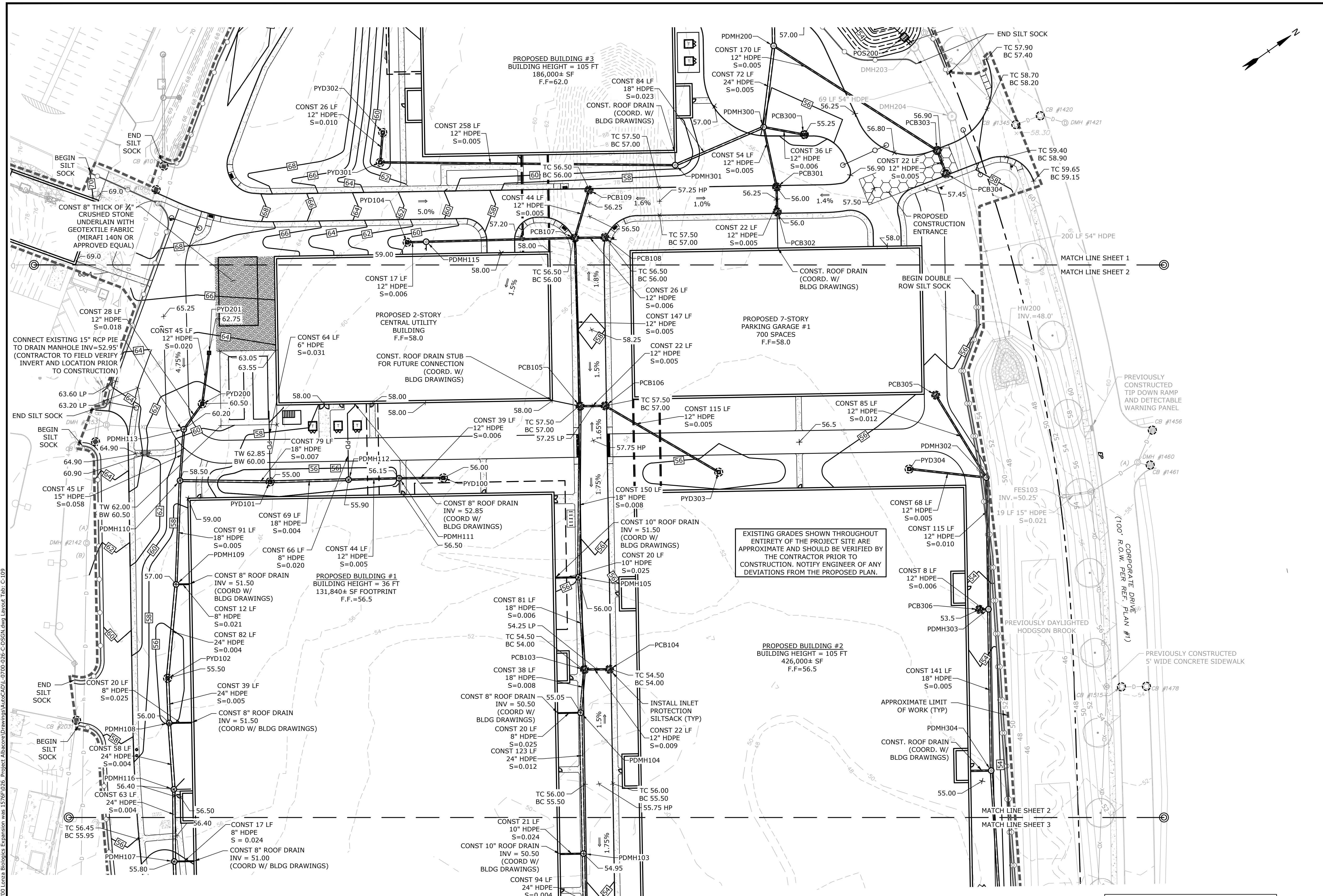
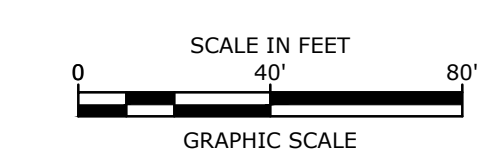
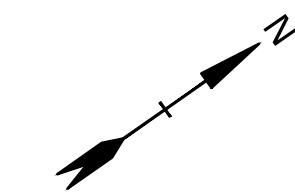
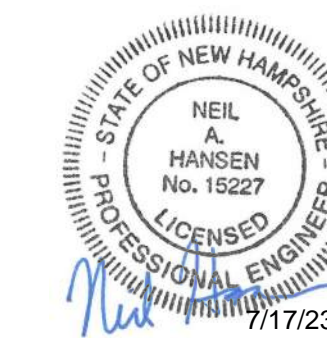
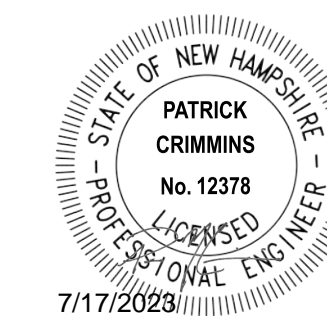
1. INSTALL EROSION CONTROL BARRIERS AS SHOWN AS FIRST ORDER OF WORK.
2. SEE GENERAL EROSION CONTROL NOTES ON DETAIL SHEETS.
3. PROVIDE INLET PROTECTION AROUND ALL EXISTING AND PROPOSED CATCHBASIN INLETS WITHIN THE WORK LIMITS. MAINTAIN FOR THE DURATION OF THE PROJECT UNTIL PAVEMENT HAS BEEN INSTALLED.
4. INSTALL STABILIZED CONSTRUCTION ENTRANCES.
5. INSPECT INLET PROTECTION AND SILT FENCES DAILY AND AFTER EACH RAIN STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER HEIGHT.
6. ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED SHALL RECEIVE 6" LOAM, SEED, FERTILIZER AND MULCH.
7. CONSTRUCT EXCELSIOR MAT ON ALL SLOPES STEEPER THAN 3:1.
8. PRIOR TO ANY WORK OR SOIL DISTURBANCE COMMENCING ON THE SUBJECT PROPERTY, INCLUDING MOVING OF EARTH, THE APPLICANT SHALL INSTALL ALL EROSION AND SILTATION MITIGATION AND CONTROL MEASURES AS REQUIRED BY STATE AND LOCAL PERMITS AND APPROVALS.
9. CONTRACTOR SHALL BE RESPONSIBLE TO CONTROL DUST AND WIND EROSION THROUGHOUT THE CONSTRUCTION PERIOD. DUST CONTROL MEASURES SHALL INCLUDE, BUT NOT LIMITED TO, SPRINKLING WATER ON UNSTABLE SOILS SUBJECT TO ARID CONDITIONS.
10. THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION AND FINAL STABILIZATION.
11. ALL CATCHBASIN SUMPS AND PIPING SHALL BE THOROUGHLY CLEANED TO REMOVE ALL SEDIMENT AND DEBRIS AFTER THE PROJECT HAS BEEN PAVED.
12. TEMPORARY SOIL STOCKPILE SHALL BE SURROUNDED BY SILT FENCE AND SHALL BE STABILIZED BY TEMPORARY EROSION CONTROL SEEDING. STOCKPILE AREAS TO BE LOCATED AS FAR AS POSSIBLE FROM THE DELINEATED EDGE OF WETLAND.
13. SAFETY FENCING SHALL BE PROVIDED AROUND STOCKPILES OVER 10 FT.
14. CONCRETE TRUCKS WILL BE REQUIRED TO WASH OUT (IF NECESSARY) SHOOT ONLY WITHIN AREAS WHERE CONCRETE HAS BEEN PLACED. NO OTHER WASH OUT WILL BE ALLOWED.

LEGEND

---	MATCH LINE
---	PROPOSED PROPERTY LINE
---	PROPOSED CONTOUR LINE
---	PROPOSED DRAIN LINE (TYP)
---	PROPOSED SILT SOCK
○	INLET PROTECTION SILT SACK
⊙	PROPOSED CATCHBASIN
⊙	PROPOSED DOUBLE GRATE CATCHBASIN
⊙	PROPOSED DRAIN MANHOLE
---	CONSTRUCT
---	BUILDING
---	TYP
---	COORD
---	RD
---	VF
---	TC
---	BC



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EXISTING GRADES SHOWN THROUGHOUT ENTIRETY OF THE PROJECT SITE ARE APPROXIMATE AND SHOULD BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. NOTIFY ENGINEER OF ANY DEVIATIONS FROM THE PROPOSED PLAN.

SEE SHEET C-108 FOR LEGEND GRADING, DRAINAGE & EROSION CONTROL NOTES, & DRAINAGE STRUCTURE TABLE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

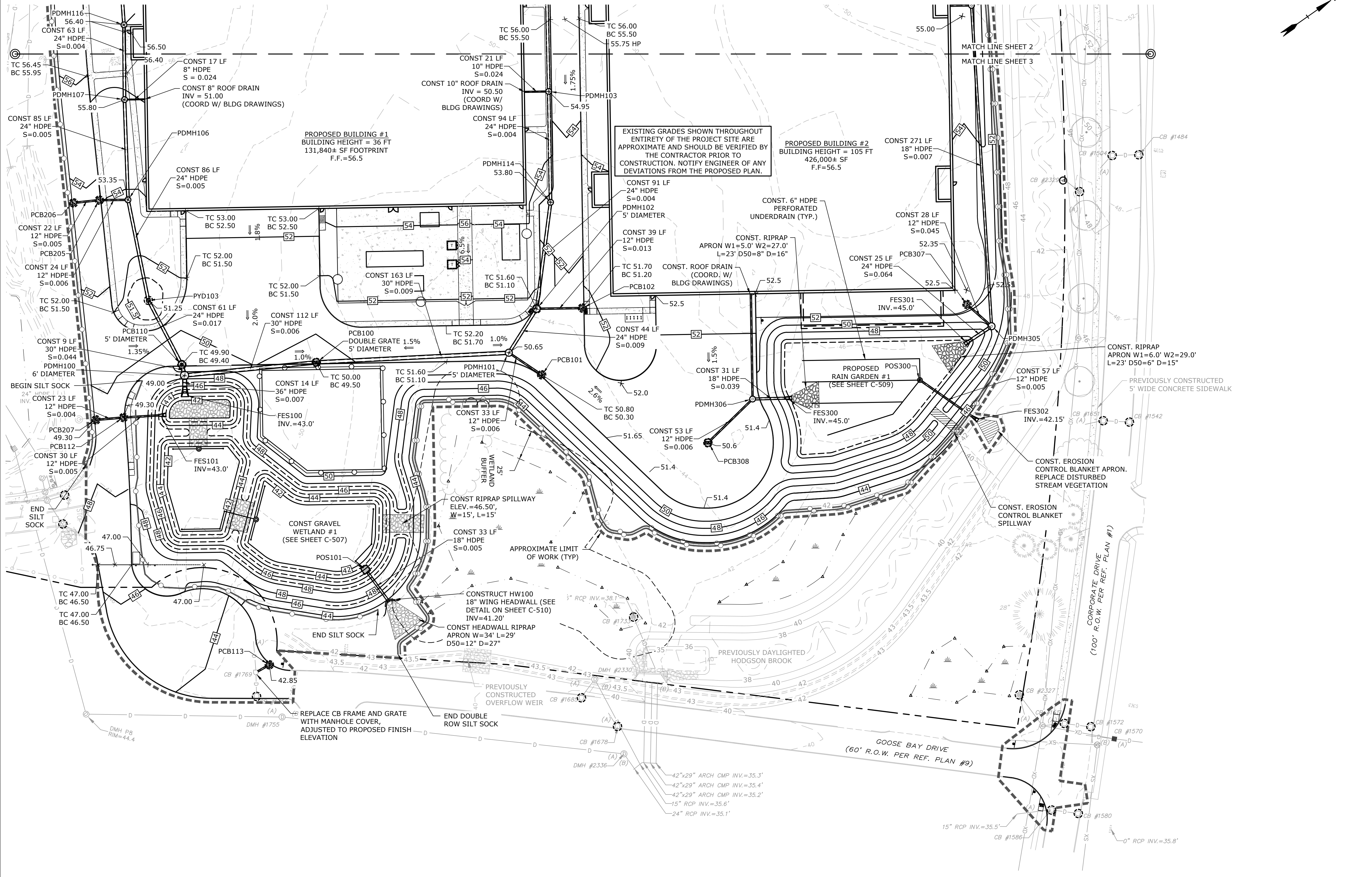
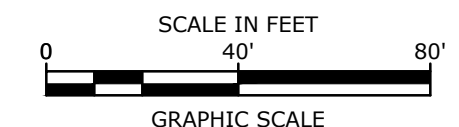
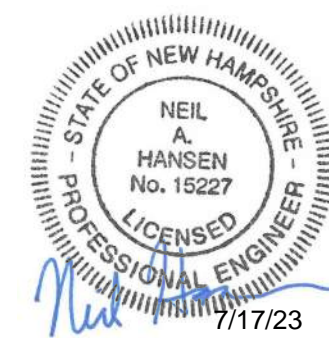
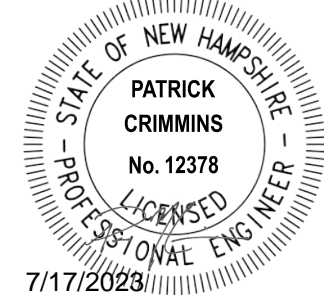
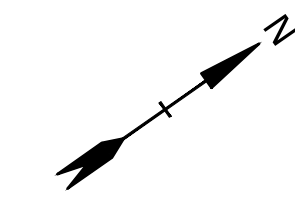
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GRADING, DRAINAGE & EROSION CONTROL PLAN

SCALE: AS SHOWN

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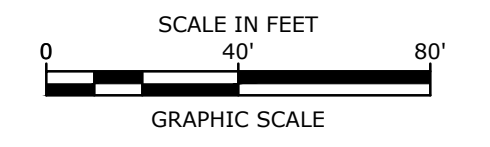
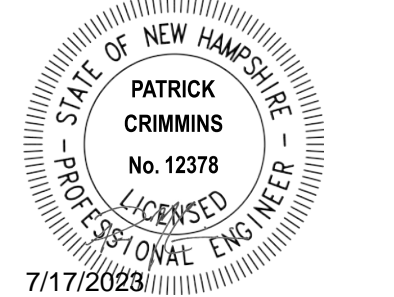
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LEGEND

---	MATCH LINE
D	EXISTING STORM DRAIN
SS	EXISTING SANITARY SEWER
W	EXISTING WATER
G	EXISTING GAS
E	EXISTING UNDERGROUND ELECTRIC
OHW	EXISTING OVERHEAD UTILITY
---	PROPOSED STORM DRAIN
---	PROPOSED SANITARY SEWER
PW	PROPOSED WATER
G	PROPOSED GAS
---	PROPOSED UNDERGROUND ELECTRIC
---	PROPOSED UNDERGROUND COMMUNICATION
⊙	EXISTING CATCHBASIN
⊙	EXISTING DRAIN MANHOLE
⊙	EXISTING SEWER MANHOLE
⊙	EXISTING HYDRANT
⊙	EXISTING WATER VALVE
⊙	EXISTING ELECTRIC MANHOLE
⊙	EXISTING TELEPHONE MANHOLE
⊙	PROPOSED CATCHBASIN
⊙	PROPOSED DOUBLE GRATE CATCHBASIN
⊙	PROPOSED DRAIN MANHOLE
⊙	PROPOSED SEWER MANHOLE
⊙	PROPOSED WATER VALVE
⊙	PROPOSED FDC CONNECTION
⊙	PROPOSED HYDRANT
⊙	PROPOSED GAS VALVE
⊙	PROPOSED ELECTRIC MANHOLE
⊙	PROPOSED TRANSFORMER PAD
⊙	PROPOSED LIGHT POLE BASE
---	CONST. BUILDING
---	CONST. TYPICAL
---	COORD. COORDINATE
---	VIF. VERIFY IN FIELD
---	DI. DUCTILE IORN
---	COM. COMMUNICATION
---	FRP. FIBERGLASS REINFORCED POLYMER MORTAR PIPE

UTILITY NOTES:

- THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES, AND RELOCATE EXISTING UTILITIES REQUIRED TO COMPLETE THE WORK AT NO ADDITIONAL COST TO THE OWNER.
- COORDINATE ALL UTILITY WORK WITH APPROPRIATE UTILITY COMPANY.
NATURAL GAS - UNITIL
WATER - CITY OF PORTSMOUTH DPW
SEWER - CITY OF PORTSMOUTH DPW
ELECTRIC - EVERSOURCE
COMMUNICATIONS - FAIRPOINT, COMCAST, FIRSTLIGHT
- SEE EXISTING CONDITIONS PLAN FOR BENCHMARK INFORMATION.
- SEE GRADING, DRAINAGE & EROSION CONTROL PLAN FOR PROPOSED GRADING AND EROSION CONTROL MEASURES.
- ALL WATER MAIN INSTALLATIONS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE.
- ALL WATER MAIN INSTALLATIONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION PRIOR TO ACTIVATING THE SYSTEM. CONTRACTOR SHALL COORDINATE CHLORINATION AND TESTING WITH THE CITY OF PORTSMOUTH WATER DEPARTMENT.
- ALL SEWER PIPE SHALL BE FIBERGLASS REINFORCED POLYMER MORTAR (FRP) PIPE UNLESS OTHERWISE STATED.
- ALL WORK WITHIN PORTSMOUTH ROWS SHALL BE COORDINATED WITH CITY OF PORTSMOUTH AND THE PEASE DEVELOPMENT AUTHORITY.
- CONTRACTOR SHALL MAINTAIN UTILITY SERVICES TO ABUTTING PROPERTIES THROUGHOUT CONSTRUCTION.
- CONNECTIONS TO EXISTING WATER MAIN SHALL BE CONSTRUCTED TO CITY OF PORTSMOUTH STANDARDS.
- EXISTING UTILITIES TO BE REMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER SERVICES.
- ALL ELECTRICAL MATERIAL WORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC CODE, LATEST EDITION, AND ALL APPLICABLE STATE AND LOCAL CODES.
- THE EXACT LOCATION OF NEW UTILITY SERVICES AND CONNECTIONS SHALL BE COORDINATED WITH THE BUILDING DRAWINGS AND THE UTILITY COMPANIES.
- ADJUST ALL MANHOLES, CATCH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE.
- ALL UNDERGROUND CONDUITS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING CABLES.
- THE CONTRACTOR SHALL OBTAIN, PAY FOR, AND COMPLY WITH ALL REQUIRED PERMITS, ARRANGE FOR ALL INSPECTIONS, AND SUBMIT COPIES OF ACCEPTANCE CERTIFICATES TO THE OWNER PRIOR TO THE COMPLETION OF THIS PROJECT.
- THE CONTRACTOR SHALL PROVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS, CONNECTORS, COVER PLATES, AND OTHER MISCELLANEOUS ITEMS NOT NECESSARILY DETAILED ON THESE DRAWINGS TO RENDER INSTALLATION OF UTILITIES COMPLETE AND OPERATIONAL.
- CONTRACTOR SHALL PROVIDE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR NATURAL GAS SERVICES.
- A 10-FOOT MINIMUM EDGE TO EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL WATER AND SANITARY SEWER LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION SHALL BE PROVIDED AT ALL WATER/SANITARY SEWER CROSSINGS.
- THE CONTRACTOR SHALL CONTACT "DIG-SAFE" 72 HOURS PRIOR TO COMMENCING CONSTRUCTION. THE CONTRACTOR SHALL HAVE THE "DIG-SAFE" NUMBER ON SITE AT ALL TIMES.
- CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
- SAWCUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN.
- HYDRANTS, GATE VALVES, FITTINGS, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF PORTSMOUTH AND THE PEASE DEVELOPMENT AUTHORITY.
- COORDINATE TESTING OF SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH.
- ALL SEWER PIPE WITH LESS THAN 6' OF COVER IN PAVED AREAS OR LESS THAN 4' OF COVER IN UNPAVED AREAS SHALL BE INSULATED.
- CONTRACTOR SHALL COORDINATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, MANHOLE CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RELOCATION, AND TRANSFORMER CONSTRUCTION WITH POWER COMPANY.
- CONTRACTOR SHALL PHASE UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN CONSTRUCTION, AS TO MAINTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL COORDINATE TEMPORARY SERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER.
- SITE LIGHTING SPECIFICATIONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND SIGN ILLUMINATION SHALL BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER.
- CONTRACTOR SHALL CONSTRUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE FOUNDATION WALLS AND CONNECT THESE TO SERVICE STUBS FROM THE BUILDING.
- EXISTING SEWER MAIN AND STRUCTURES IN GOOSE BAY DRIVE ARE BASED ON A PROPOSED DESIGN BY UNDERWOOD ENGINEERS, DATED JULY 28, 2017, AND WAS CONSTRUCTED IN SUMMER 2018. THE PROPOSED ON-SITE SEWER DESIGN ELEVATIONS ARE BASED ON THE UNDERWOOD PLAN DURING CONSTRUCTION. THE CONTRACTOR SHALL COORDINATE SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH, AND VERIFY ALL INVERTS PRIOR TO CONSTRUCTION.
- LOCATION SHOWN IS APPROXIMATE ONLY. FINAL DESIGN OF NATURAL GAS SERVICE TO BE COMPLETED BY UNITIL. WORK IN CORPORATE DRIVE MAY NEED TO BE COMPLETED IN CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE. COORDINATE WITH CITY OF PORTSMOUTH AND UNITIL.
- LOCATION AND TYPE SHOWN IS APPROXIMATE ONLY. FINAL DESIGN OF ELECTRIC SERVICE AND ASSOCIATED INFRASTRUCTURE TO BE COMPLETED BY EVERSOURCE. WORK IN CORPORATE DRIVE MAY NEED TO BE COMPLETED IN CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE. COORDINATE WITH CITY OF PORTSMOUTH AND EVERSOURCE.
- FINAL LOCATION OF ALL WATER METER AND VALVES SHALL BE COORDINATED WITH THE CITY OF PORTSMOUTH DPW PRIOR TO CONSTRUCTION.
- FINAL LOCATION OF FIRE HYDRANTS, FIRE DEPARTMENT CONNECTIONS AND DRY STAND PIPES WILL BE COORDINATED WITH THE BUILDING DRAWINGS AND APPROVED BY THE PORTSMOUTH FIRE DEPARTMENT PRIOR TO CONSTRUCTION.
- THE APPLICANT SHALL HAVE A SITE SURVEY CONDUCTED BY A RADIO COMMUNICATIONS CARRIER APPROVED BY THE CITY'S COMMUNICATIONS DIVISION. THE RADIO COMMUNICATIONS CARRIER MUST BE FAMILIAR AND CONVERSANT WITH THE POLICE AND RADIO CONFIGURATION. IF THE SITE SURVEY INDICATES IT IS NECESSARY TO INSTALL A SIGNAL REPEATER EITHER ON OR NEAR THE PROPOSED PROJECT, THOSE COSTS SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER. THE OWNER SHALL COORDINATE WITH THE SUPERVISOR OF RADIO COMMUNICATIONS FOR THE CITY.
- CONTRACTOR SHALL PERFORM TEST PITS TO VERIFY INVERT ELEVATIONS IN FIELD PRIOR TO CONSTRUCTION AND SHALL NOTIFY ENGINEER IF ELEVATION DIFFERS FROM PLAN.
- CONTRACTOR SHALL DISPOSE OF ASBESTOS CEMENT PIPES IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS SHOULD ANY BE FOUND DURING CONSTRUCTION.



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

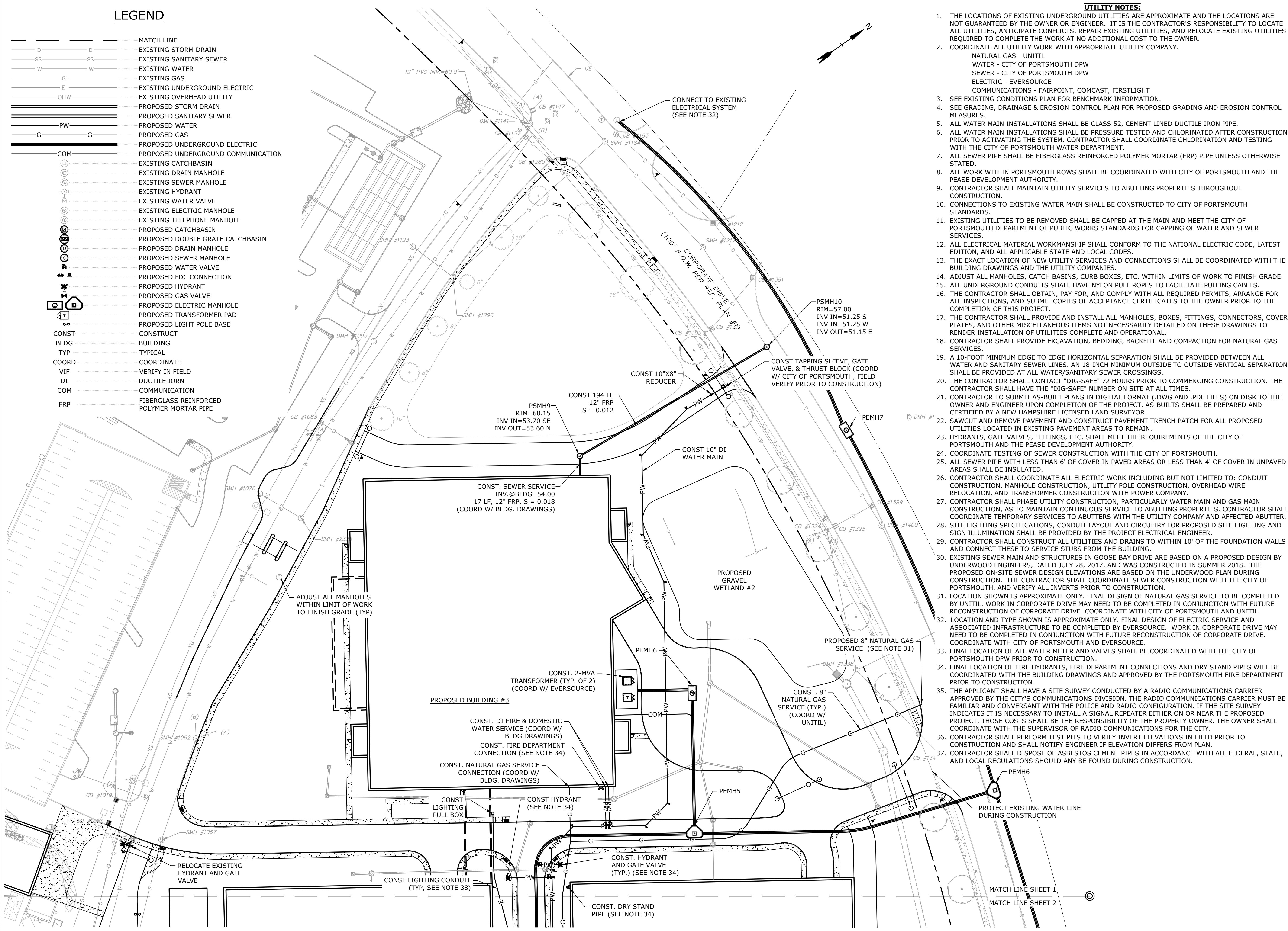
PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

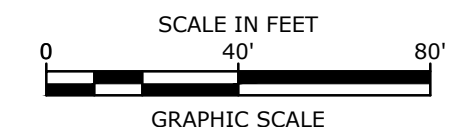
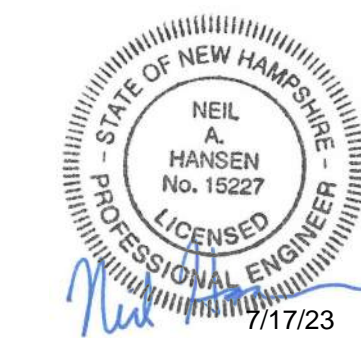
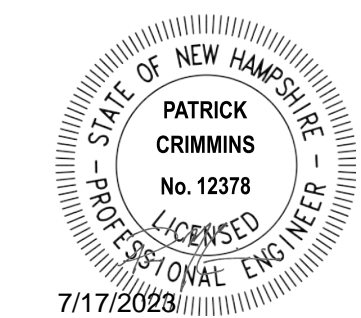
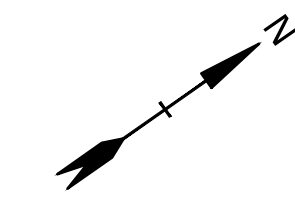
UTILITIES PLAN

SCALE: AS SHOWN

C-111

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Proposed Industrial Development

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New Hampshire

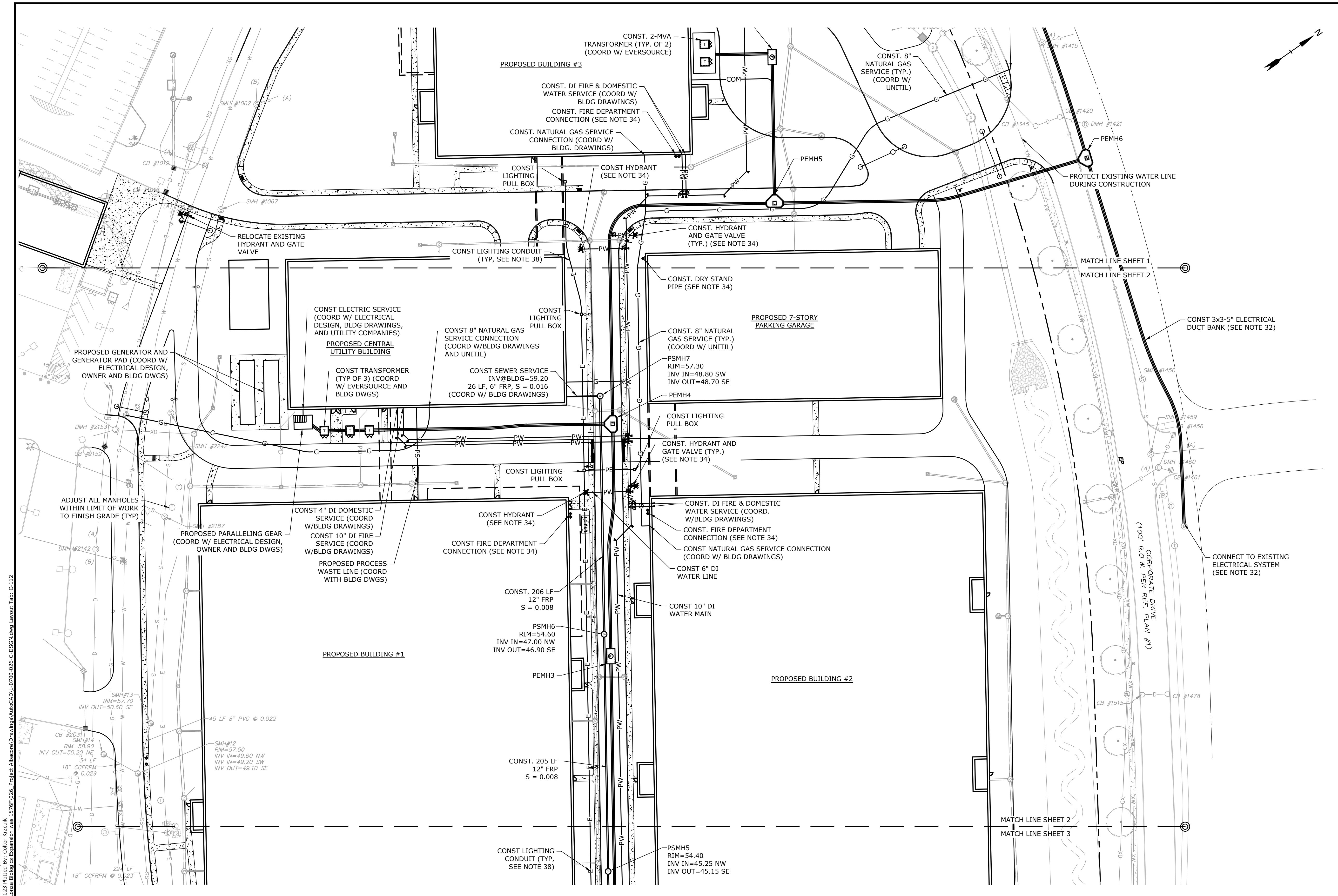
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UTILITIES PLAN

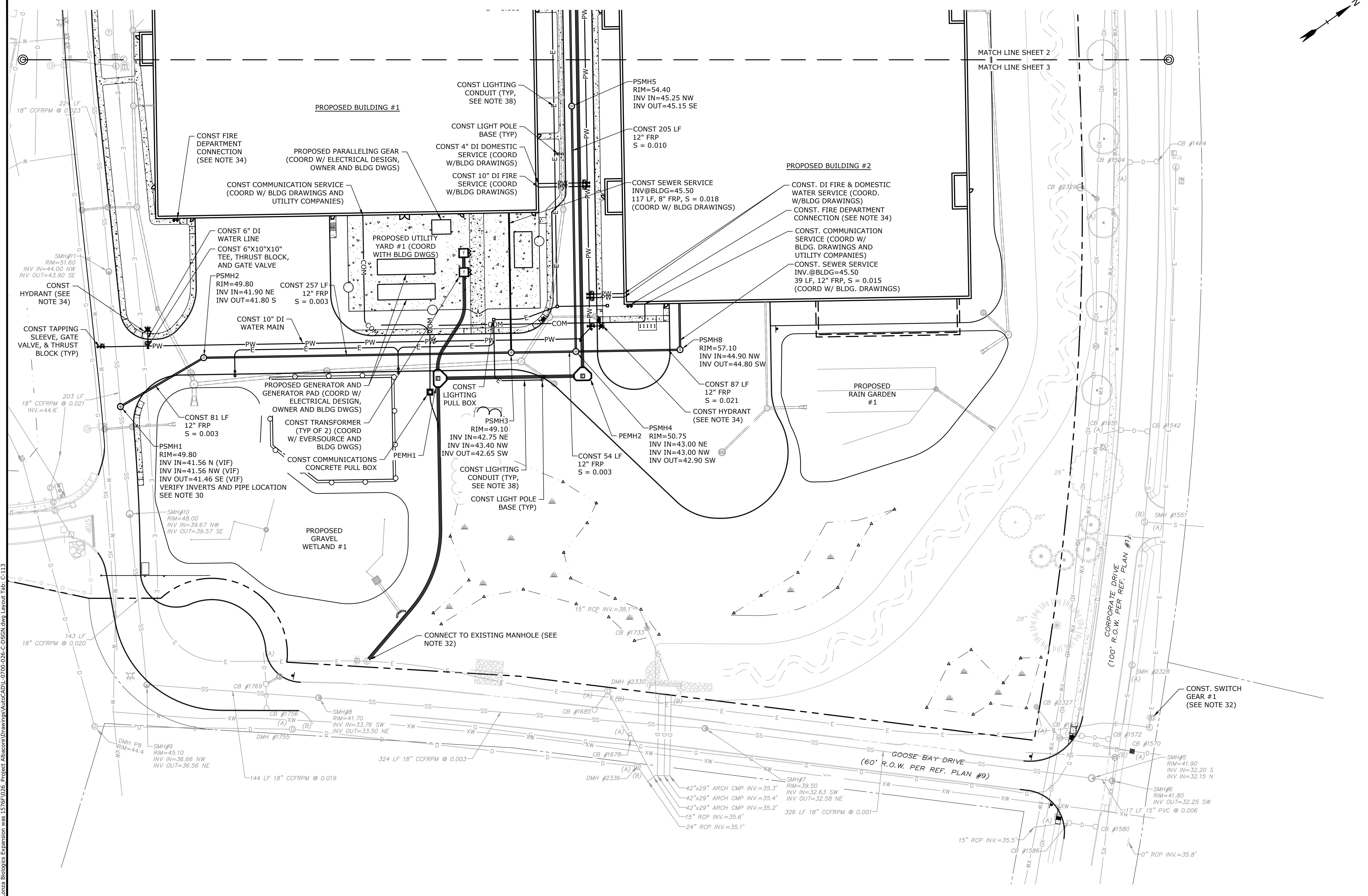
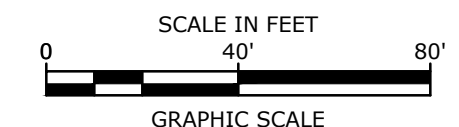
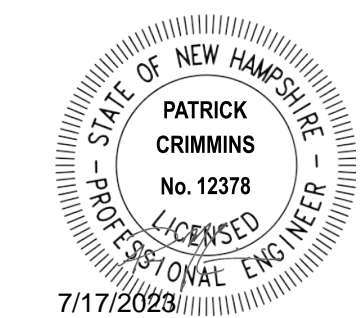
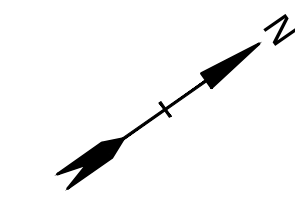
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C-112



SEE SHEET C-111 FOR UTILITY NOTES AND LEGEND

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Proposed Industrial Development

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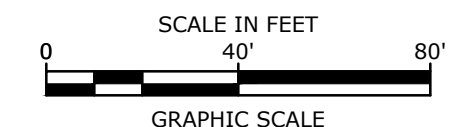
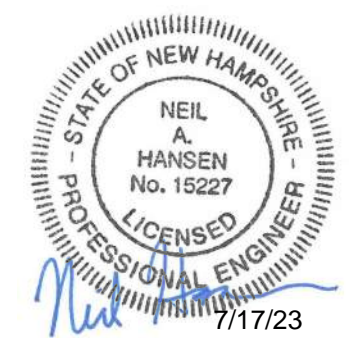
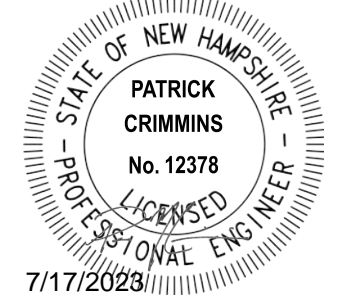
UTILITIES PLAN

SCALE: AS SHOWN

C-113

SEE SHEET C-111 FOR UTILITY NOTES AND LEGEND

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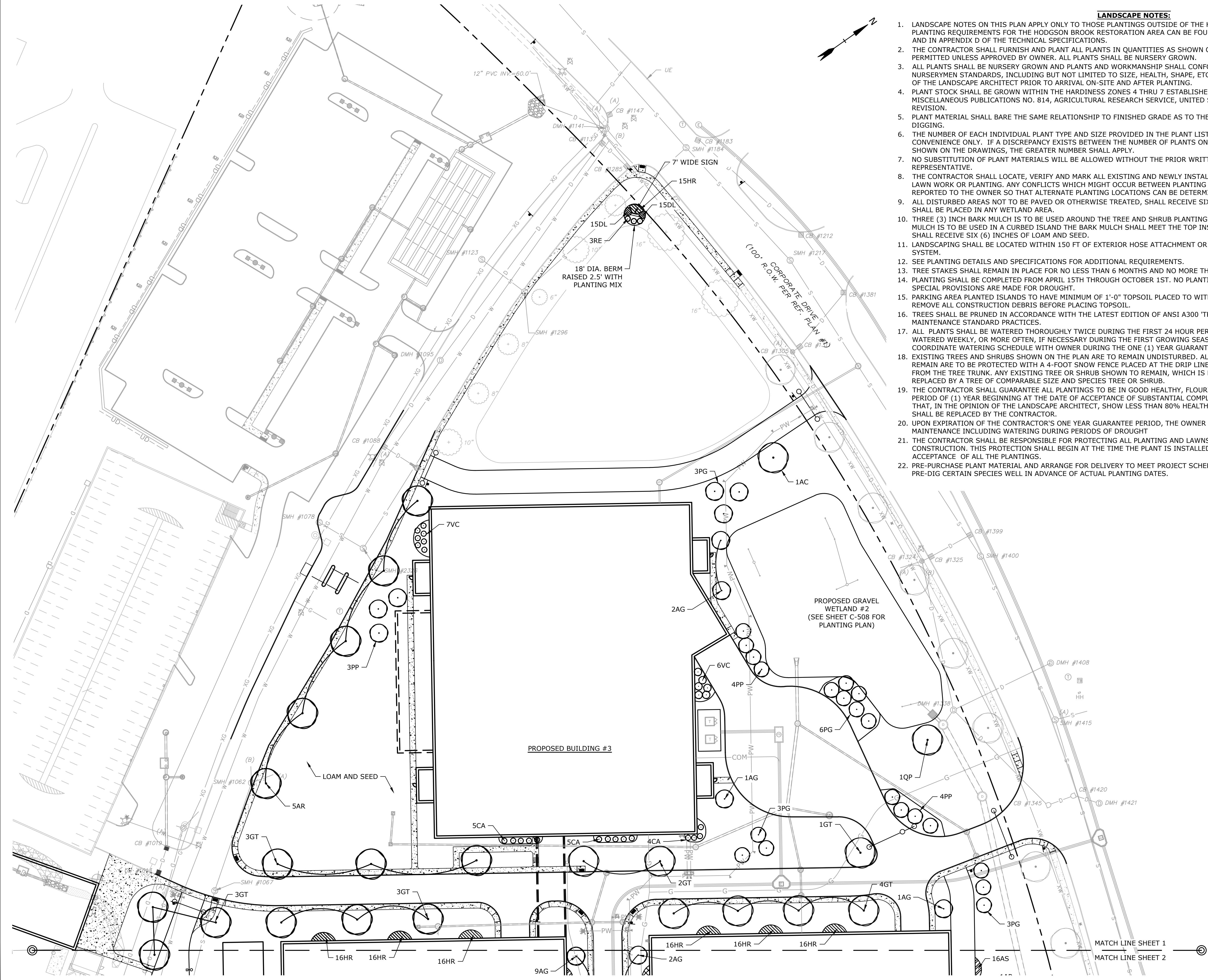
LANDSCAPE PLAN

SCALE: AS SHOWN

C-114

LANDSCAPE NOTES:

- LANDSCAPE NOTES ON THIS PLAN APPLY ONLY TO THOSE PLANTINGS OUTSIDE OF THE HODGSON BROOK RESTORATION AREA. PLANTING REQUIREMENTS FOR THE HODGSON BROOK RESTORATION AREA CAN BE FOUND ON PLAN SHEETS C-701 THROUGH C-714 AND IN APPENDIX D OF THE TECHNICAL SPECIFICATIONS.
- THE CONTRACTOR SHALL FURNISH AND PLANT ALL PLANTS IN QUANTITIES AS SHOWN ON THIS PLAN. NO SUBSTITUTIONS WILL BE PERMITTED UNLESS APPROVED BY OWNER. ALL PLANTS SHALL BE NURSERY GROWN.
- ALL PLANTS SHALL BE NURSERY GROWN AND PLANTS AND WORKMANSHIP SHALL CONFORM TO THE AMERICAN ASSOCIATION OF NURSERYMEN STANDARDS, INCLUDING BUT NOT LIMITED TO SIZE, HEALTH, SHAPE, ETC., AND SHALL BE SUBJECT TO THE APPROVAL OF THE LANDSCAPE ARCHITECT PRIOR TO ARRIVAL ON-SITE AND AFTER PLANTING.
- PLANT STOCK SHALL BE GROWN WITHIN THE HARDINESS ZONES 4 THRU 7 ESTABLISHED BY THE PLANT HARDINESS ZONE MAP, MISCELLANEOUS PUBLICATIONS NO. 814, AGRICULTURAL RESEARCH SERVICE, UNITED STATES DEPARTMENT AGRICULTURE, LATEST REVISION.
- PLANT MATERIAL SHALL BARE THE SAME RELATIONSHIP TO FINISHED GRADE AS TO THE ORIGINAL PLANTING GRADE PRIOR TO DIGGING.
- THE NUMBER OF EACH INDIVIDUAL PLANT TYPE AND SIZE PROVIDED IN THE PLANT LIST OR ON THE PLAN IS FOR THE CONTRACTOR'S CONVENIENCE ONLY. IF A DISCREPANCY EXISTS BETWEEN THE NUMBER OF PLANTS ON THE LABEL AND THE NUMBER OF SYMBOLS SHOWN ON THE DRAWINGS, THE GREATER NUMBER SHALL APPLY.
- NO SUBSTITUTION OF PLANT MATERIALS WILL BE ALLOWED WITHOUT THE PRIOR WRITTEN APPROVAL OF THE OWNER'S REPRESENTATIVE.
- THE CONTRACTOR SHALL LOCATE, VERIFY AND MARK ALL EXISTING AND NEWLY INSTALLED UNDERGROUND UTILITIES PRIOR TO ANY LAWN WORK OR PLANTING. ANY CONFLICTS WHICH MIGHT OCCUR BETWEEN PLANTING AND UTILITIES SHALL IMMEDIATELY BE REPORTED TO THE OWNER SO THAT ALTERNATE PLANTING LOCATIONS CAN BE DETERMINED.
- ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED, SHALL RECEIVE SIX (6) INCHES OF LOAM AND SEED. NO FILL SHALL BE PLACED IN ANY WETLAND AREA.
- THREE (3) INCH BARK MULCH IS TO BE USED AROUND THE TREE AND SHRUB PLANTING AS SPECIFIED IN THE DETAILS. WHERE BARK MULCH IS TO BE USED IN A CURBED ISLAND THE BARK MULCH SHALL MEET THE TOP INSIDE EDGE OF THE CURB. ALL OTHER AREAS SHALL RECEIVE SIX (6) INCHES OF LOAM AND SEED.
- LANDSCAPING SHALL BE LOCATED WITHIN 150 FT OF EXTERIOR HOSE ATTACHMENT OR SHALL BE PROVIDED WITH AN IRRIGATION SYSTEM.
- SEE PLANTING DETAILS AND SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS.
- TREE STAKES SHALL REMAIN IN PLACE FOR NO LESS THAN 6 MONTHS AND NO MORE THAN 1 YEAR.
- PLANTING SHALL BE COMPLETED FROM APRIL 15TH THROUGH OCTOBER 1ST. NO PLANTING DURING JULY AND AUGUST UNLESS SPECIAL PROVISIONS ARE MADE FOR DROUGHT.
- PARKING AREA PLANTED ISLANDS TO HAVE MINIMUM OF 1'-0" TOPSOIL PLACED TO WITHIN 3 INCHES OF THE TOP OF CURB ELEVATION REMOVE ALL CONSTRUCTION DEBRIS BEFORE PLACING TOPSOIL.
- TREES SHALL BE PRUNED IN ACCORDANCE WITH THE LATEST EDITION OF ANSI A300 'TREES, SHRUBS AND OTHER WOOD PLANT MAINTENANCE STANDARD PRACTICES.
- ALL PLANTS SHALL BE WATERED THOROUGHLY TWICE DURING THE FIRST 24 HOUR PERIOD AFTER PLANTING. ALL PLANTS SHALL BE WATERED WEEKLY, OR MORE OFTEN, IF NECESSARY DURING THE FIRST GROWING SEASON. LANDSCAPE CONTRACTOR SHALL COORDINATE WATERING SCHEDULE WITH OWNER DURING THE ONE (1) YEAR GUARANTEE PERIOD.
- EXISTING TREES AND SHRUBS SHOWN ON THE PLAN ARE TO REMAIN UNDISTURBED. ALL EXISTING TREES AND SHRUBS SHOWN TO REMAIN ARE TO BE PROTECTED WITH A 4-FOOT SNOW FENCE PLACED AT THE DRIP LINE OF THE BRANCHES OR AT 8 FEET MINIMUM FROM THE TREE TRUNK. ANY EXISTING TREE OR SHRUB SHOWN TO REMAIN, WHICH IS REMOVED DURING CONSTRUCTION, SHALL BE REPLACED BY A TREE OF COMPARABLE SIZE AND SPECIES TREE OR SHRUB.
- THE CONTRACTOR SHALL GUARANTEE ALL PLANTINGS TO BE IN GOOD HEALTHY, FLOURISHING AND ACCEPTABLE CONDITION FOR A PERIOD OF (1) YEAR BEGINNING AT THE DATE OF ACCEPTANCE OF SUBSTANTIAL COMPLETION. ALL GRASSES, TREES AND SHRUBS THAT, IN THE OPINION OF THE LANDSCAPE ARCHITECT, SHOW LESS THAN 80% HEALTHY GROWTH AT THE END OF ONE YEAR PERIOD SHALL BE REPLACED BY THE CONTRACTOR.
- UPON EXPIRATION OF THE CONTRACTOR'S ONE YEAR GUARANTEE PERIOD, THE OWNER SHALL BE RESPONSIBLE FOR LANDSCAPE MAINTENANCE INCLUDING WATERING DURING PERIODS OF DROUGHT
- THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL PLANTING AND LAWNS AGAINST DAMAGE FROM ONGOING CONSTRUCTION. THIS PROTECTION SHALL BEGIN AT THE TIME THE PLANT IS INSTALLED AND CONTINUE UNTIL THE FORMAL ACCEPTANCE OF ALL THE PLANTINGS.
- PRE-PURCHASE PLANT MATERIAL AND ARRANGE FOR DELIVERY TO MEET PROJECT SCHEDULE AS REQUIRED IT MAY BE NECESSARY TO PRE-DIG CERTAIN SPECIES WELL IN ADVANCE OF ACTUAL PLANTING DATES.

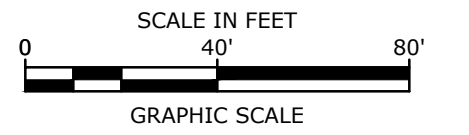
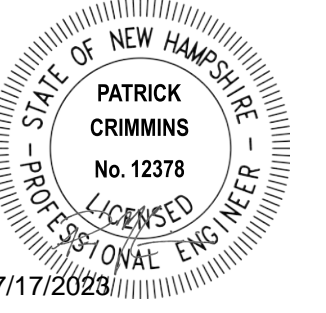
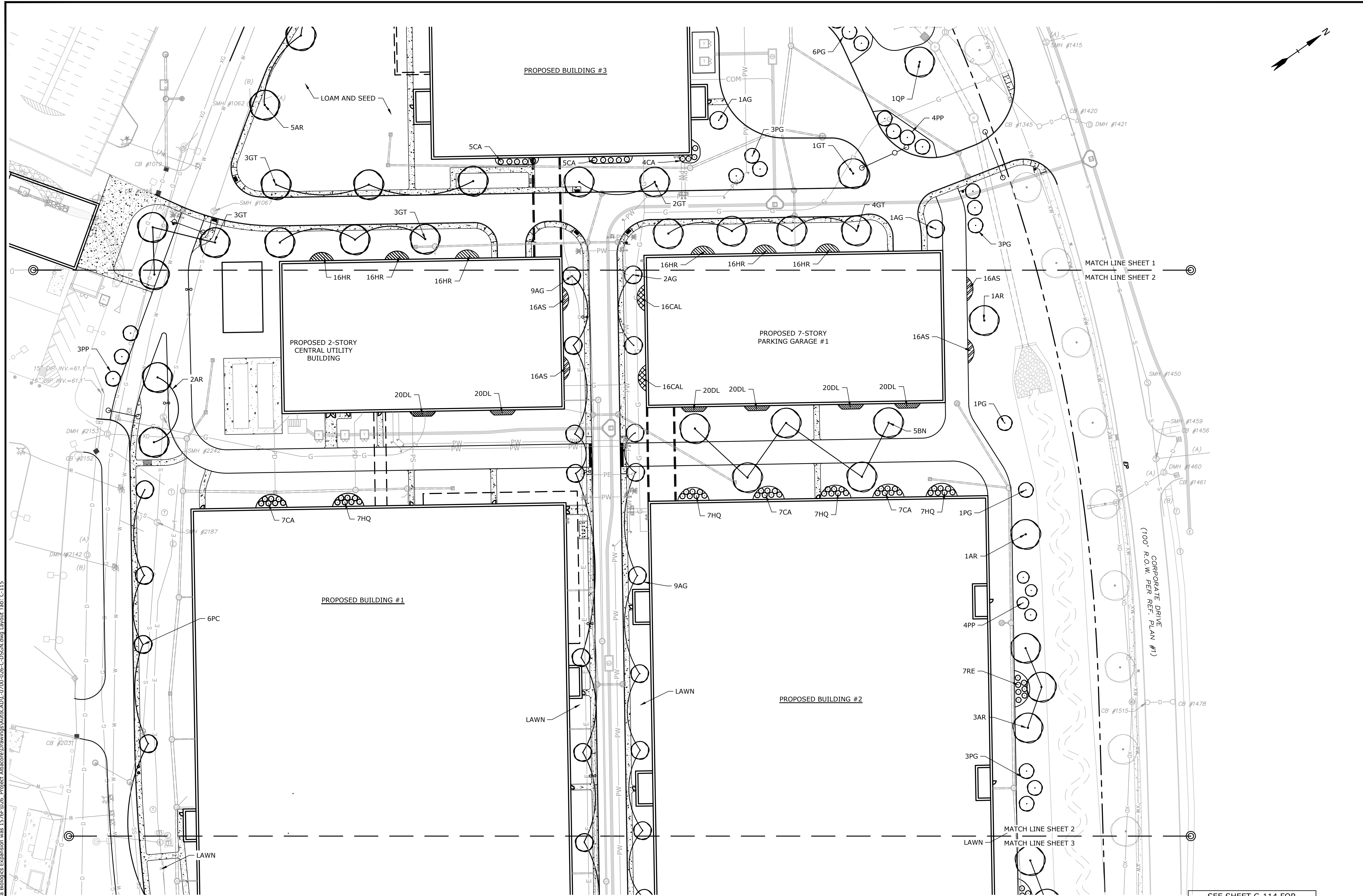


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SEE SHEET C-116 FOR PLANT SCHEDULE

MATCH LINE SHEET 1
MATCH LINE SHEET 2

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Proposed Industrial Development

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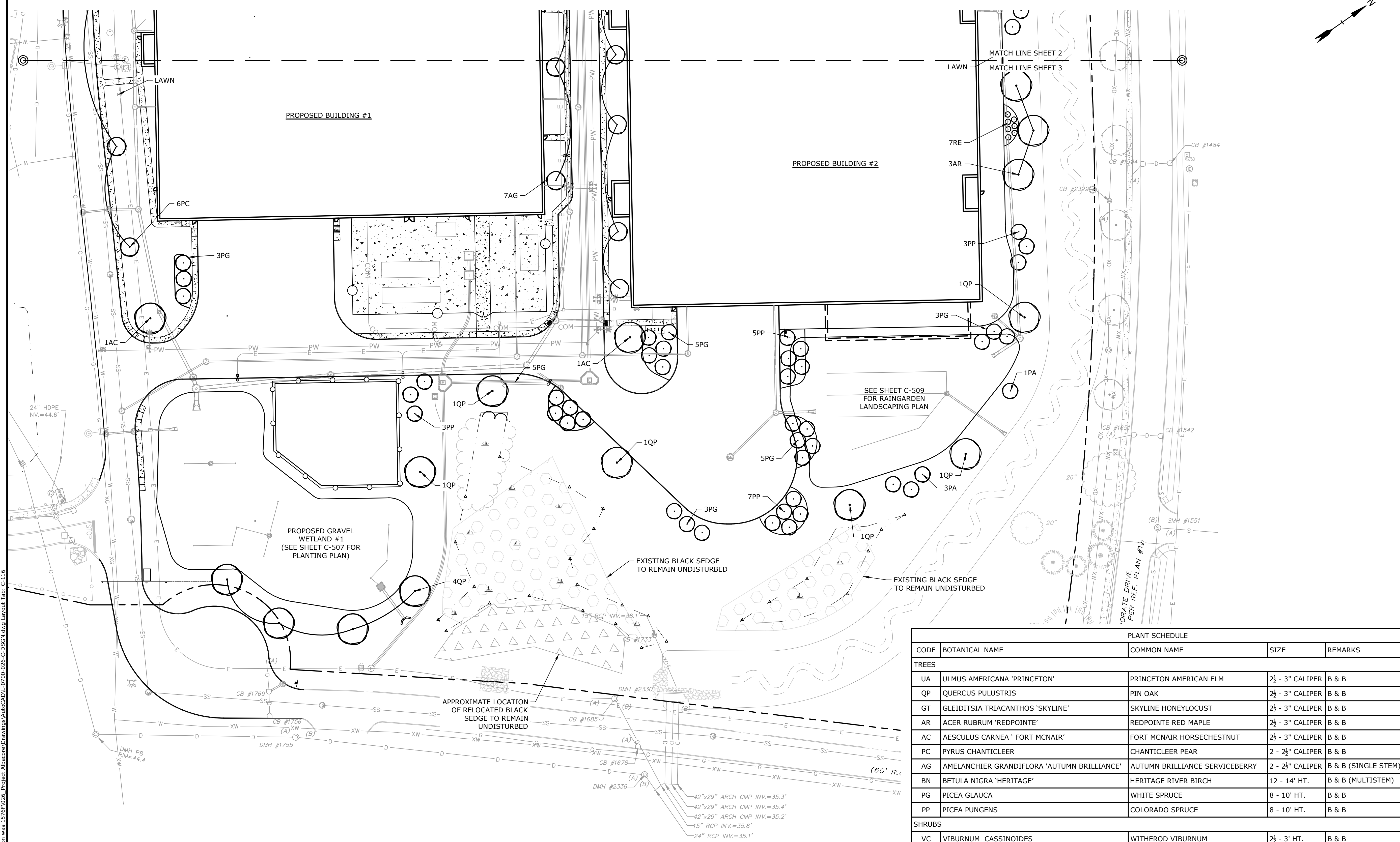
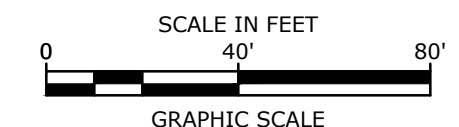
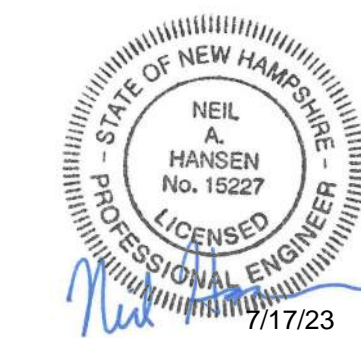
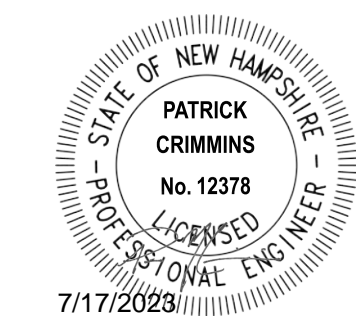
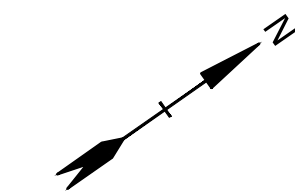
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APPROVED BY:	PMC

SEE SHEET C-114 FOR LANDSCAPING NOTES

SEE SHEET C-116 FOR PLANT SCHEDULE

LANDSCAPE PLAN

SCALE: AS SHOWN



PLANT SCHEDULE				
CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS
TREES				
UA	ULMUS AMERICANA 'PRINCETON'	PRINCETON AMERICAN ELM	2½ - 3" CALIPER	B & B
QP	QUERCUS PULSTRIS	PIN OAK	2½ - 3" CALIPER	B & B
GT	GLEDITSIA TRIACANTHOS 'SKYLINE'	SKYLINE HONEYLOCUST	2½ - 3" CALIPER	B & B
AR	ACER RUBRUM 'REDPOINTE'	REDPOINTE RED MAPLE	2½ - 3" CALIPER	B & B
AC	AESCULUS CARNEA 'FORT MCNAIR'	FORT MCNAIR HORSECHESTNUT	2½ - 3" CALIPER	B & B
PC	PYRUS CHANTICLEER	CHANTICLEER PEAR	2 - 2½" CALIPER	B & B
AG	AMELANCHIER GRANDIFLORA 'AUTUMN BRILLIANCE'	AUTUMN BRILLIANCE SERVICEBERRY	2 - 2½" CALIPER	B & B (SINGLE STEM)
BN	BETULA NIGRA 'HERITAGE'	HERITAGE RIVER BIRCH	12 - 14' HT.	B & B (MULTISTEM)
PG	PICEA GLAUCA	WHITE SPRUCE	8 - 10' HT.	B & B
PP	PICEA PUNGENS	COLORADO SPRUCE	8 - 10' HT.	B & B
SHRUBS				
VC	VIBURNUM CASSINOIDES	WITHEROD VIBURNUM	2½ - 3' HT.	B & B
RE	RHODODENDRON 'ENGLISH ROSEUM'	ENGLISH ROSEUM RHODODENDRON	2½ - 3' HT.	B & B
CA	CLETHERA ALNIFOLIA	SUMMERSWEET CLETHERA	7 GALLON	CONTAINER
HQ	HYDRANGEA QUERCIFOLIA 'SNOW QUEEN'	SNOW QUEEN OAKLEAF HYDRANGEA	2½ - 3' HT.	B & B
GROUNDCOVERS & PERENNIALS				
DL	HEMEROCALLIS 'STELLA DORO'	STELLA DORO DAYLILY	2 GALLON	CONTAINER
HR	HOSTA 'ROYAL STANDARD'	ROYAL STANDARD HOSTA	2 GALLON	CONTAINER
AS	ASTILBE 'VISIONS IN PINK'	VISIONS IN PINK ASTILBE	2 GALLON	CONTAINER
CAL	CALAMAGROSTIS 'KARL FOERSTER'	KARL FOERSTER FEATHER REED GRASS	3 GALLON	CONTAINER

SEE SHEET C-114 FOR LANDSCAPING NOTES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

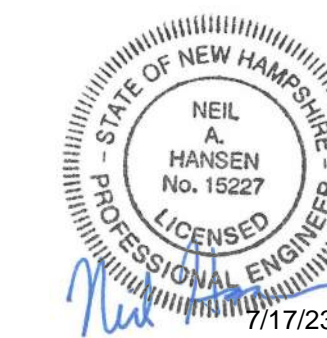
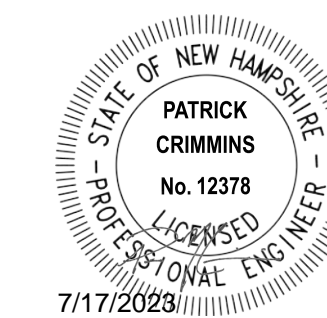
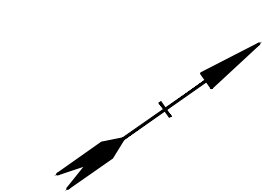
MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
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 DRAWN BY: CJK
 CHECKED: NAH
 APPROVED: PMC

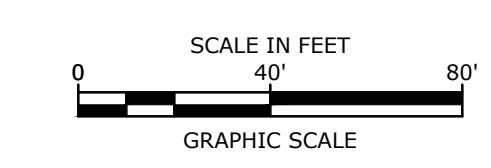
LANDSCAPE PLAN

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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
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Symbol	Qty	Label	Arrangement	Description	MANUFACTURER
□	6	S3	Single	MRM-LED-091-S11-3-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 48C (20' AFG)	LSI INDUSTRIES, INC.
□	7	S4	Single	MRM-LED-091-S11-PT-UNV-DIM-30-70CRI-CXX / 450-B3-S11G-20-S-GA-48C (20' AFG)	LSI INDUSTRIES, INC.
□	5	S5-1	Single	MRM-LED-091-S11-5W-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 48C (20' AFG)	LSI INDUSTRIES, INC.
□	7	W3	Single	XMM-3-LED-121-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
□	22	W4	Single	XMM-PT-LED-121-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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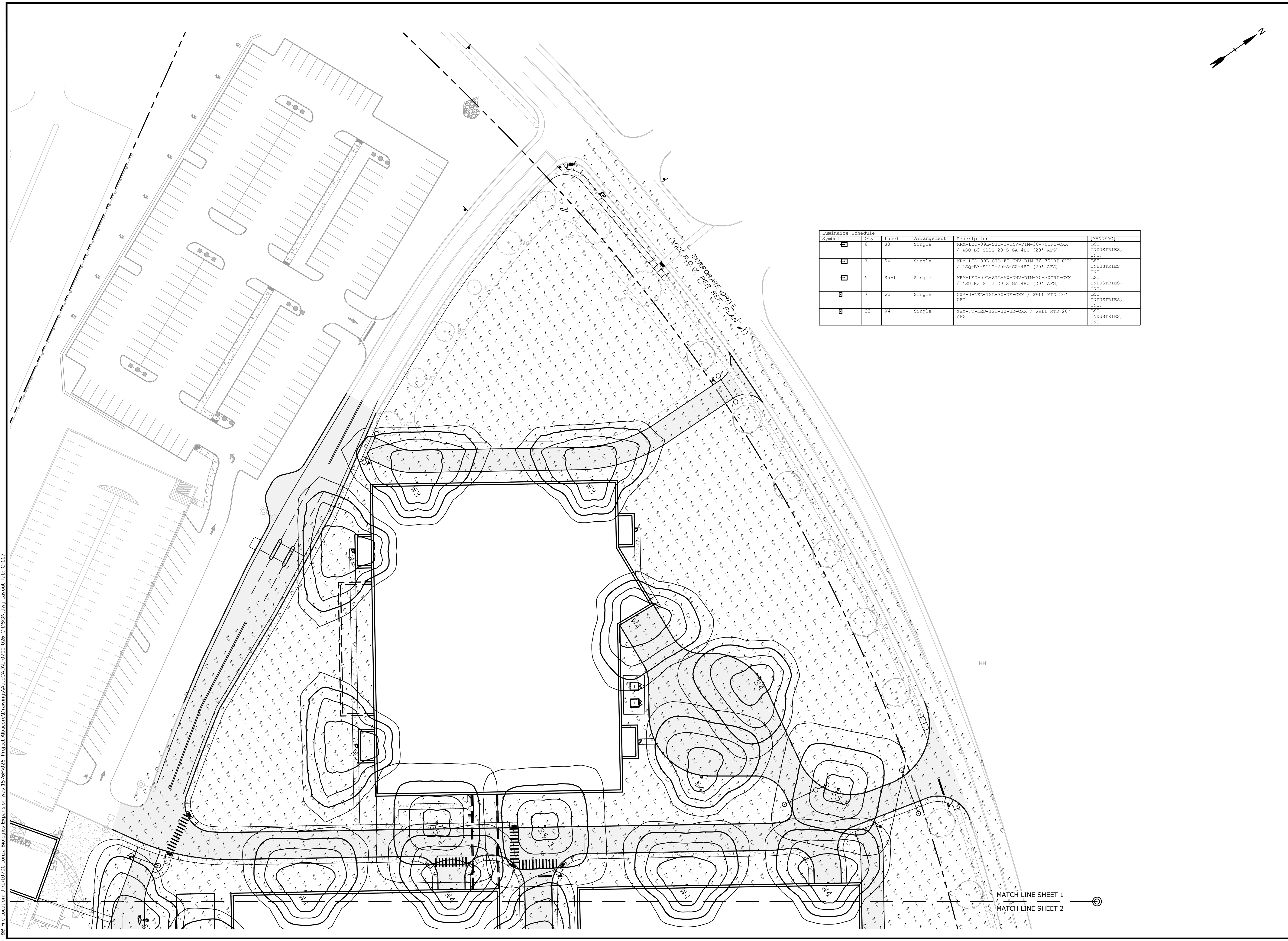
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APPROVED:	PMC

PHOTOMETRIC LIGHTING PLAN

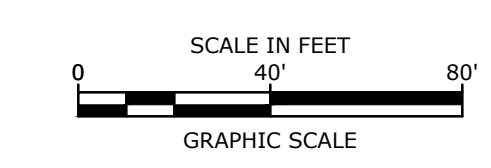
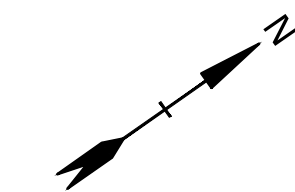
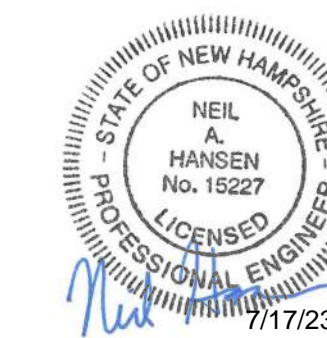
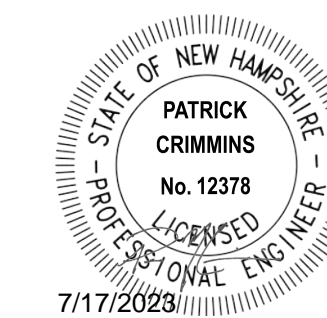
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MATCH LINE SHEET 1
MATCH LINE SHEET 2



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

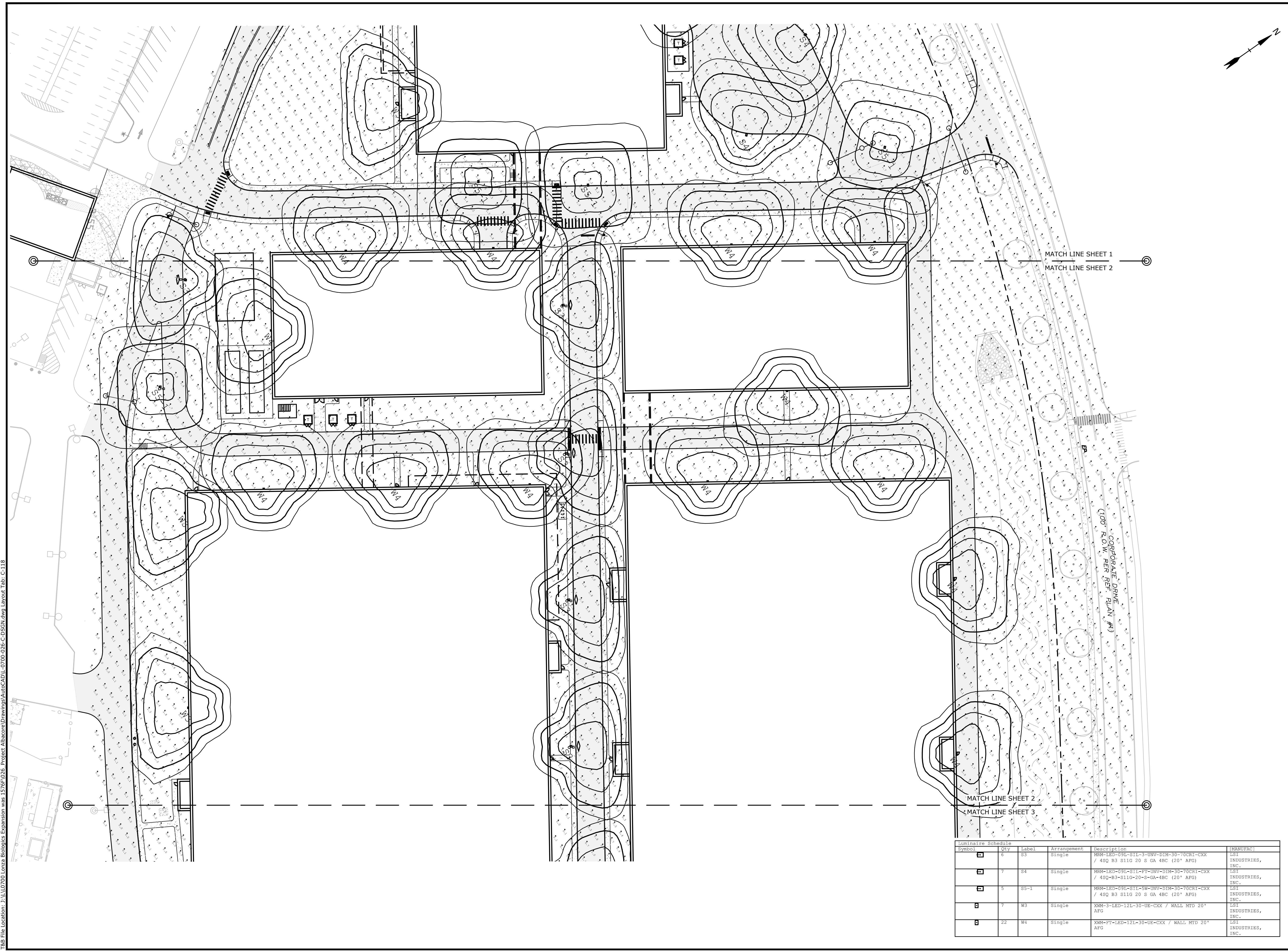
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PHOTOMETRIC LIGHTING PLAN

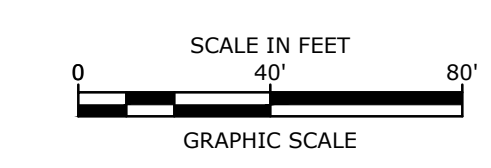
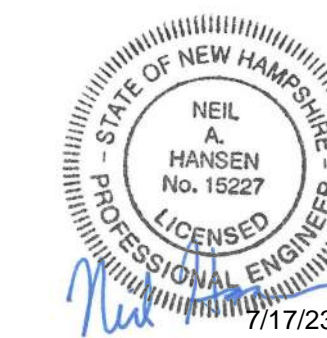
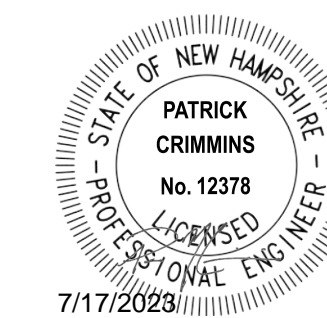
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☐	6	S3	Single	MRR-LED-09L-S11-3-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
☐	7	S4	Single	MRR-LED-09L-S11-FT-UNV-DIM-30-70CRI-CXX / 450 B3 S11G-20-S-GA-4BC (20' AFG)	LSI INDUSTRIES, INC.
☐	5	SS-1	Single	MRR-LED-09L-S11-5W-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
☐	7	W3	Single	XWM-3-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
☐	22	W4	Single	XWM-PT-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.

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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

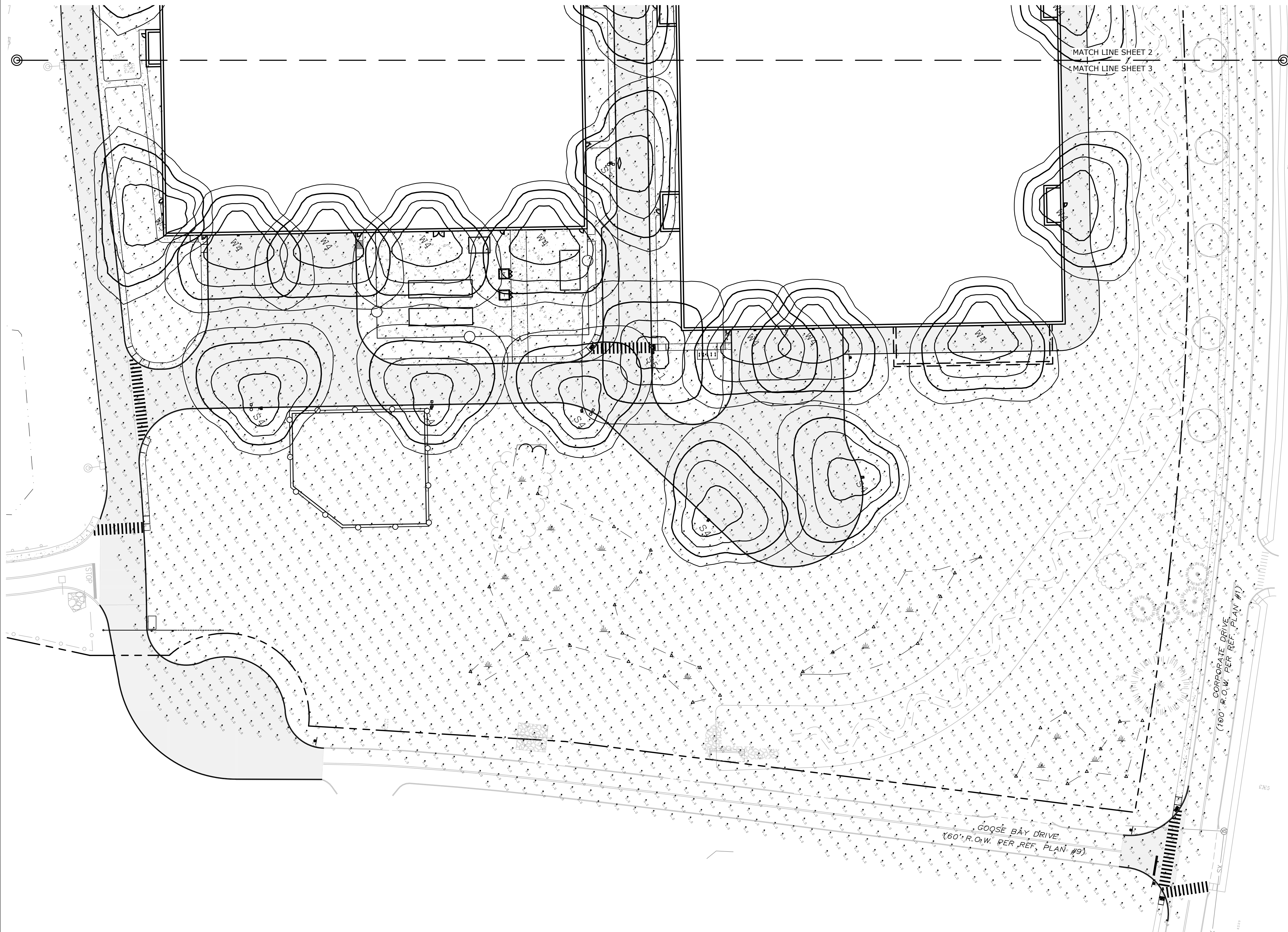
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DRAWN BY: CJK
CHECKED: NAH
APPROVED: PMC

PHOTOMETRIC LIGHTING PLAN

SCALE: AS SHOWN

C-119



Symbol	Qty	Label	Arrangement	Description	MANUFACT.
[Symbol]	6	S3	Single	MRR-LED-09L-S11-3-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	7	S4	Single	MRR-LED-09L-S11-FT-UNV-DIM-30-70CRI-CXX / 450 B3 S11G-20-S-GA-4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	5	SS-1	Single	MRR-LED-09L-S11-5W-UNV-DIM-30-70CRI-CXX / 450 B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	7	W3	Single	XWM-3-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
[Symbol]	22	W4	Single	XWM-PT-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.

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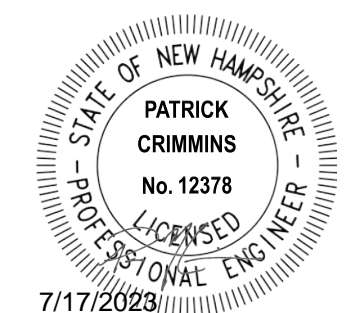
PHASE 2 PLAN SET

APRIL 3, 2018

REVISED: JULY 17, 2023



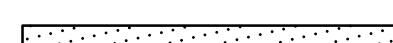
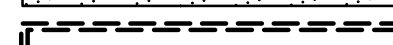


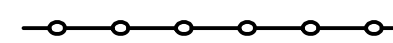







LIST OF DRAWINGS		
SHEET NO.	SHEET TITLE	LAST REVISED
	PHASE 2 PLAN SET COVER SHEET	7/17/2023
C-161	PHASE 2 DEMOLITION PLAN	7/17/2023
C-162	PHASE 2 DEMOLITION PLAN	7/17/2023
C-163	PHASE 2 DEMOLITION PLAN	7/17/2023
C-163.1	PHASE 2 PRE-CONSTRUCTION LAYOUT PLAN	7/17/2023
C-164	PHASE 2 OVERALL SITE PLAN	7/17/2023
C-165	PHASE 2 SITE PLAN	7/17/2023
C-166	PHASE 2 SITE PLAN	7/17/2023
C-167	PHASE 2 SITE PLAN	7/17/2023
C-168	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-169	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-170	PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN	7/17/2023
C-171	PHASE 2 UTILITIES PLAN	7/17/2023
C-172	PHASE 2 UTILITIES PLAN	7/17/2023
C-173	PHASE 2 UTILITIES PLAN	7/17/2023
C-174	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-175	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-176	PHASE 2 LANDSCAPE PLAN	7/17/2023
C-177	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-178	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
C-179	PHASE 2 PHOTOMETRIC LIGHTING PLAN	7/17/2023
A-1110	GROUND FLOOR PLAN - BL1	7/12/2023
A-2001	OVERALL BUILDINGS ELEVATIONS	7/12/2023
A-2002	BUILDING ELEVATIONS - BL1	7/12/2023
A-2003	BUILDING ELEVATIONS - BL1	7/12/2023
A310-000	GROUND FLOOR PLAN - CUB	7/12/2023
A500-000	BUILDING ELEVATIONS (N-S) - CUB	7/12/2023
A500-001	BUILDING ELEVATIONS (E-W) - CUB	7/12/2023

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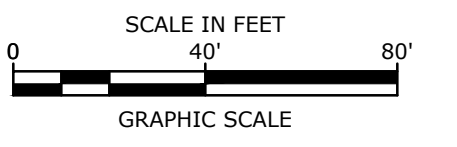
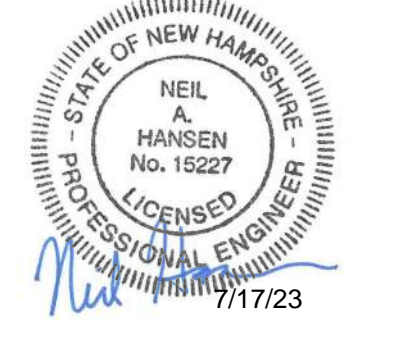
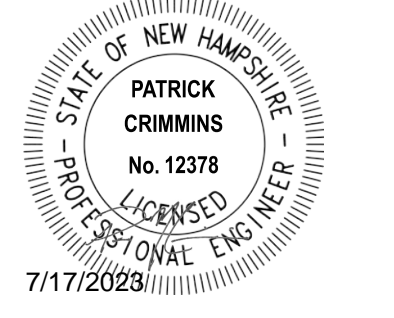
COMPLETE SET 28 SHEETS

LEGEND

-  APPROXIMATE LIMIT OF PROPOSED SAW CUT
-  LIMIT OF WORK
-  TREELINE TO BE REMOVED
-  APPROXIMATE LIMIT OF PAVEMENT TO BE REMOVED
-  LOCATION OF PROPOSED BUILDING
-  PROPOSED CONSTRUCTION ENTRANCE
-  PROPOSED SILT SOCK
-  PROPOSED TEMPORARY SNOW FENCE
-  PROPOSED TREE PROTECTION BARRIER
-  TBR TO BE REMOVED
-  BLDG TO BE REMOVED
-  TYP TYPICAL
-  CONST COORDINATE
-  CONST CONSTRUCT

DEMOLITION NOTES:

1. THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES AND RELOCATE EXISTING UTILITIES REQUIRED TO COMPLETE THE WORK.
2. THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES. CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
3. ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTOR UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES EXCEPT AS SPECIFIED IN NOTE #25.
4. COORDINATE REMOVAL, RELOCATION, DISPOSAL OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY.
5. ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO MATCH ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
6. SAW CUT AND REMOVE PAVEMENT ONE (1) FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN ALL AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO REMAIN.
7. IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL OF THE PERMIT APPROVALS.
8. THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR NECESSARY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION.
9. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL DEMOLITION AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK, EXCEPT FOR WORK NOTED TO BE COMPLETED BY OTHERS AND AS SPECIFIED IN NOTE #25.
10. UTILITIES SHALL BE TERMINATED AT THE MAIN LINE PER UTILITY COMPANY AND THE CITY OF PORTSMOUTH STANDARDS. THE CONTRACTOR SHALL REMOVE ALL ABANDONED UTILITIES LOCATED WITHIN THE LIMITS OF WORK.
11. CONTRACTOR SHALL VERIFY ORIGIN OF ALL DRAINS AND UTILITIES PRIOR TO REMOVAL/TERMINATION TO DETERMINE IF DRAINS OR UTILITY IS ACTIVE, AND SERVICES ANY ON OR OFF-SITE STRUCTURE TO REMAIN. THE CONTRACTOR SHALL NOTIFY ENGINEER IMMEDIATELY OF ANY SUCH UTILITY FOUND AND SHALL MAINTAIN THESE UTILITIES UNTIL PERMANENT SOLUTION IS IN PLACE.
12. PAVEMENT REMOVAL LIMITS ARE SHOWN FOR CONTRACTOR'S CONVENIENCE. ADDITIONAL PAVEMENT REMOVAL MAY BE REQUIRED DEPENDING ON THE CONTRACTOR'S OPERATION. CONTRACTOR TO VERIFY FULL LIMITS OF PAVEMENT REMOVAL PRIOR TO BID.
13. THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE PADS, UTILITIES AND PAVEMENT WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ITEMS TO BE REMOVED INCLUDE BUT ARE NOT LIMITED TO: CONCRETE, PAVEMENT, CURBS, LIGHTING, MANHOLES, CATCH BASINS, UNDER GROUND PIPING, POLES, STAIRS, SIGNS, FENCES, RAMPS, WALLS, BOLLARDS, BUILDING SLABS, FOUNDATION, TREES AND LANDSCAPING.
14. COORDINATE ALL WORK WITHIN THE PUBLIC RIGHT OF WAYS WITH THE CITY OF PORTSMOUTH AND PEASE DEVELOPMENT AUTHORITY.
15. REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL STUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF SITE IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL LAWS AND REGULATIONS.
16. CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED BY THE CONTRACTOR, THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO REPLACE DISTURBED MONUMENTS.
17. PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS/CURB INLETS WITHIN CONSTRUCTION LIMITS AS WELL AS CATCH BASINS/CURB INLETS THAT MAY RECEIVE RUNOFF FROM CONSTRUCTION ACTIVITIES. INLET PROTECTION BARRIERS SHALL BE MAINTAINED FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE "HIGH FLOW SILT SACK" BY ACF ENVIRONMENTAL OR EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN EVENT OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED OR SEDIMENT HAS ACCUMULATED TO 1/3 THE DESIGN DEPTH OF THE BARRIER.
18. THE CONTRACTOR SHALL PHASE DEMOLITION AND CONSTRUCTION AS REQUIRED TO PROVIDE CONTINUOUS SERVICE TO EXISTING BUSINESSES THROUGHOUT THE CONSTRUCTION PERIOD. EXISTING BUSINESS SERVICES INCLUDE, BUT ARE NOT LIMITED TO ELECTRICAL, COMMUNICATION, FIRE PROTECTION, DOMESTIC WATER AND SEWER SERVICES. TEMPORARY SERVICES, IF REQUIRED, SHALL COMPLY WITH ALL FEDERAL, STATE, LOCAL AND UTILITY COMPANY STANDARDS. CONTRACTOR SHALL PROVIDE DETAILED CONSTRUCTION SCHEDULE TO OWNER PRIOR TO ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
19. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
20. THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
21. SAW CUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL UTILITIES TO BE REMOVED AND PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN.
22. THE CONTRACTOR SHALL ACQUIRE A PDA DIG PERMIT BEFORE ANY EARTH DISTURBANCE CAN TAKE PLACE. ALLOW 7 CALENDAR DAYS FOR PROCESSING.
23. ALL MONITORING WELLS WITHIN LIMIT OF WORK SHALL BE PROTECTED DURING CONSTRUCTION. IF ANY MONITORING WELL NEEDS TO BE REMOVED OR ADJUSTED THIS WORK SHALL BE COORDINATED WITH THE PEASE DEVELOPMENT AUTHORITY.
24. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS PRIOR TO CONSTRUCTION.
25. ALL EXCESS SOIL RESULTING FROM THE CONSTRUCTION SHALL REMAIN ON SITE. COORDINATE WITH OWNER AND PEASE DEVELOPMENT AUTHORITY ON FINAL LOCATION OF EXCESS MATERIALS.
26. BEFORE ANY DEWATERING IS PERFORMED, COORDINATION BETWEEN THE OWNER, CONTRACTOR, PDA, NHDES AND THE AIR FORCE IS REQUIRED TO DETERMINE PROPER PROCEDURES AND PERMITTING REQUIRED. AT A MINIMUM A NHDES TEMPORARY DISCHARGE PERMIT IS REQUIRED.



Proposed Industrial Development
Lonza Biologics

Portsmouth, New Hampshire

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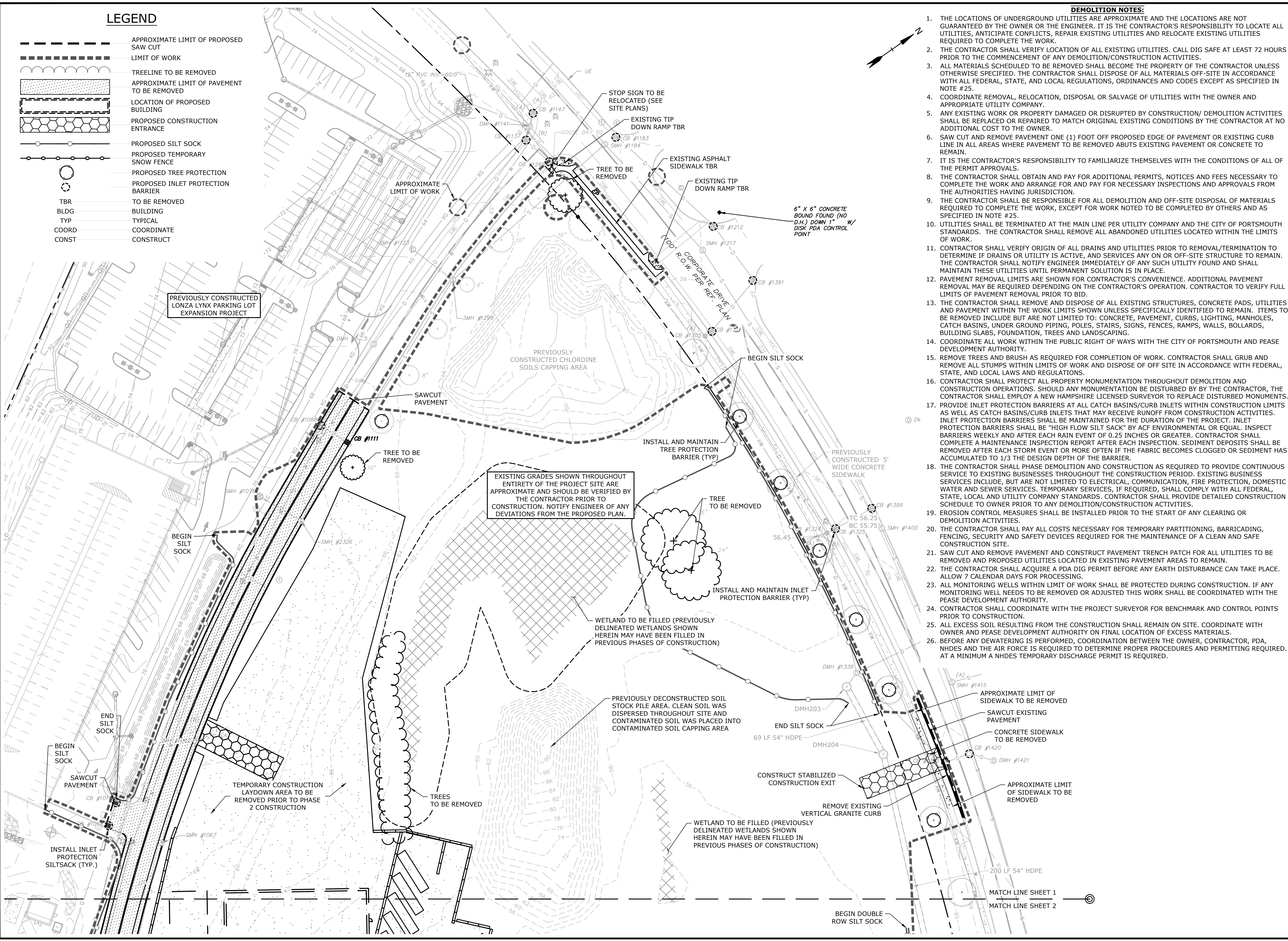
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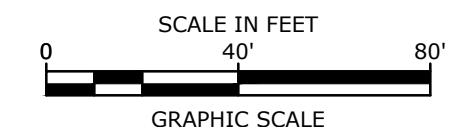
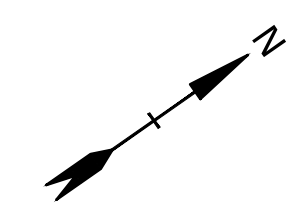
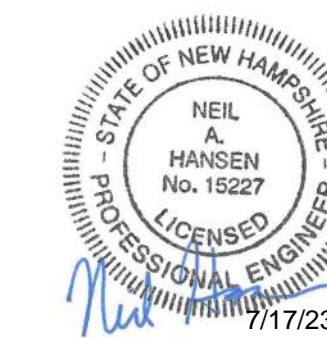
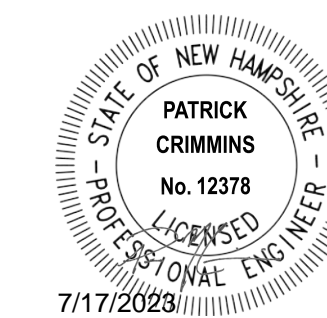
PHASE 2 DEMOLITION PLAN

SCALE: AS SHOWN

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Last Save Date: July 13, 2023 3:42 PM BY: CKRZCUIK
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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

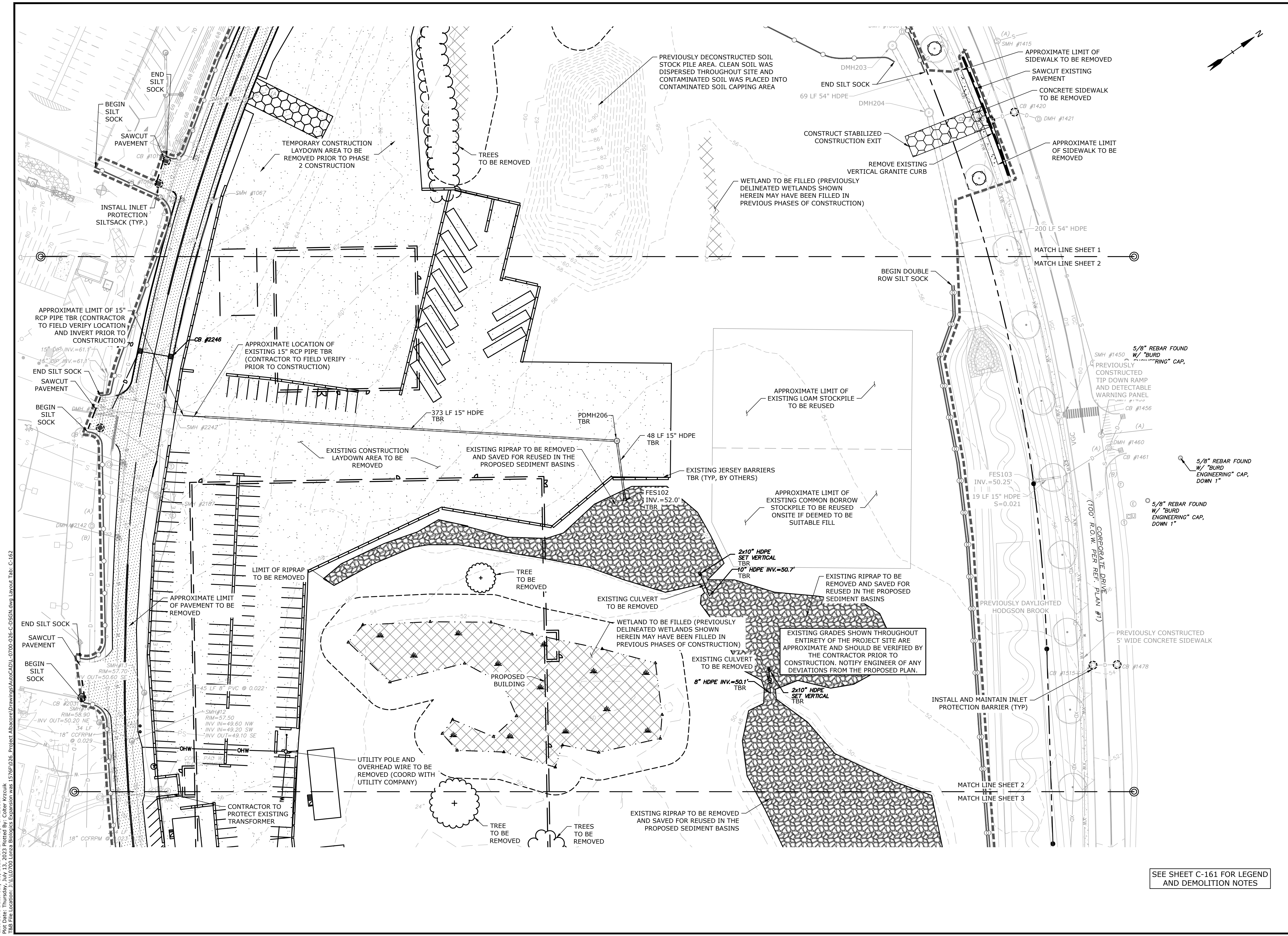
MARK	DATE	DESCRIPTION
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J	3/15/2023	Phase 1B Issued for Preliminary Pricing
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G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CIK
CHECKED:	NAH
APPROVED:	PMC

PHASE 2 DEMOLITION PLAN

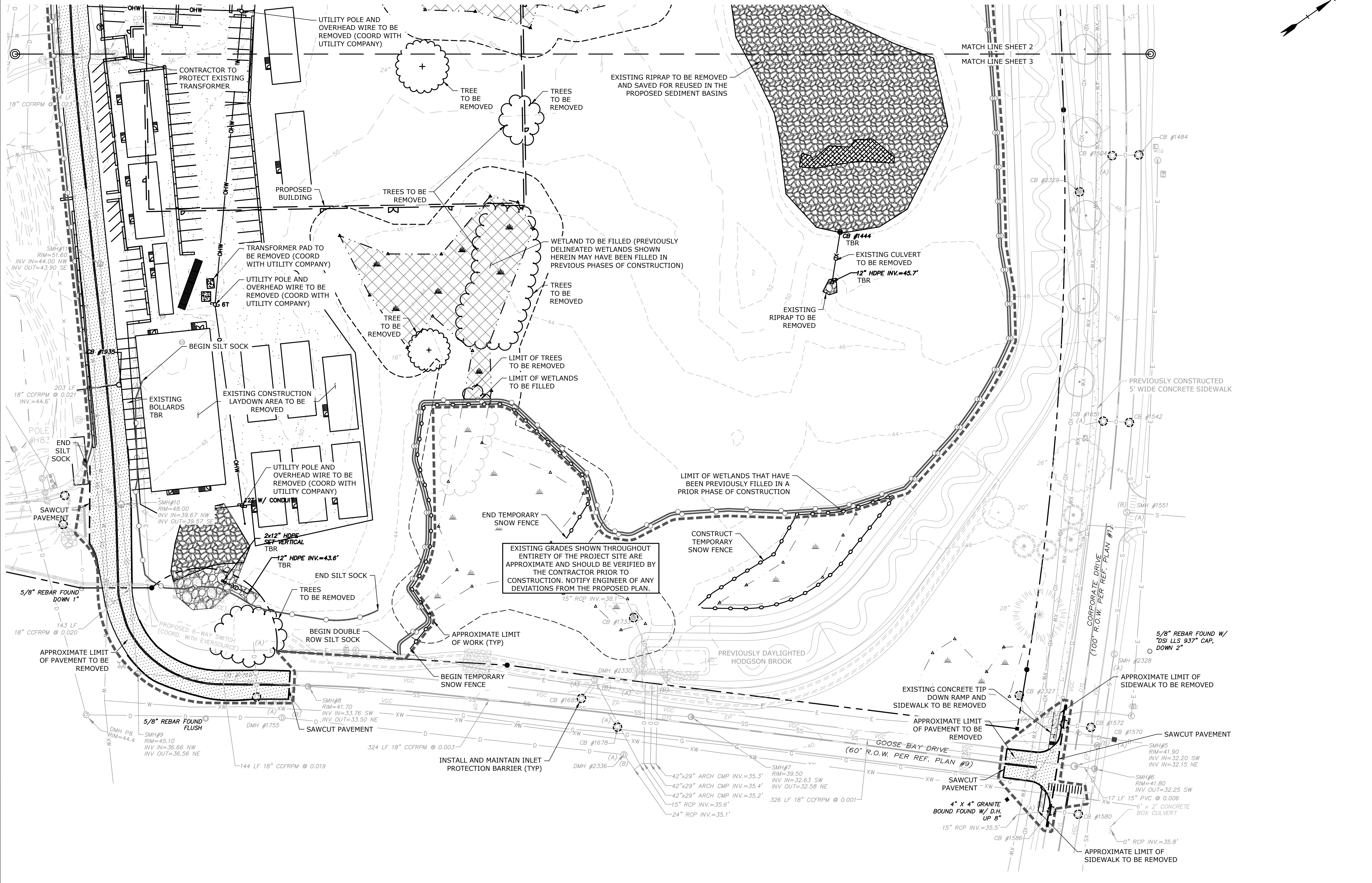
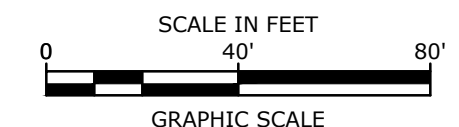
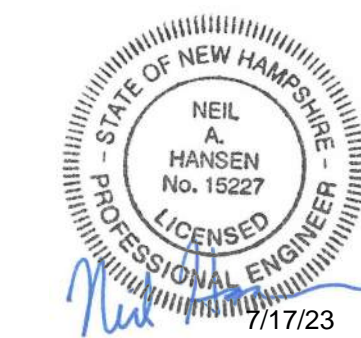
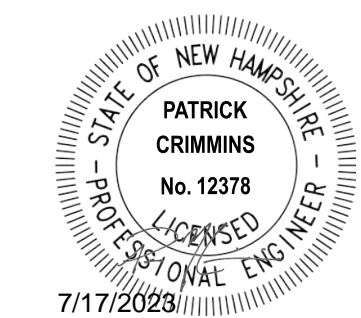
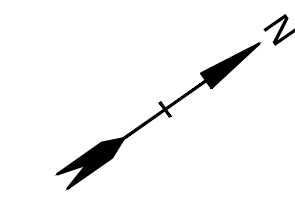
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SEE SHEET C-161 FOR LEGEND AND DEMOLITION NOTES

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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
 Plot File Location: J:\0700\Lonza Biologics Expansion\187526-026-C-DSGN.dwg Layout Tab: C-162



EXISTING GRADES SHOWN THROUGHOUT ENTIRETY OF THE PROJECT SITE ARE APPROXIMATE AND SHOULD BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. NOTIFY ENGINEER OF ANY DEVIATIONS FROM THE PROPOSED PLAN.

SEE SHEET C-161 FOR LEGEND AND DEMOLITION NOTES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

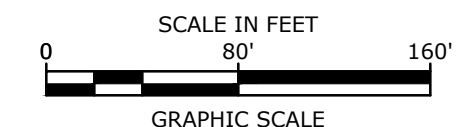
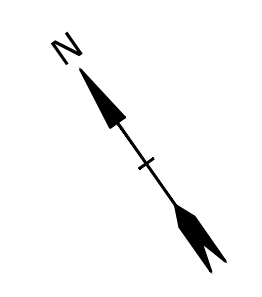
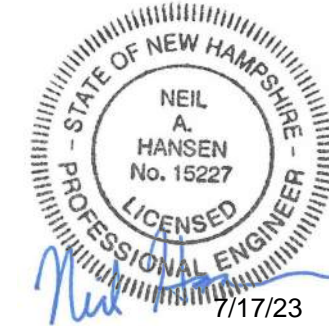
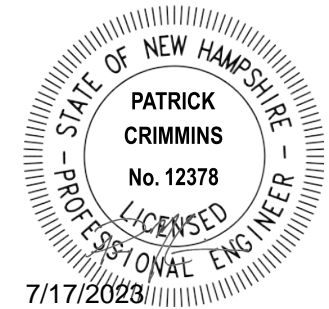
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PHASE 2 DEMOLITION PLAN

SCALE: AS SHOWN

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 P&E File Location: J:\0700 Lonza Biologics Expansion.was 12.752.026 Project Abstract: Drawings\AutoCAD\0700-026-C-DSGN.dwg Layout Tab: C-163



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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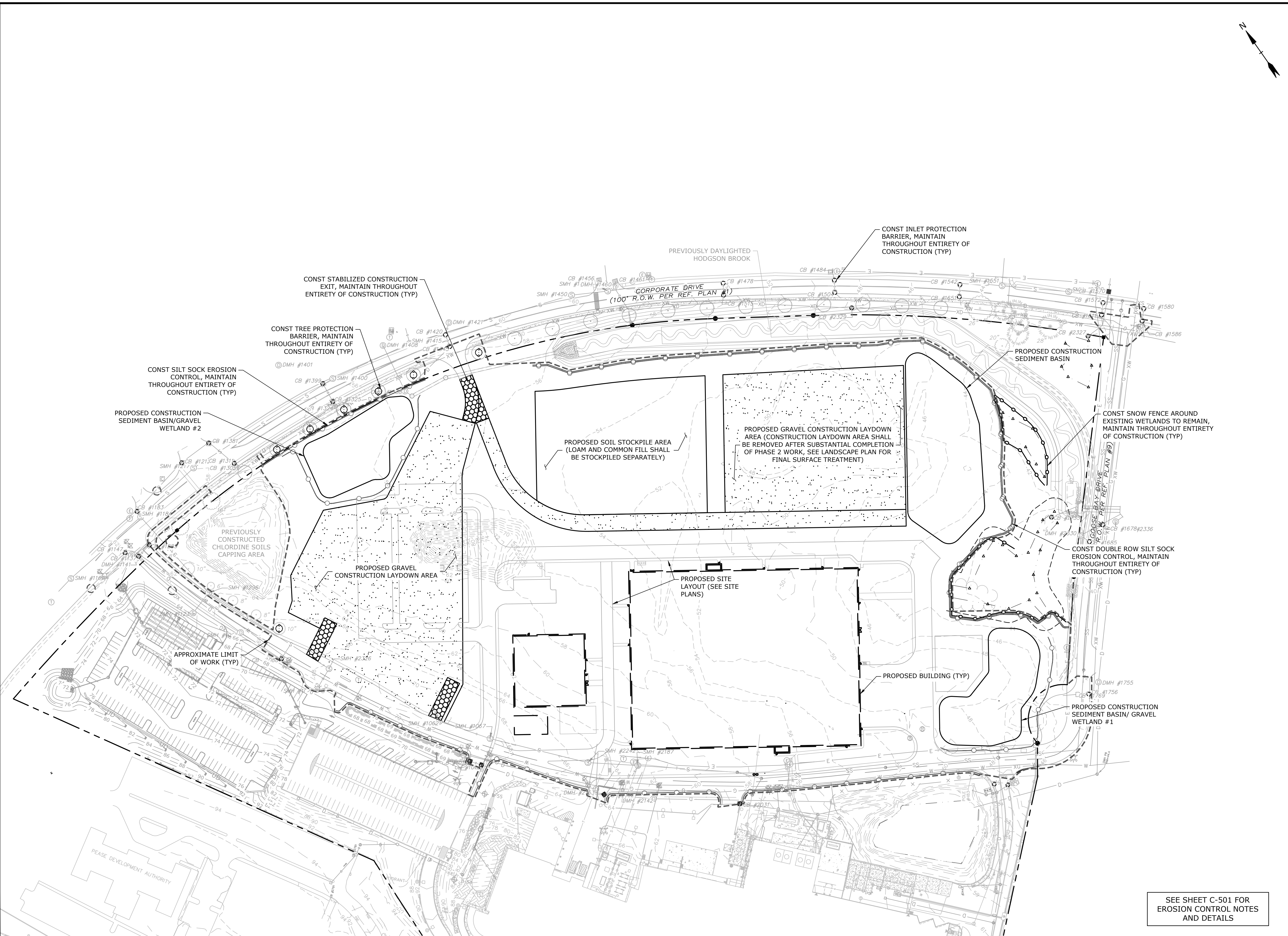
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DRAWN BY:	CJK
CHECKED BY:	NAH
APPROVED BY:	PMC

PHASE 2 PRE-CONSTRUCTION LAYOUT PLAN

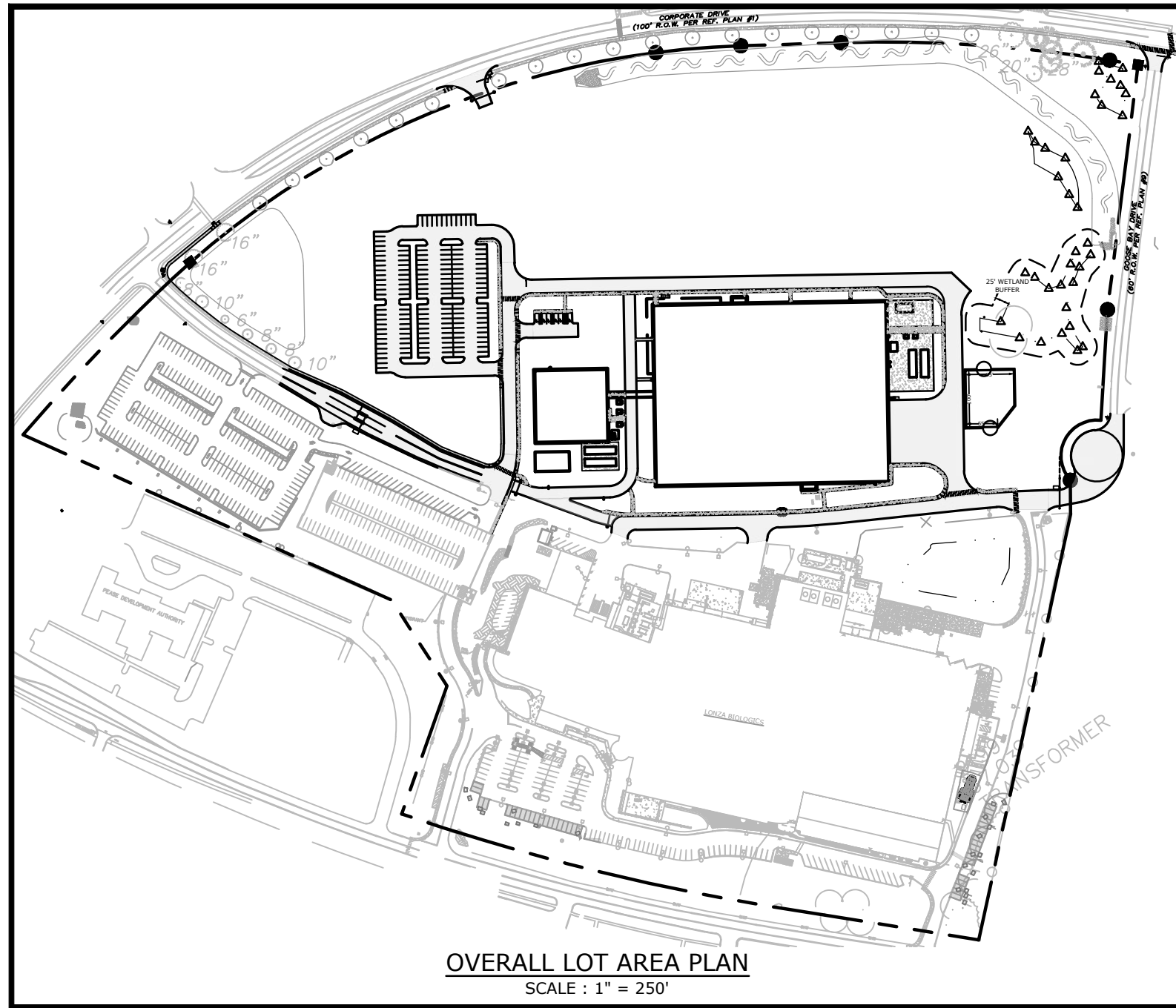
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SEE SHEET C-501 FOR EROSION CONTROL NOTES AND DETAILS



SITE DATA

LOCATION: TAX MAP 305, LOTS 1 & 2
70 & 80 CORPORATE DRIVE
PORTSMOUTH, NH

TAX MAP 305, LOT 6
101 INTERNATIONAL DRIVE
PORTSMOUTH, NH

ZONING DISTRICT: AIRPORT, BUSINESS & COMMERCIAL (ABC)

DIMENSIONAL REQUIREMENTS:

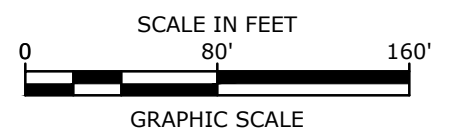
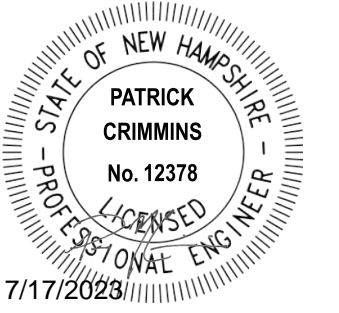
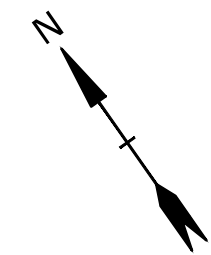
	REQUIRED	PROVIDED
MINIMUM LOT AREA:	5 AC	43.4± AC
MINIMUM STREET FRONTAGE:	200 FT	1,038 FT
MINIMUM FRONT YARD SETBACK:	70 FT	70 FT
SIDE SETBACK:	30 FT	30 FT
REAR SETBACK:	50 FT	51 FT
MINIMUM OPEN SPACE:	25 %	59.9± %

MAXIMUM STRUCTURE HEIGHT SHALL NOT EXCEED FAA CRITERIA.

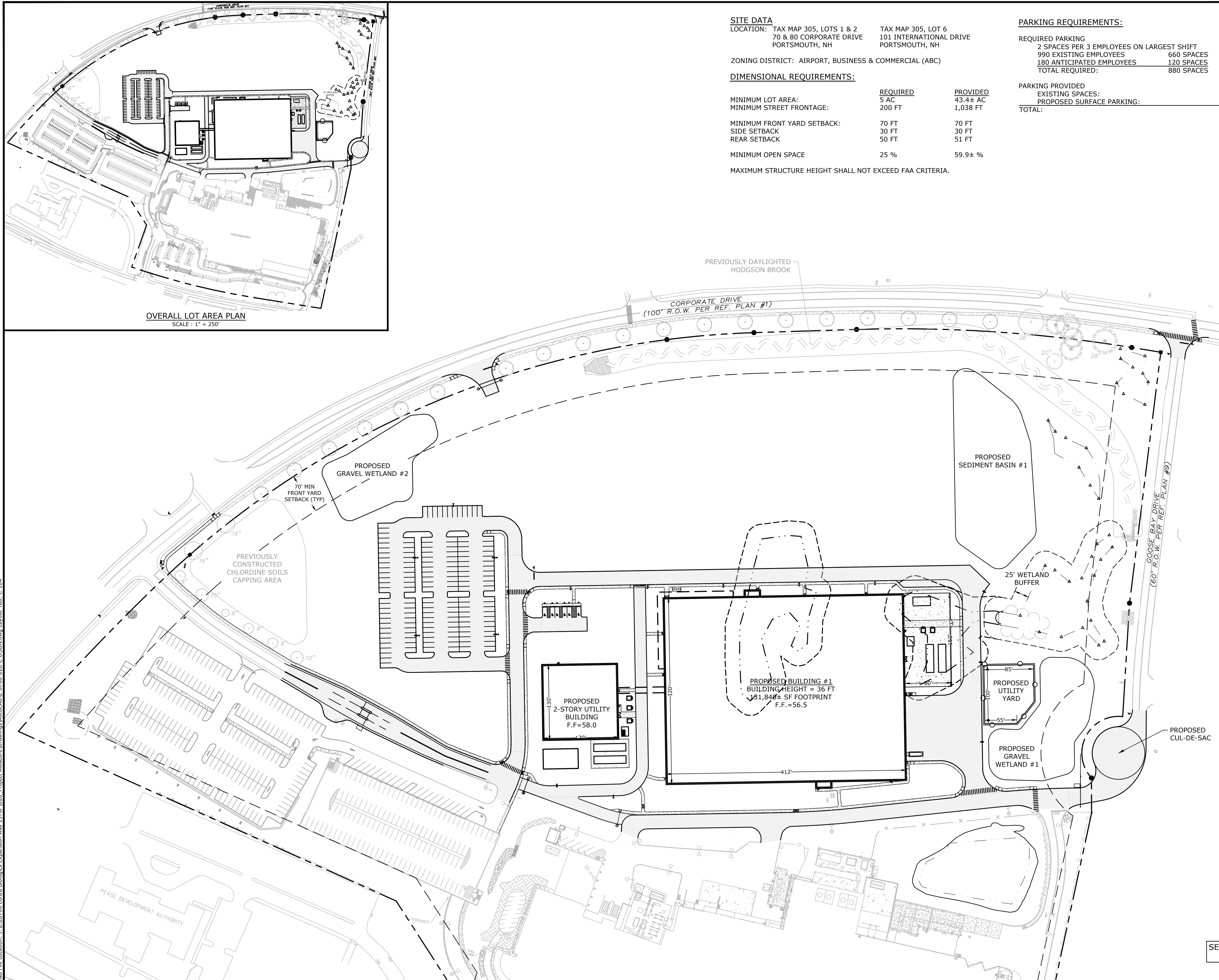
PARKING REQUIREMENTS:

REQUIRED PARKING	PROVIDED
2 SPACES PER 3 EMPLOYEES ON LARGEST SHIFT	801 SPACES
990 EXISTING EMPLOYEES	156 SPACES
180 ANTICIPATED EMPLOYEES	120 SPACES
TOTAL REQUIRED:	957 SPACES

PARKING PROVIDED	PROVIDED
EXISTING SPACES:	801 SPACES
PROPOSED SURFACE PARKING:	156 SPACES
TOTAL:	957 SPACES



Last Save Date: July 14, 2023 11:10 AM By: CKRZCUIK
 Plot Date: Monday, July 17, 2023 Plotted By: Colter Krzcuik
 P&E File Location: J:\110720 Lonza Biologics Expansion.was 15765.026 Project Abstract: Drawings\AutoCAD\11-0720-026-C-DSGN.dwg Layout Tab: C-164



Proposed Industrial Development

Lonza Biologics

Portsmouth,
New Hampshire

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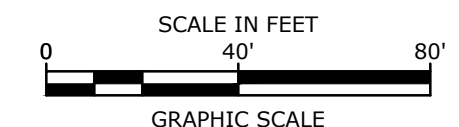
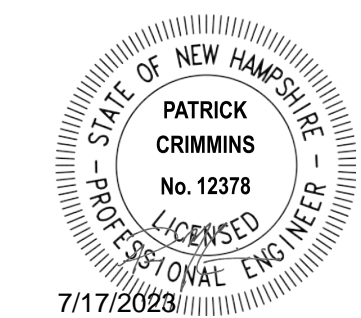
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 DATE: 04/03/2018
 FILE: L-0700-026-C-DSGN.dwg
 DRAWN BY: CJK
 CHECKED: NAH
 APPROVED: PMC

PHASE 2 OVERALL SITE PLAN

SCALE: AS SHOWN

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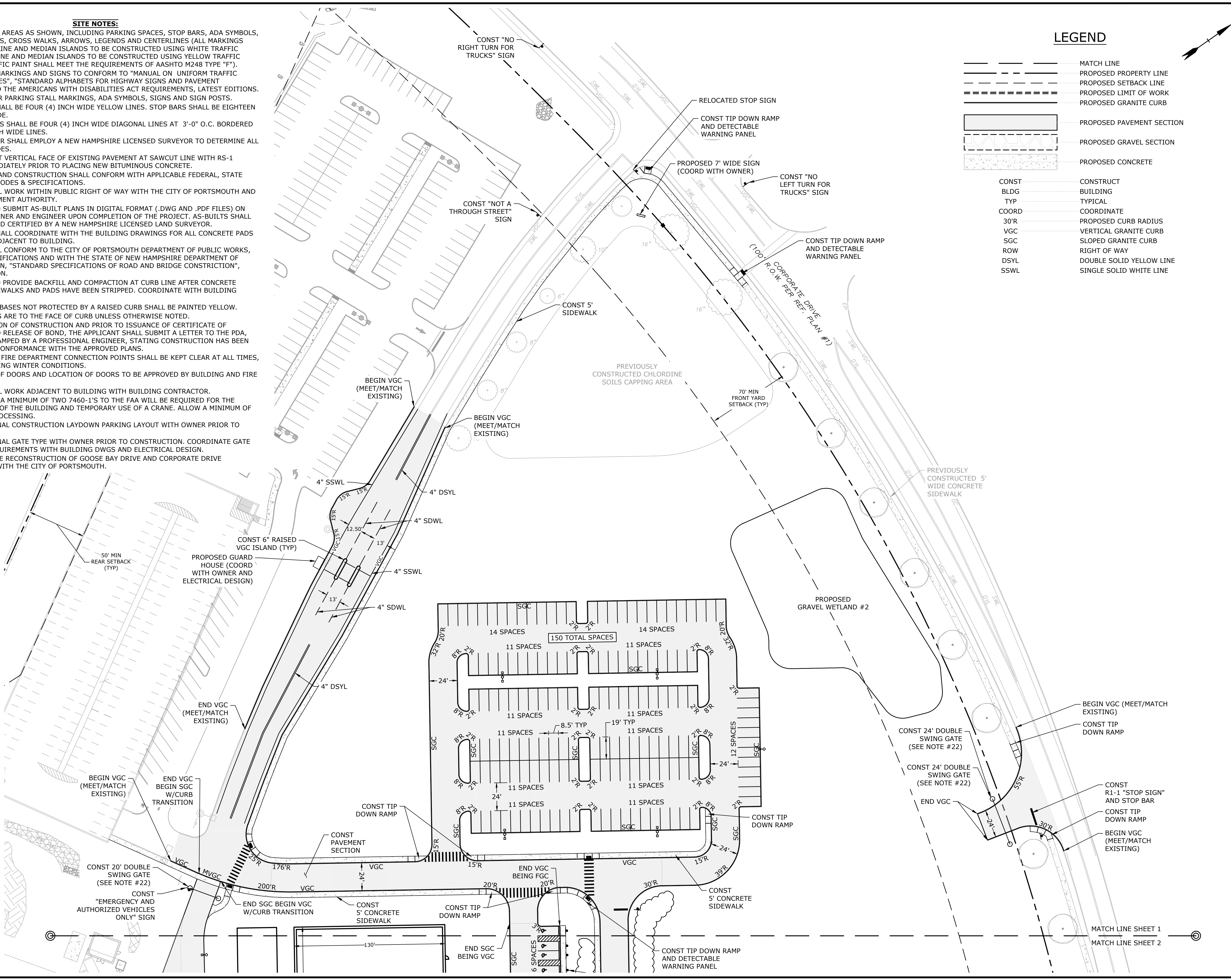
SEE SHEET C-165 FOR LEGEND AND SITE NOTES



LEGEND

- MATCH LINE
- PROPOSED PROPERTY LINE
- PROPOSED SETBACK LINE
- PROPOSED LIMIT OF WORK
- PROPOSED GRANITE CURB
- PROPOSED PAVEMENT SECTION
- PROPOSED GRAVEL SECTION
- PROPOSED CONCRETE
- CONST _____ CONSTRUCT
- BLDG _____ BUILDING
- TYP _____ TYPICAL
- COORD _____ COORDINATE
- 30'R _____ PROPOSED CURB RADIUS
- VGC _____ VERTICAL GRANITE CURB
- SGC _____ SLOPED GRANITE CURB
- ROW _____ RIGHT OF WAY
- DSYL _____ DOUBLE SOLID YELLOW LINE
- SSWL _____ SINGLE SOLID WHITE LINE

- SITE NOTES:**
1. STRIPE PARKING AREAS AS SHOWN, INCLUDING PARKING SPACES, STOP BARS, ADA SYMBOLS, PAINTED ISLANDS, CROSS WALKS, ARROWS, LEGENDS AND CENTERLINES (ALL MARKINGS EXCEPT CENTERLINE AND MEDIAN ISLANDS TO BE CONSTRUCTED USING WHITE TRAFFIC PAINT. CENTERLINE AND MEDIAN ISLANDS TO BE CONSTRUCTED USING YELLOW TRAFFIC PAINT. ALL TRAFFIC PAINT SHALL MEET THE REQUIREMENTS OF AASHTO M248 TYPE "F").
 2. ALL PAVEMENT MARKINGS AND SIGNS TO CONFORM TO "MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES", "STANDARD ALPHABETS FOR HIGHWAY SIGNS AND PAVEMENT MARKINGS", AND THE AMERICANS WITH DISABILITIES ACT REQUIREMENTS, LATEST EDITIONS.
 3. SEE DETAILS FOR PARKING STALL MARKINGS, ADA SYMBOLS, SIGNS AND SIGN POSTS.
 4. CENTERLINES SHALL BE FOUR (4) INCH WIDE YELLOW LINES. STOP BARS SHALL BE EIGHTEEN (18) INCHES WIDE.
 5. PAINTED ISLANDS SHALL BE FOUR (4) INCH WIDE DIAGONAL LINES AT 3'-0" O.C. BORDERED BY FOUR (4) INCH WIDE LINES.
 6. THE CONTRACTOR SHALL EMPLOY A NEW HAMPSHIRE LICENSED SURVEYOR TO DETERMINE ALL LINES AND GRADES.
 7. CLEAN AND COAT VERTICAL FACE OF EXISTING PAVEMENT AT SAWCUT LINE WITH RS-1 EMULSION IMMEDIATELY PRIOR TO PLACING NEW BITUMINOUS CONCRETE.
 8. ALL MATERIALS AND CONSTRUCTION SHALL CONFORM WITH APPLICABLE FEDERAL, STATE AND/OR TOWN CODES & SPECIFICATIONS.
 9. COORDINATE ALL WORK WITHIN PUBLIC RIGHT OF WAY WITH THE CITY OF PORTSMOUTH AND PEASE DEVELOPMENT AUTHORITY.
 10. CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
 11. CONTRACTOR SHALL COORDINATE WITH THE BUILDING DRAWINGS FOR ALL CONCRETE PADS & SIDEWALKS ADJACENT TO BUILDING.
 12. ALL WORK SHALL CONFORM TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS, STANDARD SPECIFICATIONS AND WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, "STANDARD SPECIFICATIONS OF ROAD AND BRIDGE CONSTRUCTION", CURRENT EDITION.
 13. CONTRACTOR TO PROVIDE BACKFILL AND COMPACTION AT CURB LINE AFTER CONCRETE FORMS FOR SIDEWALKS AND PADS HAVE BEEN STRIPPED. COORDINATE WITH BUILDING CONTRACTOR.
 14. ALL LIGHT POLE BASES NOT PROTECTED BY A RAISED CURB SHALL BE PAINTED YELLOW.
 15. ALL DIMENSIONS ARE TO THE FACE OF CURB UNLESS OTHERWISE NOTED.
 16. UPON COMPLETION OF CONSTRUCTION AND PRIOR TO ISSUANCE OF CERTIFICATE OF OCCUPANCY AND RELEASE OF BOND, THE APPLICANT SHALL SUBMIT A LETTER TO THE PDA, SIGNED AND STAMPED BY A PROFESSIONAL ENGINEER, STATING CONSTRUCTION HAS BEEN COMPLETED IN CONFORMANCE WITH THE APPROVED PLANS.
 17. FIRE LANES AND FIRE DEPARTMENT CONNECTION POINTS SHALL BE KEPT CLEAR AT ALL TIMES, INCLUDING DURING WINTER CONDITIONS.
 18. FINAL NUMBER OF DOORS AND LOCATION OF DOORS TO BE APPROVED BY BUILDING AND FIRE DEPARTMENTS.
 19. COORDINATE ALL WORK ADJACENT TO BUILDING WITH BUILDING CONTRACTOR.
 20. SUBMISSION OF A MINIMUM OF TWO 7460-1'S TO THE FAA WILL BE REQUIRED FOR THE CONSTRUCTION OF THE BUILDING AND TEMPORARY USE OF A CRANE. ALLOW A MINIMUM OF 45 DAYS FOR PROCESSING.
 21. COORDINATE FINAL CONSTRUCTION LAYDOWN PARKING LAYOUT WITH OWNER PRIOR TO CONSTRUCTION.
 22. COORDINATE FINAL GATE TYPE WITH OWNER PRIOR TO CONSTRUCTION. COORDINATE GATE ELECTRICAL REQUIREMENTS WITH BUILDING DWGS AND ELECTRICAL DESIGN.
 23. COORDINATE THE RECONSTRUCTION OF GOOSE BAY DRIVE AND CORPORATE DRIVE INTERSECTION WITH THE CITY OF PORTSMOUTH.



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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
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Proposed Industrial Development

Lonza Biologicals

Portsmouth, New Hampshire

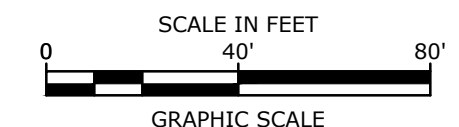
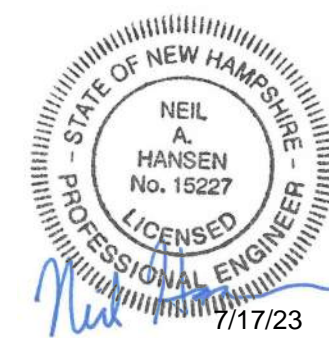
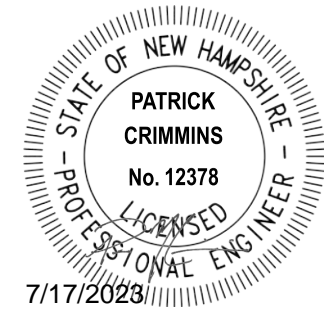
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PHASE 2 SITE PLAN

SCALE: AS SHOWN

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Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

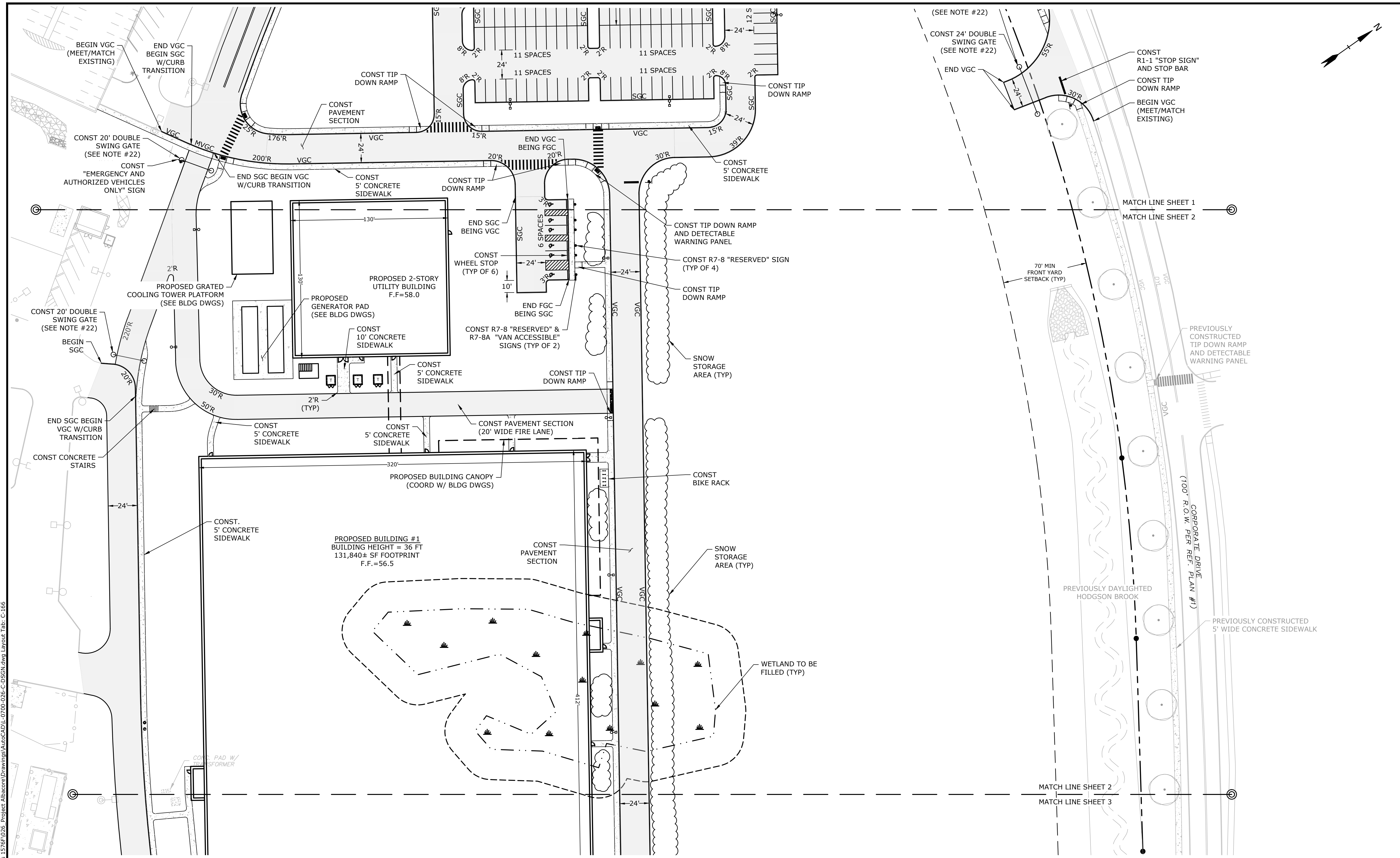
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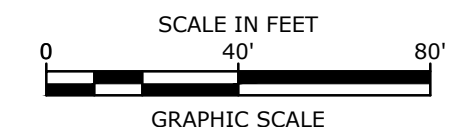
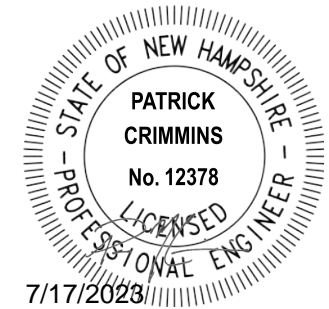
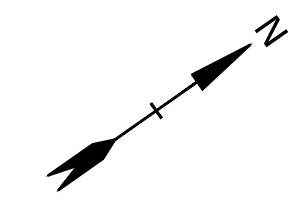
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SEE SHEET C-165 FOR LEGEND AND SITE NOTES

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Proposed Industrial Development

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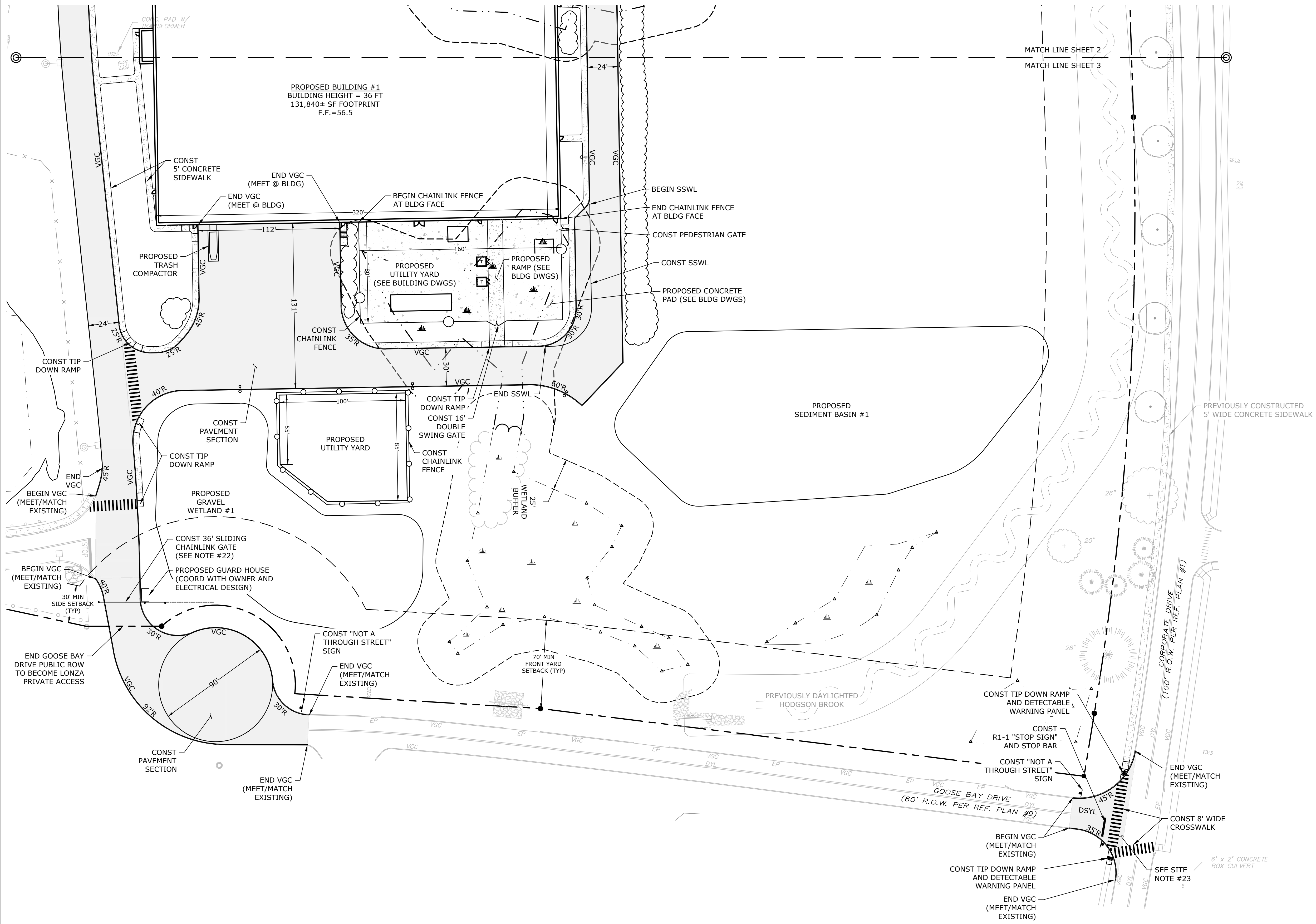
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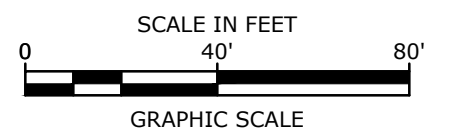
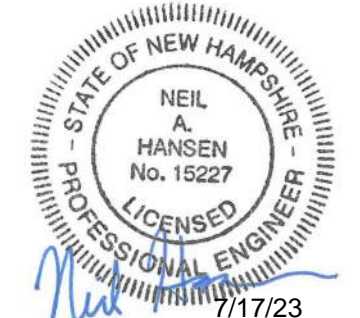
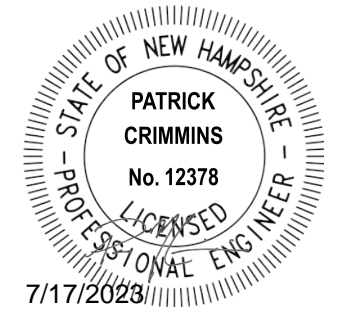
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SEE SHEET C-165 FOR LEGEND AND SITE NOTES

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GRADING AND DRAINAGE NOTES:

1. COMPACTION REQUIREMENTS:
 - BELOW PAVED OR CONCRETE AREAS 95%
 - TRENCH BEDDING MATERIAL AND SAND BLANKET BACKFILL 95%
 - BELOW LOAM AND SEED AREAS 90%
2. ALL STORM DRAINAGE PIPES SHALL BE HIGH DENSITY POLYETHYLENE (HANCOR HI-Q, ADS N-12 OR APPROVED EQUAL), UNLESS OTHERWISE SPECIFIED.
3. SEE UTILITIES PLAN FOR ALL SITE UTILITY INFORMATION.
4. ADJUST ALL MANHOLES, CATCHBASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE.
5. CONTRACTOR SHALL PROVIDE A FINISH PAVEMENT SURFACE AND LAWN AREAS FREE OF LOW SPOTS AND PONDING AREAS. CRITICAL AREAS INCLUDE BUILDING ENTRANCES, EXITS, RAMPS AND LOADING DOCK AREAS ADJACENT TO THE BUILDING.
6. CONTRACTOR SHALL THOROUGHLY CLEAN ALL CATCHBASINS AND DRAIN LINES, WITHIN THE LIMIT OF WORK, OF SEDIMENT IMMEDIATELY UPON COMPLETION OF CONSTRUCTION.
7. ALL MATERIALS AND CONSTRUCTION SHALL CONFORM WITH APPLICABLE FEDERAL, STATE AND LOCAL CODES.
8. ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED SHALL RECEIVE 6" LOAM, SEED FERTILIZER AND MULCH.
9. ALL STORM DRAIN CONSTRUCTION SHALL BE IN ACCORDANCE WITH THE NHDOT STANDARD SPECIFICATIONS FOR HIGHWAYS AND BRIDGES, LATEST EDITION.
10. ALL PROPOSED CATCHBASINS SHALL BE EQUIPPED WITH OIL/GAS SEPARATOR HOODS AND 4' SUMPS.
11. CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
12. CONTRACTOR SHALL COORDINATE WITH THE PROJECT SURVEYOR FOR BENCHMARK AND CONTROL POINTS PRIOR TO CONSTRUCTION.
13. ALL WORK SHALL CONFORM TO THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS, STANDARD SPECIFICATIONS, AND WITH THE STATE OF NEW HAMPSHIRE DEPARTMENT OF TRANSPORTATION, "STANDARD SPECIFICATIONS OF ROAD AND BRIDGE CONSTRUCTION", CURRENT EDITION.
14. PER COORDINATION WITH THE PDA, GROUNDWATER DISCHARGE FROM THE PROPOSED FOUNDATION DRAIN AND UNDER-SLAB DRAIN OF BUILDING 1 AND THE CENTRAL UTILITY BUILDING WILL BE CONNECTED TO THE ONSITE DRAINAGE SYSTEM. IF TREATMENT OF THE GROUNDWATER DISCHARGE IS DETERMINED TO BE REQUIRED DURING THE BUILDING PERMITTING PROCESS AND RE-INFILTRATION IS NOT PERMITTED, A CARBON FILTRATION SYSTEM WILL BE NEEDED.

EROSION CONTROL NOTES:

1. INSTALL EROSION CONTROL BARRIERS AS SHOWN AS FIRST ORDER OF WORK.
2. SEE GENERAL EROSION CONTROL NOTES ON DETAIL SHEETS.
3. PROVIDE INLET PROTECTION AROUND ALL EXISTING AND PROPOSED CATCHBASIN INLETS WITHIN THE WORK LIMITS. MAINTAIN FOR THE DURATION OF THE PROJECT UNTIL PAVEMENT HAS BEEN INSTALLED.
4. INSTALL STABILIZED CONSTRUCTION ENTRANCES.
5. INSPECT INLET PROTECTION AND SILT FENCES DAILY AND AFTER EACH RAIN STORM OF 0.25 INCH OR GREATER. REPAIR/MODIFY PROTECTION AS NECESSARY TO MAXIMIZE EFFICIENCY OF FILTER. REPLACE ALL FILTERS WHEN SEDIMENT IS 1/3 THE FILTER HEIGHT.
6. ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED SHALL RECEIVE 6" LOAM, SEED, FERTILIZER AND MULCH.
7. CONSTRUCT EXCelsior MAT ON ALL SLOPES STEEPER THAN 3:1.
8. PRIOR TO ANY WORK OR SOIL DISTURBANCE COMMENCING ON THE SUBJECT PROPERTY, INCLUDING MOVING OF EARTH, THE APPLICANT SHALL INSTALL ALL EROSION AND SILTATION MITIGATION AND CONTROL MEASURES AS REQUIRED BY STATE AND LOCAL PERMITS AND APPROVALS.
9. CONTRACTOR SHALL BE RESPONSIBLE TO CONTROL DUST AND WIND EROSION THROUGHOUT THE CONSTRUCTION PERIOD. DUST CONTROL MEASURES SHALL INCLUDE, BUT NOT LIMITED TO, SPRINKLING WATER ON UNSTABLE SOILS SUBJECT TO ARID CONDITIONS.
10. THE CONTRACTOR SHALL REMOVE AND PROPERLY DISPOSE OF ALL TEMPORARY EROSION CONTROL DEVICES UPON COMPLETION OF CONSTRUCTION AND FINAL STABILIZATION.
11. ALL CATCHBASIN SUMPS AND PIPING SHALL BE THOROUGHLY CLEANED TO REMOVE ALL SEDIMENT AND DEBRIS AFTER THE PROJECT HAS BEEN PAVED.
12. TEMPORARY SOIL STOCKPILE SHALL BE SURROUNDED BY SILT FENCE AND SHALL BE STABILIZED BY TEMPORARY EROSION CONTROL SEEDING. STOCKPILE AREAS TO BE LOCATED AS FAR AS POSSIBLE FROM THE DELINEATED EDGE OF WETLAND.
13. SAFETY FENCING SHALL BE PROVIDED AROUND STOCKPILES OVER 10 FT.
14. CONCRETE TRUCKS WILL BE REQUIRED TO WASH OUT (IF NECESSARY) SHOOT ONLY WITHIN AREAS WHERE CONCRETE HAS BEEN PLACED. NO OTHER WASH OUT WILL BE ALLOWED.

LEGEND

---	MATCH LINE
---	PROPOSED PROPERTY LINE
---	PROPOSED CONTOUR LINE
---	PROPOSED DRAIN LINE (TYP)
---	PROPOSED SILT SOCK
○	INLET PROTECTION SILT SOCK
⊙	PROPOSED CATCHBASIN
⊙	PROPOSED DOUBLE GRATE CATCHBASIN
⊙	PROPOSED DRAIN MANHOLE
---	CONSTRUCT
---	BUILDING
---	TYP
---	COORD
---	RD
---	VIF
---	TC
---	BC

Proposed Industrial Development

Lonza Biologics

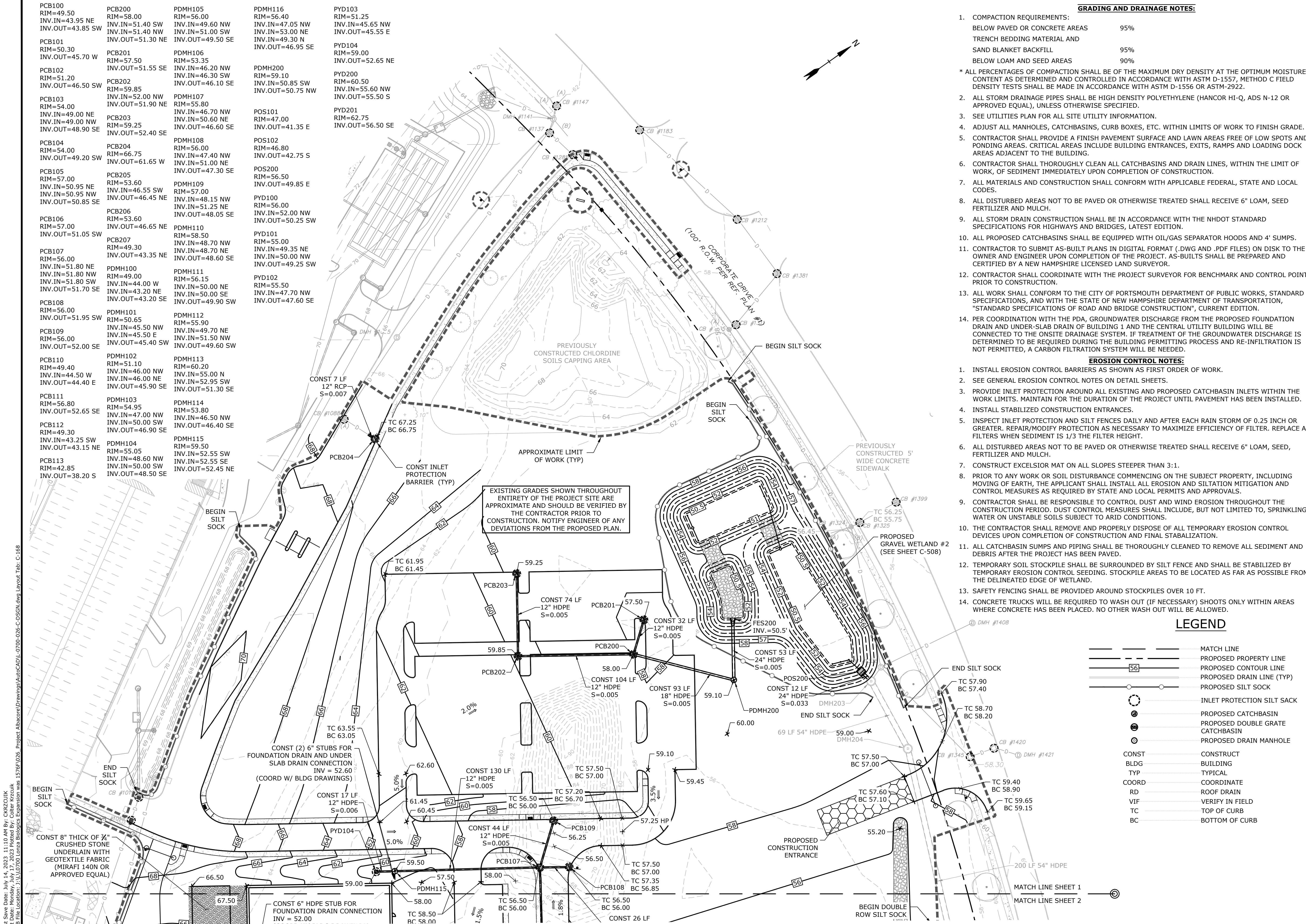
Portsmouth, New Hampshire

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L	7/17/2023	Amended Site Plan Review
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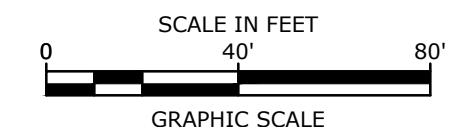
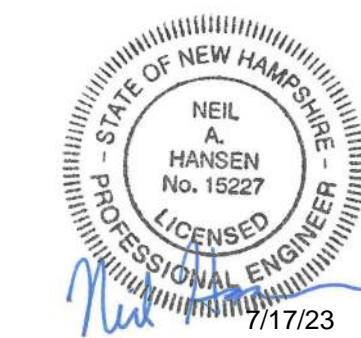
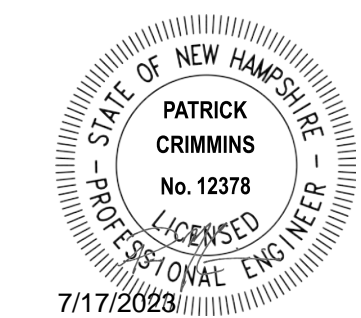
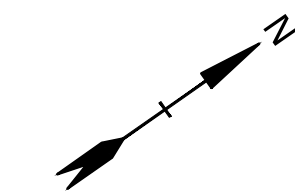
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DATE:	04/03/2018
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DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN

SCALE: AS SHOWN



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Proposed Industrial Development

Lonza Biologics

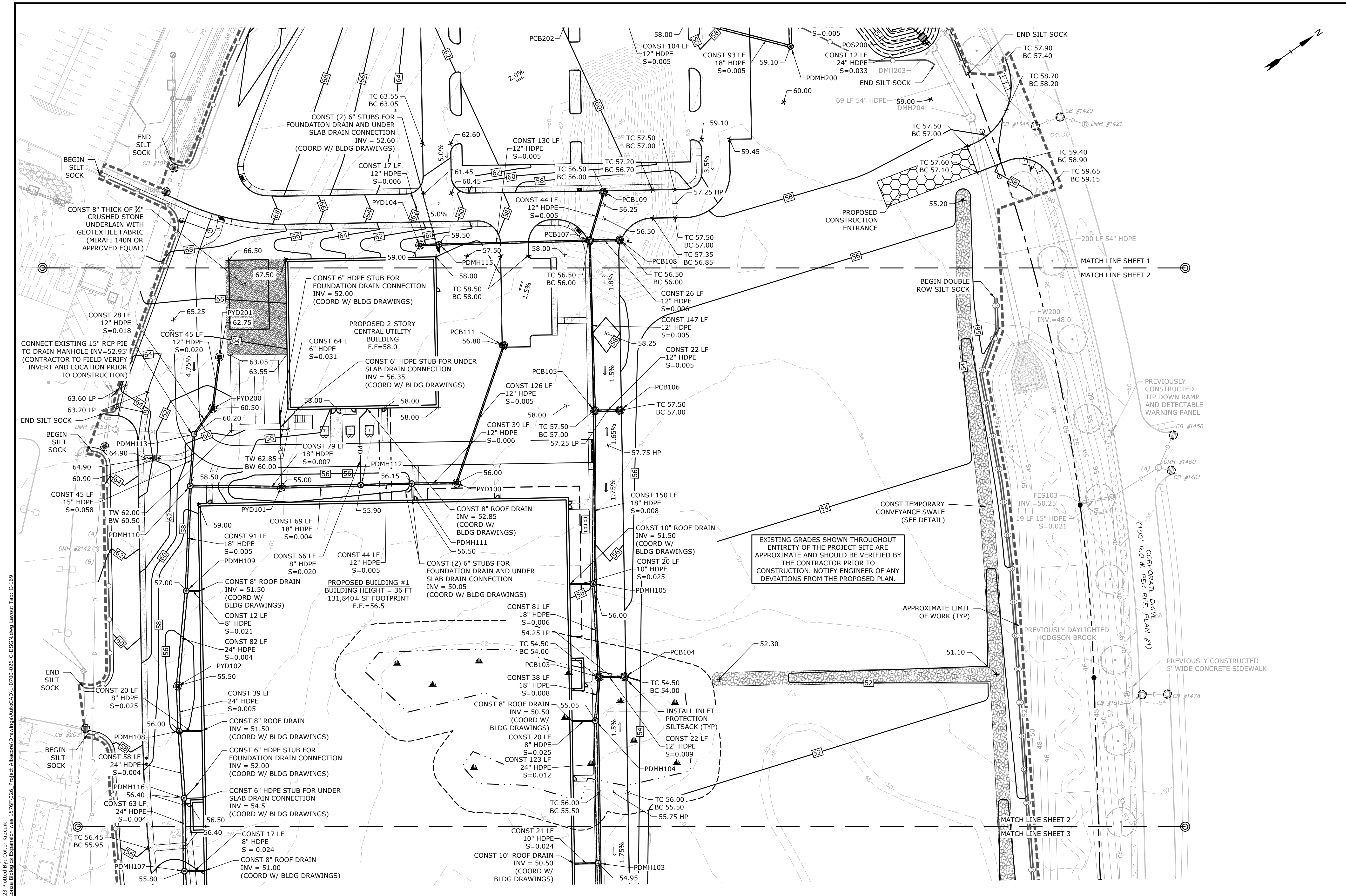
Portsmouth, New Hampshire

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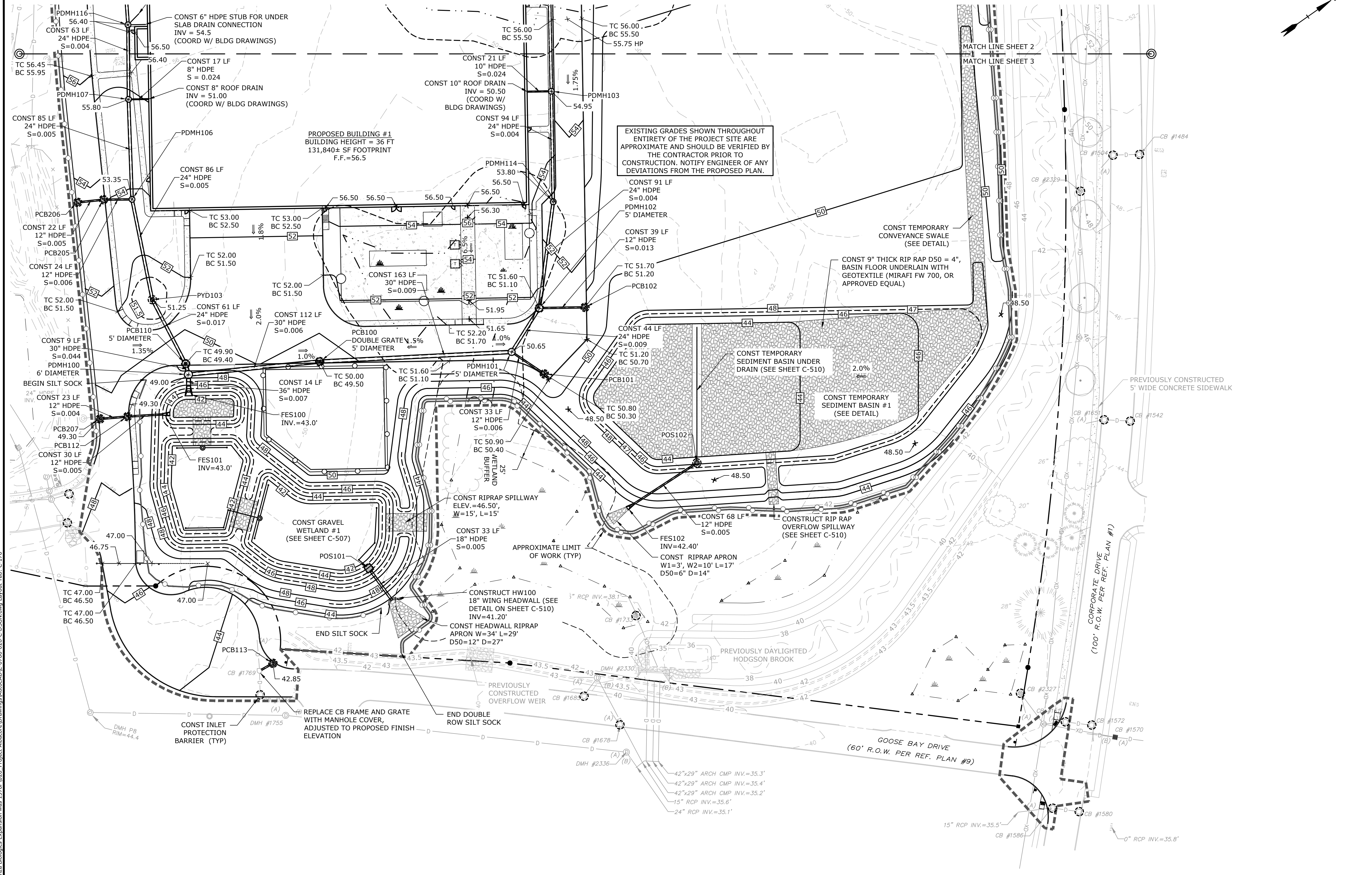
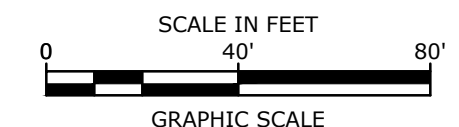
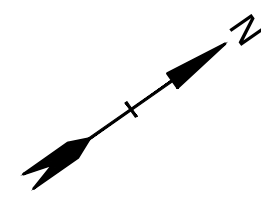
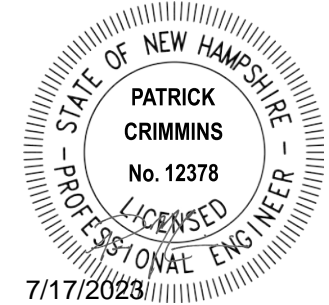
PHASE 2 GRADING, DRAINAGE & EROSION CONTROL PLAN

SCALE: AS SHOWN



SEE SHEET C-168 FOR LEGEND GRADING, DRAINAGE & EROSION CONTROL NOTES, & DRAINAGE STRUCTURE TABLE

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EXISTING GRADES SHOWN THROUGHOUT ENTIRETY OF THE PROJECT SITE ARE APPROXIMATE AND SHOULD BE VERIFIED BY THE CONTRACTOR PRIOR TO CONSTRUCTION. NOTIFY ENGINEER OF ANY DEVIATIONS FROM THE PROPOSED PLAN.

SEE SHEET C-168 FOR LEGEND GRADING, DRAINAGE & EROSION CONTROL NOTES, & DRAINAGE STRUCTURE TABLE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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PHASE 2
GRADING, DRAINAGE &
EROSION CONTROL PLAN
SCALE: AS SHOWN

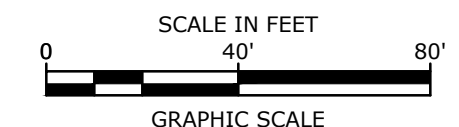
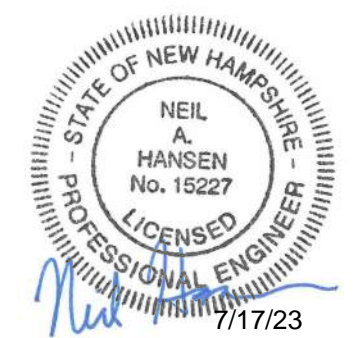
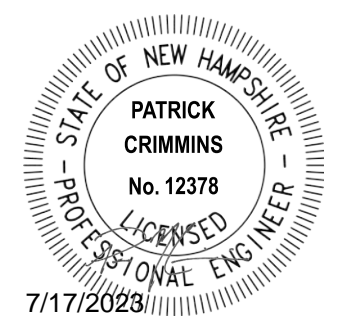
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LEGEND

---	MATCH LINE
D	EXISTING STORM DRAIN
SS	EXISTING SANITARY SEWER
W	EXISTING WATER
G	EXISTING GAS
E	EXISTING UNDERGROUND ELECTRIC
OHW	EXISTING OVERHEAD UTILITY
---	PROPOSED STORM DRAIN
---	PROPOSED SANITARY SEWER
PW	PROPOSED WATER
G	PROPOSED GAS
---	PROPOSED UNDERGROUND ELECTRIC
---	PROPOSED UNDERGROUND COMMUNICATION
⊙	EXISTING CATCHBASIN
⊙	EXISTING DRAIN MANHOLE
⊙	EXISTING SEWER MANHOLE
⊙	EXISTING HYDRANT
⊙	EXISTING WATER VALVE
⊙	EXISTING ELECTRIC MANHOLE
⊙	EXISTING TELEPHONE MANHOLE
⊙	PROPOSED CATCHBASIN
⊙	PROPOSED DOUBLE GRATE CATCHBASIN
⊙	PROPOSED DRAIN MANHOLE
⊙	PROPOSED SEWER MANHOLE
⊙	PROPOSED WATER VALVE
⊙	PROPOSED FDC CONNECTION
⊙	PROPOSED HYDRANT
⊙	PROPOSED GAS VALVE
⊙	PROPOSED ELECTRIC MANHOLE
⊙	PROPOSED TRANSFORMER PAD
⊙	PROPOSED LIGHT POLE BASE
□	CONSTRUCT
BLDG	BUILDING
TYP	TYPICAL
COORD	COORDINATE
VIF	VERIFY IN FIELD
DI	DUCTILE IORN
COM	COMMUNICATION
FRP	FIBERGLASS REINFORCED POLYMER MORTAR PIPE

UTILITY NOTES:

- THE LOCATIONS OF EXISTING UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR ENGINEER. IT IS THE CONTRACTOR'S RESPONSIBILITY TO LOCATE ALL UTILITIES, ANTICIPATE CONFLICTS, REPAIR EXISTING UTILITIES, AND RELOCATE EXISTING UTILITIES REQUIRED TO COMPLETE THE WORK AT NO ADDITIONAL COST TO THE OWNER.
- COORDINATE ALL UTILITY WORK WITH APPROPRIATE UTILITY COMPANY.
NATURAL GAS - UNITIL
WATER - CITY OF PORTSMOUTH DPW
SEWER - CITY OF PORTSMOUTH DPW
ELECTRIC - EVERSOURCE
COMMUNICATIONS - FAIRPOINT, COMCAST, FIRSTLIGHT
- SEE EXISTING CONDITIONS PLAN FOR BENCHMARK INFORMATION.
- SEE GRADING, DRAINAGE & EROSION CONTROL PLAN FOR PROPOSED GRADING AND EROSION CONTROL MEASURES.
- ALL WATER MAIN INSTALLATIONS SHALL BE CLASS 52, CEMENT LINED DUCTILE IRON PIPE.
- ALL WATER MAIN INSTALLATIONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION PRIOR TO ACTIVATING THE SYSTEM. CONTRACTOR SHALL COORDINATE CHLORINATION AND TESTING WITH THE CITY OF PORTSMOUTH WATER DEPARTMENT.
- ALL SEWER PIPE SHALL BE FIBERGLASS REINFORCED POLYMER MORTAR (FRP) PIPE UNLESS OTHERWISE STATED.
- ALL WORK WITHIN PORTSMOUTH ROWS SHALL BE COORDINATED WITH CITY OF PORTSMOUTH AND THE PEASE DEVELOPMENT AUTHORITY.
- CONTRACTOR SHALL MAINTAIN UTILITY SERVICES TO ABUTTING PROPERTIES THROUGHOUT CONSTRUCTION.
- CONNECTIONS TO EXISTING WATER MAIN SHALL BE CONSTRUCTED TO CITY OF PORTSMOUTH STANDARDS.
- EXISTING UTILITIES TO BE REMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER SERVICES.
- ALL ELECTRICAL MATERIAL WORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC CODE, LATEST EDITION, AND ALL APPLICABLE STATE AND LOCAL CODES.
- THE EXACT LOCATION OF NEW UTILITY SERVICES AND CONNECTIONS SHALL BE COORDINATED WITH THE BUILDING DRAWINGS AND THE UTILITY COMPANIES.
- ADJUST ALL MANHOLES, CATCH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE.
- ALL UNDERGROUND CONDUITS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING CABLES.
- THE CONTRACTOR SHALL OBTAIN, PAY FOR, AND COMPLY WITH ALL REQUIRED PERMITS, ARRANGE FOR ALL INSPECTIONS, AND SUBMIT COPIES OF ACCEPTANCE CERTIFICATES TO THE OWNER PRIOR TO THE COMPLETION OF THIS PROJECT.
- THE CONTRACTOR SHALL PROVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS, CONNECTORS, COVER PLATES, AND OTHER MISCELLANEOUS ITEMS NOT NECESSARILY DETAILED ON THESE DRAWINGS TO RENDER INSTALLATION OF UTILITIES COMPLETE AND OPERATIONAL.
- CONTRACTOR SHALL PROVIDE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR NATURAL GAS SERVICES.
- A 10-FOOT MINIMUM EDGE TO EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL WATER AND SANITARY SEWER LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION SHALL BE PROVIDED AT ALL WATER/SANITARY SEWER CROSSINGS.
- THE CONTRACTOR SHALL CONTACT "DIG-SAFE" 72 HOURS PRIOR TO COMMENCING CONSTRUCTION. THE CONTRACTOR SHALL HAVE THE "DIG-SAFE" NUMBER ON SITE AT ALL TIMES.
- CONTRACTOR TO SUBMIT AS-BUILT PLANS IN DIGITAL FORMAT (.DWG AND .PDF FILES) ON DISK TO THE OWNER AND ENGINEER UPON COMPLETION OF THE PROJECT. AS-BUILTS SHALL BE PREPARED AND CERTIFIED BY A NEW HAMPSHIRE LICENSED LAND SURVEYOR.
- SAWCUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN.
- HYDRANTS, GATE VALVES, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF PORTSMOUTH AND THE PEASE DEVELOPMENT AUTHORITY.
- COORDINATE TESTING OF SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH.
- ALL SEWER PIPE WITH LESS THAN 6' OF COVER IN PAVED AREAS OR LESS THAN 4' OF COVER IN UNPAVED AREAS SHALL BE INSULATED.
- CONTRACTOR SHALL COORDINATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, MANHOLE CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RELOCATION, AND TRANSFORMER CONSTRUCTION WITH POWER COMPANY.
- CONTRACTOR SHALL PHASE UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN CONSTRUCTION, AS TO MAINTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL COORDINATE TEMPORARY SERVICES TO ABUTTERS WITH THE UTILITY COMPANY AND AFFECTED ABUTTER.
- SITE LIGHTING SPECIFICATIONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND SIGN ILLUMINATION SHALL BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER.
- CONTRACTOR SHALL CONSTRUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE FOUNDATION WALLS AND CONNECT THESE TO SERVICE STUBS FROM THE BUILDING.
- EXISTING SEWER MAIN AND STRUCTURES IN GOOSE BAY DRIVE ARE BASED ON A PROPOSED DESIGN BY UNDERWOOD ENGINEERS, DATED JULY 28, 2017, AND WAS CONSTRUCTED IN SUMMER 2018. THE PROPOSED ON-SITE SEWER DESIGN ELEVATIONS ARE BASED ON THE UNDERWOOD PLAN DURING CONSTRUCTION. THE CONTRACTOR SHALL COORDINATE SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH, AND VERIFY ALL INVERTS PRIOR TO CONSTRUCTION.
- LOCATION SHOWN IS APPROXIMATE ONLY. FINAL DESIGN OF NATURAL GAS SERVICE TO BE COMPLETED BY UNITIL. WORK IN CORPORATE DRIVE MAY NEED TO BE COMPLETED IN CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE. COORDINATE WITH CITY OF PORTSMOUTH AND UNITIL.
- LOCATION AND TYPE SHOWN IS APPROXIMATE ONLY. FINAL DESIGN OF ELECTRIC SERVICE AND ASSOCIATED INFRASTRUCTURE TO BE COMPLETED BY EVERSOURCE. WORK IN CORPORATE DRIVE MAY NEED TO BE COMPLETED IN CONJUNCTION WITH FUTURE RECONSTRUCTION OF CORPORATE DRIVE. COORDINATE WITH CITY OF PORTSMOUTH AND EVERSOURCE.
- FINAL LOCATION OF ALL WATER METER AND VALVES SHALL BE COORDINATED WITH THE CITY OF PORTSMOUTH DPW PRIOR TO CONSTRUCTION.
- FINAL LOCATION OF FIRE HYDRANTS, FIRE DEPARTMENT CONNECTIONS AND DRY STAND PIPES WILL BE COORDINATED WITH THE BUILDING DRAWINGS AND APPROVED BY THE PORTSMOUTH FIRE DEPARTMENT PRIOR TO CONSTRUCTION.
- THE APPLICANT SHALL HAVE A SITE SURVEY CONDUCTED BY A RADIO COMMUNICATIONS CARRIER APPROVED BY THE CITY'S COMMUNICATIONS DIVISION. THE RADIO COMMUNICATIONS CARRIER MUST BE FAMILIAR AND CONVERSANT WITH THE POLICE AND RADIO CONFIGURATION. IF THE SITE SURVEY INDICATES IT IS NECESSARY TO INSTALL A SIGNAL REPEATER EITHER ON OR NEAR THE PROPOSED PROJECT, THOSE COSTS SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER. THE OWNER SHALL COORDINATE WITH THE SUPERVISOR OF RADIO COMMUNICATIONS FOR THE CITY.
- CONTRACTOR SHALL PERFORM TEST PITS TO VERIFY INVERT ELEVATIONS IN FIELD PRIOR TO CONSTRUCTION AND SHALL NOTIFY ENGINEER IF ELEVATION DIFFERS FROM PLAN.
- CONTRACTOR SHALL DISPOSE OF ASBESTOS CEMENT PIPES IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS SHOULD ANY BE FOUND DURING CONSTRUCTION.



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

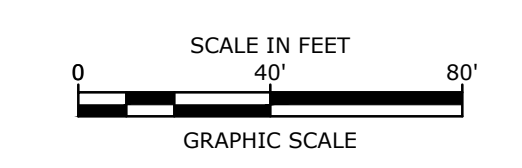
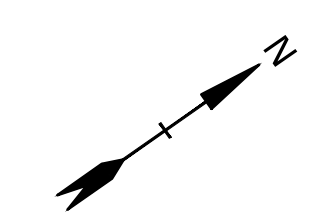
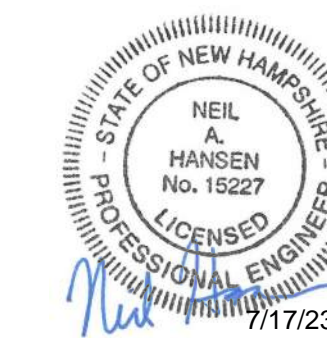
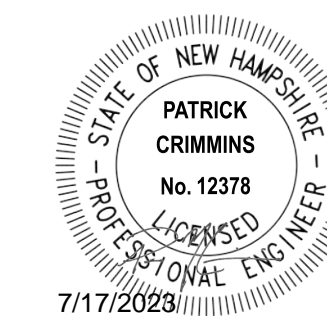
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CHECKED:	NAH
APPROVED:	PMC

PHASE 2 UTILITIES PLAN

SCALE: AS SHOWN

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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
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Proposed Industrial Development

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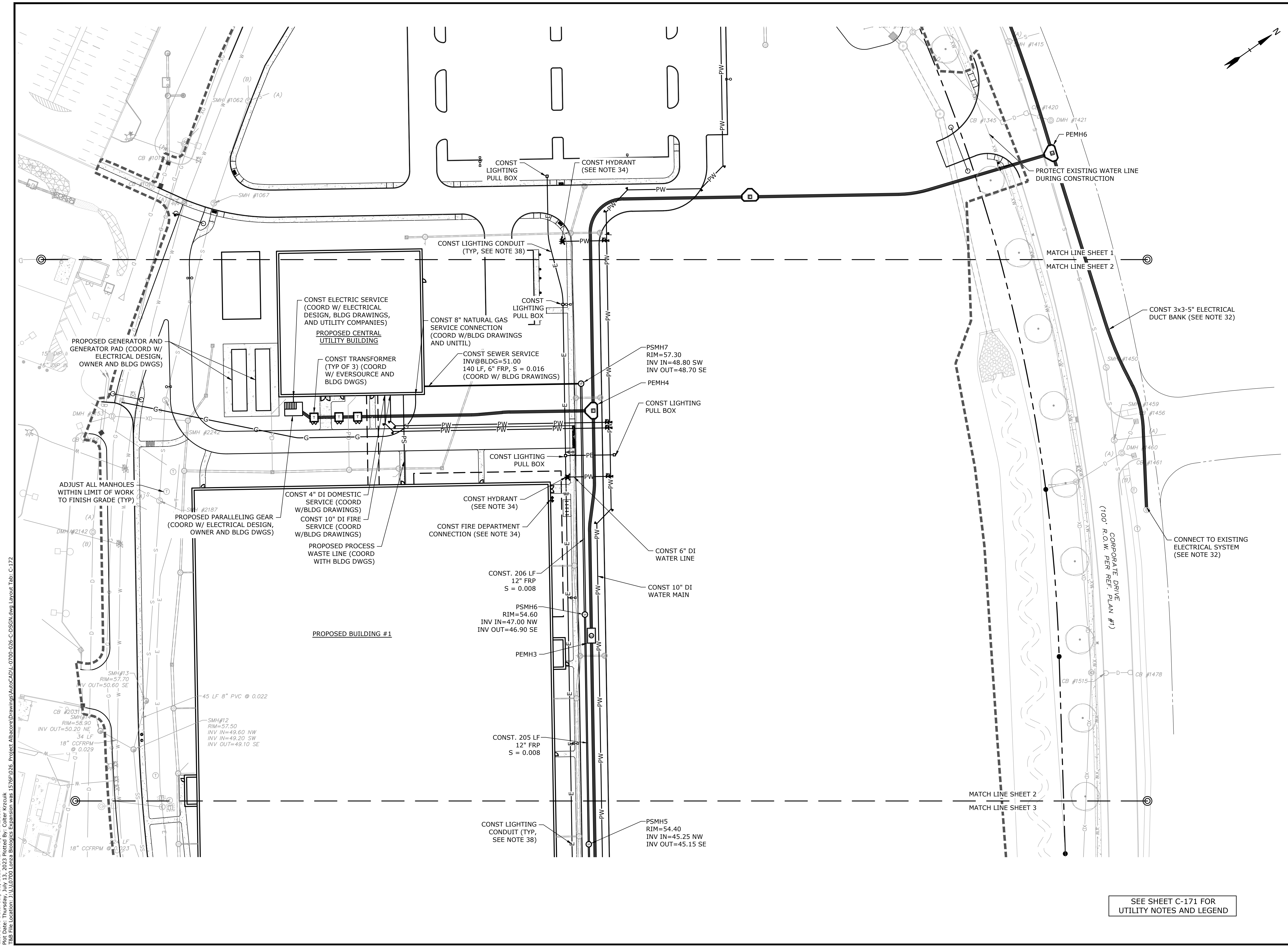
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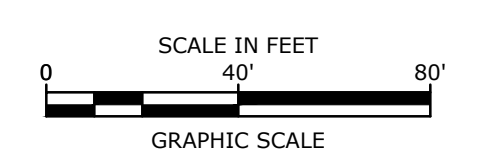
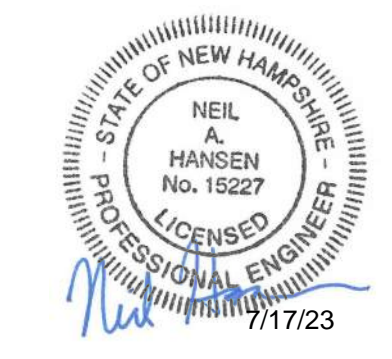
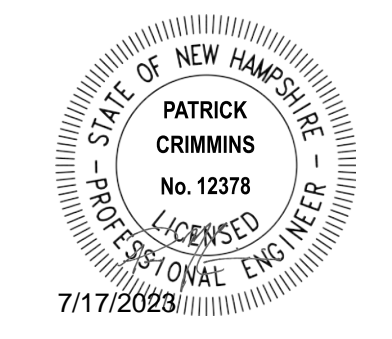
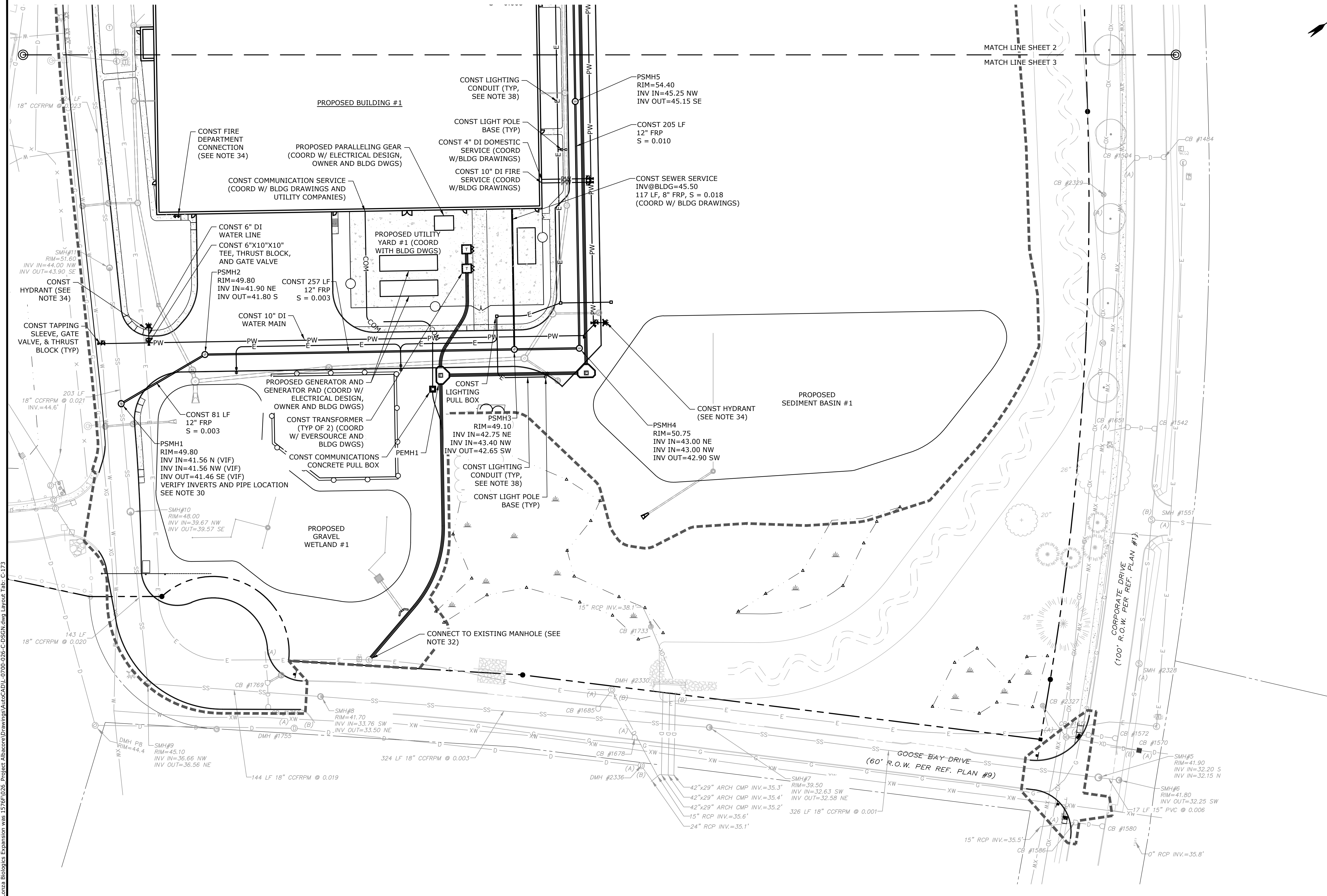
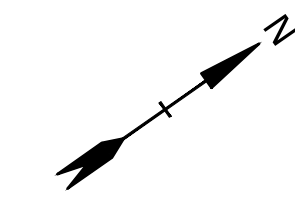
PHASE 2 UTILITIES PLAN

SCALE: AS SHOWN



SEE SHEET C-171 FOR UTILITY NOTES AND LEGEND

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Proposed Industrial Development

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Portsmouth, New Hampshire

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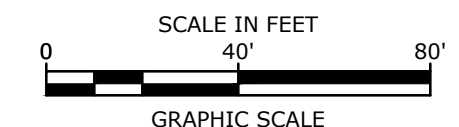
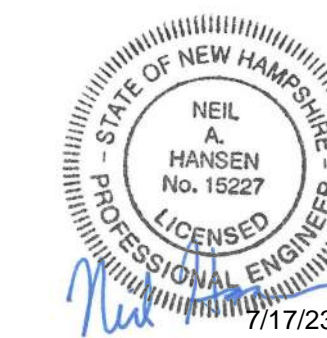
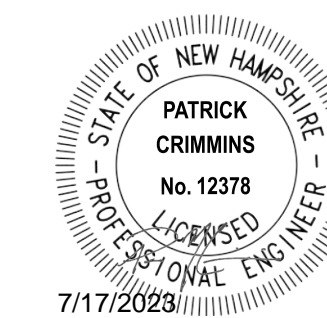
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APPROVED:	PMC

PHASE 2 UTILITIES PLAN

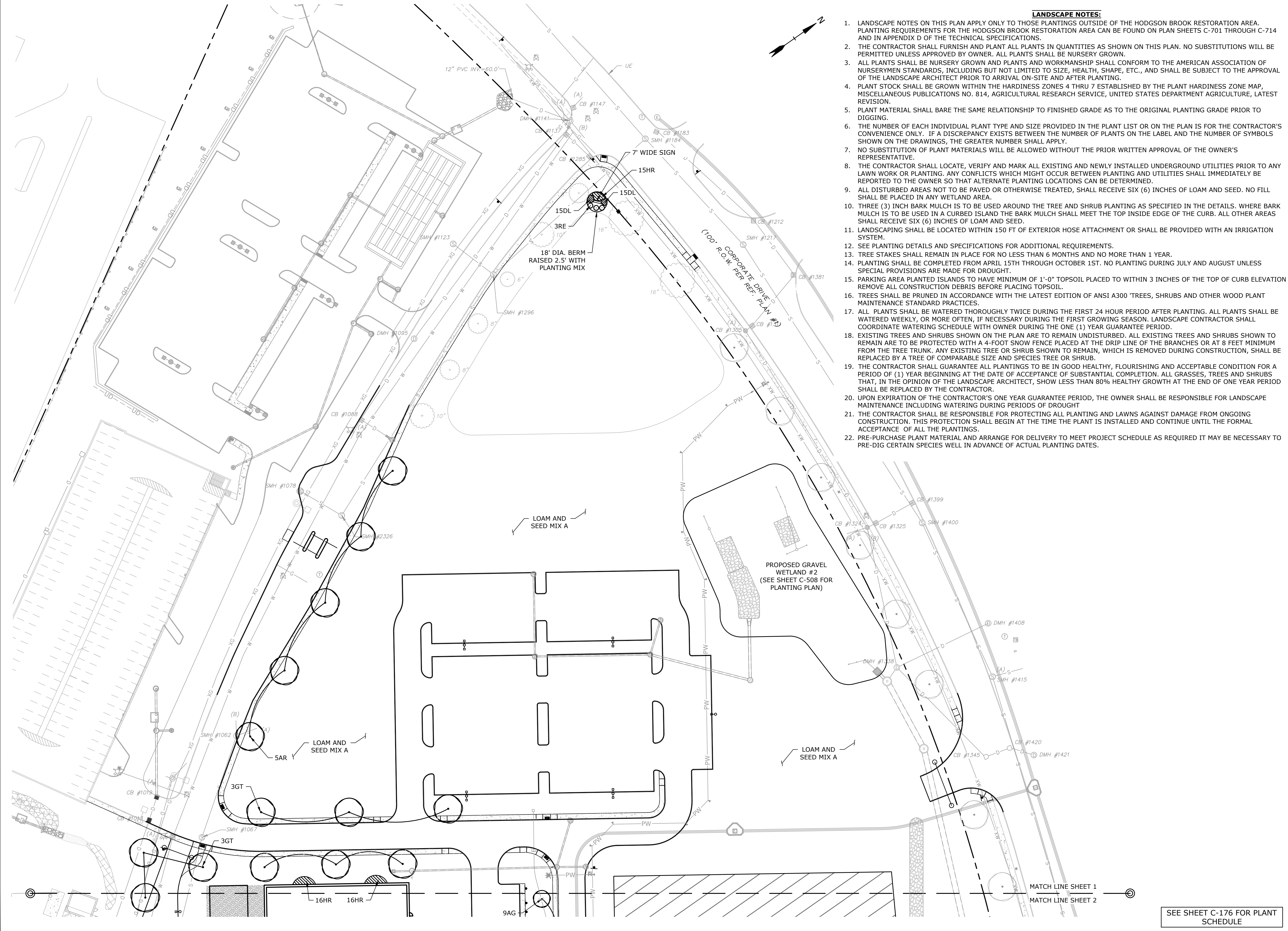
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SEE SHEET C-171 FOR UTILITY NOTES AND LEGEND

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- LANDSCAPE NOTES:**
- LANDSCAPE NOTES ON THIS PLAN APPLY ONLY TO THOSE PLANTINGS OUTSIDE OF THE HODGSON BROOK RESTORATION AREA. PLANTING REQUIREMENTS FOR THE HODGSON BROOK RESTORATION AREA CAN BE FOUND ON PLAN SHEETS C-701 THROUGH C-714 AND IN APPENDIX D OF THE TECHNICAL SPECIFICATIONS.
 - THE CONTRACTOR SHALL FURNISH AND PLANT ALL PLANTS IN QUANTITIES AS SHOWN ON THIS PLAN. NO SUBSTITUTIONS WILL BE PERMITTED UNLESS APPROVED BY OWNER. ALL PLANTS SHALL BE NURSERY GROWN.
 - ALL PLANTS SHALL BE NURSERY GROWN AND PLANTS AND WORKMANSHIP SHALL CONFORM TO THE AMERICAN ASSOCIATION OF NURSERYMEN STANDARDS, INCLUDING BUT NOT LIMITED TO SIZE, HEALTH, SHAPE, ETC., AND SHALL BE SUBJECT TO THE APPROVAL OF THE LANDSCAPE ARCHITECT PRIOR TO ARRIVAL ON-SITE AND AFTER PLANTING.
 - PLANT STOCK SHALL BE GROWN WITHIN THE HARDINESS ZONES 4 THRU 7 ESTABLISHED BY THE PLANT HARDINESS ZONE MAP, MISCELLANEOUS PUBLICATIONS NO. 814, AGRICULTURAL RESEARCH SERVICE, UNITED STATES DEPARTMENT AGRICULTURE, LATEST REVISION.
 - PLANT MATERIAL SHALL BARE THE SAME RELATIONSHIP TO FINISHED GRADE AS TO THE ORIGINAL PLANTING GRADE PRIOR TO DIGGING.
 - THE NUMBER OF EACH INDIVIDUAL PLANT TYPE AND SIZE PROVIDED IN THE PLANT LIST OR ON THE PLAN IS FOR THE CONTRACTOR'S CONVENIENCE ONLY. IF A DISCREPANCY EXISTS BETWEEN THE NUMBER OF PLANTS ON THE LABEL AND THE NUMBER OF SYMBOLS SHOWN ON THE DRAWINGS, THE GREATER NUMBER SHALL APPLY.
 - NO SUBSTITUTION OF PLANT MATERIALS WILL BE ALLOWED WITHOUT THE PRIOR WRITTEN APPROVAL OF THE OWNER'S REPRESENTATIVE.
 - THE CONTRACTOR SHALL LOCATE, VERIFY AND MARK ALL EXISTING AND NEWLY INSTALLED UNDERGROUND UTILITIES PRIOR TO ANY LAWN WORK OR PLANTING. ANY CONFLICTS WHICH MIGHT OCCUR BETWEEN PLANTING AND UTILITIES SHALL IMMEDIATELY BE REPORTED TO THE OWNER SO THAT ALTERNATE PLANTING LOCATIONS CAN BE DETERMINED.
 - ALL DISTURBED AREAS NOT TO BE PAVED OR OTHERWISE TREATED, SHALL RECEIVE SIX (6) INCHES OF LOAM AND SEED. NO FILL SHALL BE PLACED IN ANY WETLAND AREA.
 - THREE (3) INCH BARK MULCH IS TO BE USED AROUND THE TREE AND SHRUB PLANTING AS SPECIFIED IN THE DETAILS. WHERE BARK MULCH IS TO BE USED IN A CURBED ISLAND THE BARK MULCH SHALL MEET THE TOP INSIDE EDGE OF THE CURB. ALL OTHER AREAS SHALL RECEIVE SIX (6) INCHES OF LOAM AND SEED.
 - LANDSCAPING SHALL BE LOCATED WITHIN 150 FT OF EXTERIOR HOSE ATTACHMENT OR SHALL BE PROVIDED WITH AN IRRIGATION SYSTEM.
 - SEE PLANTING DETAILS AND SPECIFICATIONS FOR ADDITIONAL REQUIREMENTS.
 - TREE STAKES SHALL REMAIN IN PLACE FOR NO LESS THAN 6 MONTHS AND NO MORE THAN 1 YEAR.
 - PLANTING SHALL BE COMPLETED FROM APRIL 15TH THROUGH OCTOBER 1ST. NO PLANTING DURING JULY AND AUGUST UNLESS SPECIAL PROVISIONS ARE MADE FOR DROUGHT.
 - PARKING AREA PLANTED ISLANDS TO HAVE MINIMUM OF 1'-0" TOPSOIL PLACED TO WITHIN 3 INCHES OF THE TOP OF CURB ELEVATION REMOVE ALL CONSTRUCTION DEBRIS BEFORE PLACING TOPSOIL.
 - TREES SHALL BE PRUNED IN ACCORDANCE WITH THE LATEST EDITION OF ANSI A300 'TREES, SHRUBS AND OTHER WOOD PLANT MAINTENANCE STANDARD PRACTICES.
 - ALL PLANTS SHALL BE WATERED THOROUGHLY TWICE DURING THE FIRST 24 HOUR PERIOD AFTER PLANTING. ALL PLANTS SHALL BE WATERED WEEKLY, OR MORE OFTEN, IF NECESSARY DURING THE FIRST GROWING SEASON. LANDSCAPE CONTRACTOR SHALL COORDINATE WATERING SCHEDULE WITH OWNER DURING THE ONE (1) YEAR GUARANTEE PERIOD.
 - EXISTING TREES AND SHRUBS SHOWN ON THE PLAN ARE TO REMAIN UNDISTURBED. ALL EXISTING TREES AND SHRUBS SHOWN TO REMAIN ARE TO BE PROTECTED WITH A 4-FOOT SNOW FENCE PLACED AT THE DRIP LINE OF THE BRANCHES OR AT 8 FEET MINIMUM FROM THE TREE TRUNK. ANY EXISTING TREE OR SHRUB SHOWN TO REMAIN, WHICH IS REMOVED DURING CONSTRUCTION, SHALL BE REPLACED BY A TREE OF COMPARABLE SIZE AND SPECIES TREE OR SHRUB.
 - THE CONTRACTOR SHALL GUARANTEE ALL PLANTINGS TO BE IN GOOD HEALTHY, FLOURISHING AND ACCEPTABLE CONDITION FOR A PERIOD OF (1) YEAR BEGINNING AT THE DATE OF ACCEPTANCE OF SUBSTANTIAL COMPLETION. ALL GRASSES, TREES AND SHRUBS THAT, IN THE OPINION OF THE LANDSCAPE ARCHITECT, SHOW LESS THAN 80% HEALTHY GROWTH AT THE END OF ONE YEAR PERIOD SHALL BE REPLACED BY THE CONTRACTOR.
 - UPON EXPIRATION OF THE CONTRACTOR'S ONE YEAR GUARANTEE PERIOD, THE OWNER SHALL BE RESPONSIBLE FOR LANDSCAPE MAINTENANCE INCLUDING WATERING DURING PERIODS OF DROUGHT
 - THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING ALL PLANTING AND LAWNS AGAINST DAMAGE FROM ONGOING CONSTRUCTION. THIS PROTECTION SHALL BEGIN AT THE TIME THE PLANT IS INSTALLED AND CONTINUE UNTIL THE FORMAL ACCEPTANCE OF ALL THE PLANTINGS.
 - PRE-PURCHASE PLANT MATERIAL AND ARRANGE FOR DELIVERY TO MEET PROJECT SCHEDULE AS REQUIRED IT MAY BE NECESSARY TO PRE-DIG CERTAIN SPECIES WELL IN ADVANCE OF ACTUAL PLANTING DATES.



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
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DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

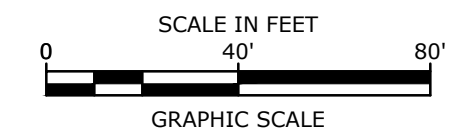
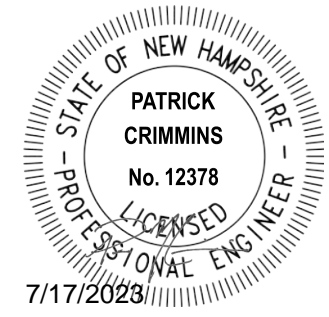
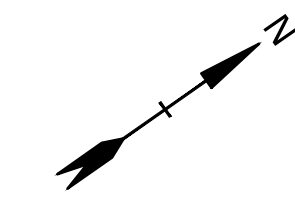
PHASE 2 LANDSCAPE PLAN

SCALE: AS SHOWN

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SEE SHEET C-176 FOR PLANT SCHEDULE



Proposed Industrial Development

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Portsmouth, New Hampshire

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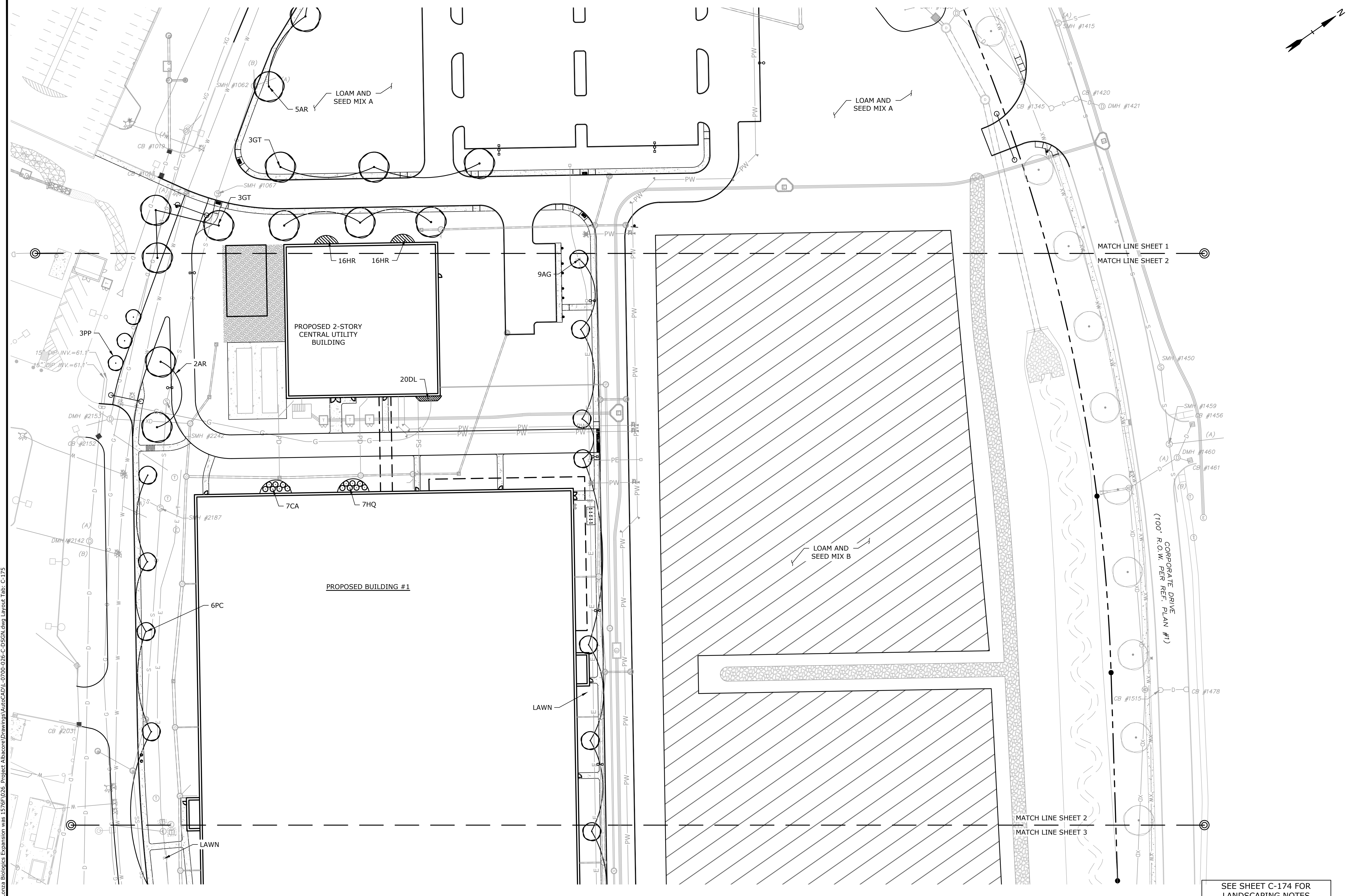
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PHASE 2 LANDSCAPE PLAN

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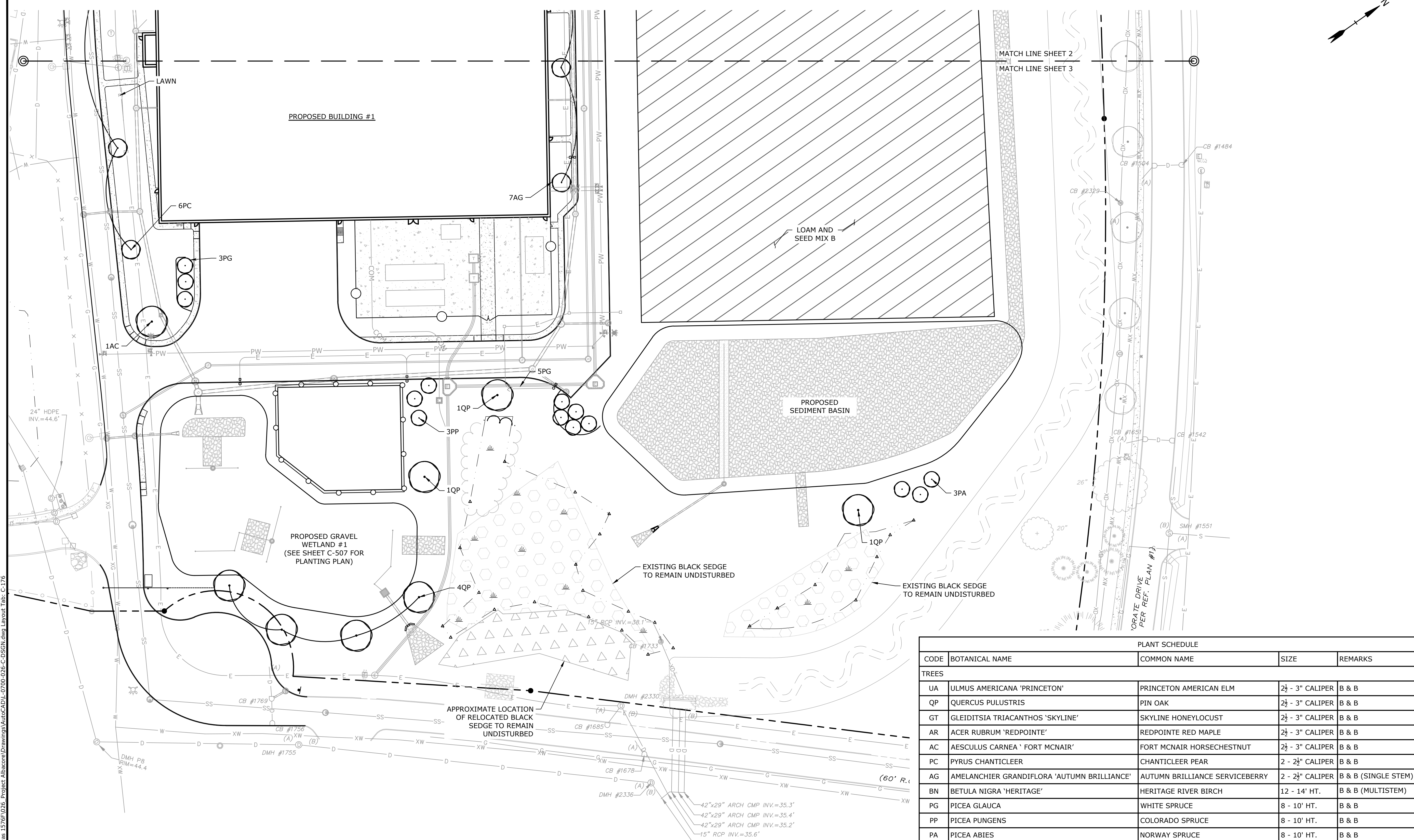
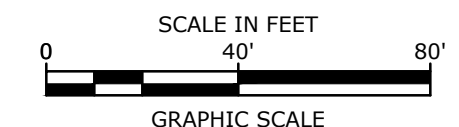
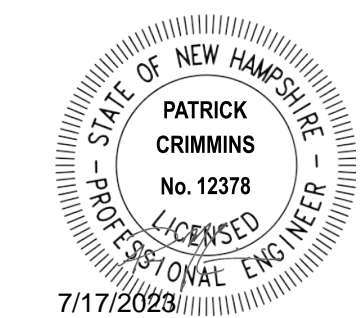
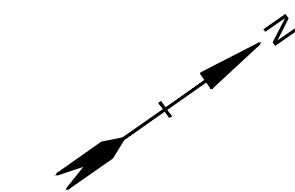
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SEE SHEET C-174 FOR LANDSCAPING NOTES

SEE SHEET C-176 FOR PLANT SCHEDULE



- SEED MIX NOTES**
- SEED MIX "A" SHALL CONTAIN THE FOLLOWING SEED REQUIREMENTS AND BE APPLIED AT A RATE OF 40LB/AC OR APPROVED EQUAL.

SEED MIX	% BY WEIGHT
"REBEL II" TALL FESCUE	70%
"PALMER" PERENNIAL RYEGRASS	20%
"BARON" KENTUCKY BLUEGRASS	10%
 - SEED MIX "B" SHALL BE NEW ENGLAND CONSERVATION/WILDLIFE MIX OR APPROVED EQUAL APPLIED AT A RATE OF 25LB/AC.

SEE SHEET C-174 FOR LANDSCAPING NOTES

PLANT SCHEDULE				
CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS
TREES				
UA	ULMUS AMERICANA 'PRINCETON'	PRINCETON AMERICAN ELM	2½ - 3" CALIPER	B & B
QP	QUERCUS PULUSTRIS	PIN OAK	2½ - 3" CALIPER	B & B
GT	GLEIDITSIA TRIACANTHOS 'SKYLINE'	SKYLINE HONEYLOCUST	2½ - 3" CALIPER	B & B
AR	ACER RUBRUM 'REDPOINTE'	REDPOINTE RED MAPLE	2½ - 3" CALIPER	B & B
AC	AESCULUS CARNEA 'FORT MCNAIR'	FORT MCNAIR HORSECHESTNUT	2½ - 3" CALIPER	B & B
PC	PYRUS CHANTICLEER	CHANTICLEER PEAR	2 - 2½" CALIPER	B & B
AG	AMELANCHIER GRANDIFLORA 'AUTUMN BRILLIANCE'	AUTUMN BRILLIANCE SERVICEBERRY	2 - 2½" CALIPER	B & B (SINGLE STEM)
BN	BETULA NIGRA 'HERITAGE'	HERITAGE RIVER BIRCH	12 - 14' HT.	B & B (MULTISTEM)
PG	PICEA GLAUCA	WHITE SPRUCE	8 - 10' HT.	B & B
PP	PICEA PUNGENS	COLORADO SPRUCE	8 - 10' HT.	B & B
PA	PICEA ABIES	NORWAY SPRUCE	8 - 10' HT.	B & B
SHRUBS				
VC	VIBURNUM CASSINOIDES	WITHEROD VIBURNUM	2½ - 3' HT.	B & B
RE	RHODODENDRON 'ENGLISH ROSEUM'	ENGLISH ROSEUM RHODODENDRON	2½ - 3' HT.	B & B
CA	CLETHERA ALNIFOLIA	SUMMERSWEET CLETHERA	7 GALLON	CONTAINER
HQ	HYDRANGEA QUERCIFOLIA 'SNOW QUEEN'	SNOW QUEEN OAKLEAF HYDRANGEA	2½ - 3' HT.	B & B
GROUNDCOVERS & PERENNIALS				
DL	HEMEROCALLIS 'STELLA DORO'	STELLA DORO DAYLILY	2 GALLON	CONTAINER
HR	HOSTA 'ROYAL STANDARD'	ROYAL STANDARD HOSTA	2 GALLON	CONTAINER
AS	ASTILBE 'VISIONS IN PINK'	VISIONS IN PINK ASTILBE	2 GALLON	CONTAINER
CAL	CALAMAGROSTIS 'KARL FOERSTER'	KARL FOERSTER FEATHER REED GRASS	3 GALLON	CONTAINER

Proposed Industrial Development

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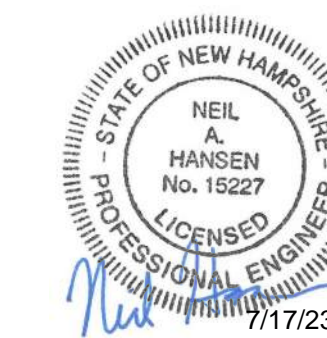
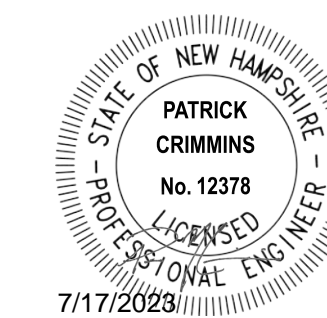
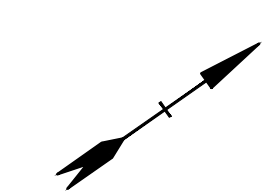
Portsmouth, New Hampshire

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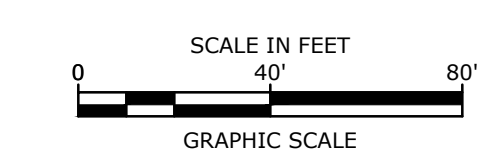
PHASE 2 LANDSCAPE PLAN

SCALE: AS SHOWN

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Symbol	Qty	Label	Arrangement	Description	(MANUFAC)
[Symbol]	4	P3-2	Back-Back	XWM-LED-12L-S1L-5W-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 D180 GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	7	S3	Single	MRM-LED-09L-S1L-1-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	3	S4	Single	MRM-LED-09L-S1L-FT-UNV-DIM-30-70CRI-CXX / 48Q-B3-S11G-20-S-GA-4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	1	S5-1	Single	MRM-LED-09L-S1L-5W-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	9	W3	Single	XWM-3-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
[Symbol]	10	W4	Single	XWM-FT-LED-12L-30-UE-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.



Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

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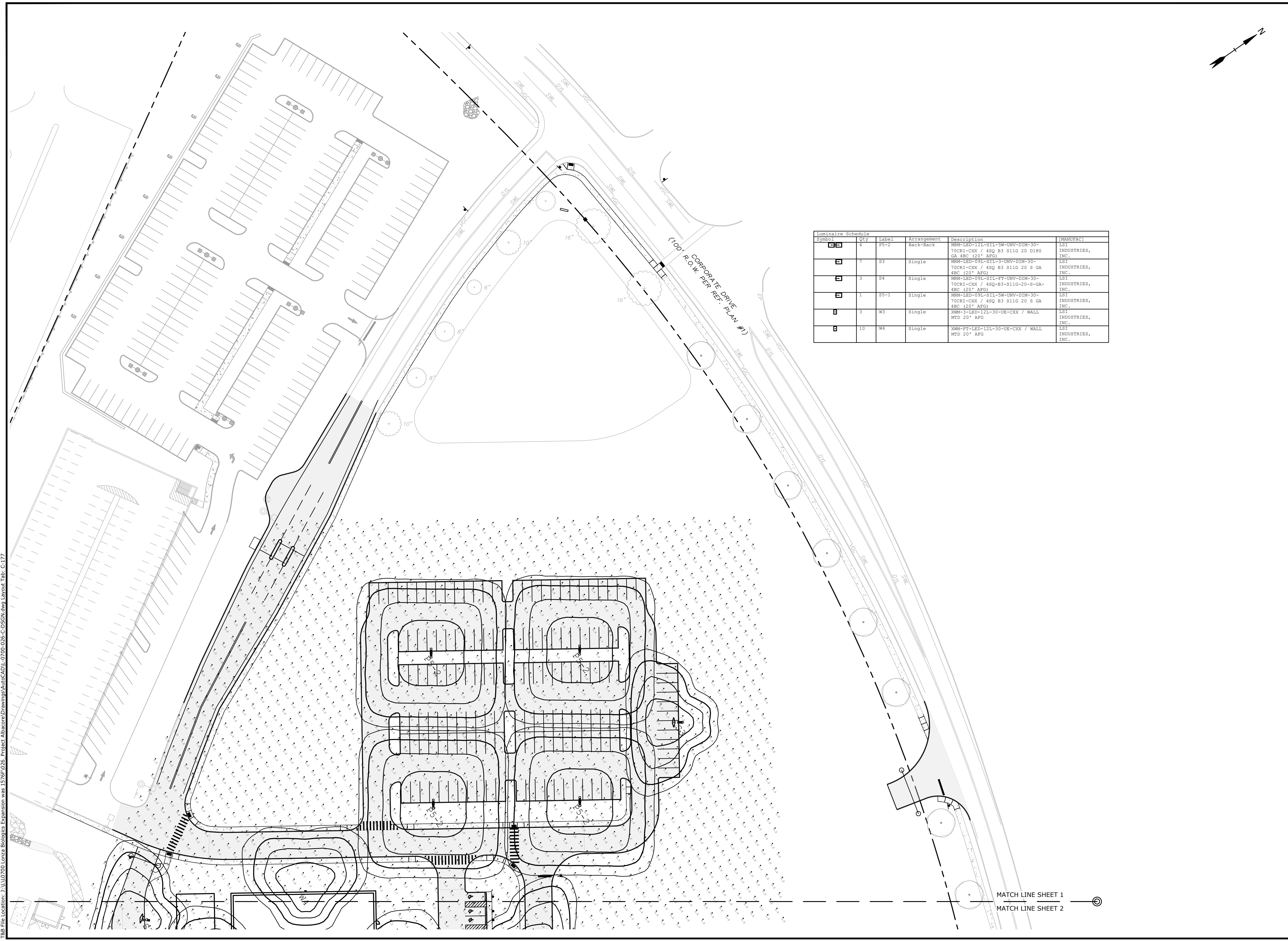
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 DATE: 04/03/2018
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PHASE 2 PHOTOMETRIC LIGHTING PLAN

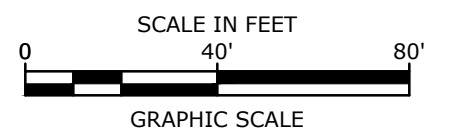
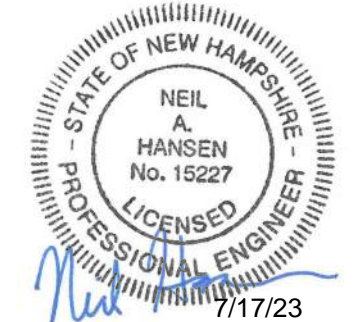
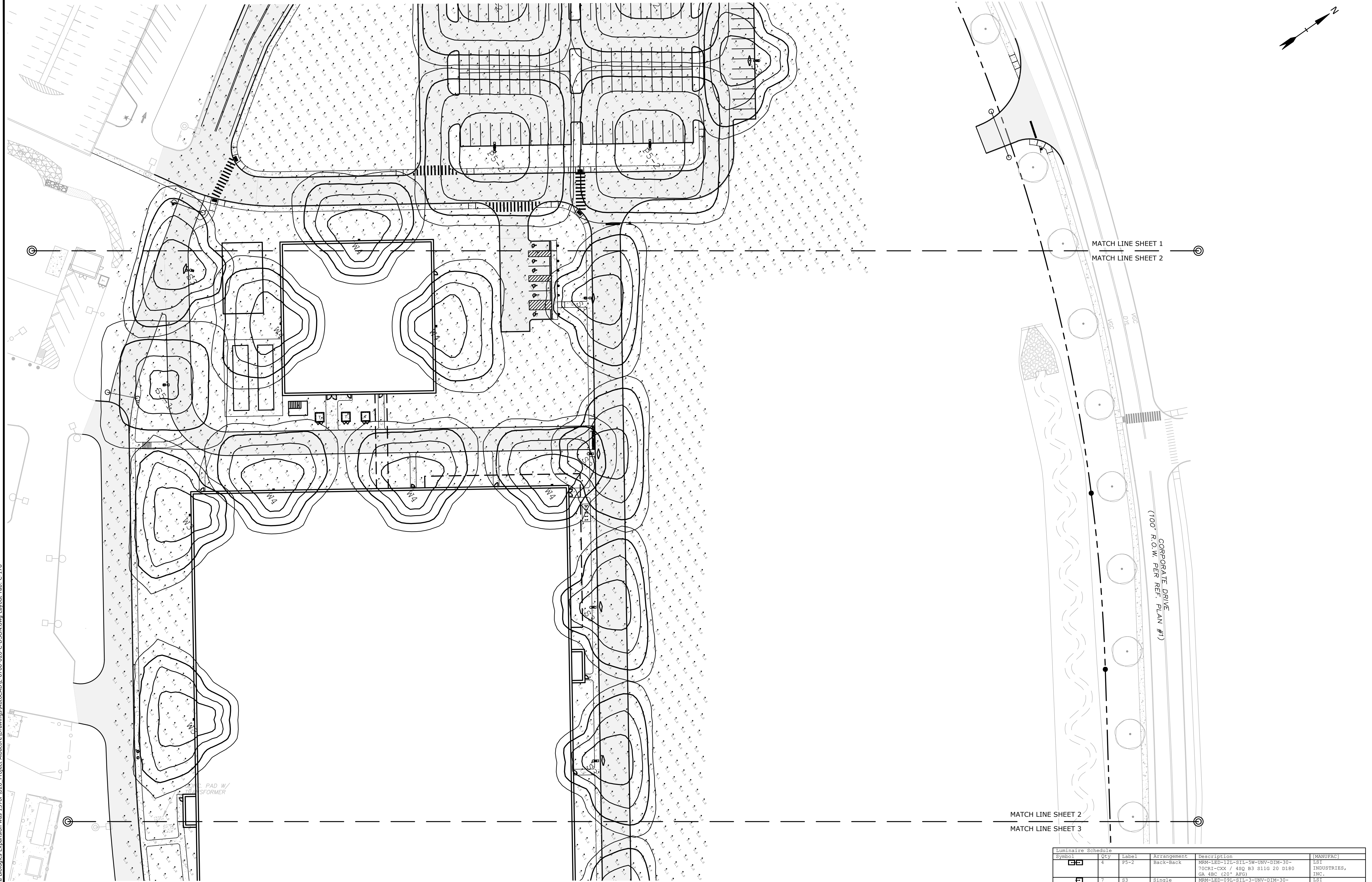
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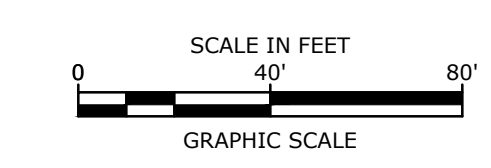
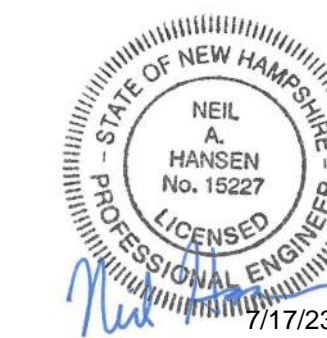
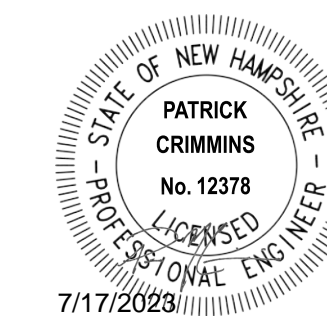
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DATE: 04/03/2018

FILE: L-0700-026-C-DSGN.dwg
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PHASE 2 PHOTOMETRIC LIGHTING PLAN

SCALE: AS SHOWN

Symbol	Qty	Label	Arrangement	Description	MANUFAC
[Symbol]	4	P3-2	Back-Back	MRM-LED-12L-81L-5W-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 D180 GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	7	S3	Single	MRM-LED-12L-81L-3-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	3	S4	Single	MRM-LED-12L-81L-5W-UNV-DIM-30-70CRI-CXX / 48Q-B3-S11G-20-S-GA-4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	1	S5-1	Single	MRM-LED-12L-81L-5W-UNV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	3	W3	Single	XWM-3-LED-12L-30-UB-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
[Symbol]	10	W4	Single	XWM-FT-LED-12L-30-UB-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.



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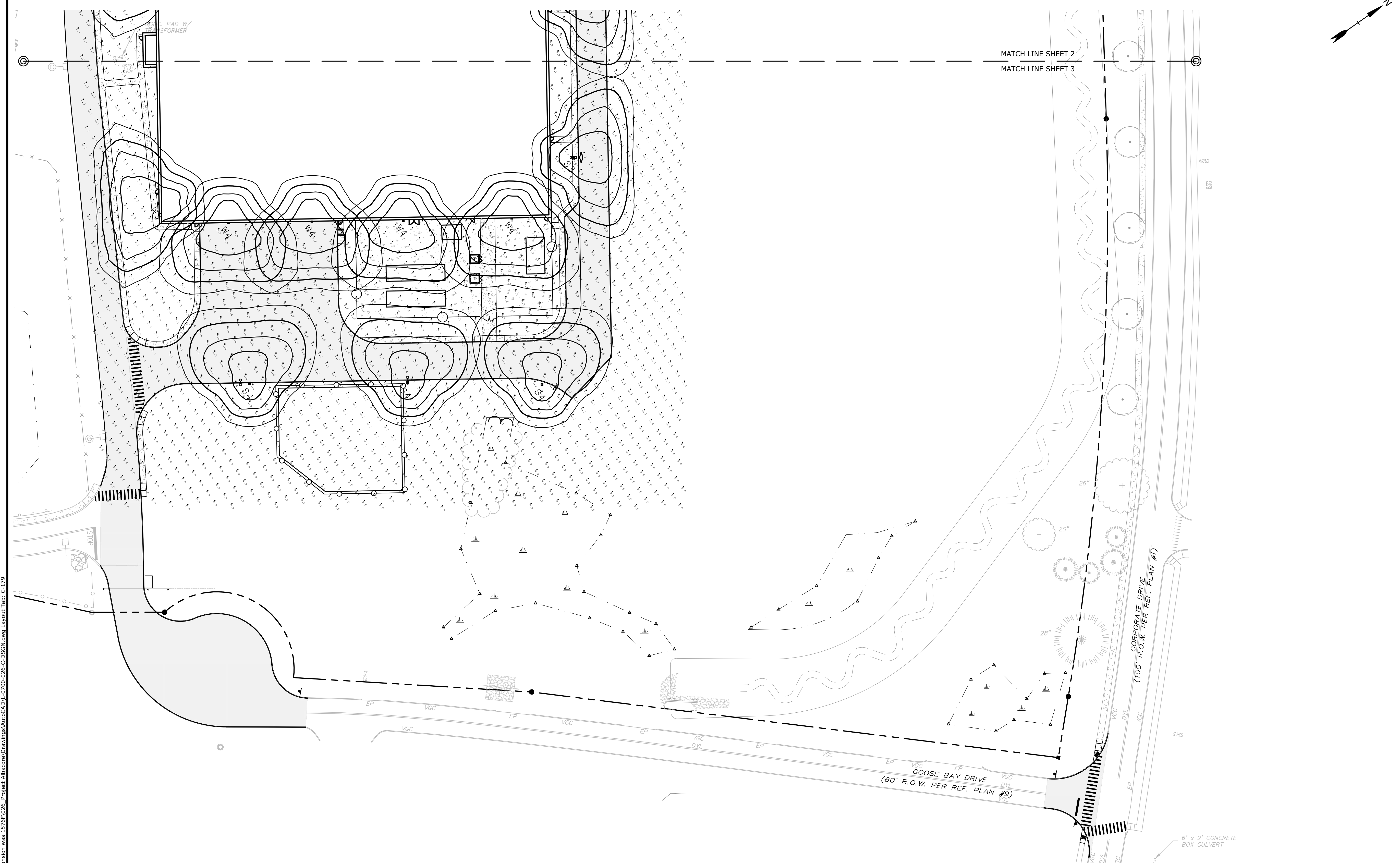
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PHASE 2 PHOTOMETRIC LIGHTING PLAN

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Symbol	Qty	Label	Arrangement	Description	MANUFACT
[Symbol]	4	P3-2	Back-Back	MM-LED-12L-81L-5W-UV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 D180 GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	7	S3	Single	MM-LED-12L-81L-3-UV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	3	S4	Single	MM-LED-12L-81L-5W-UV-DIM-30-70CRI-CXX / 48Q B3 S11G-20-S-GA-4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	1	S5-1	Single	MM-LED-12L-81L-5W-UV-DIM-30-70CRI-CXX / 48Q B3 S11G 20 S GA 4BC (20' AFG)	LSI INDUSTRIES, INC.
[Symbol]	3	W3	Single	XMM-3-LED-12L-30-UB-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.
[Symbol]	10	W4	Single	XMM-PT-LED-12L-30-UB-CXX / WALL MTD 20' AFG	LSI INDUSTRIES, INC.

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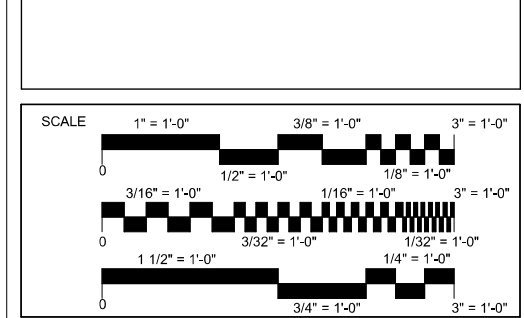
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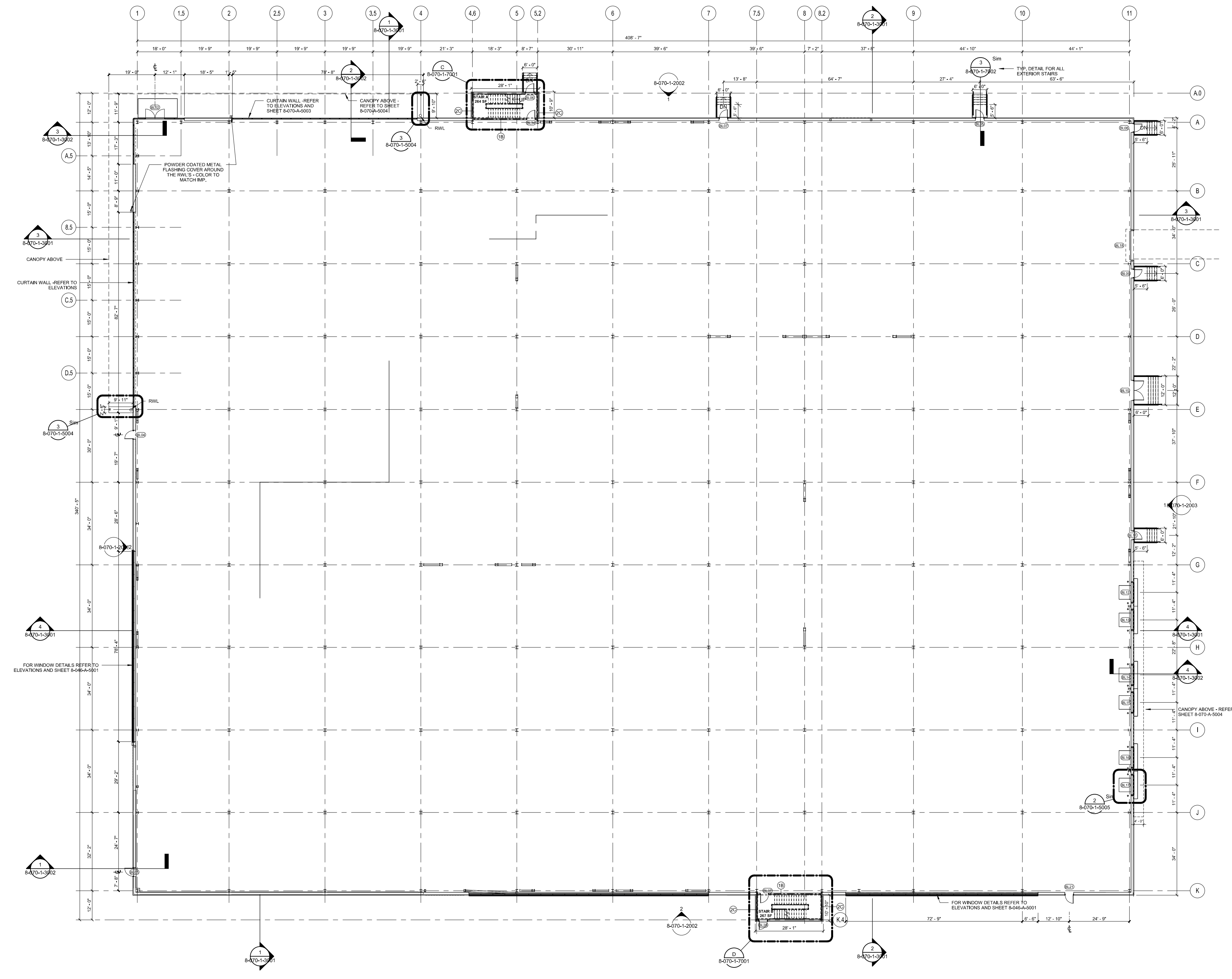
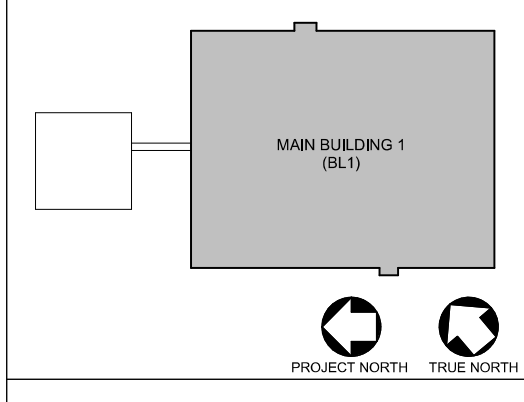
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LONZA ALBACORE PROJECT



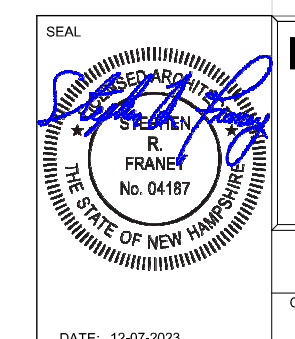
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PREP FILES:	ENGINEER
	ARCHITECT
	DESIGNER



A GROUND FLOOR PLAN - BL1
 8-070-1-1110 1/16" = 1'-0"

ISSUED FOR CONSTRUCTION



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 Lonza Biologics, Inc.
 107 International Ave.
 Portsmouth, NH 03801
 P: (603) 234-6100
 www.lonza.com

DRAWING TITLE
GROUND FLOOR PLAN - BL1

Drawn By	Date Drawn	Project Number	Phase Number	DWG Filename	Revision
AD		MAD23047.01			
Checked By	Date Checked	Scale	Drawing Number		
JMJ		1/16" = 1'-0"	8-070-1-1110		0

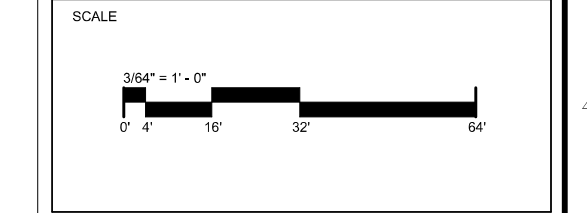
DATE: 12-07-2023

NOTE: FOR THE ELEVATION'S DESCRIPTION REFER TO NEXT TWO SHEETS - 8-070-A-2002 AND 8-070-A-2003

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 FAX: (781) 848-5508
 IPS Professional Engineers and Architects, P.C.

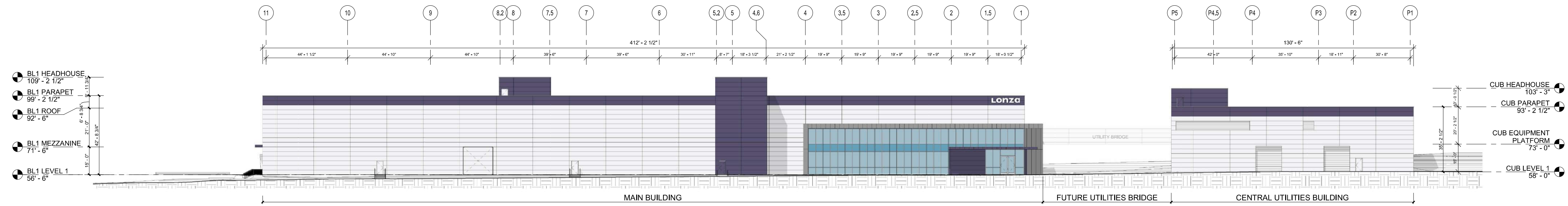
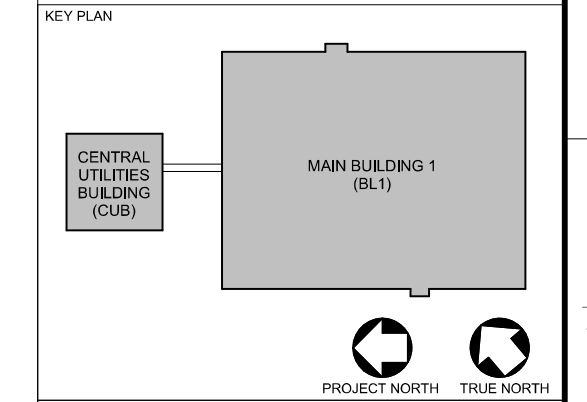
REVISION	DATE	DESCRIPTION	BY
A	12-MAR-23	DESIGN SUBMITTAL ISSUE (30% DD)	SPS
B	12-MAR-23	ISSUE (50% DD)	SPS
C	12-MAR-23	PERMIT ISSUE	SPS
D	12-JUL-23	CONSTRUCTION ISSUE	SPS

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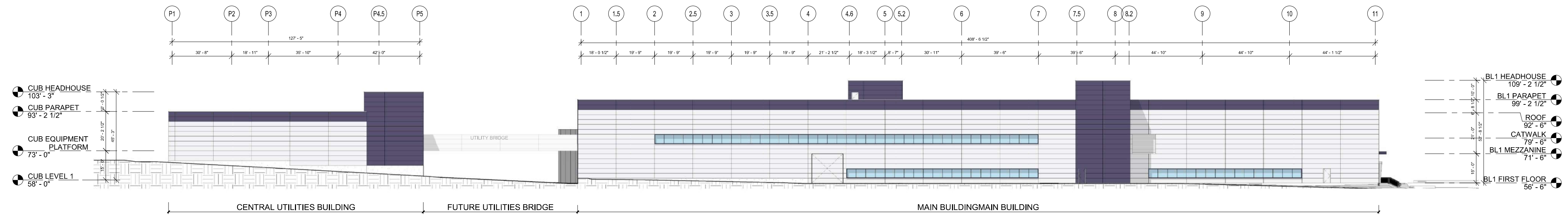


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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER



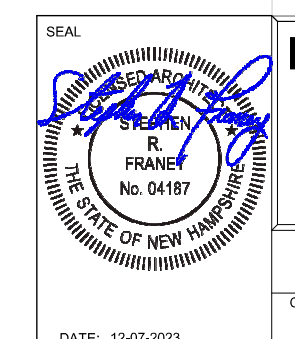
1 EAST BUILDINGS ELEVATIONS
 8-070-1-2001 3/8" = 1'-0"



2 WEST BUILDINGS ELEVATIONS
 8-070-1-2001 3/8" = 1'-0"

Reserved for Master Stamp Block

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DRAWING TITLE				
OVERALL BUILDINGS ELEVATIONS				
Drawn By	Date Drawn	Project Number	PS&D Number	DWG Filename
AD		MAD23047.01		
Checked By	Date Checked	Scale	Revision	
JMJ		3/8" = 1'-0"	0	
DATE: 12-07-2023		Drawing Number: 8-070-1-2001		

BUILDING THERMAL ENVELOPE NOTES

- CONTRACTOR TO ENSURE THAT THE BUILDING THERMAL ENVELOPE PERFORMANCE IS ENHANCED AND FULLY MAINTAINED AT ALL LOCATIONS ALL AROUND THE BUILDING ENVELOPE, INCLUDING BUT NOT LIMITED TO PROVIDING A CONTINUOUS AIR SEALING / BARRIERS ALL AROUND THE BUILDING ENVELOPE, THERMAL BREAKS AND AVOIDING ANY THERMAL BRIDGES.
- MAXIMUM AIR LEAKAGE MUST BE ≤ 0.40 CFM/F² WHEN TESTED AT A PRESSURE DIFFERENTIAL OF 0.3 INCH WATER GAUGE (75 PA)
- ALL EXTERIOR DOORS TO HAVE WEATHERSEALS

LEGEND

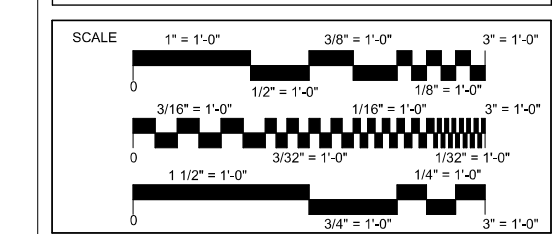
- IMP1 :**
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT
- IMP2 :**
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT
- CW :**
THERMALLY BROKEN CURTAIN WALL SYSTEM EQUAL TO 1600 WALL SYSTEM
1 BY KAWNEER OR APPROVED EQUAL (HURRICANE IMPACT RESISTANT).
- GL1 :**
1" THICK IMPACT RESISTANT INSULATED LAMINATED GLASS. OB: 1/2" BLUE SOLARBAN 70 XL SURFACE 1/2 INCH (1 W/90% ARGON FILL) INTERLAYER 1/4" CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL. PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT SAMPLES FOR ARCHITECT APPROVAL. U VALUE:0.25
- GL2 :**
1" THICK IMPACT RESISTANT INSULATED (INSULATION & BACKPAN ARE REQUIRED) LAMINATED SPANDREL GLASS 3-1670 OB: 1/2" SOLAR GREY + 1/2 INCH (1 W/90% ARGON FILL) INTERLAYER INTERLAYER 1/4" CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL. PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT SAMPLES FOR ARCHITECT APPROVAL. U VALUE:0.25
- MF:** POWDER COATED METAL FLASHING COVER AROUND THE RWLS - COLOR TO MATCH IMP.
- ROOF:** WHITE EPDM ROOF SYSTEM - R VALUE OF 44



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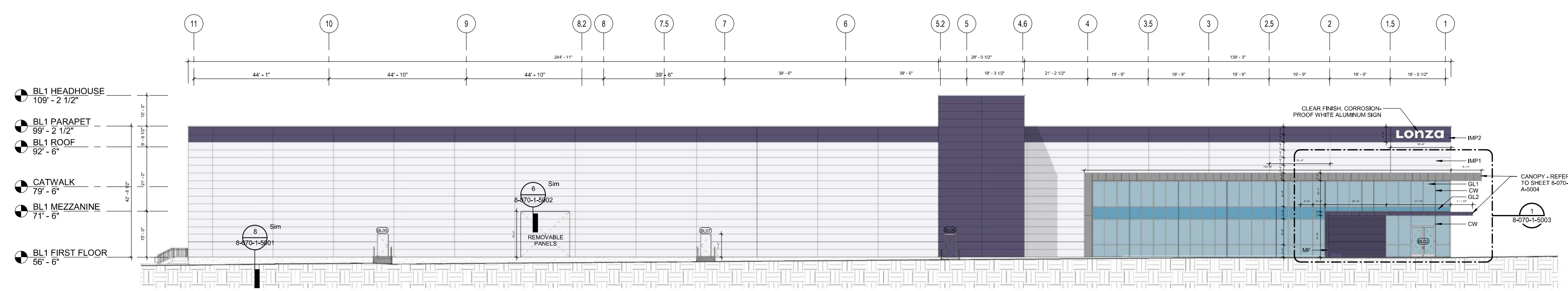
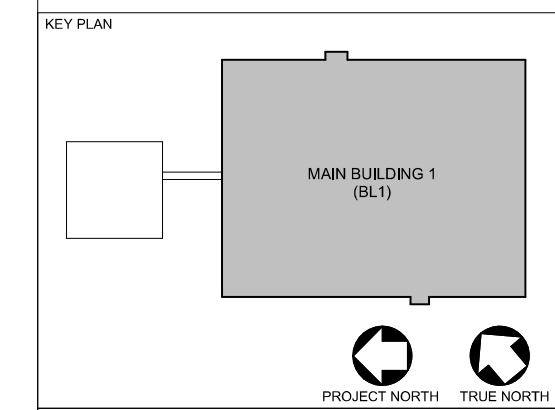
REVISION	DATE	DESCRIPTION	BY
A	12-MAR-23	ISSUE SUBMIT FOR ISSUE (30% DD)	SHS
B	12-MAR-23	ISSUE (50% DD)	SHS
C	12-MAR-23	ISSUE (60% DD)	SHS
D	12-MAR-23	ISSUE (70% DD)	SHS
E	12-MAR-23	ISSUE (80% DD)	SHS
F	12-MAR-23	ISSUE (90% DD)	SHS
G	12-MAR-23	ISSUE (100% DD)	SHS

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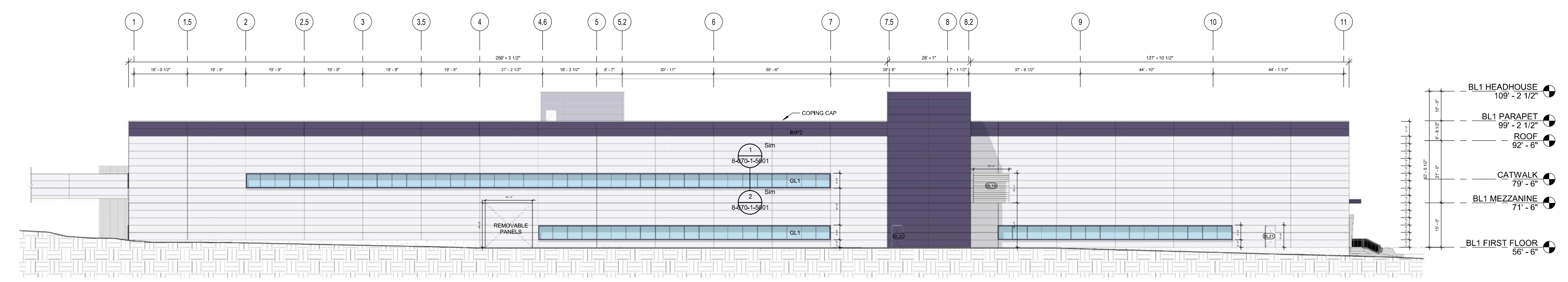


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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER

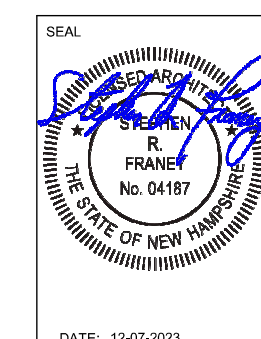


1 EAST ELEVATION - BL1
8-070-1-2002 1/16" = 1'-0"



2 WEST ELEVATION - BL1
8-070-1-2002 1/16" = 1'-0"

- BL1 HEADHOUSE 109' - 2 1/2"
- BL1 PARAPET 99' - 2 1/2"
- ROOF 92' - 6"
- CATWALK 79' - 6"
- BL1 MEZZANINE 71' - 6"
- BL1 FIRST FLOOR 56' - 6"



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DRAWING TITLE
BUILDING ELEVATIONS - BL1

Drawn By AD	Date Drawn	Project Number MAD23047.01	P&ID Number	DWG Filename	Revision 0
Checked By JMJ	Date Checked	Scale As indicated	Drawing Number 8-070-1-2002		

DATE: 12-07-2023

ISSUED FOR CONSTRUCTION

LEGEND

IMP1 :
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT

IMP2 :
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT

CW :
THERMALLY BROKEN CURTAIN WALL SYSTEM EQUAL TO 1600 WALL SYSTEM
1 BY KAWNEER OR APPROVED EQUAL (HURRICANE IMPACT RESISTANT).

GL1 :
1" THICK IMPACT RESISTANT INSULATED LAMINATED GLASS. OB. 1/4" BLUE SOLARBAN 70 XL SURFACE 1/2 INCH 1 W90% ARGON FILL INTERLAYER. 11/4" CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL. PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT SAMPLES FOR ARCHITECT APPROVAL. U VALUE: 0.25

GL2 :
1" THICK IMPACT RESISTANT INSULATED (INSULATION & BACKPAN ARE REQUIRED) LAMINATED SPANDREL GLASS 3-1870 OB. 1/4" SOLAR GREY + 1/2 INCH (W90% ARGON FILL) INTERLAYER INTERLAYER. 1/4" CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL. PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT SAMPLES FOR ARCHITECT APPROVAL.

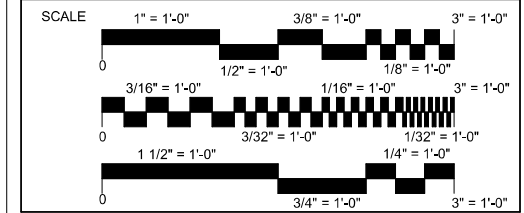
MF: POWDER COATED METAL FLASHING COVER AROUND THE RWL'S - COLOR TO MATCH IMP.

ROOF: WHITE EPDM ROOF SYSTEM - R VALUE OF 44

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REVISION	DATE	DESCRIPTION	BY
A	12-MAR-23	ISSUE SUBMIT FOR ISSUE (30% DD)	AD
B	12-MAR-23	ISSUE (50% DD)	AD
C	12-MAR-23	ISSUE (60% DD)	AD
D	12-JUL-23	ISSUE (70% DD)	AD
E	12-JUL-23	ISSUE (80% DD)	AD
F	12-JUL-23	ISSUE (90% DD)	AD
G	12-JUL-23	ISSUE (100% DD)	AD

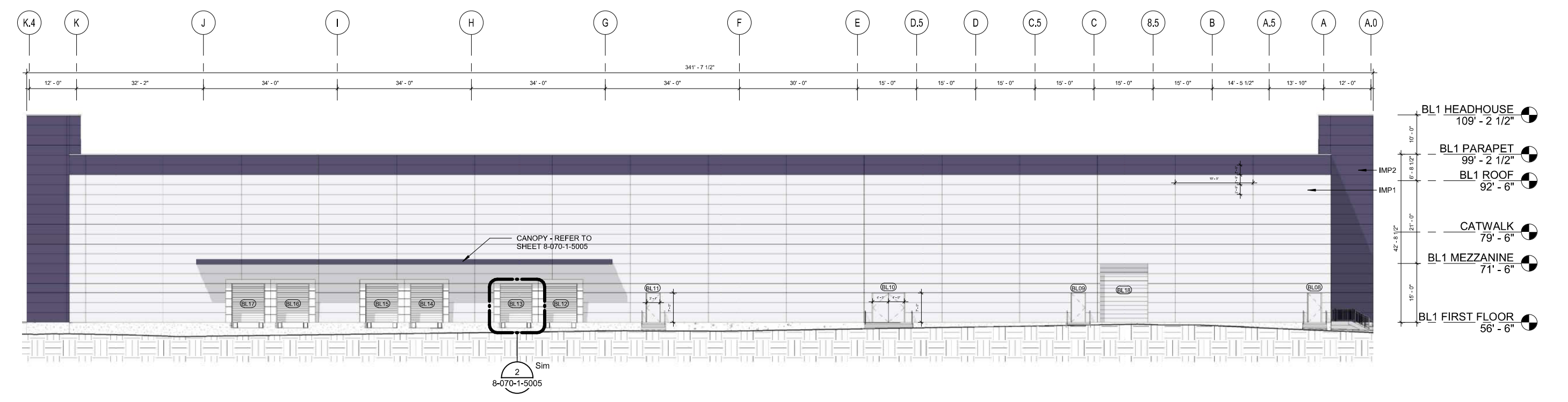
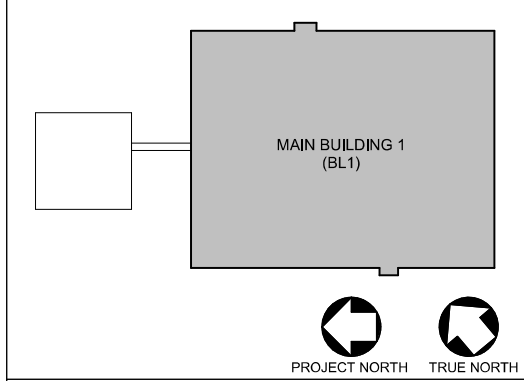
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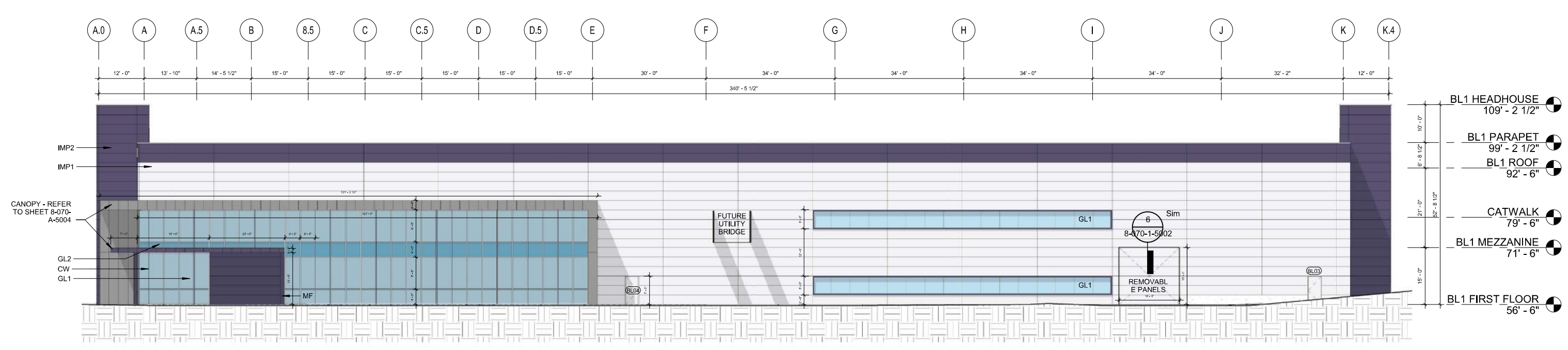
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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER



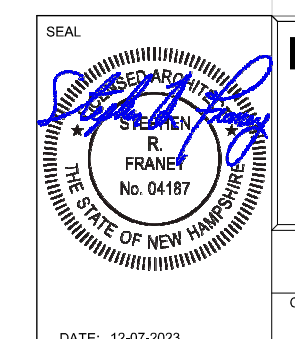
1 SOUTH ELEVATION - BL1
8470-1-2003 1/16" = 1'-0"



2 NORTH ELEVATION - BL1
8470-1-2003 1/16" = 1'-0"

Reserved for Master Stamp Block

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www.lonza.com

DRAWING TITLE
BUILDING ELEVATIONS - BL1

Drawn By	Date Drawn	Project Number	P&ID Number	DWG Filename	Revision
AD		MAD23047.01			0
Checked By	Date Checked	Scale	Drawing Number		
JMJ		As indicated	8-070-1-2003		



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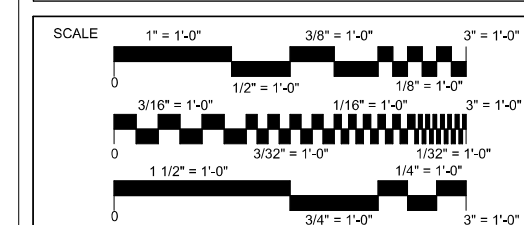
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 Burlington, MA 01903
 PHONE: (803) 570-3650
 FAX: (781) 848-5508

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REVISION	DATE	DESCRIPTION	BY
A	12-07-23	DESIGN SUBMITTAL PER ISSUE 001 (50)	SPS
B	12-08-23	CUB RED ISSUE (70% 50)	SPS
C	12-08-23	PLUMB ISSUE	SPS
D	12-20-23	CONSTRUCTION ISSUE	SPS

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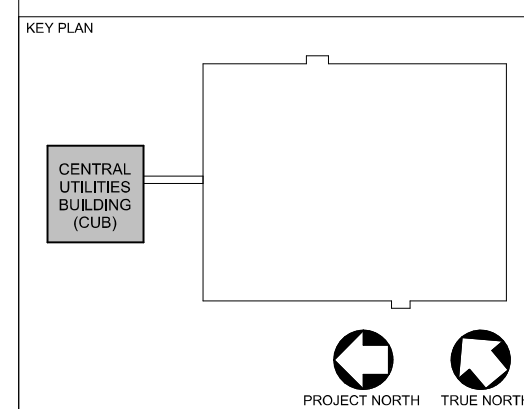
LONZA ALBACORE PROJECT



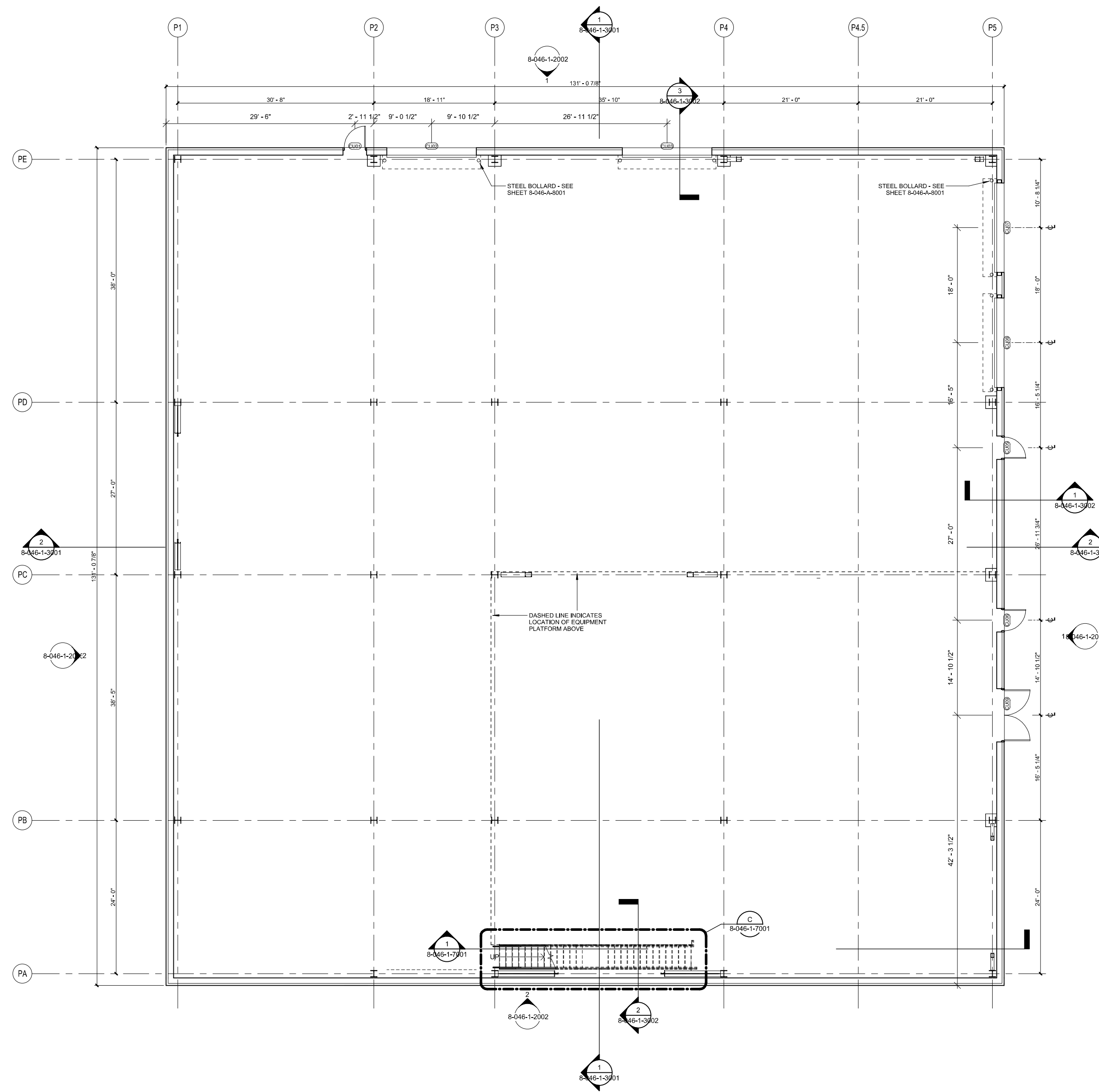
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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER



NOTE: APPLY SPRAY-ON CEMENTitious FIBERPROOFING TO ALL STRUCTURAL FRAMING ELEMENTS (COLUMNS, CROSS BRACINGS AND BEAMS).

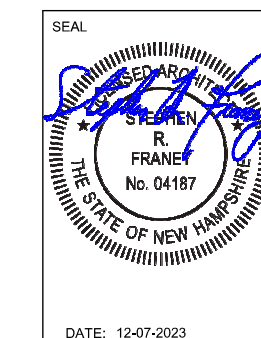


A GROUND FLOOR PLAN - CUB
 B-046-1-1110 1/8" = 1'-0"

7/12/2023 1:59:39 PM

Autodesk User: JZCUB_3987_Lonza_Albacore2305_ARCH_Lonza4

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Lonza Biologics, Inc. 101 International Ave Trenton, NJ, USA T: (609) 395-6100 F: (609) 395-6222 www.lonza.com		GROUND FLOOR PLAN - CUB	
Drawn By AD	Date Drawn MAD23047.01	Project Number MAD23047.01	Revision 0
Checked By JMJ	Date Checked	Scale 1/8" = 1'-0"	DWG Filename 8-046-1-1110

Reserved
for
Master
Stamp
Block

LEGEND

IMP1 :
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT - EMBOSSED EXTERIOR
FINISH OF 22-GAUGE G-90 GALVANIZED STEEL WITH PVDF AND SMP ZINC
EXTERIOR COATINGS

IMP2 :
4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
COLOR: MATT PURPLE, R153 G148 B176, 15% TINT - EMBOSSED EXTERIOR
FINISH OF 22-GAUGE G-90 GALVANIZED STEEL WITH PVDF AND SMP ZINC
EXTERIOR COATINGS

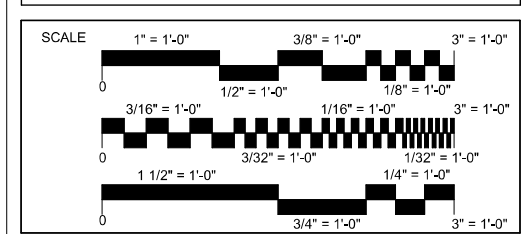
LV :
- 4" STORM-RESISTANT LOUVER W/ 52% FREE AREA - SEE SHEET 8-046-A-5002

GL1 :
1" THICK IMPACT RESISTANT INSULATED LAMINATED GLASS OB: X' BLUE
SOLARBAN 60 #2 SURFACE 1/2 INCH (W/90% ARGON FILL) INTERLAYER 1/4"
CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL .
PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT
SAMPLES FOR ARCHITECT APPROVAL. U VALUE:0.25

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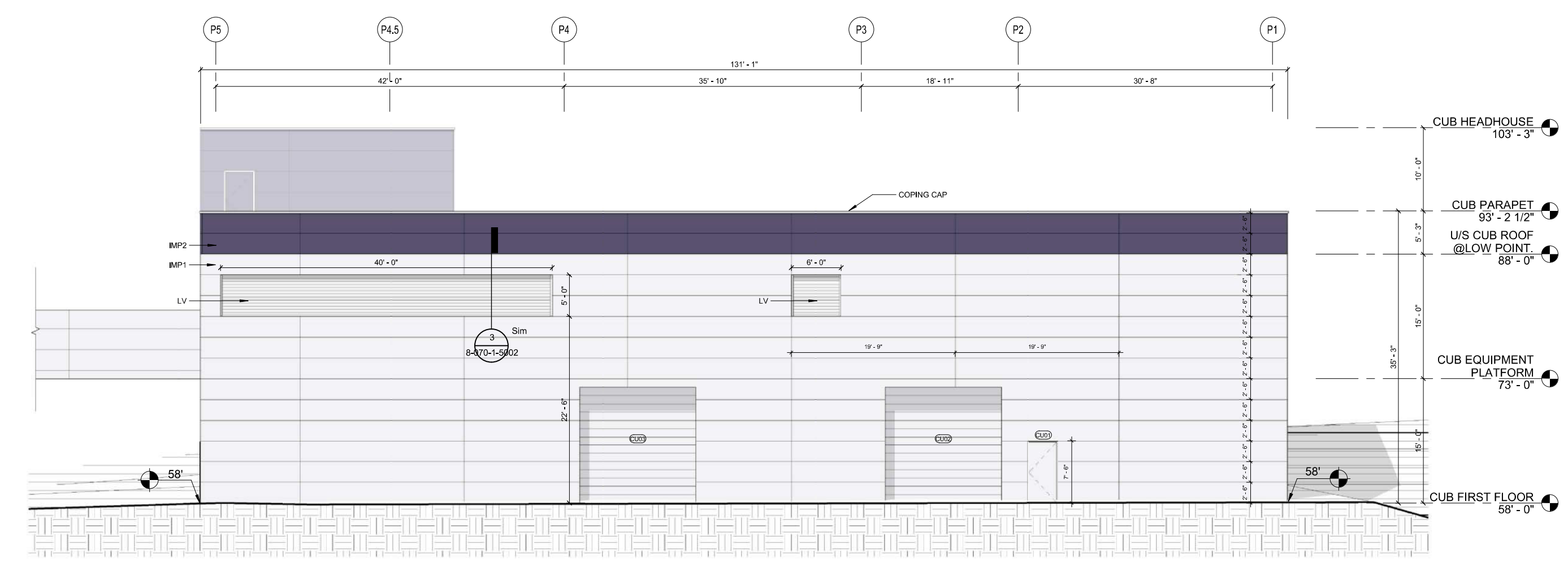
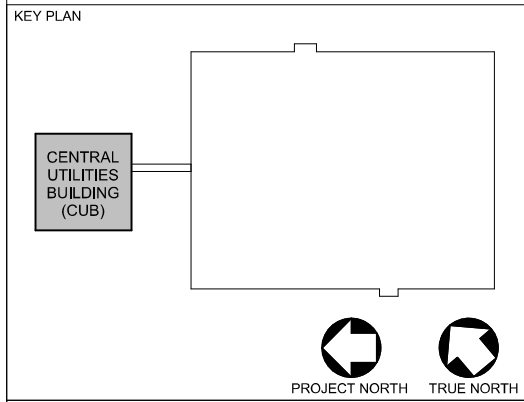
REVISION	DATE	DESCRIPTION	BY
A	12-07-2023	DESIGN SUBMITTAL ISSUE (30% DD)	SPS
B	12-08-23	CUB EED ISSUE (30% DD)	SPS
C	12-08-23	PLUMB ISSUE	SPS
D	12-21-23	CONSTRUCTION ISSUE	SPS

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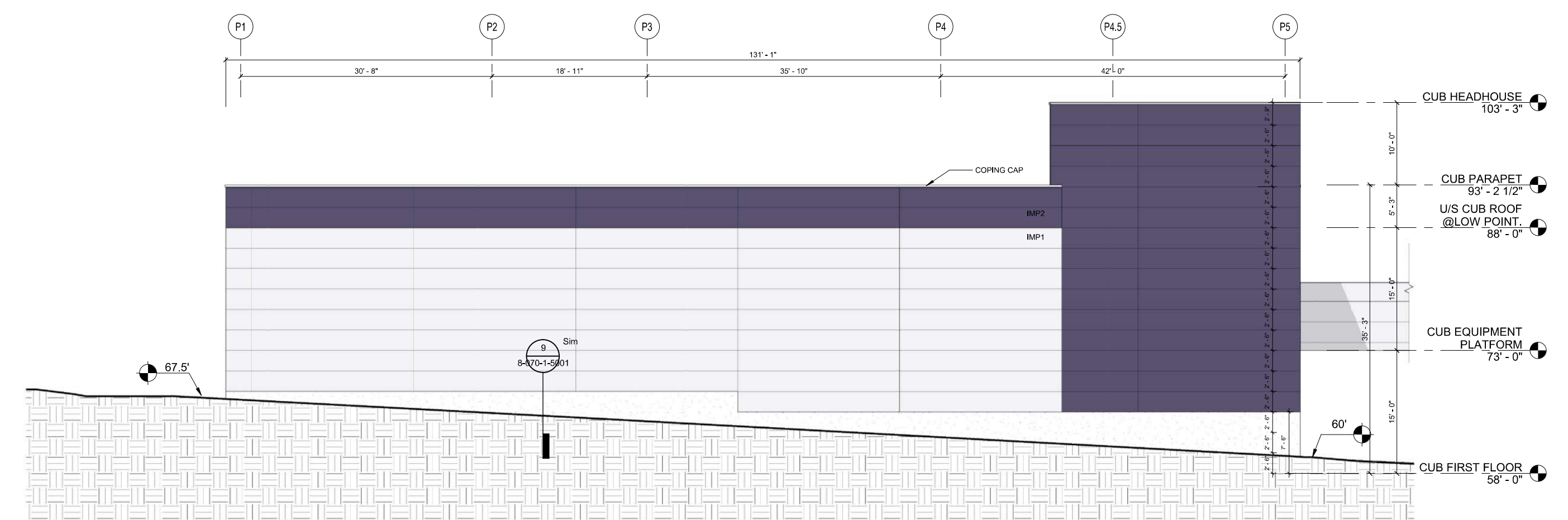


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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER

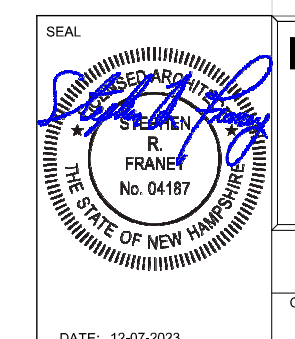


1 EAST ELEVATION - CUB.
8-046-1-2002 1/8" = 1'-0"



2 WEST ELEVATION - CUB.
8-046-1-2002 1/8" = 1'-0"

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DRAWING TITLE
BUILDING ELEVATIONS - CUB

Drawn By	Date Drawn	Project Number	P&ID Number	DWG Filename	Revision
AD		MAD23047.01			0
Checked By	Date Checked	Scale	Drawing Number		
JMJ		As indicated	8-046-1-2002		

LEGEND

IMP1 :
 4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
 COLOR: MATT PURPLE, R153 G148 B176, 15% TINT - EMBOSSED EXTERIOR FINISH OF 22-GAUGE G-90 GALVANIZED STEEL WITH PVDF AND SMP ZINC EXTERIOR COATINGS

IMP2 :
 4" THICK INSULATED METAL PANELS TO HAVE MIN. R VALUE OF 33.5
 COLOR: MATT PURPLE, R153 G148 B176, 15% TINT - EMBOSSED EXTERIOR FINISH OF 22-GAUGE G-90 GALVANIZED STEEL WITH PVDF AND SMP ZINC EXTERIOR COATINGS

LV :
 - 4" STORM-RESISTANT LOUVER W/ 52% FREE AREA - SEE SHEET 8-046-A-5002

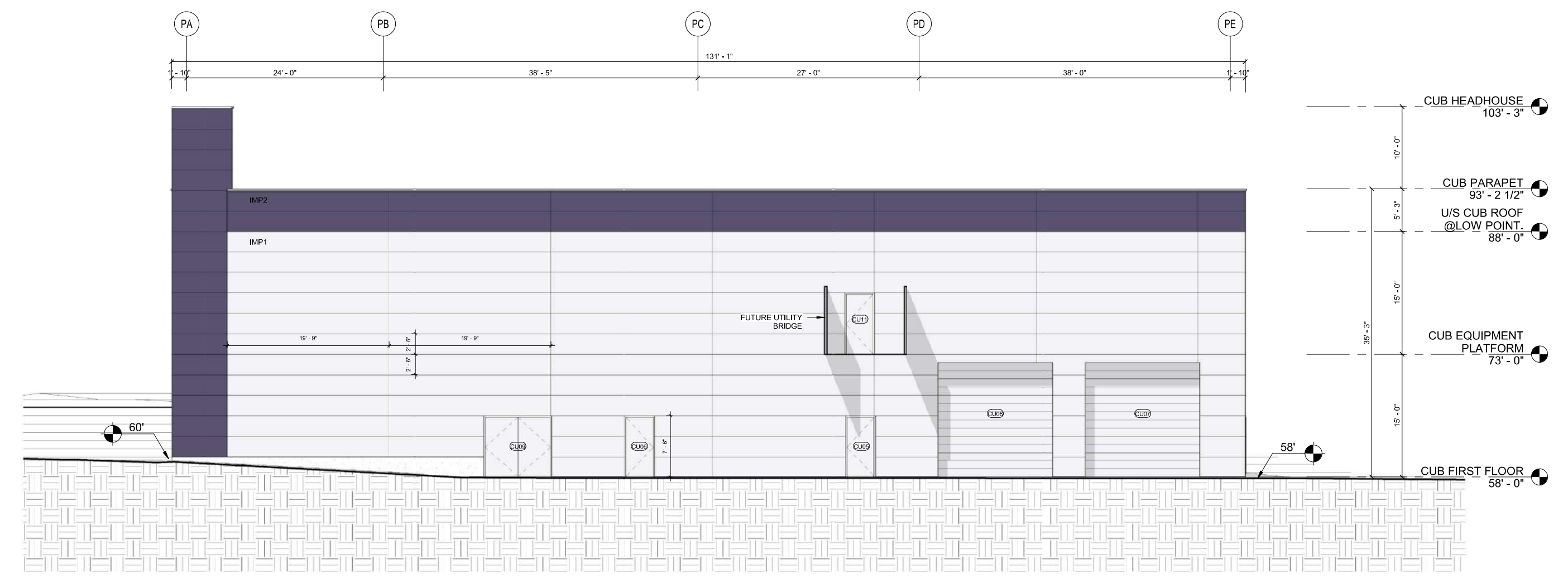
GL1 :
 1" THICK IMPACT RESISTANT INSULATED LAMINATED GLASS OB: X' BLUE SOLARBAN 60 #2 SURFACE 1/2 INCH (W/90% ARGON FILL) INTERLAYER 1/4" CLEAR AS MANUFACTURED BY VITRO AMERICA OR APPROVED EQUAL . PRIOR FABRICATION AND INSTALLATION THE CONTRACTOR SHALL SUBMIT SAMPLES FOR ARCHITECT APPROVAL. U VALUE:0.25

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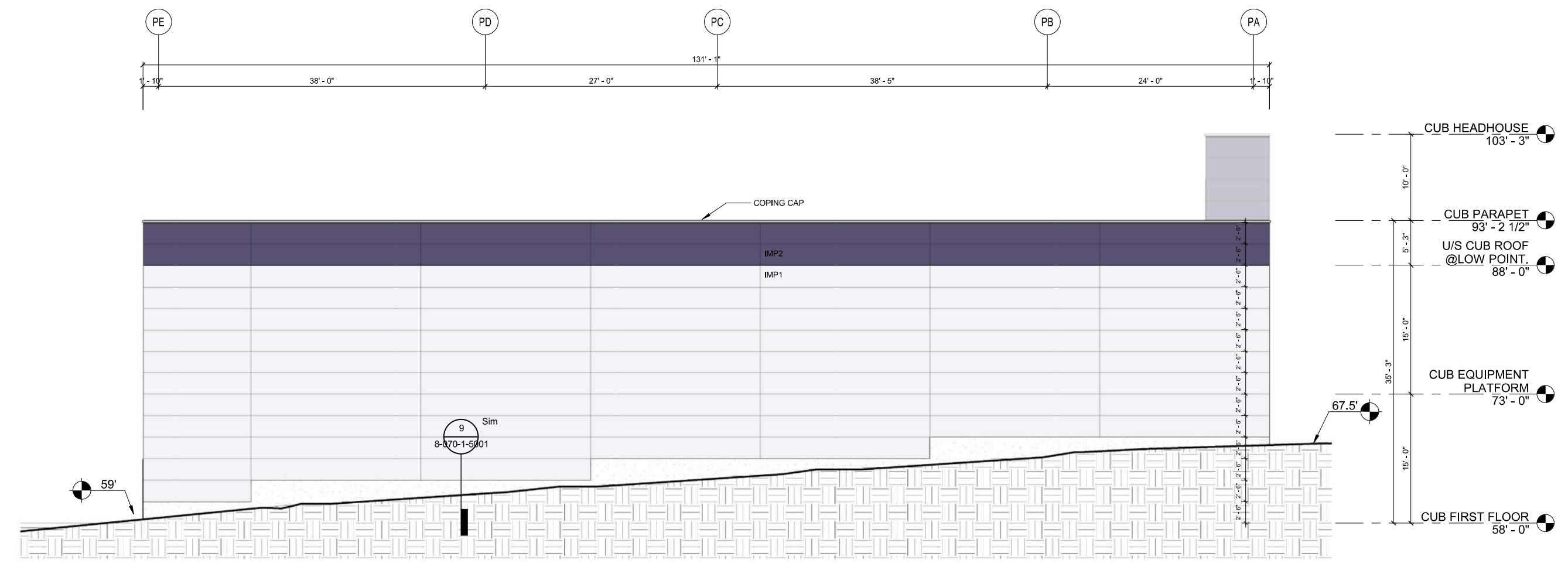
30 Corporate Drive, Suite 130
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REVISION	DATE	DESCRIPTION	BY
A	12-MAR-23	DESIGN BUILD PER ISSUE 20/150	SHS
B	16-JAN-23	CUB EED ISSUE (20/150)	SHS
C	20-NOV-22	POWER ISSUE	SHS
D	10-JULY-22	ASSEMBLY NO. 2	SHS
E	12-AUG-22	CONSTRUCTION ISSUE	SHS



1 SOUTH ELEVATION - CUB
 8-046-1-2003 1/8" = 1'-0"



2 NORTH ELEVATION - CUB
 8-046-1-2003 1/8" = 1'-0"

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SCALE: 1" = 10' 3/8" = 1'-0" 1/2" = 1'-0" 1/4" = 1'-0" 1/8" = 1'-0" 1/16" = 1'-0" 1/32" = 1'-0" 1/64" = 1'-0"

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REF FILES	ENGINEER
	ARCHITECT
	DESIGNER

PARE

KEY PLAN

PROJECT NORTH TRUE NORTH

Reserved for Master Stamp Block

ISSUED FOR CONSTRUCTION

LONZA
 Lonza Biologics, Inc.
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 www.lonza.com

DRAWING TITLE
BUILDING ELEVATIONS - CUB

Drawn By	Date Drawn	Project Number	P&ID Number	DWG Filename	Revision
AD		MAD23047.01			0
Checked By	Date Checked	Scale	Drawing Number		
JMU		As indicated	8-046-1-2003		

DATE: 12-07-2023

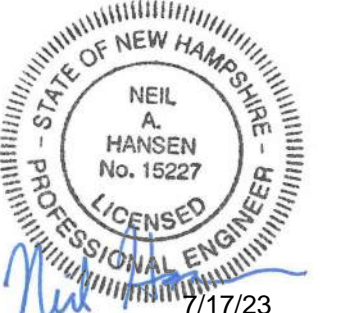
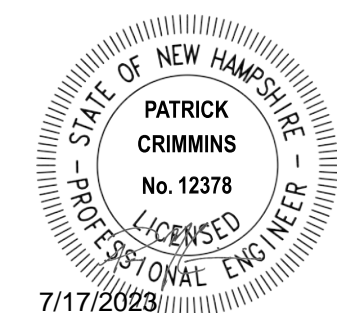
DETAILS PLAN SET

APRIL 3, 2018

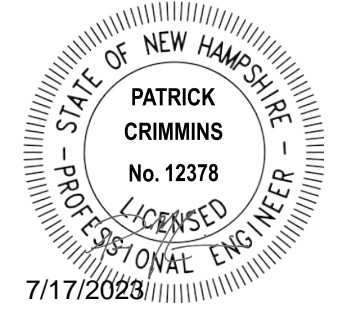
REVISED: JULY 17, 2023

LIST OF DRAWINGS		
SHEET NO.	SHEET TITLE	LAST REVISED
	DETAILS COVER SHEET	7/17/2023
C-501	EROSION CONTROL NOTES & DETAILS SHEET	7/17/2023
C-502	DETAILS SHEET	7/17/2023
C-503	DETAILS SHEET	7/17/2023
C-504	DETAILS SHEET	7/17/2023
C-505	DETAILS SHEET	7/17/2023
C-506	DETAILS SHEET	7/17/2023
C-507	DETAILS SHEET	7/17/2023
C-508	DETAILS SHEET	7/17/2023
C-509	DETAILS SHEET	7/17/2023
C-510	DETAILS SHEET	7/17/2023
C-511	DETAILS SHEET	7/17/2023
C-512	DETAILS SHEET	7/17/2023

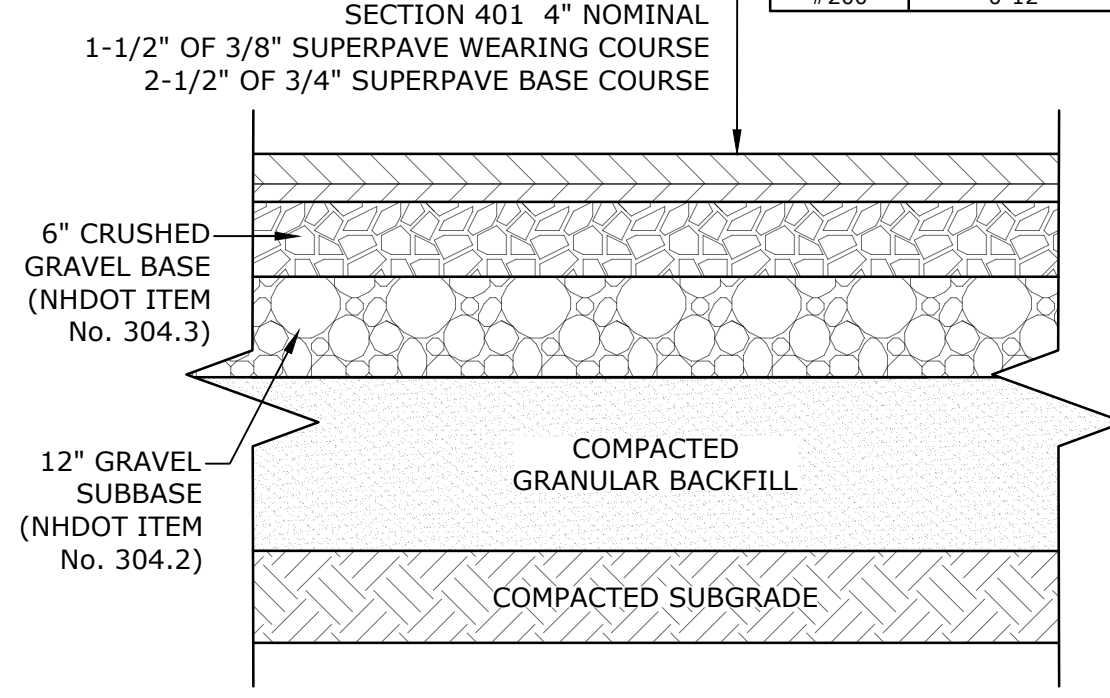
Last Save Date: July 12, 2023 4:31 PM By: CKRZCUIK
Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
P&E File Location: J:\U0700 Lenza Biologicals Expansion.was 1276P.026 - Project Abbrev: Drawings\AutoCAD\0700-026-C-COVR.dwg Layout Tab: DETAILS-CS



COMPLETE SET 13 SHEETS

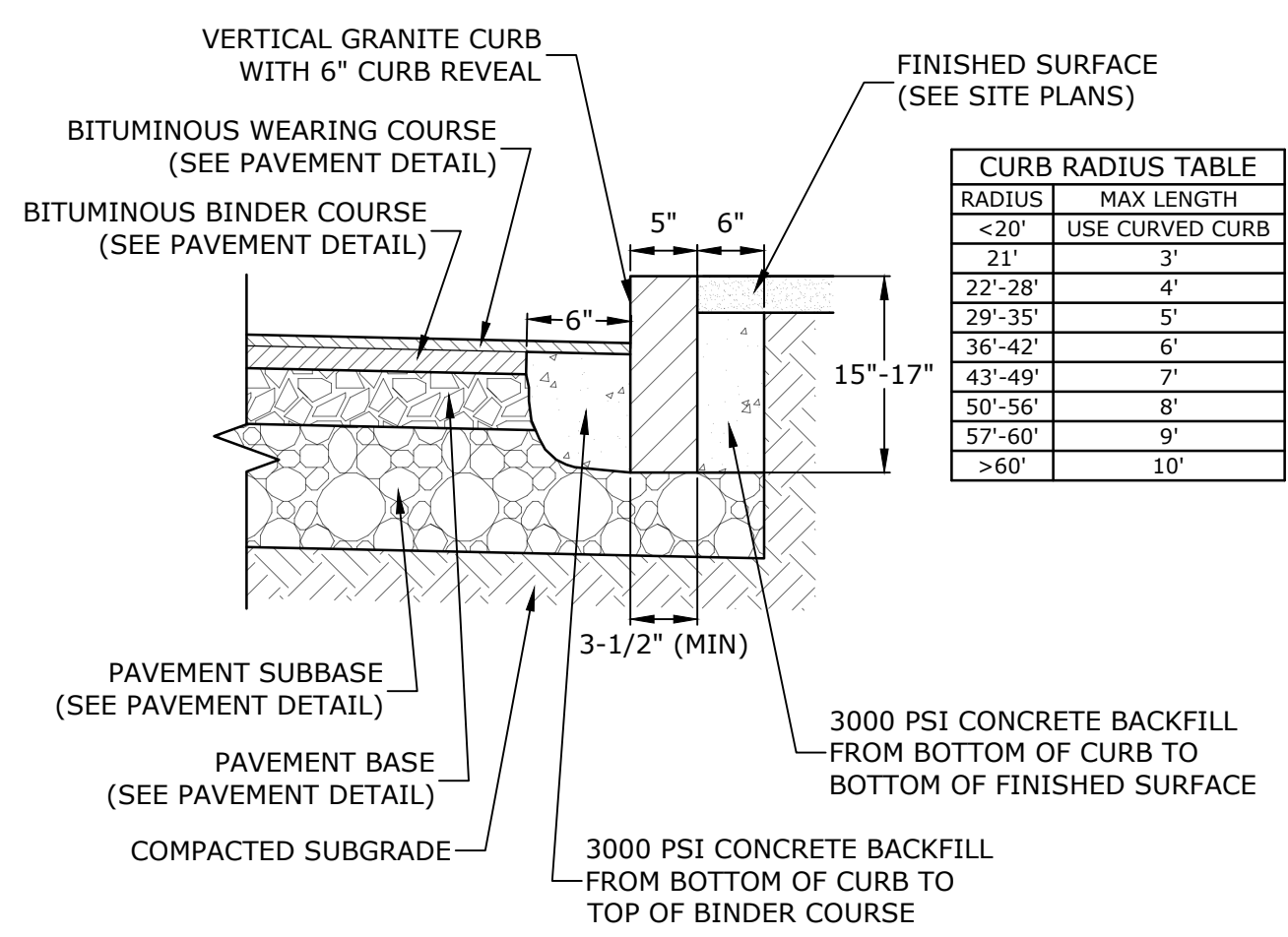


NHDOT ITEM No. 304.2 (GRAVEL)		NHDOT ITEM No. 304.3 (CRUSHED GRAVEL)	
SIEVE SIZE	% PASSING	SIEVE SIZE	% PASSING
6"	100	3"	100
#4	25-70	1"	95-100
#200	0-12	#4	55-85
		#200	27-52
			0-12



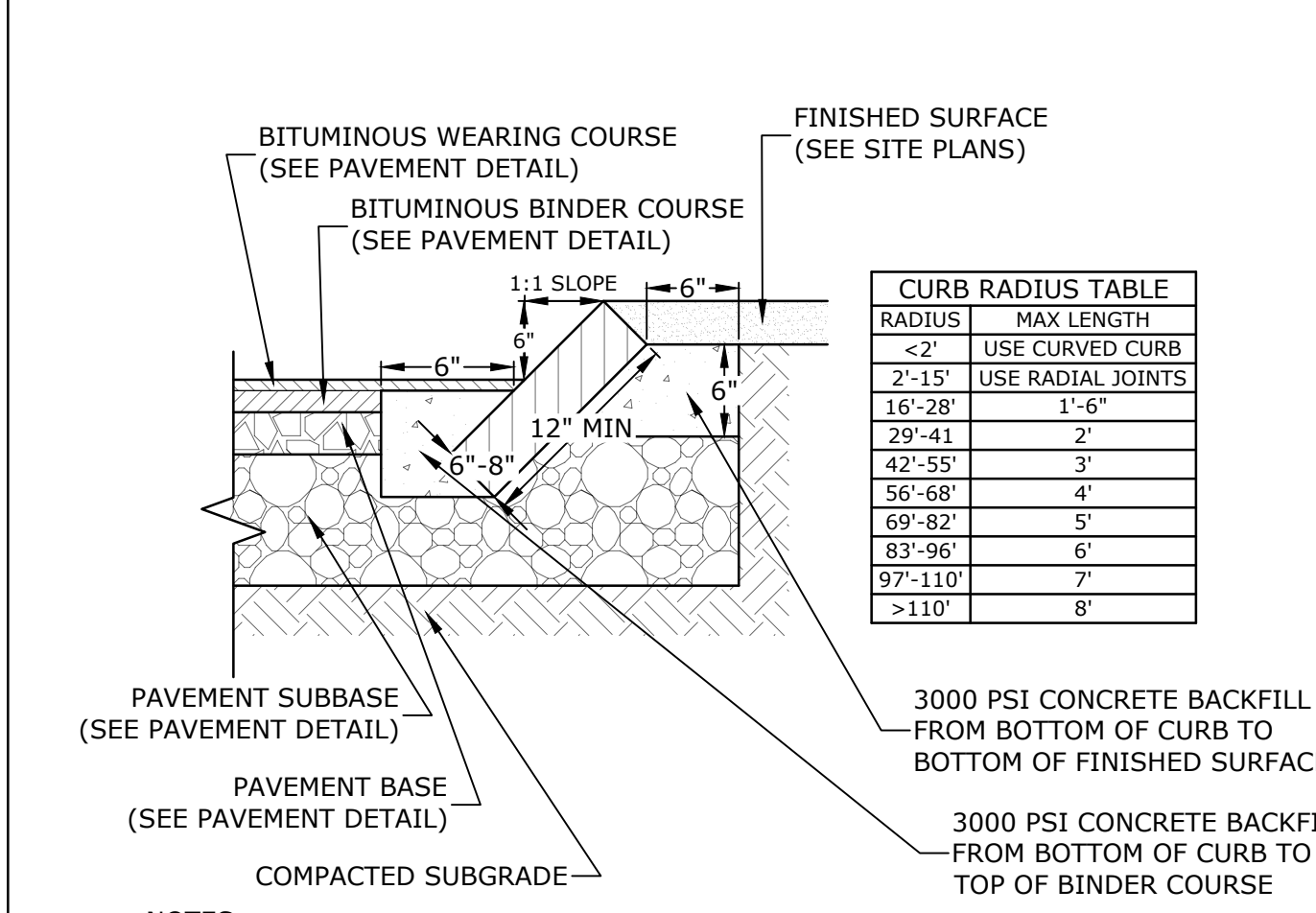
- NOTES:
- SEE SITE PLAN FOR PAVEMENT WIDTH AND LOCATION.
 - SEE GRADING, DRAINAGE AND EROSION CONTROL PLAN FOR PAVEMENT SLOPE AND CROSS-SLOPE.
 - A TACK COAT SHALL BE PLACED ON TOP OF BINDER COURSE PAVEMENT PRIOR TO PLACING WEARING COURSE.
 - FINAL PAVEMENT DESIGN TO BE DETERMINED BY GEOTECHNICAL ENGINEER.
 - NHDOT ITEM No. 304.2 MAY BE SUBSTITUTED FOR NHDOT ITEM No. 304.4, IF NHDOT ITEM No. 304.2 CAN NOT BE ACQUIRED.

TYPICAL PAVEMENT SECTION
NO SCALE



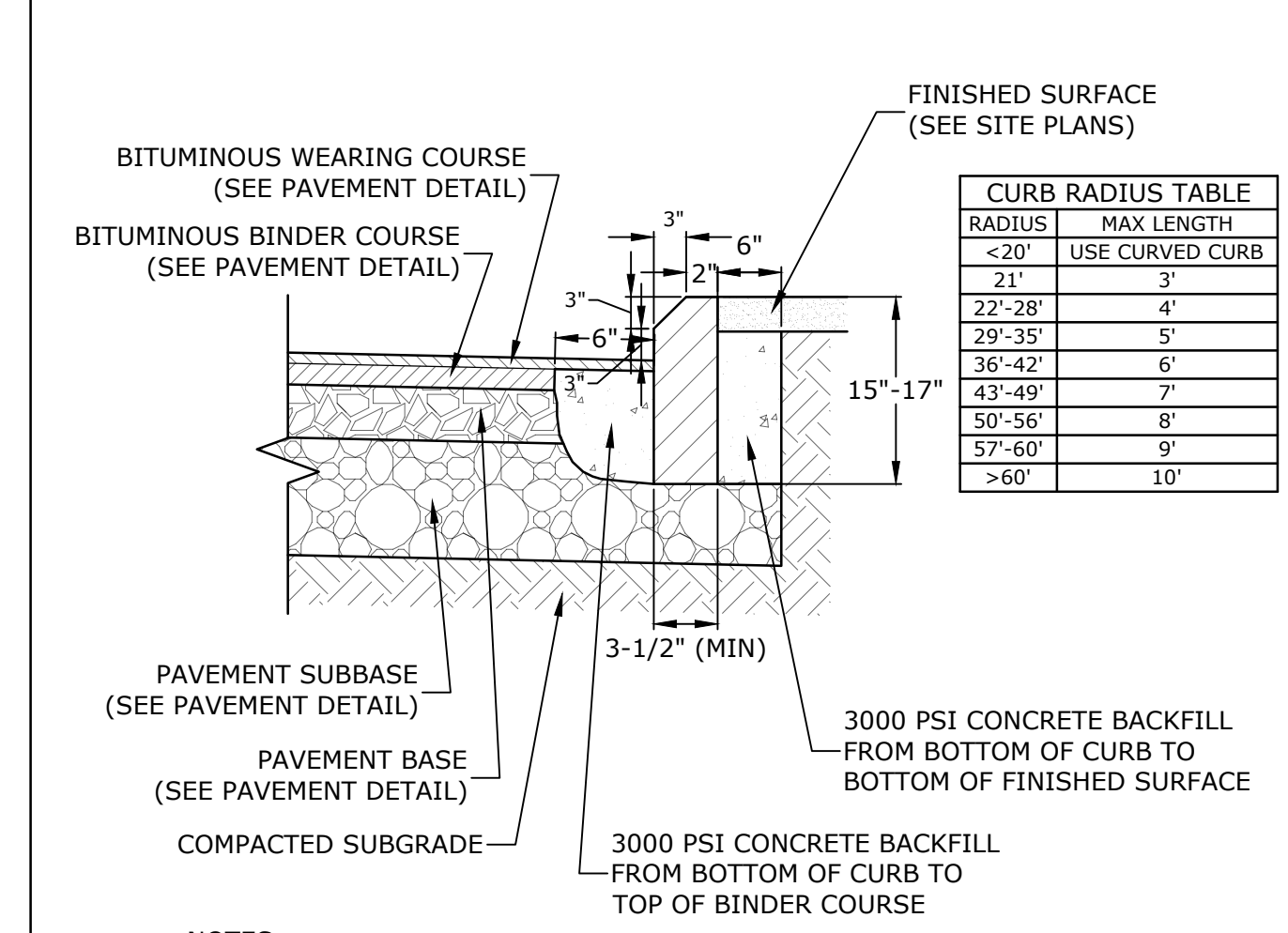
- NOTES:
- SEE SITE PLAN(S) FOR LIMITS OF VERTICAL GRANITE CURB (VGC).
 - ADJOINING STONES SHALL HAVE THE SAME OR APPROXIMATELY THE SAME LENGTH.
 - MINIMUM LENGTH OF STRAIGHT CURB STONES = 3'
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES = 10'
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES LAID ON CURVES (SEE TABLE).
 - ALL RADII 20 FEET AND SMALLER SHALL BE CONSTRUCTED USING CURVED SECTIONS.
 - JOINTS BETWEEN STONES SHALL HAVE A MAXIMUM SPACING OF 1/2" AND SHALL BE MORTARED.

VERTICAL GRANITE CURB
NO SCALE



- NOTES:
- SEE SITE PLAN(S) FOR LIMITS OF VERTICAL GRANITE CURB (VGC).
 - ADJOINING STONES SHALL HAVE THE SAME OR APPROXIMATELY THE SAME LENGTH.
 - MINIMUM LENGTH OF STRAIGHT CURB STONES = 18"
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES = 8'
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES LAID ON CURVES (SEE TABLE).
 - JOINTS BETWEEN STONES SHALL HAVE A MAXIMUM SPACING OF 1/2" AND SHALL BE MORTARED.

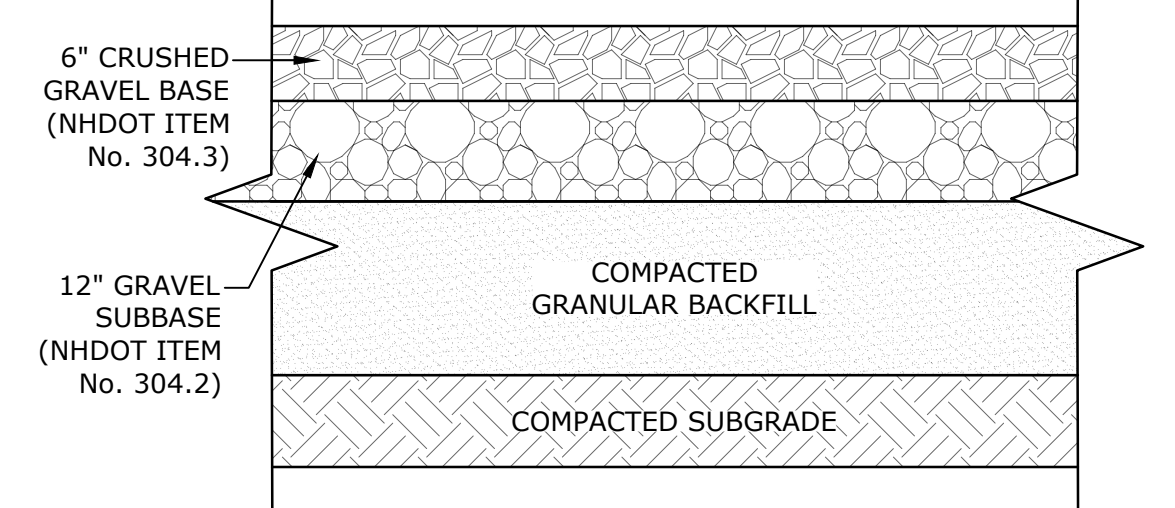
SLOPED GRANITE CURB
NO SCALE



- NOTES:
- SEE SITE PLAN(S) FOR LIMITS OF MOUNTABLE VERTICAL GRANITE CURB (MVGC).
 - ADJOINING STONES SHALL HAVE THE SAME OR APPROXIMATELY THE SAME LENGTH.
 - MINIMUM LENGTH OF STRAIGHT CURB STONES = 3'
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES = 10'
 - MAXIMUM LENGTH OF STRAIGHT CURB STONES LAID ON CURVES (SEE TABLE).
 - ALL RADII 20 FEET AND SMALLER SHALL BE CONSTRUCTED USING CURVED SECTIONS.
 - JOINTS BETWEEN STONES SHALL HAVE A MAXIMUM SPACING OF 1/2" AND SHALL BE MORTARED.

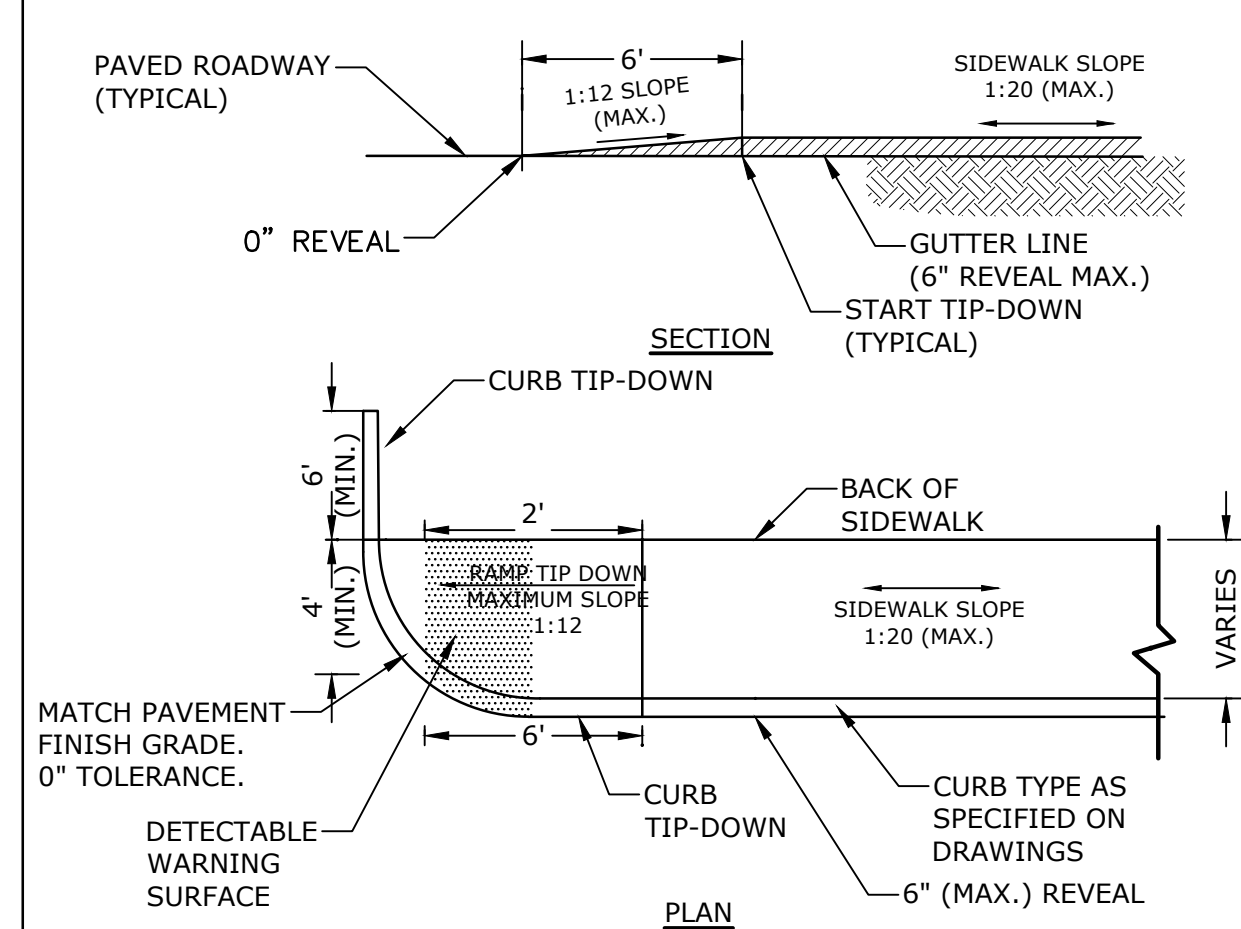
MOUNTABLE VERTICAL GRANITE CURB
NO SCALE

NHDOT ITEM No. 304.2 (GRAVEL)		NHDOT ITEM No. 304.3 (CRUSHED GRAVEL)	
SIEVE SIZE	% PASSING	SIEVE SIZE	% PASSING
6"	100	3"	100
#4	25-70	1"	95-100
#200	0-12	#4	55-85
		#200	27-52
			0-12



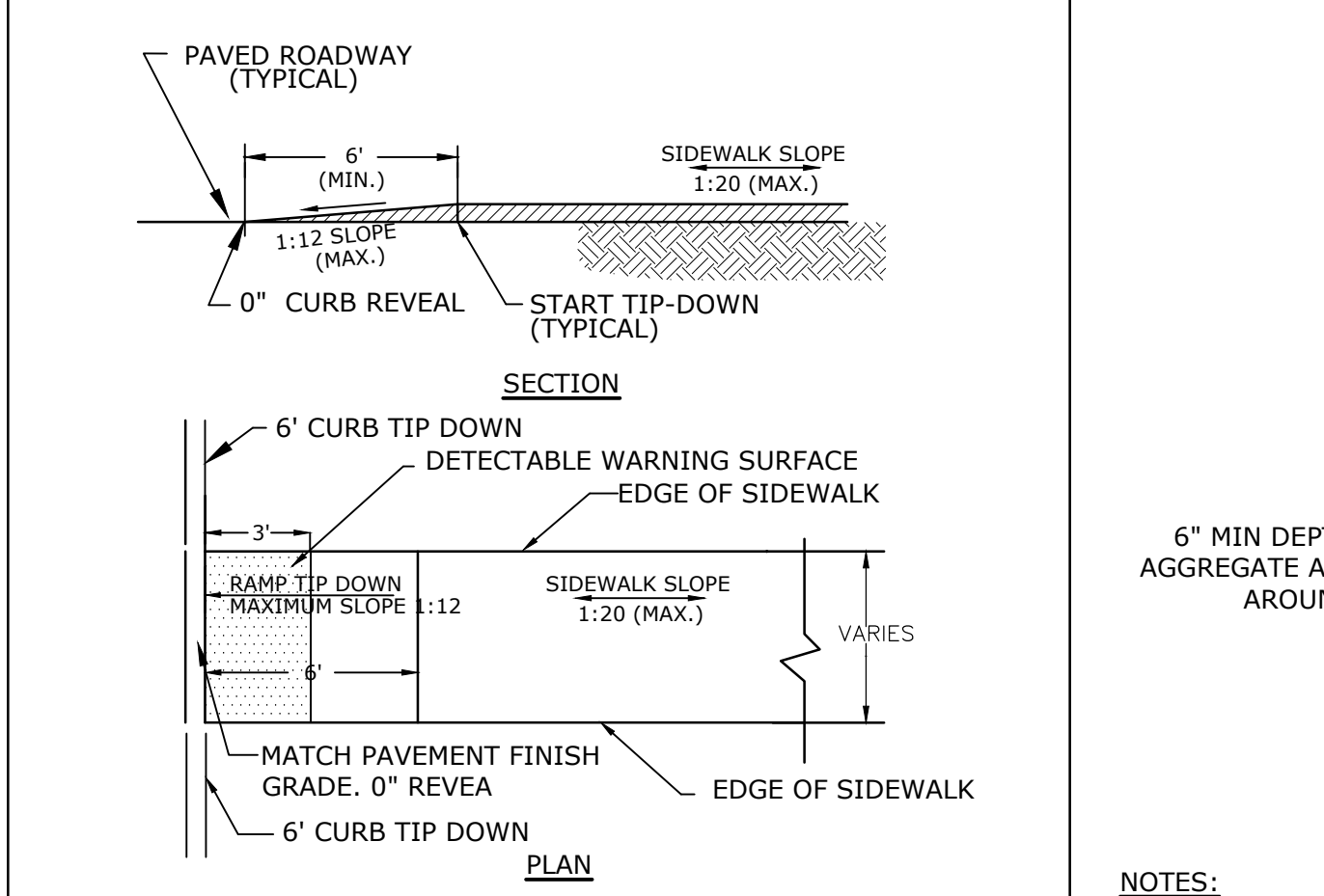
- NOTES:
- SEE SITE PLAN FOR GRAVEL WIDTH AND LOCATION.
 - SEE GRADING, DRAINAGE AND EROSION CONTROL PLAN FOR PAVEMENT SLOPE AND CROSS-SLOPE.
 - GRAVEL PARKING AREA DESIGN TO BE DETERMINED BY GEOTECHNICAL ENGINEER.
 - NHDOT ITEM No. 304.2 MAY BE SUBSTITUTED FOR NHDOT ITEM No. 304.4, IF NHDOT ITEM No. 304.2 CAN NOT BE ACQUIRED.

GRAVEL PARKING AREA SECTION
NO SCALE



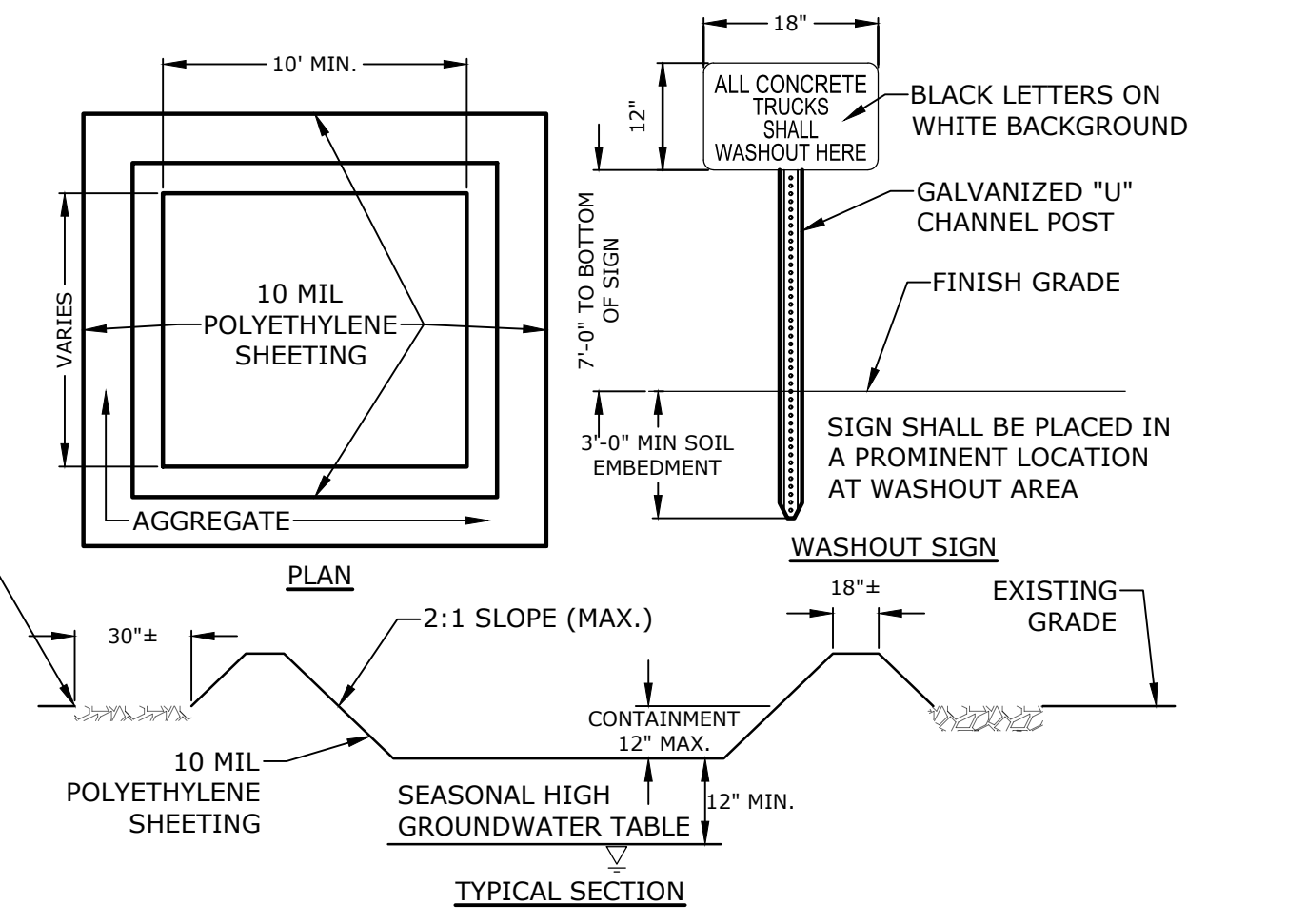
- NOTES:
- RAMPS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE AMERICANS WITH DISABILITIES ACT AND LOCAL AND STATE REQUIREMENTS.
 - PROVIDE 6" COMPACTED CRUSHED GRAVEL BASE BENEATH RAMPS.
 - DETECTABLE WARNING STRIP SHALL BE NENEAH R-4984-36B-R4984007 24" X 36" CAST IRON ADA PLATE. INSTALL PER MANUFACTURER'S RECOMMENDATIONS.

CORNER TIP DOWN RAMP
NO SCALE



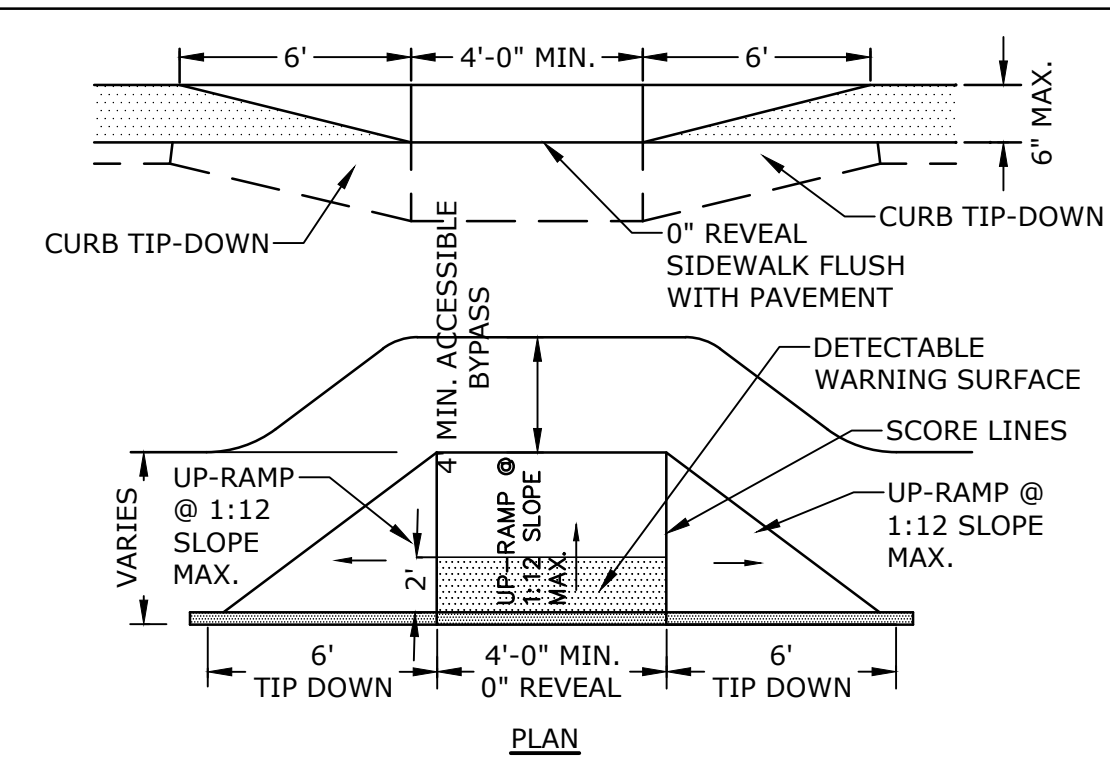
- NOTES:
- RAMPS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE AMERICANS WITH DISABILITIES ACT AND LOCAL AND STATE REQUIREMENTS.
 - PROVIDE 6" COMPACTED CRUSHED GRAVEL BASE BENEATH RAMPS.
 - DETECTABLE WARNING STRIP SHALL BE NENEAH R-4984-36B-R4984007 24" X 36" CAST IRON ADA PLATE. INSTALL PER MANUFACTURER'S RECOMMENDATIONS.

SIDEWALK TIP-DOWN RAMP
NO SCALE



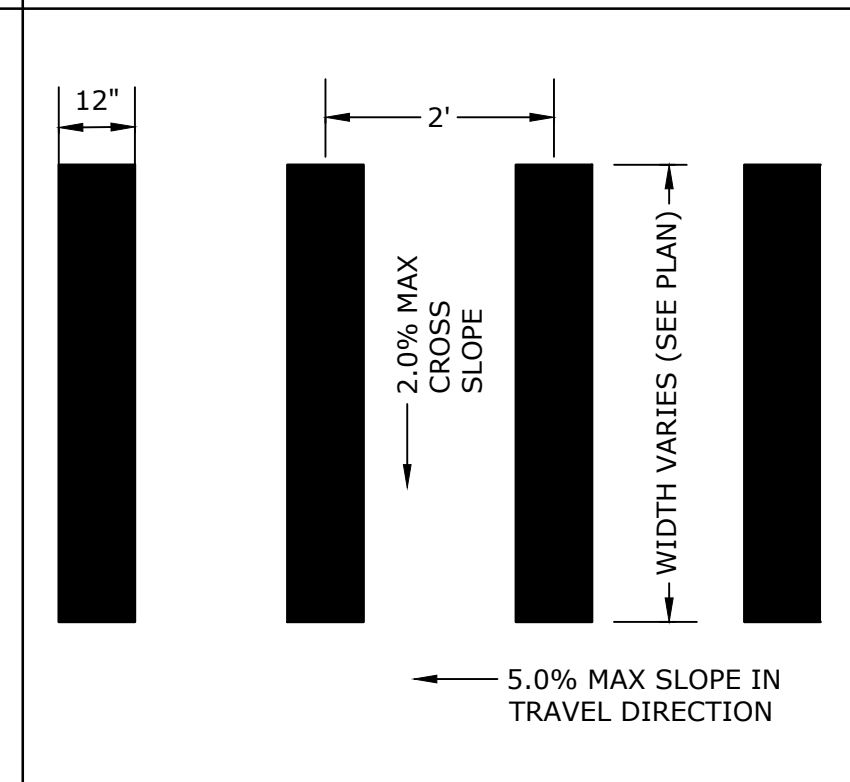
- NOTES:
- CONTAINMENT MUST BE STRUCTURALLY SOUND AND LEAK FREE AND CONTAIN ALL LIQUID WASTES.
 - CONTAINMENT DEVICES MUST BE OF SUFFICIENT QUANTITY OR VOLUME TO COMPLETELY CONTAIN THE LIQUID WASTES GENERATED.
 - WASHOUT MUST BE CLEANED OR NEW FACILITIES CONSTRUCTED AND READY TO USE ONCE WASHOUT IS 75% FULL.
 - WASHOUT AREA(S) SHALL BE INSTALLED IN A LOCATION EASILY ACCESSIBLE BY CONCRETE TRUCKS.
 - ONE OR MORE AREAS MAY BE INSTALLED ON THE CONSTRUCTION SITE AND MAY BE RELOCATED AS CONSTRUCTION PROGRESSES.
 - AT LEAST WEEKLY REMOVE ACCUMULATION OF SAND AND AGGREGATE AND DISPOSE OF PROPERLY.

CONCRETE WASHOUT AREA
NO SCALE



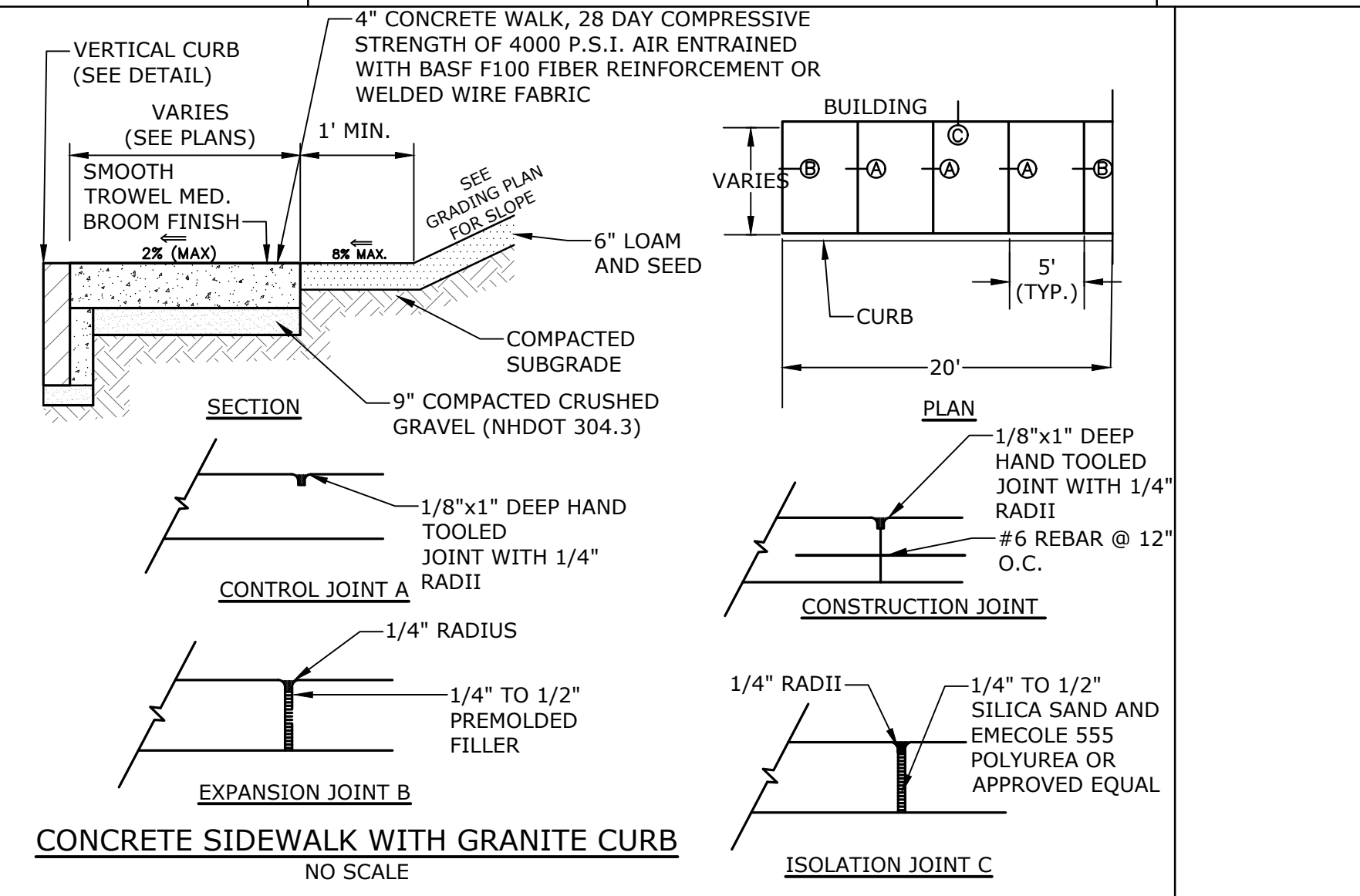
- NOTES:
- RAMPS SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE AMERICANS WITH DISABILITIES ACT AND LOCAL AND STATE REQUIREMENTS.
 - PROVIDE 6" COMPACTED CRUSHED GRAVEL BASE BENEATH RAMPS.
 - DETECTABLE WARNING STRIP SHALL BE ADA SOLUTIONS, INC. CAST IN PLACE RAMP. INSTALL PER MANUFACTURER'S RECOMMENDATIONS.

CONCRETE WHEELCHAIR ACCESSIBLE RAMP
NO SCALE

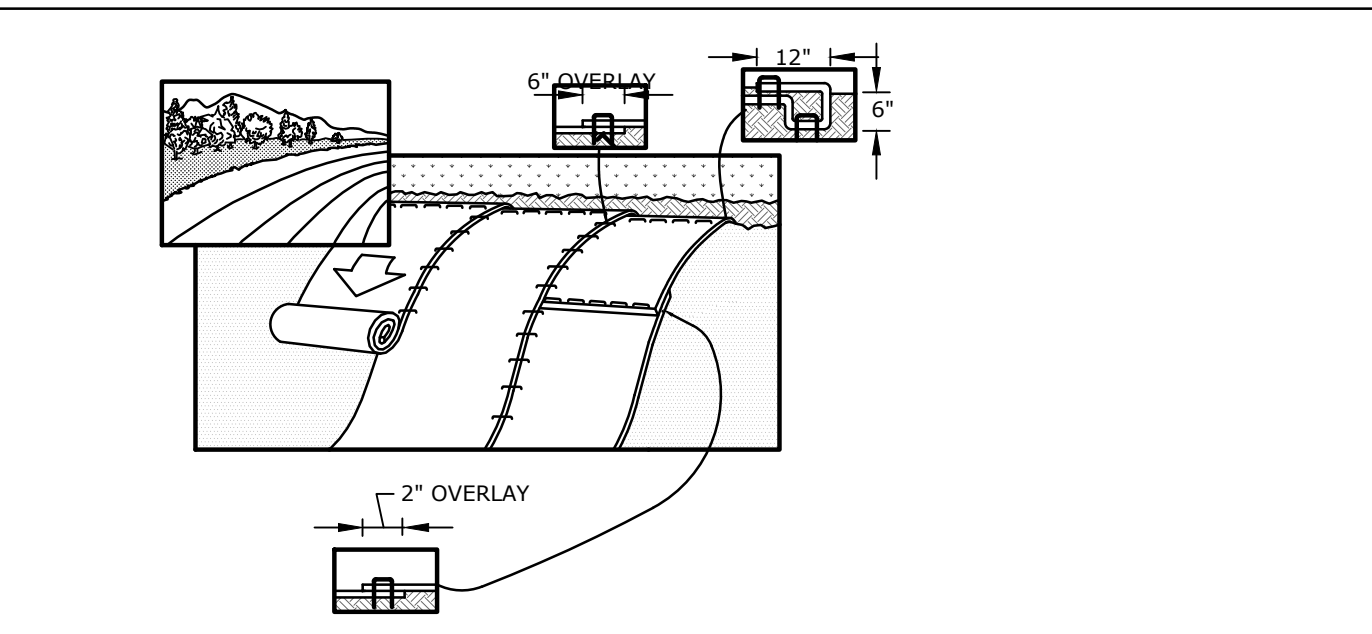


- NOTE:
- STRIPING SHALL BE CONSTRUCTED USING WHITE THERMO PLASTIC, REFLECTORIZED PAVEMENT MARKING MATERIAL MEETING THE REQUIREMENTS OF ASTM D 4505

CROSSWALK STRIPING
NO SCALE



CONCRETE SIDEWALK WITH GRANITE CURB
NO SCALE



- NOTES:
- EROSION CONTROL BLANKET SHALL BE AN ALL NATURAL PRODUCT WITH NO PHOTO DEGRADABLE COMPONENTS, NORTH AMERICAN GREEN SC150BN OR APPROVED EQUAL.
 - STAKES SHALL BE BIODEGRADABLE BIOSTAKES OR ALL NATURAL WOOD ECOSTAKES OR APPROVED EQUAL. THE LENGTH OF STAKES SHALL BE BASED OFF OF THE MANUFACTURERS RECOMMENDATION.
 - PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, COMPOST AND SEED.
 - INSTALL PER MANUFACTURER'S WRITTEN INSTRUCTION.

EROSION CONTROL BLANKET
NO SCALE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission
MARK	DATE	DESCRIPTION

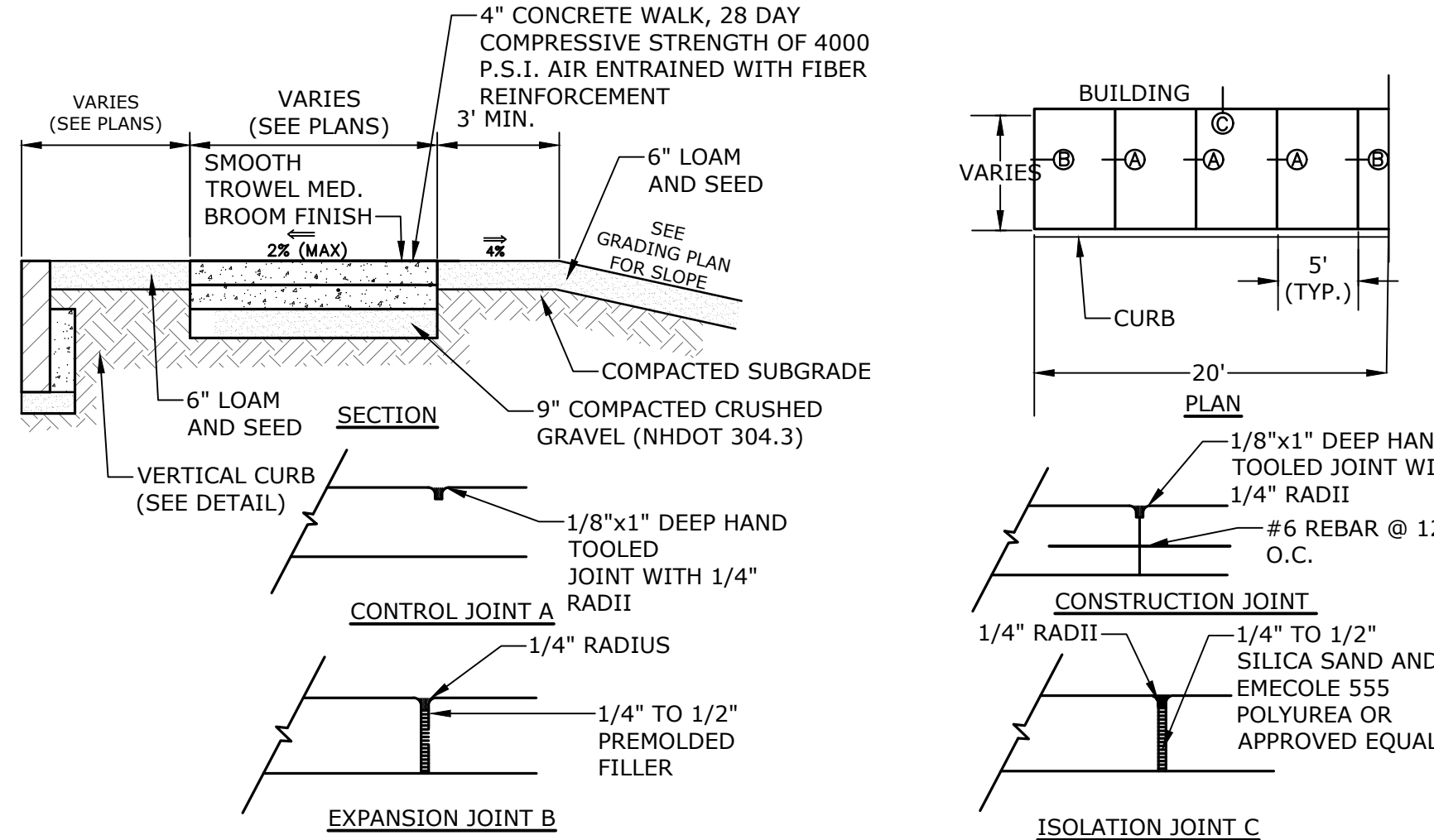
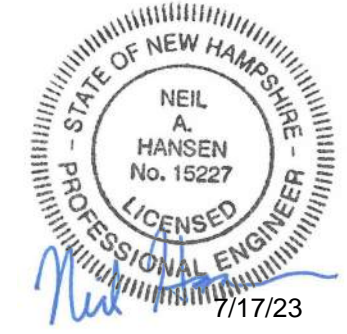
PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DTLS.dwg
DRAWN BY:	CIK
CHECKED:	NAH
APPROVED:	PMC

DETAILS SHEET

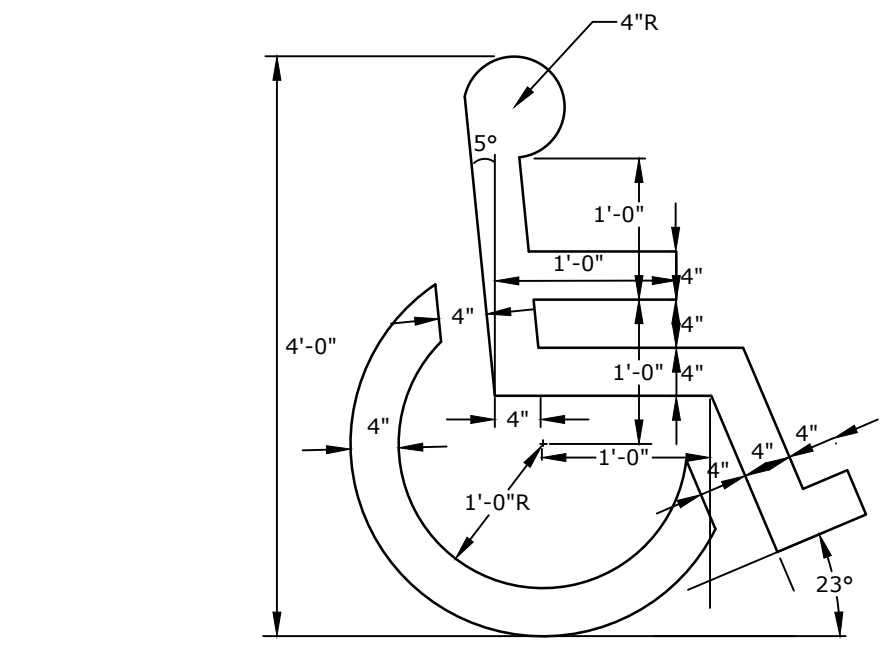
SCALE: AS SHOWN

C-502

Last Save Date: July 12, 2023 6:37 PM BY: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
 Plot Location: L:\0700\Lonza Biologics Expansion\18-1876-026 - Project\Subarea Drawings\AutoCAD\18-0700-026-C-DTLS.dwg Layout: Tab: C-502

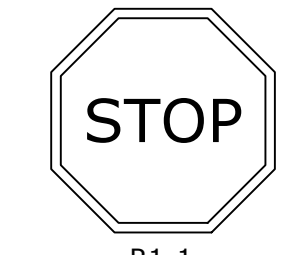


CONCRETE SIDEWALK WITH GRANITE CURB ALONG CORPORATE DRIVE
NO SCALE



ACCESSIBLE SYMBOL
NO SCALE

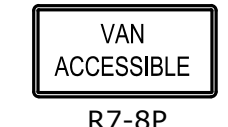
NOTES:
1. SYMBOL SHALL BE CONSTRUCTED IN ALL ACCESSIBLE SPACES USING WHITE THERMOPLASTIC, REFLECTORIZED PAVEMENT MARKING MATERIAL MEETING THE REQUIREMENTS OF ASTM D 4505.
2. SYMBOL SHALL BE CONSTRUCTED TO THE LATEST ADA, STATE AND LOCAL REQUIREMENTS.



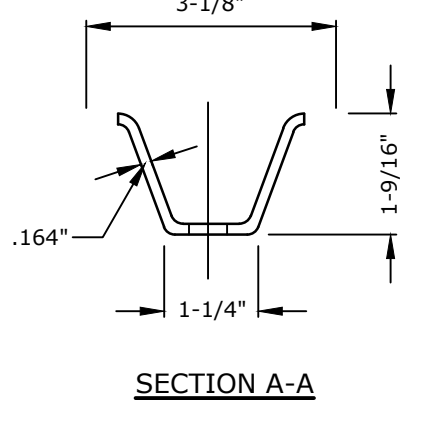
R1-1
30" X 30"
WHITE ON RED



R7-8
12" X 18"
BLUE AND GREEN ON WHITE



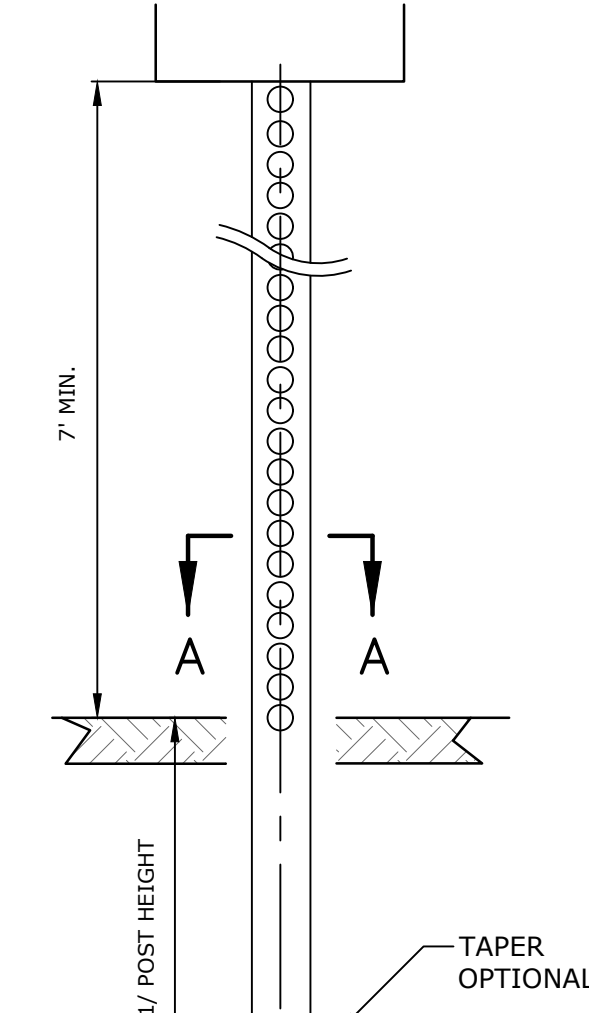
R7-8P
18" X 9"
GREEN ON WHITE



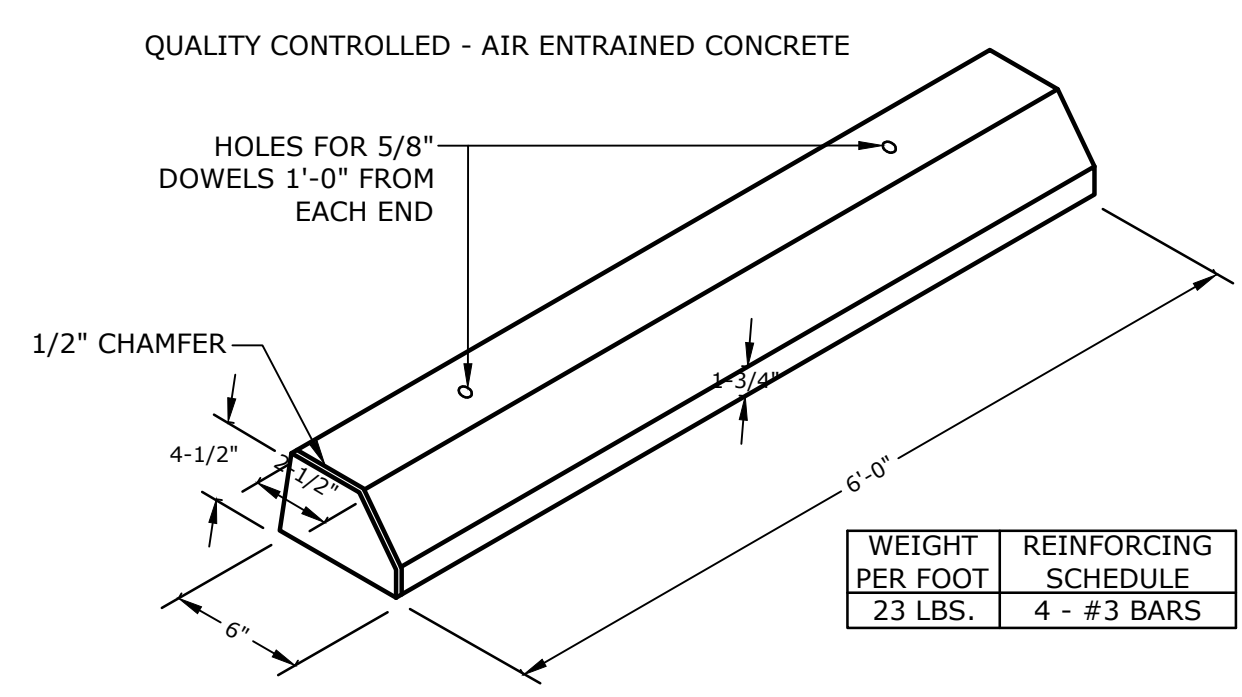
SECTION A-A

LENGTH: AS REQUIRED
WEIGHT PER LINEAR FOOT: 2.50 LBS (MIN.)
HOLES: 3/8" DIAMETER, 1" C-C FULL LENGTH
STEEL: SHALL CONFORM TO ASTM A-499 (GRADE 60) OR ASTM A-576 (GRADE 1070 - 1080)
FINISH: SHALL BE PAINTED WITH TWO COATS OF AN APPROVED MEDIUM GREEN BAKED ON OR DRIED, PAINT OF WEATHER RESISTANT QUALITY. ALL FABRICATION SHALL BE COMPLETE BEFORE PAINTING.

NOTE:
ALL SIGNS TO BE INSTALLED AS INDICATED IN THE MANUAL ON UNIFORM TRAFFIC CONTROL DEVICES, LATEST EDITION.

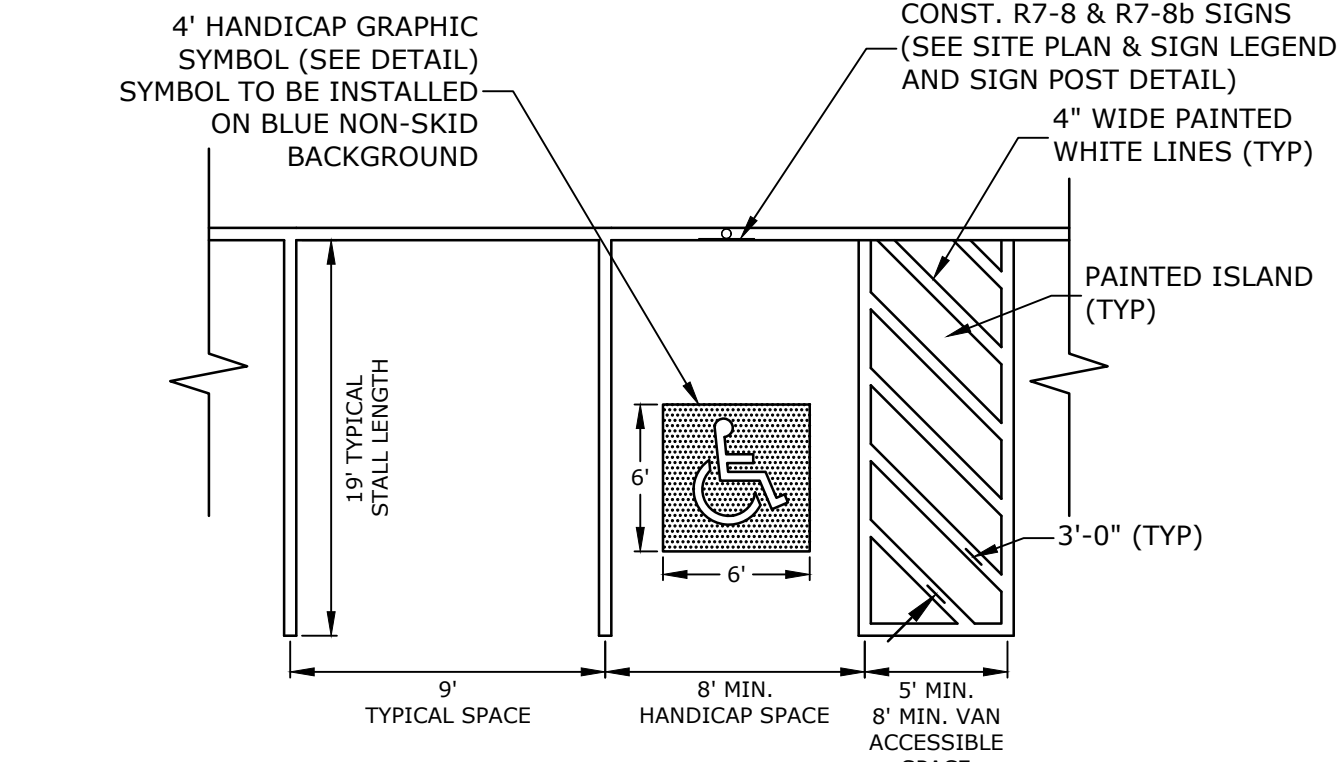


SIGN LEGEND & SIGN POST
NO SCALE



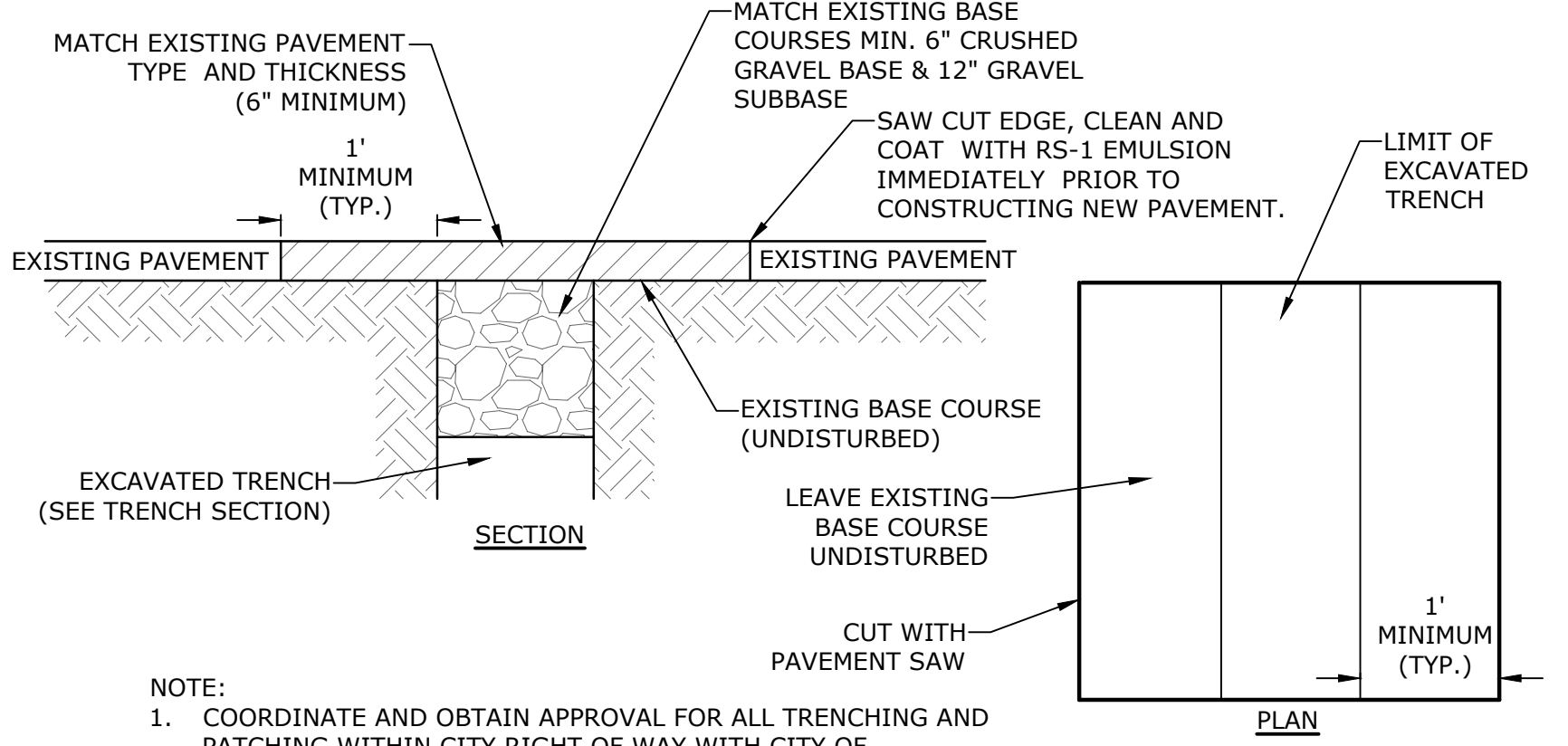
NOTE:
1. CURBING TO BE PINNED THROUGH ASPHALT PAVEMENT.

CONCRETE WHEEL STOP
NO SCALE



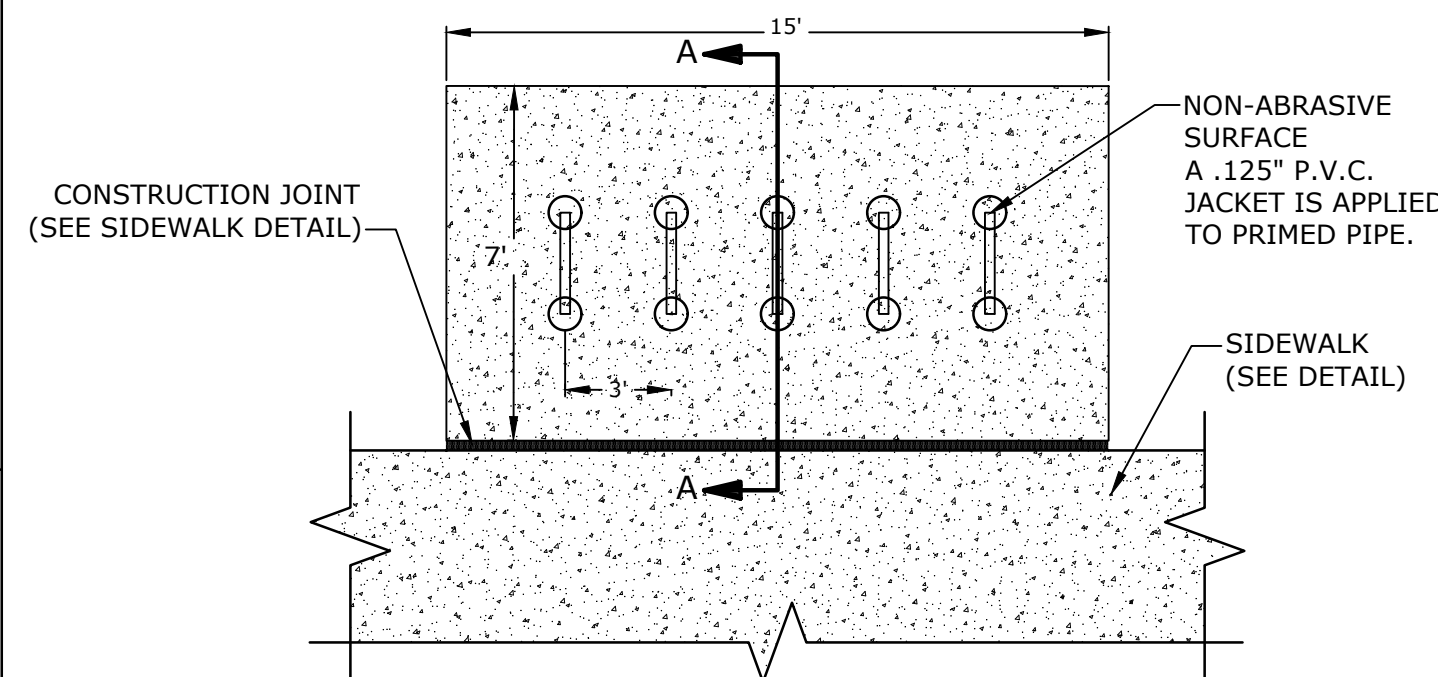
NOTE:
1. ALL PAINT SHALL BE FAST DRYING TRAFFIC PAINT, MEETING THE REQUIREMENTS OF AASHTO M248-TYPE F. PAINT SHALL BE APPLIED AS SPECIFIED BY MANUFACTURER.
2. SYMBOLS & PARKING STALLS SHALL CONFORM TO THE REQUIREMENTS OF THE AMERICANS WITH DISABILITIES ACT AND LOCAL AND STATE REQUIREMENTS.
3. FINISH PAVEMENT GRADES AT ALL HANDICAP ACCESSIBLE STALLS AND PAINTED ACCESS AISLES SHALL NOT EXCEED 2% IN ANY DIRECTION.

STALL STRIPING-SINGLE STRIPE
NO SCALE

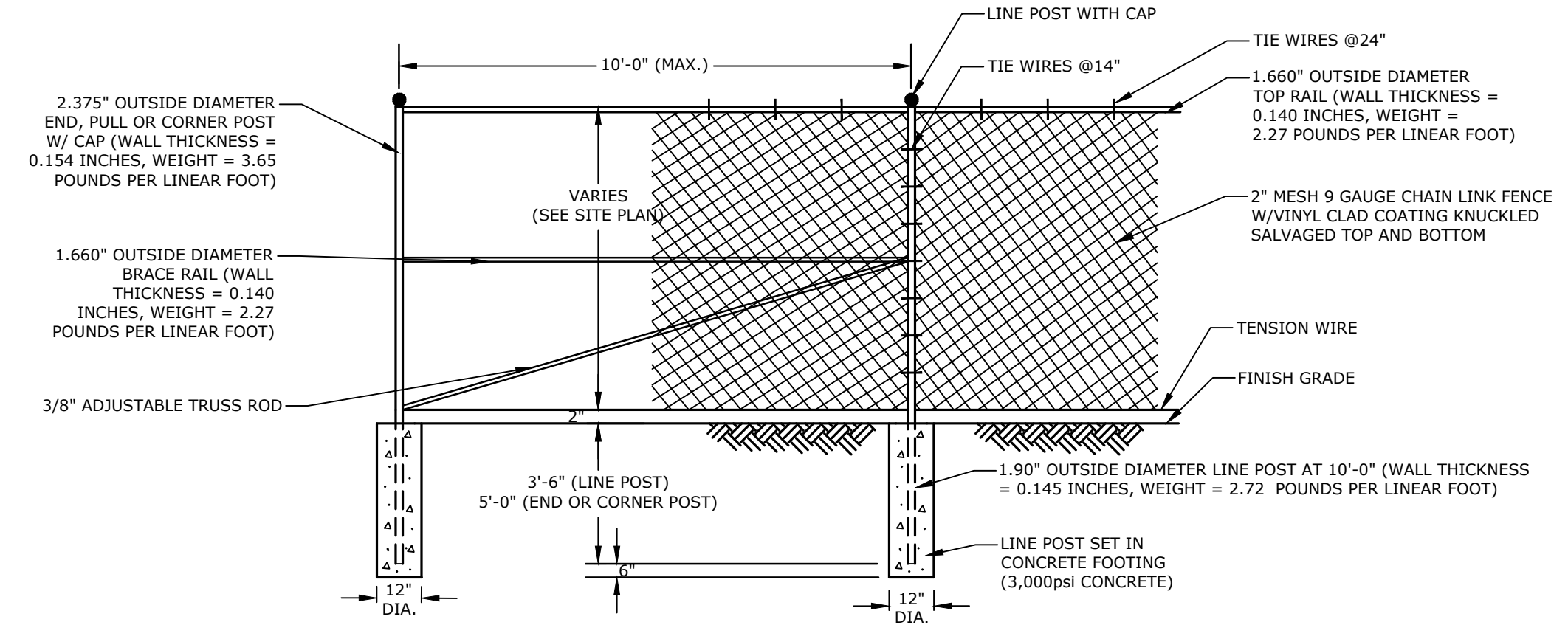


NOTE:
1. COORDINATE AND OBTAIN APPROVAL FOR ALL TRENCHING AND PATCHING WITHIN CITY RIGHT OF WAY WITH CITY OF PORTSMOUTH DPW PRIOR TO COMMENCING WORK.

ROADWAY TRENCH PATCH
NO SCALE

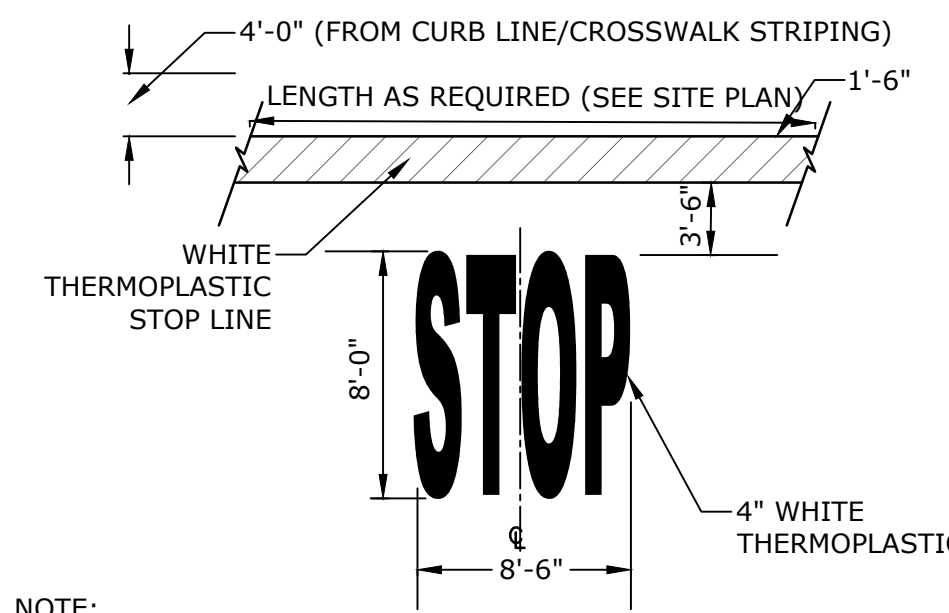


BIKE RACK
NO SCALE



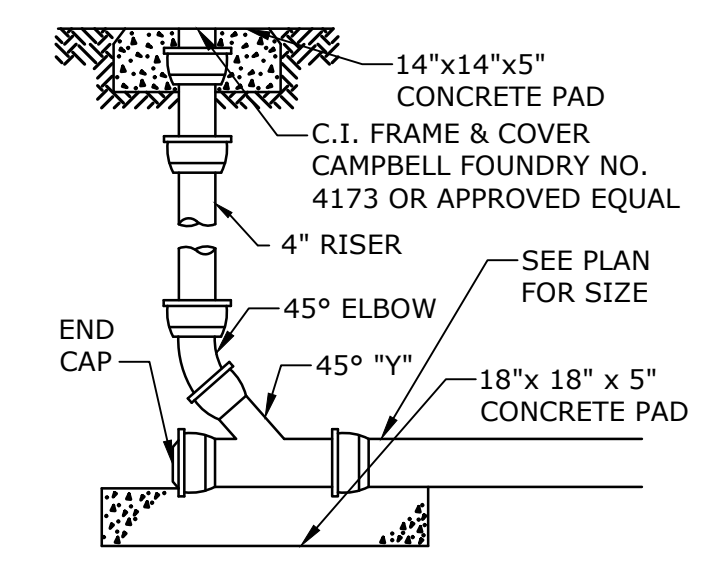
NOTES:
1. CORNER POSTS SHALL BE USED AT SHARP BREAKS IN GRADE AND CHANGES IN HORIZONTAL ALIGNMENT OF 15' OR MORE.
2. POSTS, RAILS & BRACES SHALL BE TYPE 1, SCHEDULE 40 BLACK VINYL COATED PIPE.
3. FABRIC TO BE BLACK VINYL COATED.
4. TIE WIRES SHALL BE 9 GAUGE GALVANIZED STEEL WIRE FOR ATTACHMENT OF FABRIC TO LINE POSTS.
5. TIE WIRES SHALL BE 13 GAUGE GALVANIZED STEEL WIRE FOR ATTACHMENT OF FABRIC TO RAILS AND BRACES.
6. HOG RING TIES SHALL BE 12- 1/2 GAUGE GALVANIZED STEEL WIRE FOR ATTACHMENT OF FABRIC TO TENSION WIRE.
7. COORDINATE FINAL CHAIN LINK FENCE DESIGN WITH BUILDING DRAWINGS AND UTILITY YARD CONCRETE SLAB DESIGN.

CHAIN LINK FENCE
NO SCALE



NOTE:
1. PAVEMENT MARKINGS TO BE INSTALLED IN LOCATIONS AS SHOWN ON SITE PLAN.
2. STRIPING SHALL BE CONSTRUCTED USING WHITE THERMO PLASTIC, REFLECTORIZED PAVEMENT MARKING MATERIAL MEETING THE REQUIREMENTS OF ASTM D 4505

STOP BAR AND LEGEND
NO SCALE



CLEAN-OUT
NO SCALE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
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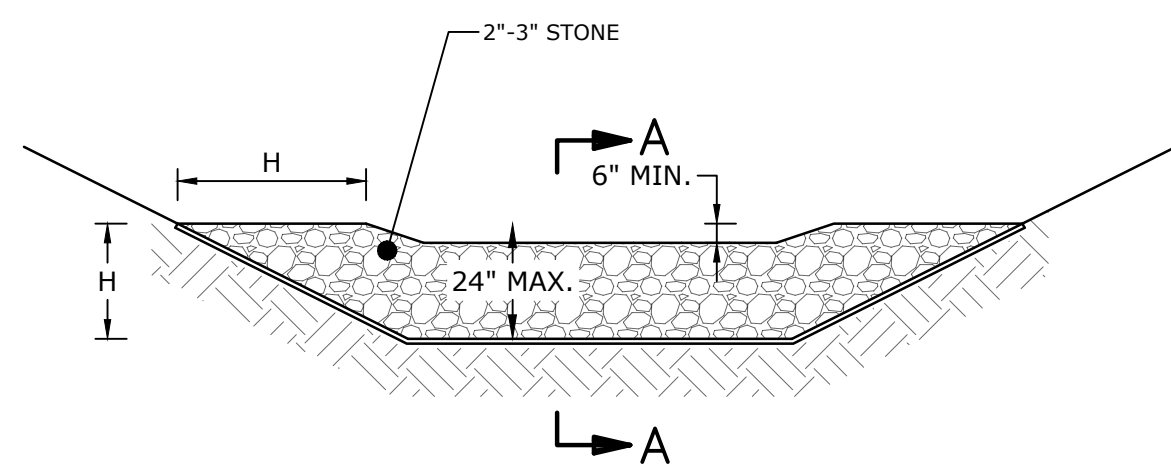
PROJECT NO: L-0700-013
DATE: 04/03/2018
FILE: L-0700-026-C-DTLS.dwg
DRAWN BY: CJK
CHECKED: NAH
APPROVED: PMC

DETAILS SHEET

SCALE: AS SHOWN

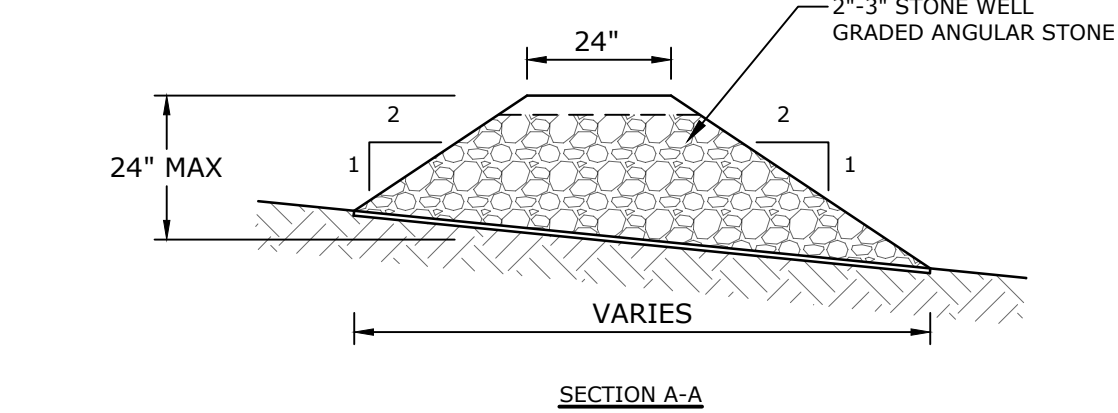
C-503

Last Save Date: July 12, 2023 6:37 PM By: CKRZCUIK
Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
File Location: J:\0700\Lonza Biologics Expansion.was 12/7/2026 - Project\Subarea\Drawings\AutoCAD\1-0700-026-C-DTLS.dwg Layout: Tab: C-503



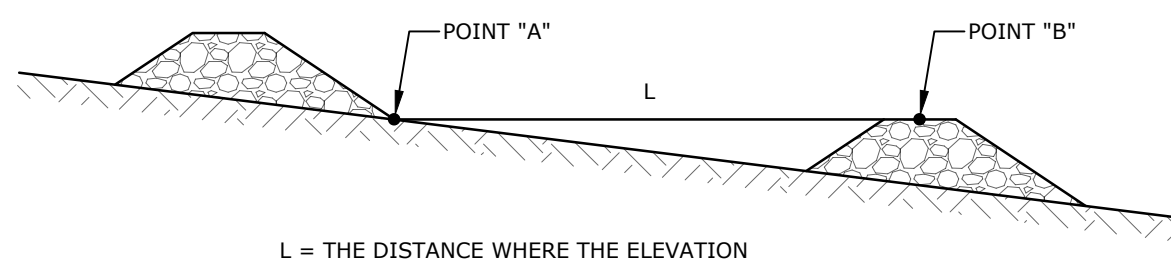
BERM STONE SIZE	
SIEVE DESIGNATION (US CUSTOMARY)	PERCENT BY WEIGHT PASSING SQUARE MESH SIEVES
12 IN	100
6 IN	84-100
3 IN	68-83
1 IN	42-55
NO. 4	8-12

- NOTES:
- CHECK DAMS SHOULD BE INSTALLED BEFORE RUNOFF IS DIRECTED TO THE SWALE OR DRAINAGE DITCH.
 - THE MAXIMUM CONTRIBUTING DRAINAGE AREA TO THE DAM SHOULD BE LESS THAN ONE ACRE.
 - THE CHECK DAM SHOULD NOT BE USED IN A FLOWING STREAM.
 - CHECK DAMS SHOWN ON THE DRAWINGS SHALL BE LEFT IN PLACE PERMANENTLY.
 - CHECK DAMS INSTALLED AS PART OF TEMPORARY EROSION CONTROL MEASURE SHALL BE REMOVED ONCE THE SWALE OR DITCH HAS BEEN STABILIZED:
 - IN TEMPORARY DITCHES AND SWALES, CHECK DAMS SHOULD BE REMOVED AND THE DITCH FILLED IN WHEN IT IS NO LONGER NEEDED.
 - IN PERMANENT STRUCTURES, CHECK DAMS SHOULD BE REMOVED WHEN PERMANENT LINING HAS BEEN ESTABLISHED. IF THE PERMANENT LINING IS VEGETATION, THEN THE CHECK DAM SHOULD BE RETAINED UNTIL THE GRASS HAS MATURED TO PROTECT THE DITCH OR SWALE. THE AREA BENEATH THE CHECK DAM MUST BE SEEDED AND MULCHED IMMEDIATELY AFTER REMOVAL.

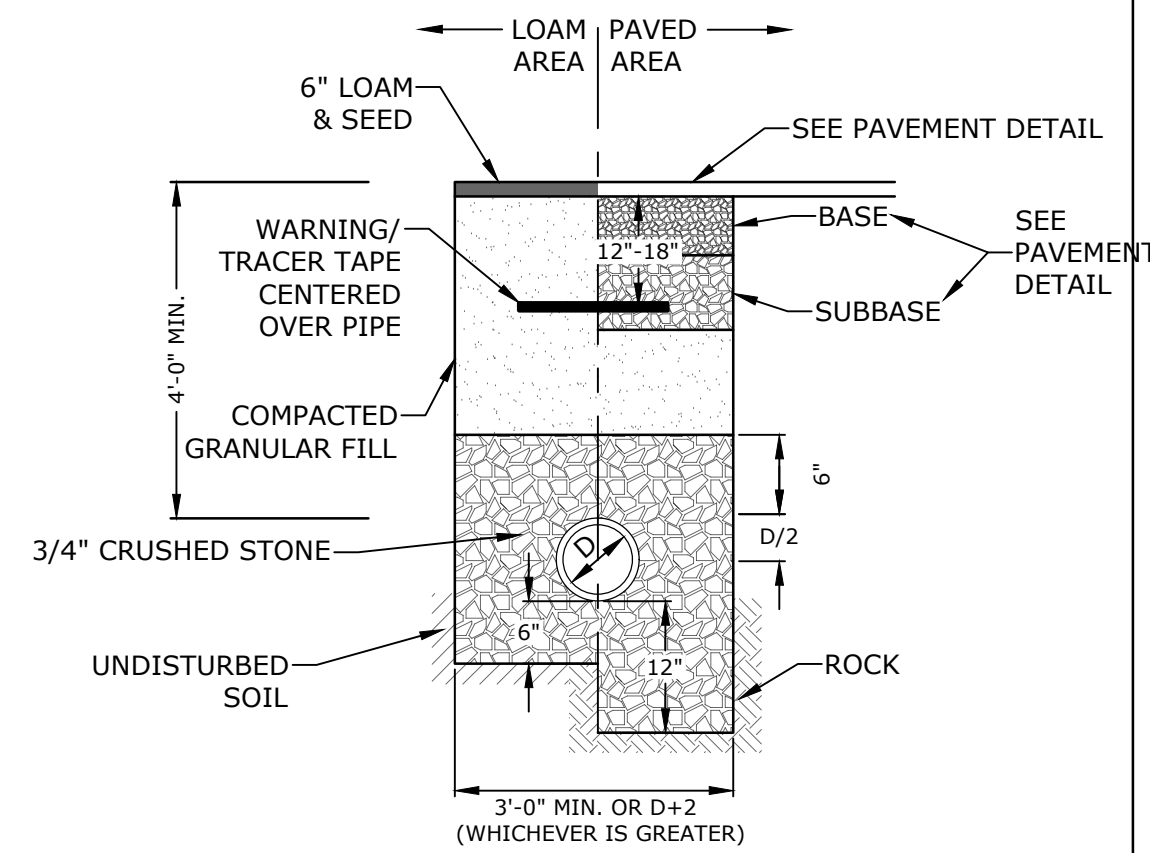


L = THE DISTANCE WHERE THE ELEVATION OF POINT "A" EQUALS THE ELEVATION OF POINT "B"

STONE CHECK DAM SPACING

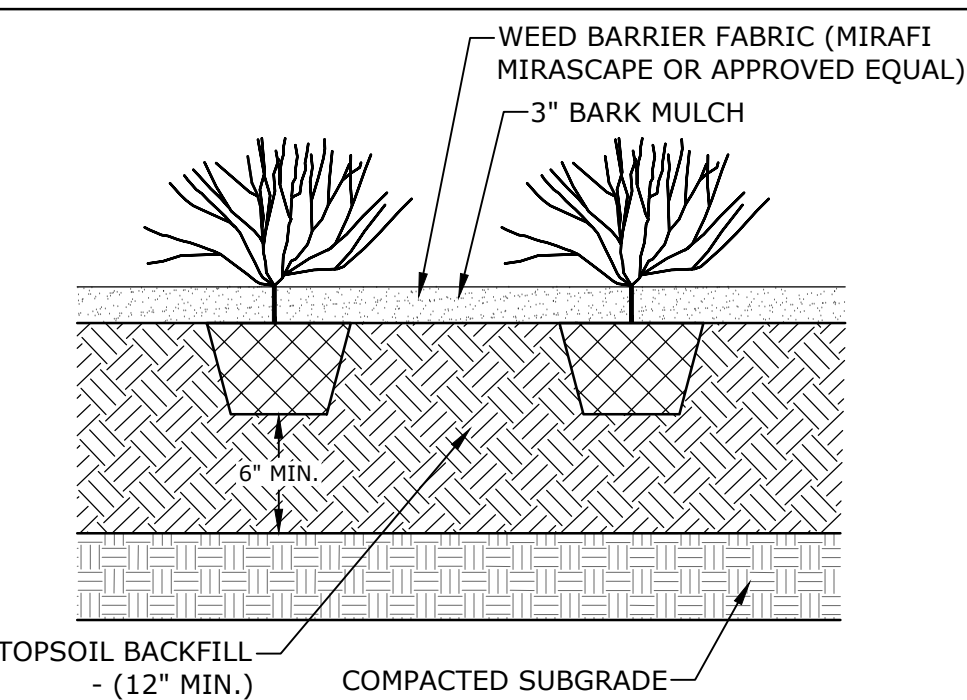


STONE CHECK DAM
NO SCALE

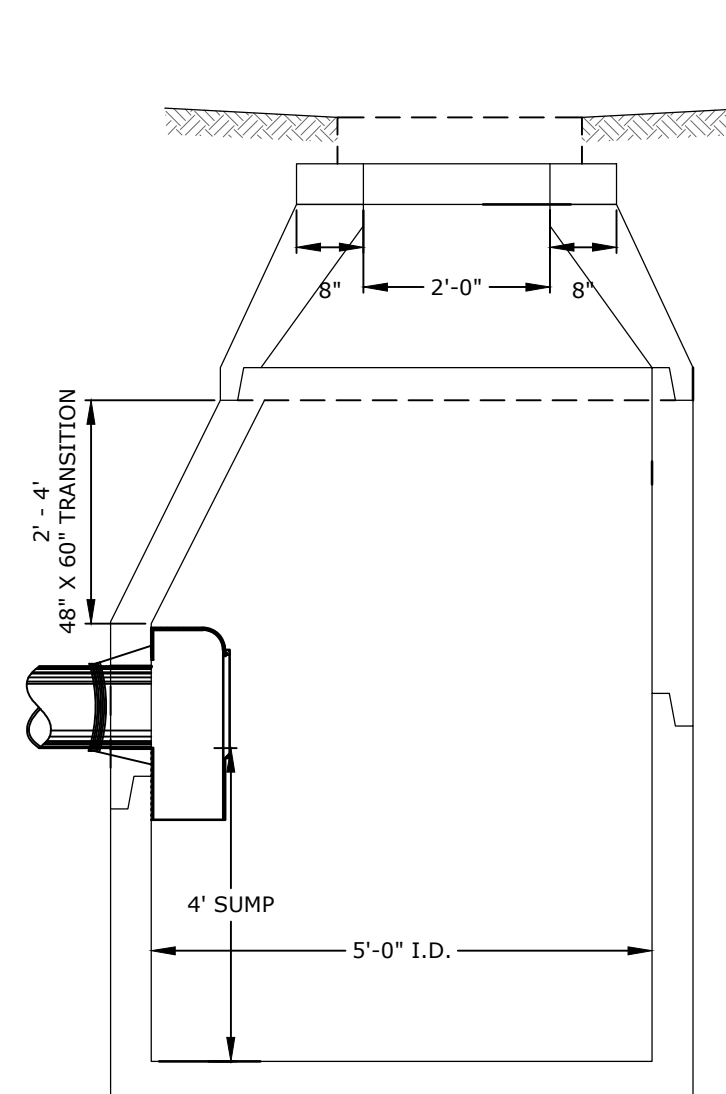


- NOTE:
- CRUSHED STONE BEDDING AND BACKFILL FOR FULL WIDTH OF THE TRENCH FROM 6" BELOW PIPE IN EARTH AND 12" BELOW PIPE IN ROCK UP TO 6" ABOVE TOP OF PIPE.
 - ALL UTILITIES SHALL BE INSTALLED PER THE INDIVIDUAL UTILITY COMPANY STANDARDS. COORDINATE ALL INSTALLATIONS WITH INDIVIDUAL UTILITY COMPANIES AND THE CITY OF PORTSMOUTH.

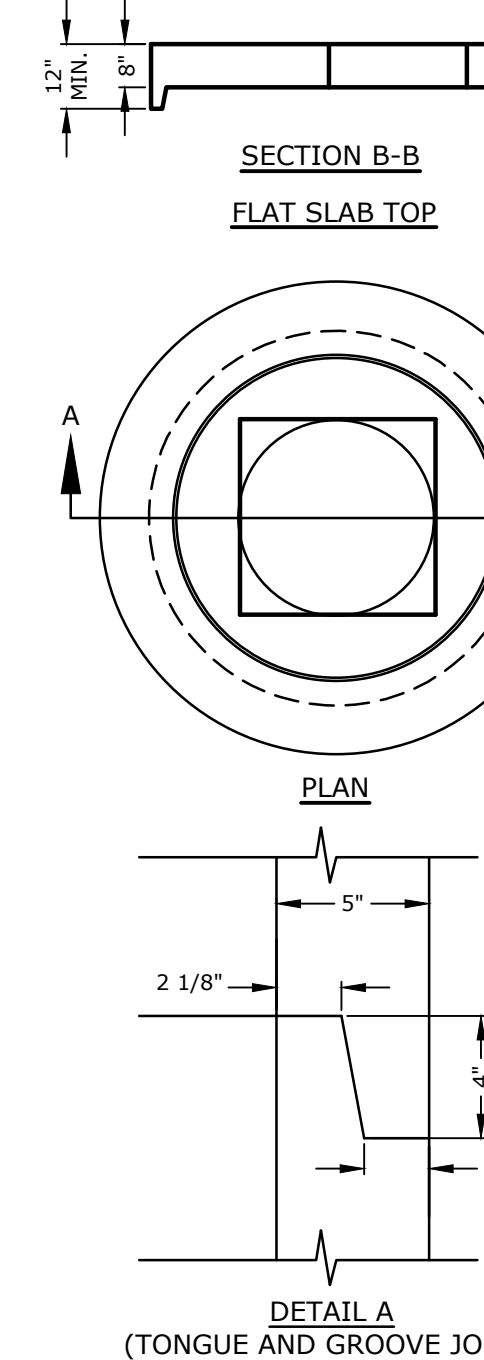
STORM DRAIN TRENCH
NO SCALE



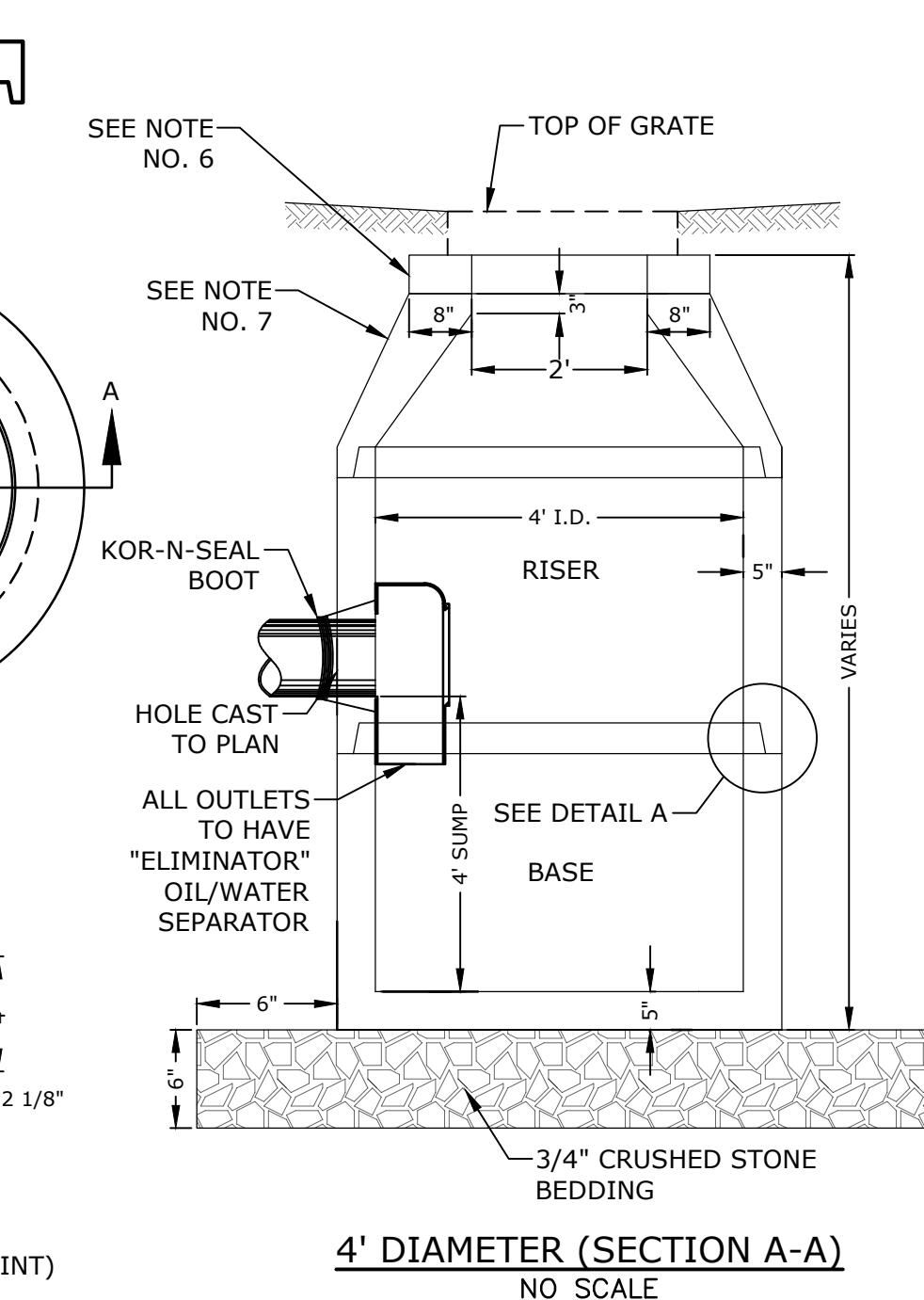
PERENNIAL PLANTING
NO SCALE



5" DIAMETER (SECTION A-A)
NO SCALE

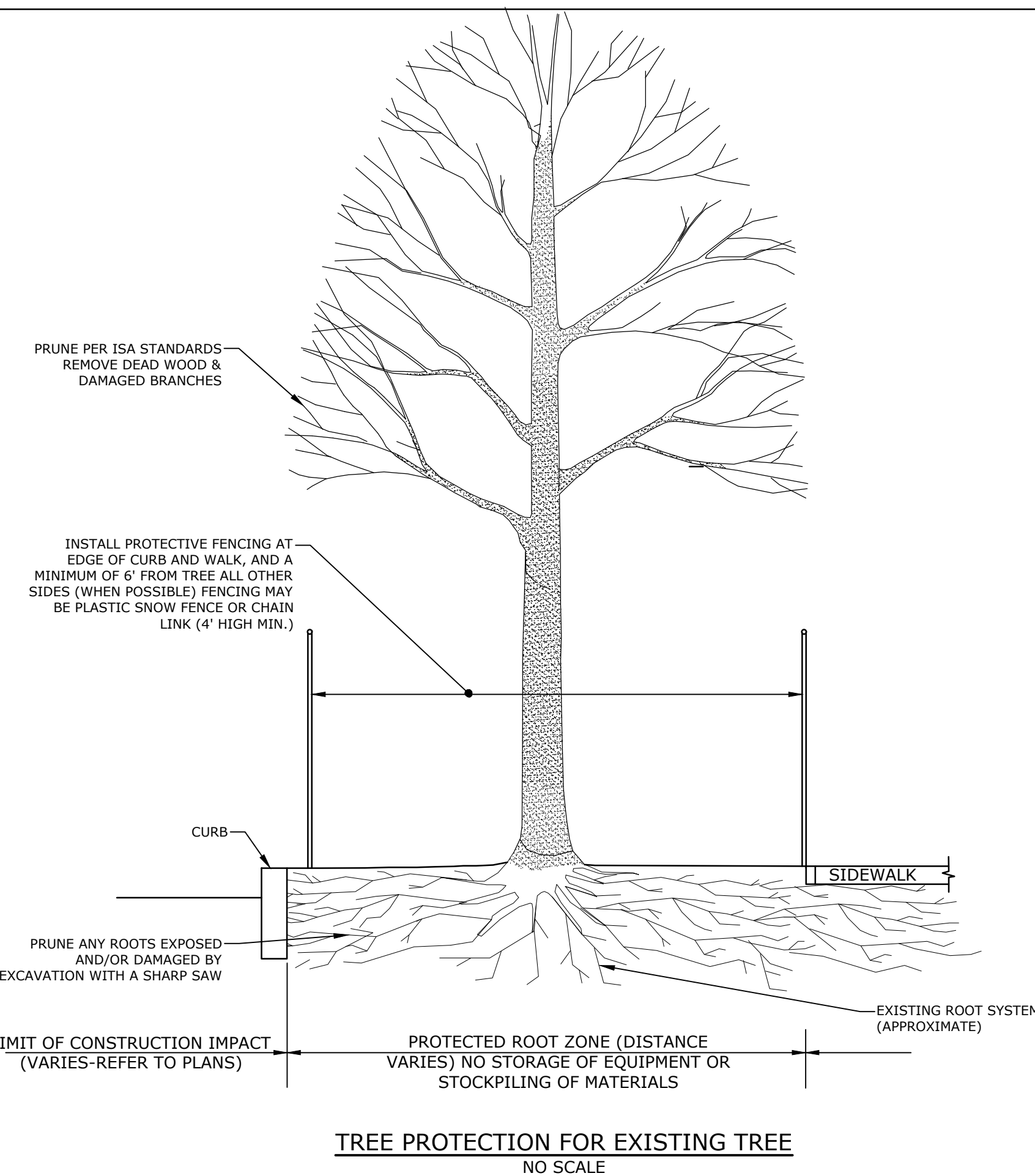


CATCH BASIN DETAIL
NO SCALE

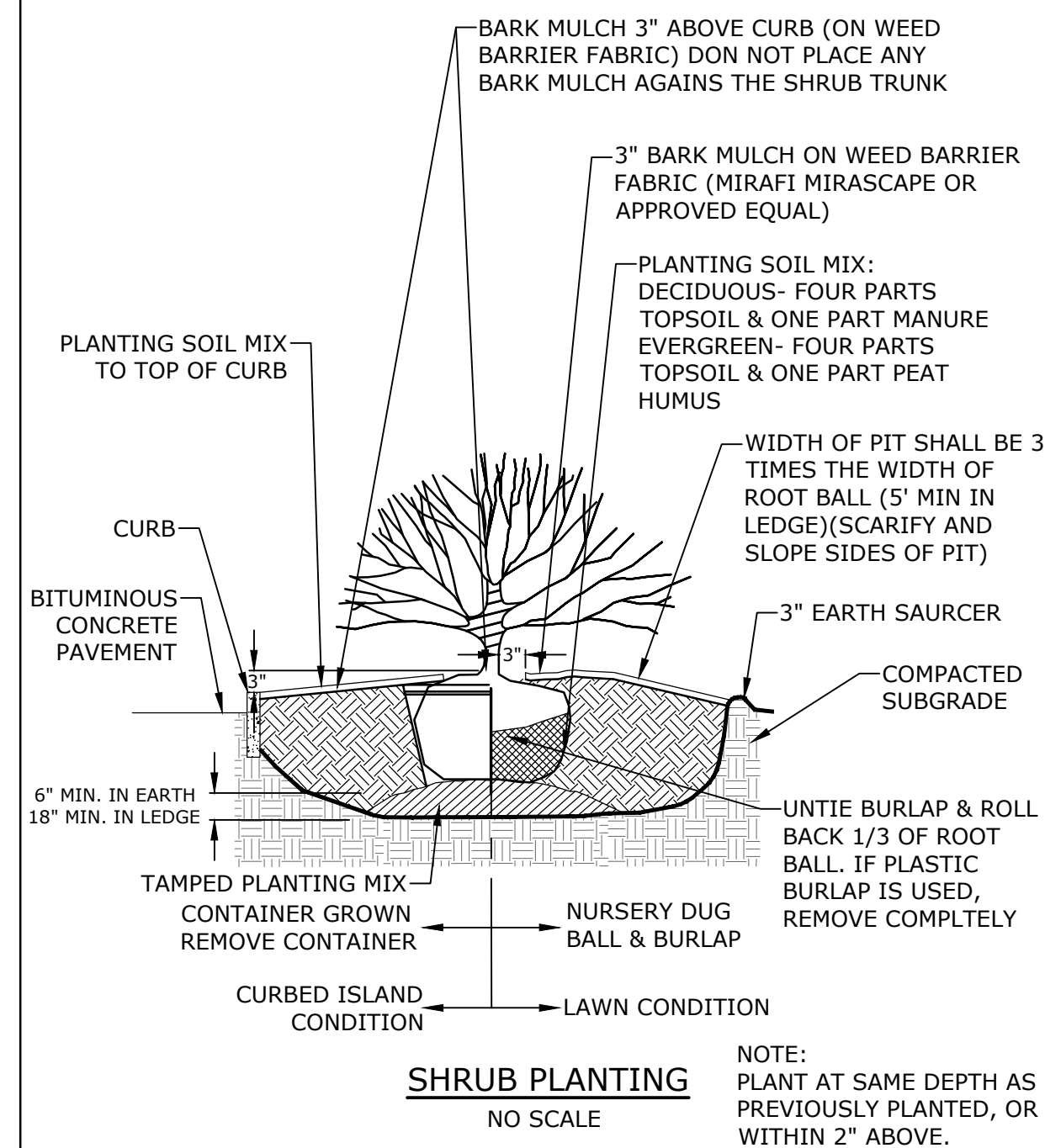


4" DIAMETER (SECTION A-A)
NO SCALE

- NOTES:
- ALL SECTIONS SHALL BE CONCRETE CLASS AA(4000 psi).
 - CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ. IN. PER LINEAR FT. IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.
 - THE TONGUE AND GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ. IN. PER LINEAR FT.
 - RISERS OF 1', 2', 3' & 4' CAN BE USED TO REACH DESIRED DEPTH.
 - THE STRUCTURES SHALL BE DESIGNED FOR H2O LOADING.
 - FITTING FRAME TO GRADE MAY BE DONE WITH PREFABRICATED ADJUSTMENT RINGS OR CLAY BRICKS (2 COURSES MAX.).
 - CONE SECTIONS MAY BE EITHER CONCENTRIC OR ECCENTRIC, OR FLAT SLAB TOPS MAY BE USED WHERE PIPE WOULD OTHERWISE ENTER INTO THE CONE SECTION OF THE STRUCTURE AND WHERE PERMITTED.
 - PIPE ELEVATIONS SHOWN ON PLANS SHALL BE FIELD VERIFIED PRIOR TO PRECASTING.
 - OUTSIDE EDGES OF PIPES SHALL PROJECT NO MORE THAN 3" BEYOND INSIDE WALL OF STRUCTURE.
 - PRECAST SECTIONS SHALL HAVE A TONGUE AND GROOVE JOINT 4" HIGH AT AN 11° ANGLE CENTERED IN THE WIDTH OF THE WALL AND SHALL BE ASSEMBLED USING AN APPROVED FLEXIBLE SEALANT IN JOINTS.
 - THE TONGUE AND GROOVE JOINT SHALL BE SEALED WITH ONE STRIP OF BUTYL RUBBER SEALANT.
 - "ELIMINATOR" OIL/WATER SEPARATOR SHALL BE INSTALLED TIGHT TO INSIDE OF CATCHBASIN.

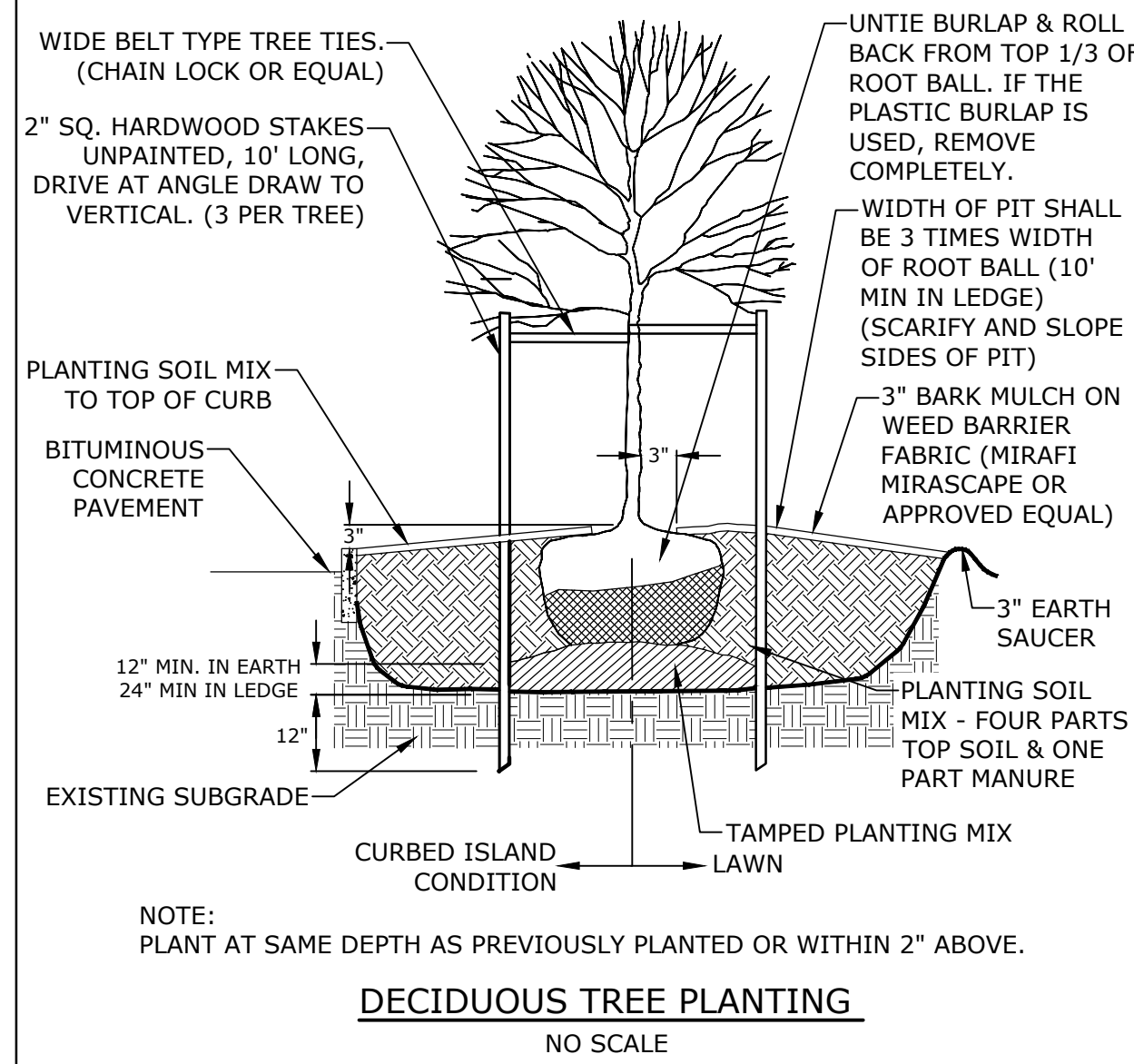


TREE PROTECTION FOR EXISTING TREE
NO SCALE



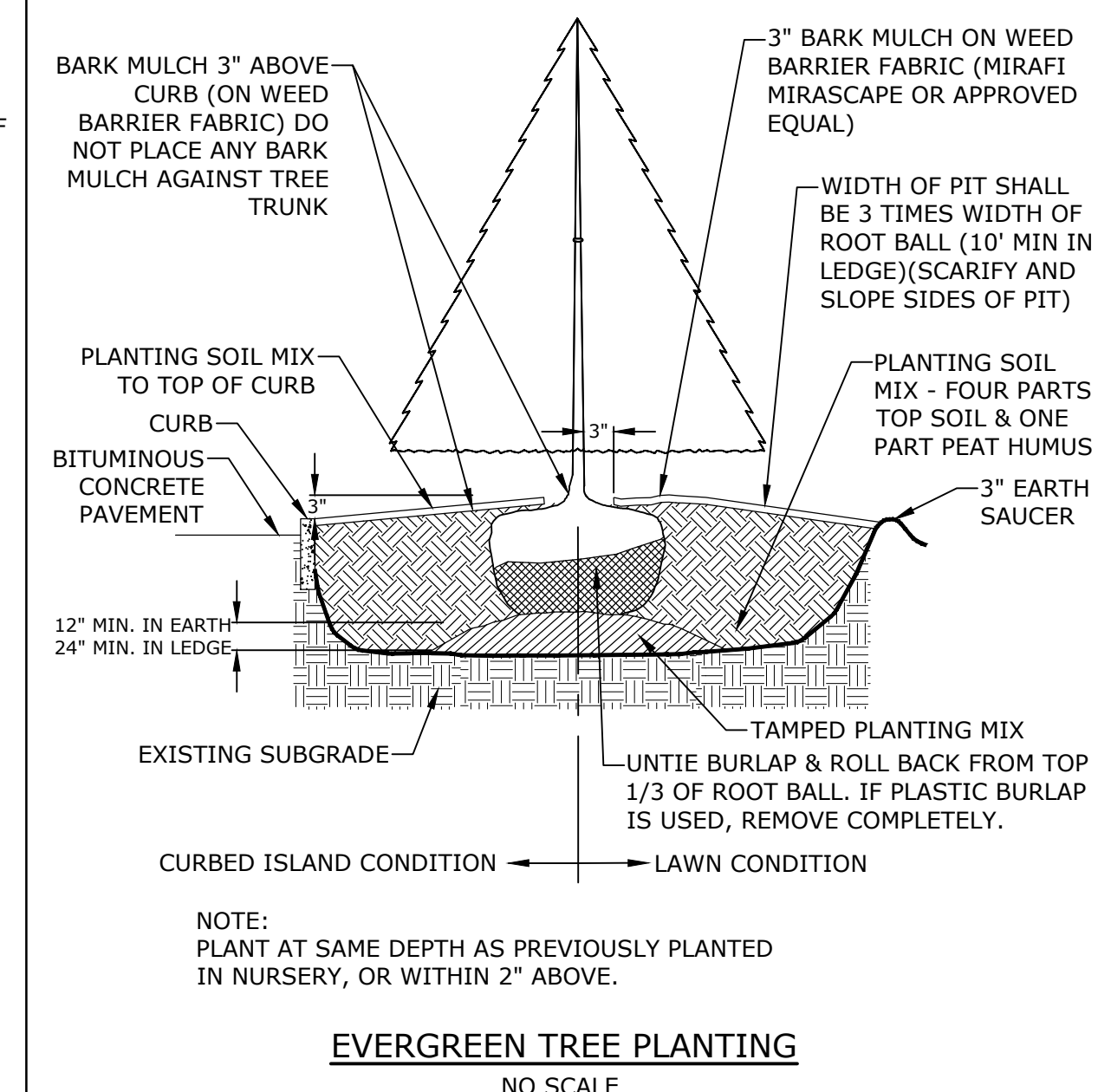
SHRUB PLANTING
NO SCALE

NOTE: PLANT AT SAME DEPTH AS PREVIOUSLY PLANTED, OR WITHIN 2" ABOVE.



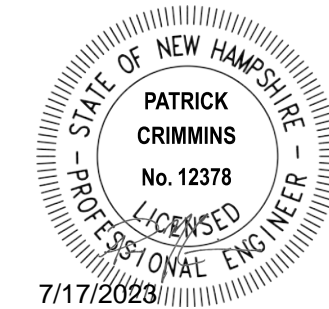
DECIDUOUS TREE PLANTING
NO SCALE

NOTE: PLANT AT SAME DEPTH AS PREVIOUSLY PLANTED OR WITHIN 2" ABOVE.



EVERGREEN TREE PLANTING
NO SCALE

NOTE: PLANT AT SAME DEPTH AS PREVIOUSLY PLANTED IN NURSERY, OR WITHIN 2" ABOVE.



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Lonza Biologics

Portsmouth, New Hampshire

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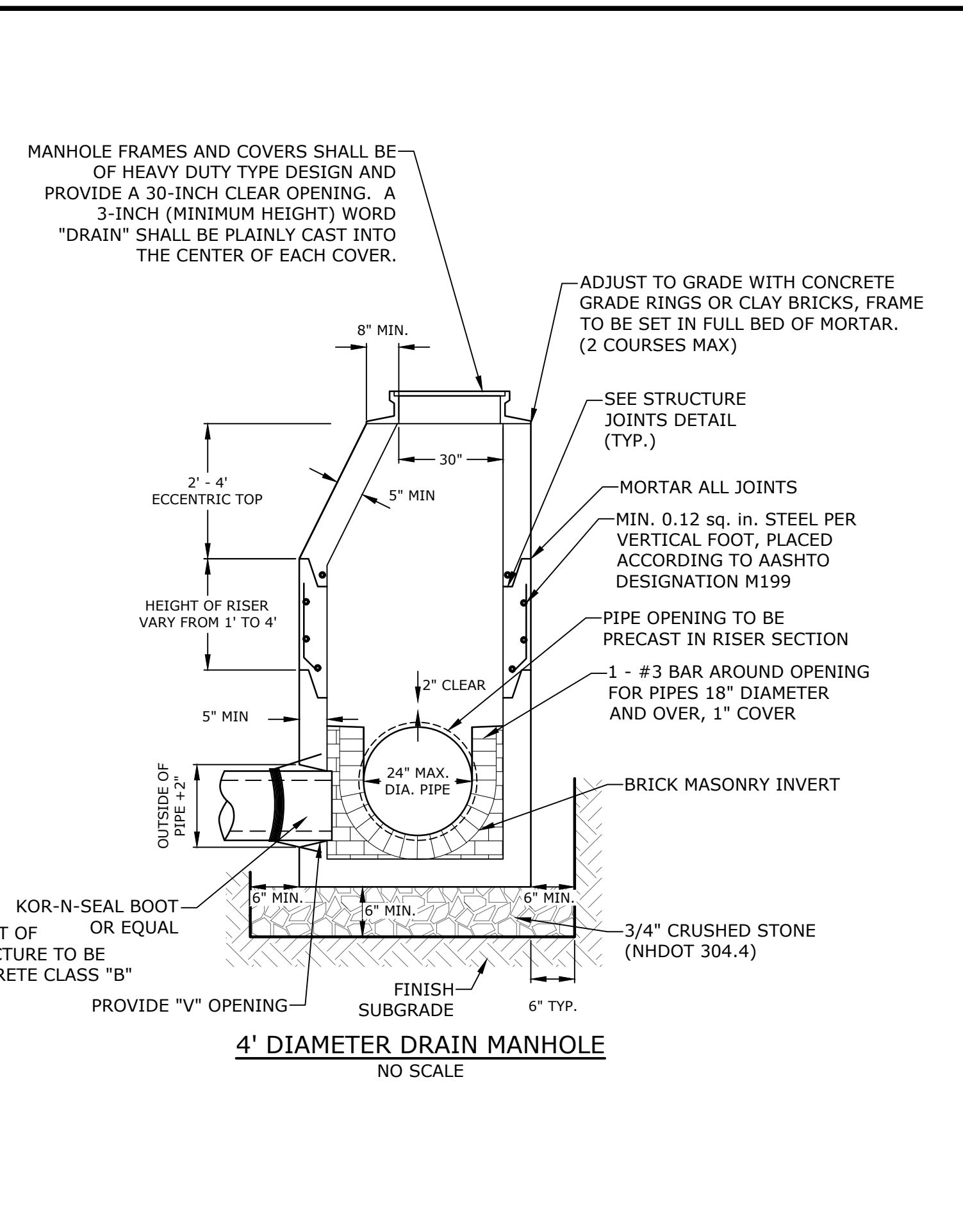
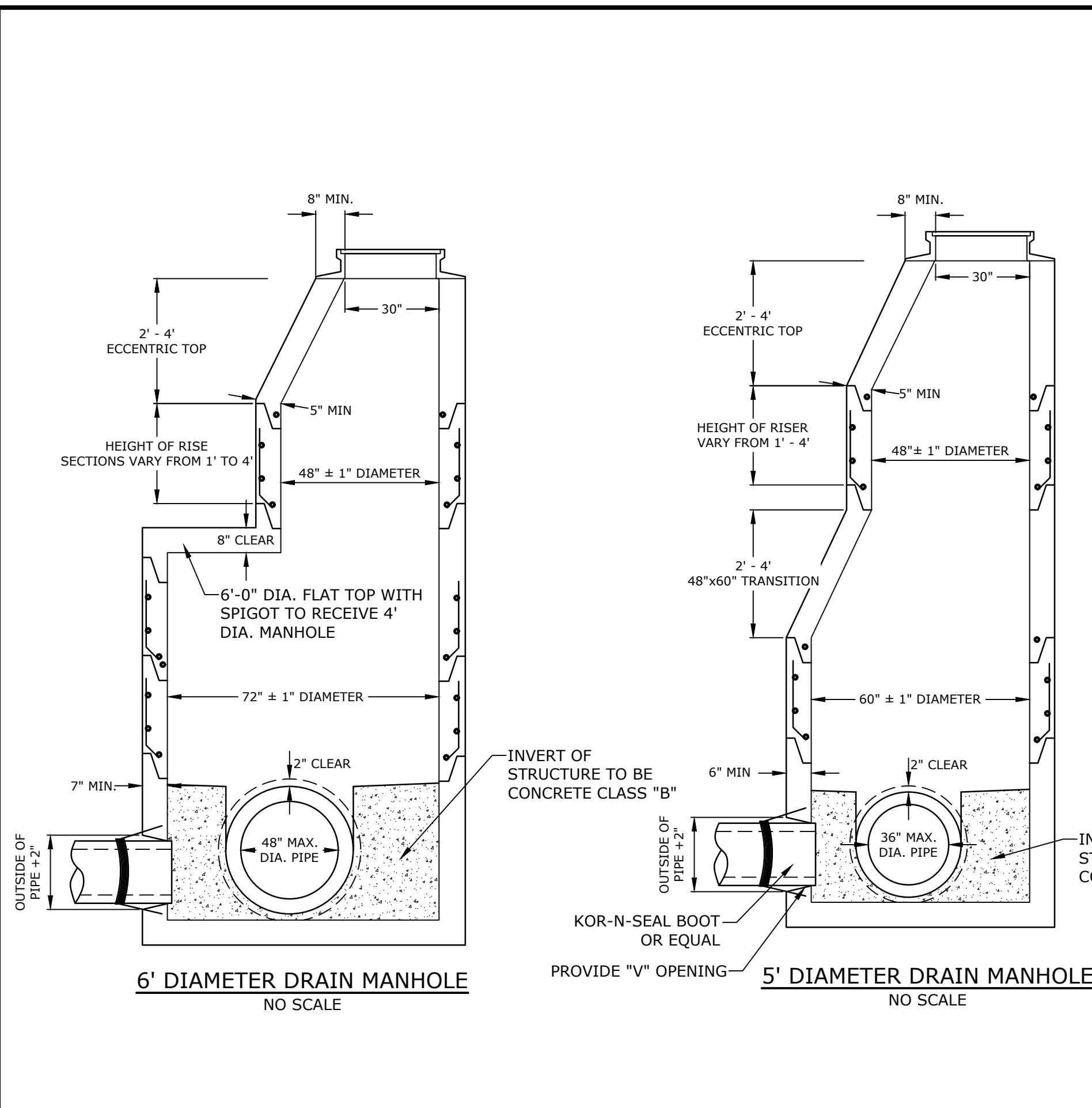
PROJECT NO: L-0700-013
 DATE: 04/03/2018
 FILE: L-0700-026-C-DTLS.dwg
 DRAWN BY: CJK
 CHECKED: NAH
 APPROVED: PMC

DETAILS SHEET

SCALE: AS SHOWN

C-504

Last Save Date: July 12, 2023 6:37 PM By: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
 Plot Location: J:\0700 Lonza Biologics Expansion.wa 12767026 - Project\Subarea Drawings\AutoCAD\0700-026-C-DTLS.dwg Layout: Tab: C-505

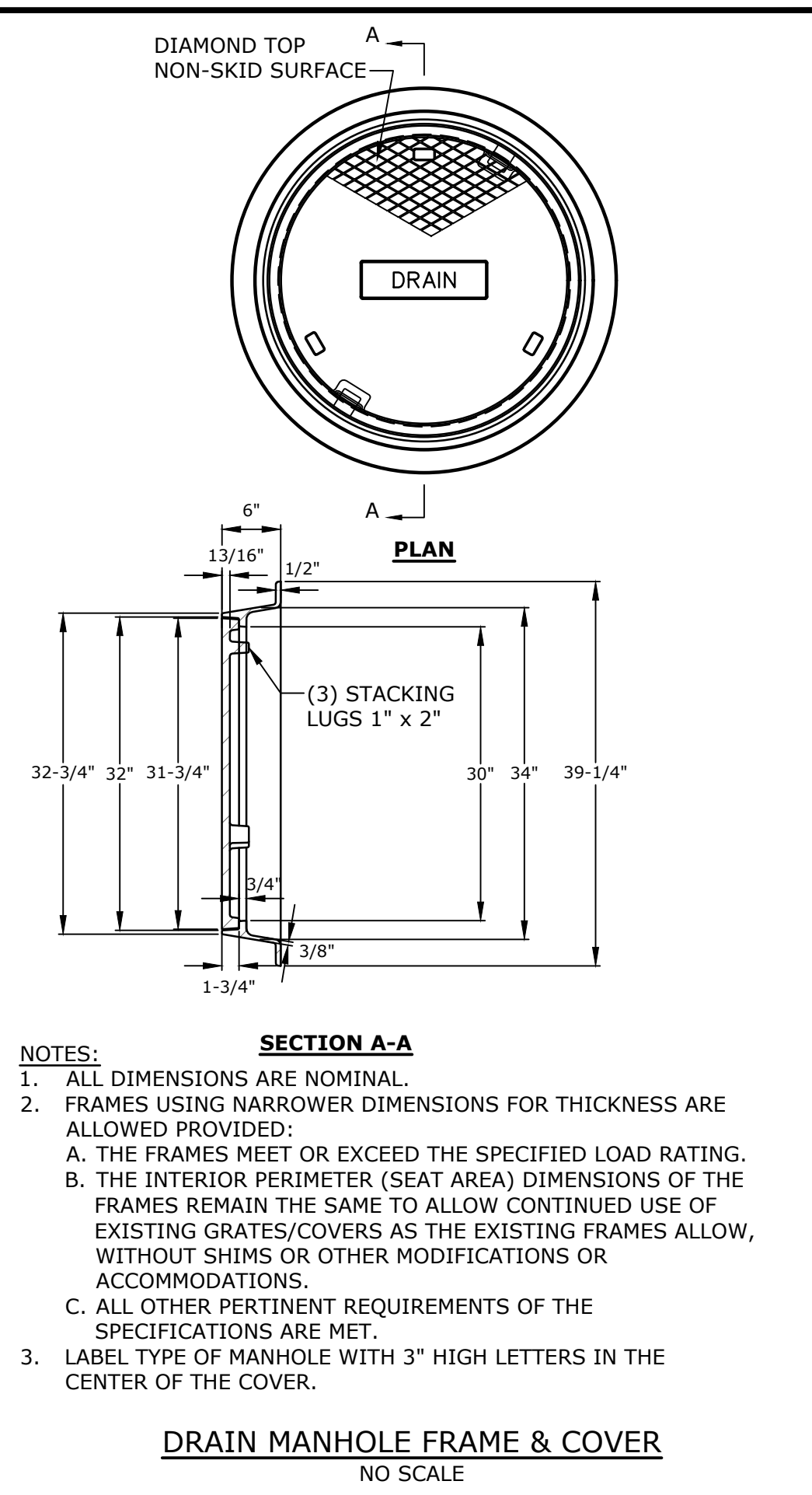


NOTES:

- ALL SECTIONS SHALL BE 4,000 PSI CONCRETE.
- CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQUARE INCHES PER LINEAR FOOT IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.
- THE TONGUE AND THE GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQUARE INCHES PER LINEAR FOOT.
- THE STRUCTURES SHALL BE DESIGNED FOR H20 LOADING.
- CONSTRUCT CRUSHED STONE BEDDING AND BACKFILL UNDER (6" MINIMUM THICKNESS)
- THE TONGUE AND GROOVE JOINT SHALL BE SEALED WITH ONE STRIP OF BUTYL RUBBER SEALANT.
- PIPE ELEVATIONS SHOWN ON PLANS SHALL BE FIELD VERIFIED PRIOR TO PRECASTING.
- OUTSIDE EDGES OF PIPES SHALL PROJECT NO MORE THAN 3" BEYOND INSIDE WALL OF STRUCTURE.
- PRECAST SECTIONS SHALL HAVE A TONGUE AND GROOVE JOINT 4" HIGH AT AN 11° ANGLE CENTERED IN THE WIDTH OF THE WALL AND SHALL BE ASSEMBLED USING AN APPROVED FLEXIBLE SEALANT IN JOINTS.
- ALL STRUCTURES WITH MULTIPLE PIPES SHALL HAVE A MINIMUM OF 12" OF INSIDE SURFACE BETWEEN HOLES, NO MORE THAN 75% OF A HORIZONTAL CROSS SECTION SHALL BE HOLES, AND THERE SHALL BE NO HOLES CLOSER THAN 3" TO JOINTS.

CORE HOLE SIZE			
PIPE SIZE	RCP CORE HOLE DIA.	PLASTIC CORE HOLE DIA.	
INCHES	INCHES	FEET	
6	18	1.5	7
12	22	1.8	18
15	26	2.2	24
18	34	2.8	32
24	42	3.5	42
30	48	4.0	48

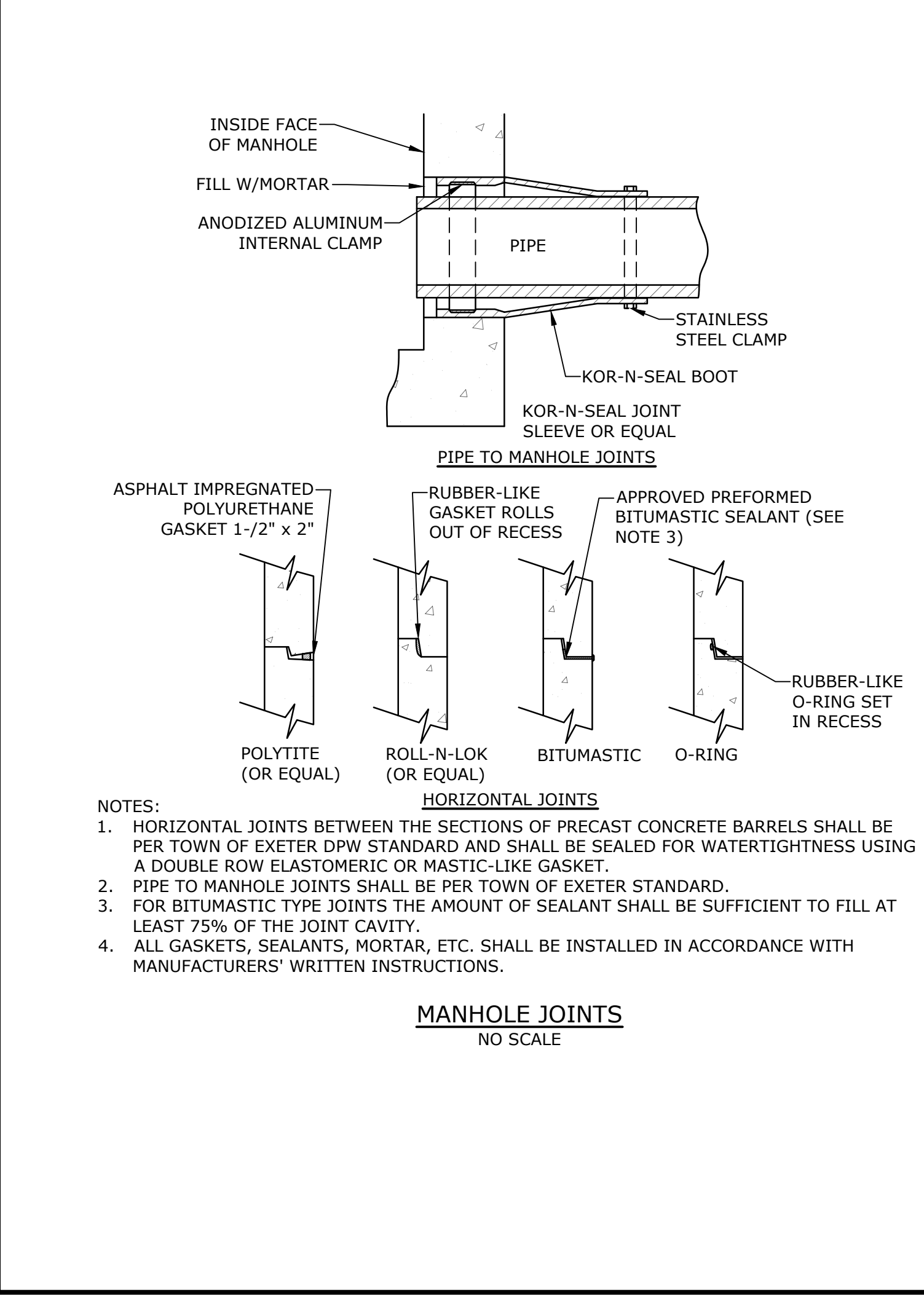
DIAMETER	WALL THICKNESS (MIN.)	FLOOR THICKNESS (MIN.)
4'	5"	6"
5'	6"	8"
6'	7"	8"



NOTES:

- ALL DIMENSIONS ARE NOMINAL.
- FRAMES USING NARROWER DIMENSIONS FOR THICKNESS ARE ALLOWED PROVIDED:
 - THE FRAMES MEET OR EXCEED THE SPECIFIED LOAD RATING.
 - THE INTERIOR PERIMETER (SEAT AREA) DIMENSIONS OF THE FRAMES REMAIN THE SAME TO ALLOW CONTINUED USE OF EXISTING GRATES/COVERS AS THE EXISTING FRAMES ALLOW, WITHOUT SHIMS OR OTHER MODIFICATIONS OR ACCOMMODATIONS.
 - ALL OTHER PERTINENT REQUIREMENTS OF THE SPECIFICATIONS ARE MET.
- LABEL TYPE OF MANHOLE WITH 3" HIGH LETTERS IN THE CENTER OF THE COVER.

DRAIN MANHOLE FRAME & COVER
NO SCALE



PIPE DIA.	S	B	H	L	W
12"	6.5"	10"	6.5"	25"	29"
15"	6.5"	10"	6.5"	25"	29"
18"	7.5"	15"	6.5"	32"	35"
24"	7.5"	18"	6.5"	36"	45"
30"	7.5"	12"	8.6"	58"	63"
36"	7.5"	25"	8.6"	58"	63"

NOTE:

- END SECTIONS MANUFACTURED BY ADVANCED DRAINAGE SYSTEMS, COLUMBUS, OHIO. END SECTIONS TO BE WELDED TO PIPE AS PER MANUFACTURER'S RECOMMENDATIONS.

HDPE END SECTION
NO SCALE

NOTE:

- GRATE TO BE CAST IRON (NHDOT TYPE B)
- FRAME AND GRATE TO BE MANUFACTURED IN THE USA

CATCH BASIN FRAME & GRATE
NO SCALE

NOTE:

- FRAME AND GRATES SHALL BE EJ FOUNDRY OR APPROVED EQUAL.
- MATERIAL SHALL BE CLASS 30B GRAY IRON AND SHALL COMPLY WITH ALTEST ASTM A48.
- FRAME AND GRATES SHALL BE HEAVY DUTY AND RATED FOR H-20 LOADING.
- 3 FLANGE FRAMES TO BE USED WITH CURB INLET.

DOUBLE CATCHBASIN FRAME & GRATE
NO SCALE

Tighe & Bond

STATE OF NEW HAMPSHIRE
PATRICK CRIMMINS
No. 12378
LICENSED PROFESSIONAL ENGINEER
7/17/2023

STATE OF NEW HAMPSHIRE
NEIL A. HANSEN
No. 15227
LICENSED PROFESSIONAL ENGINEER
7/17/2023

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

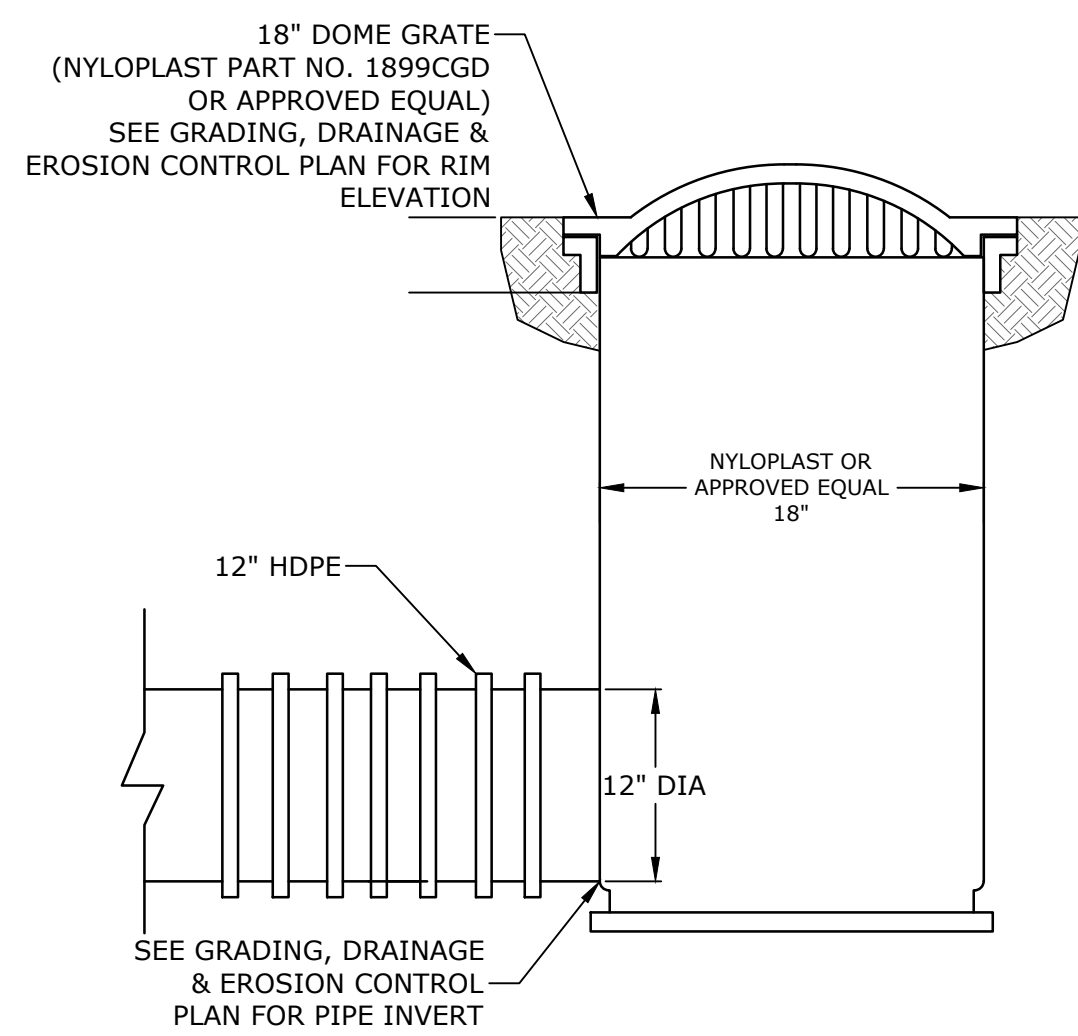
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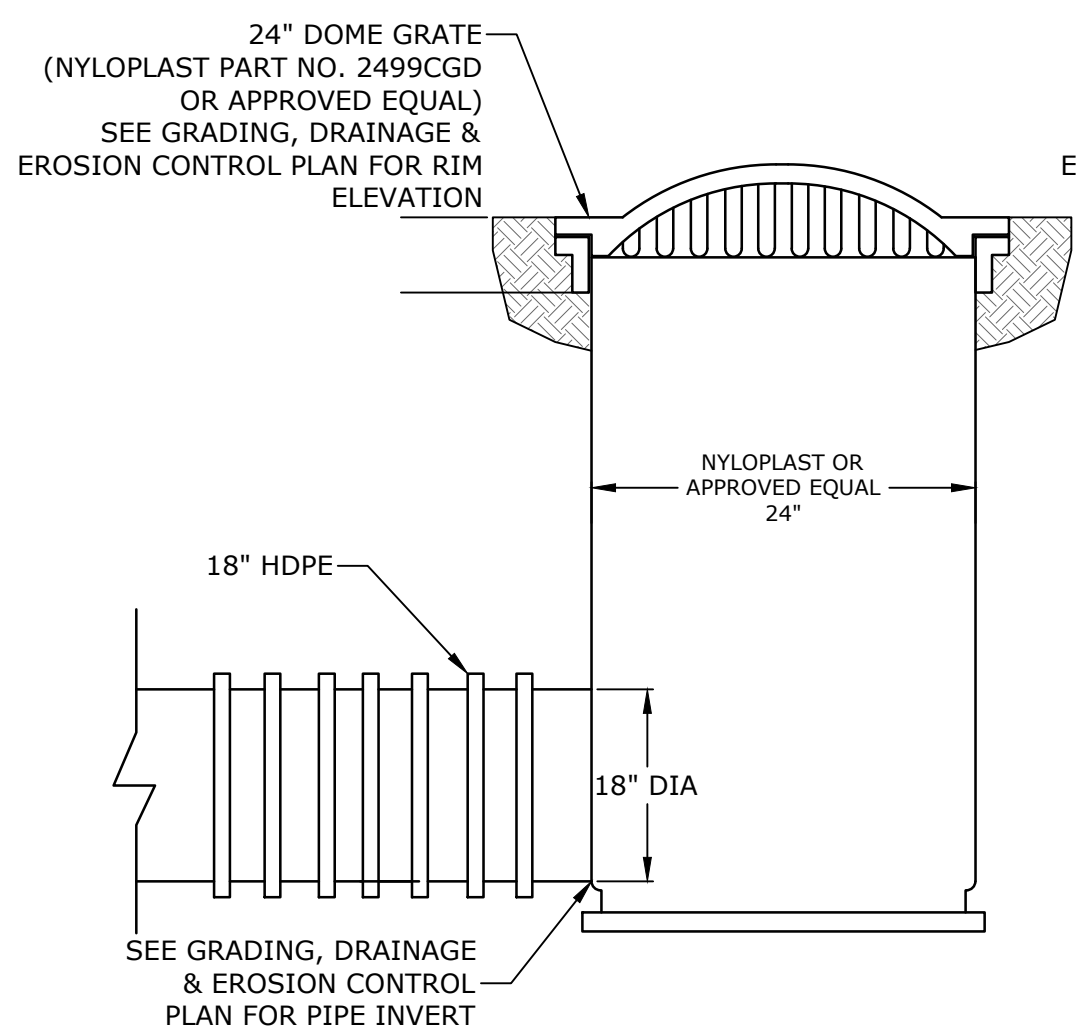
DETAILS SHEET

SCALE: AS SHOWN

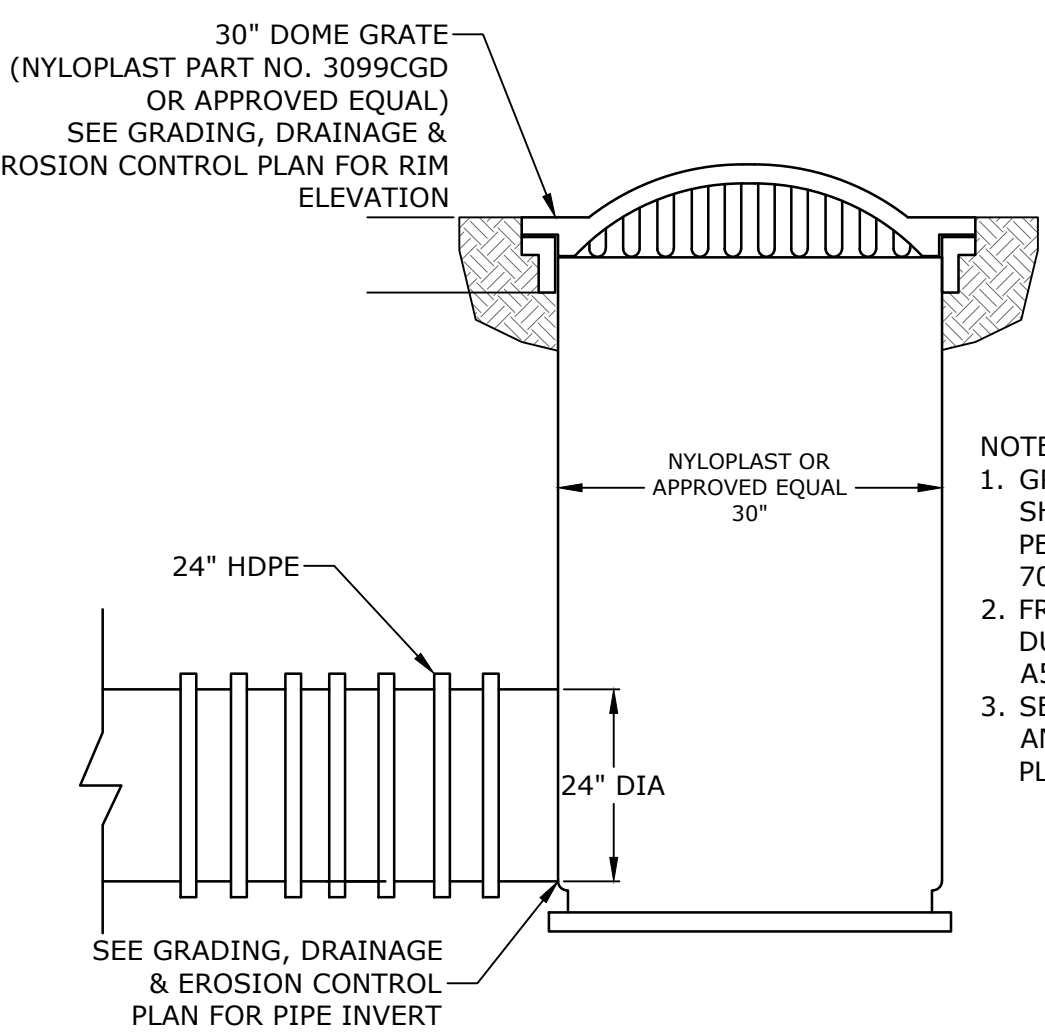
C-505



PYD100, PYD104, PYD104, PYD200, PYD201, PYD301, PYD302, PYD303, & PYD304
NO SCALE



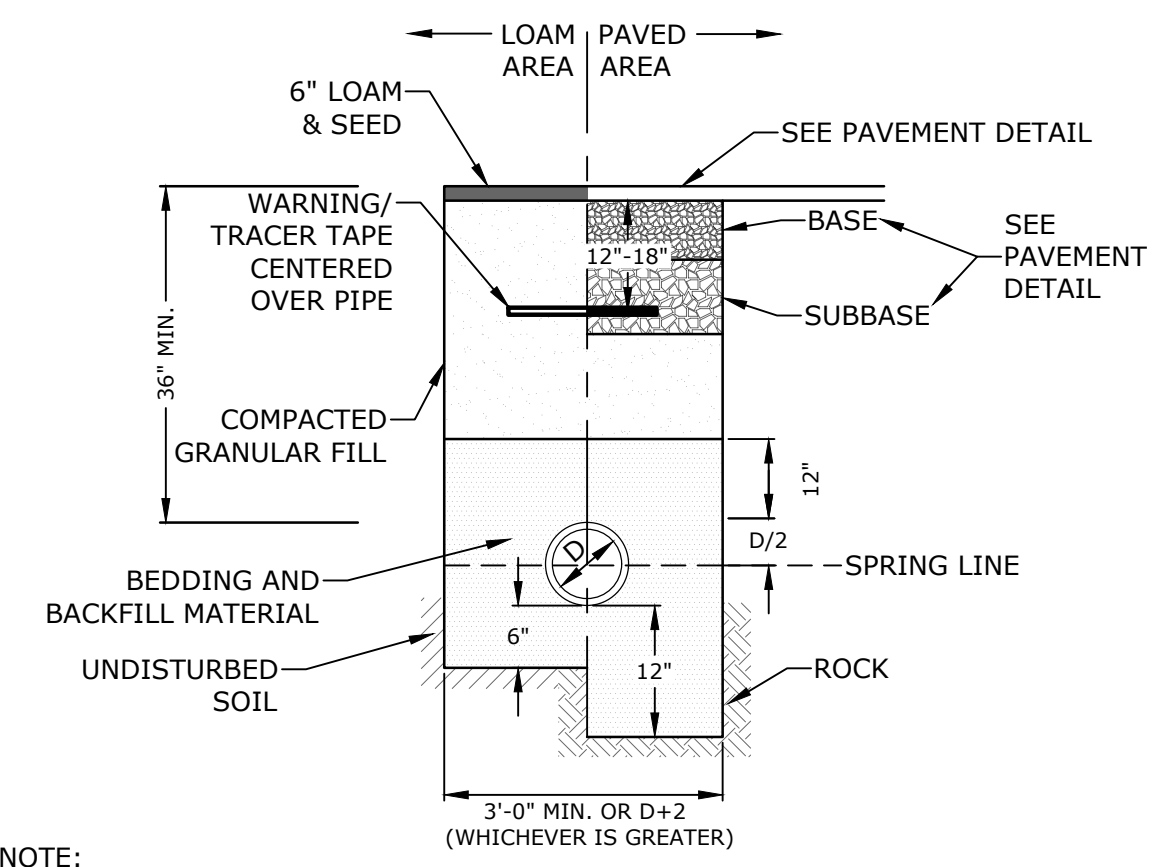
PYD101
NO SCALE



PYD102 & PYD103
NO SCALE

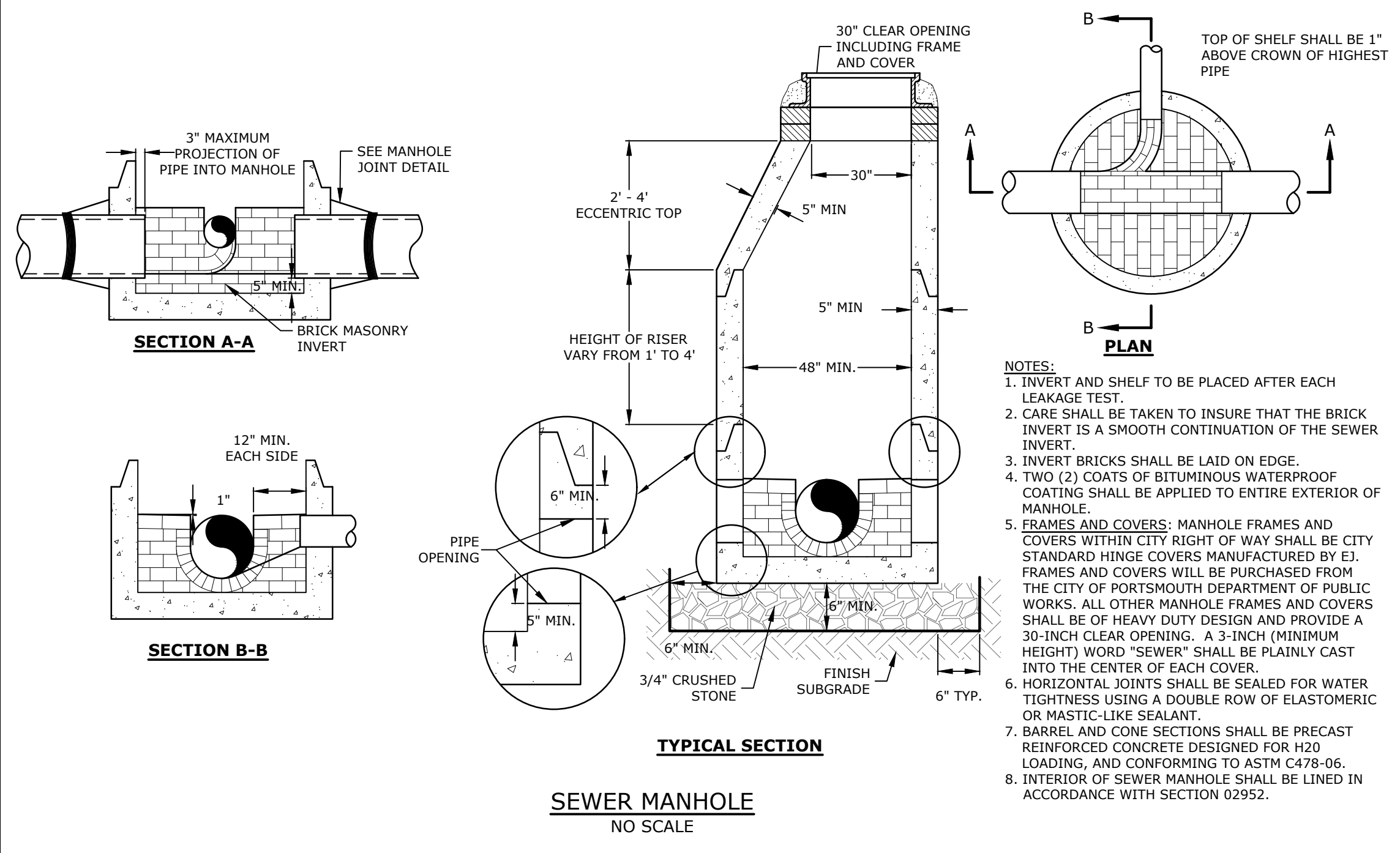
- NOTES:**
1. GRATES/SOLID COVER SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05.
 2. FRAMES SHALL BE DUCTILE IRON PER ASTM A536 GRADE 70-50-05
 3. SEE GRADING, DRAINAGE AND EROSION CONTROL PLAN FOR LOCATION.

PROPOSED YARD DRAINS
NO SCALE

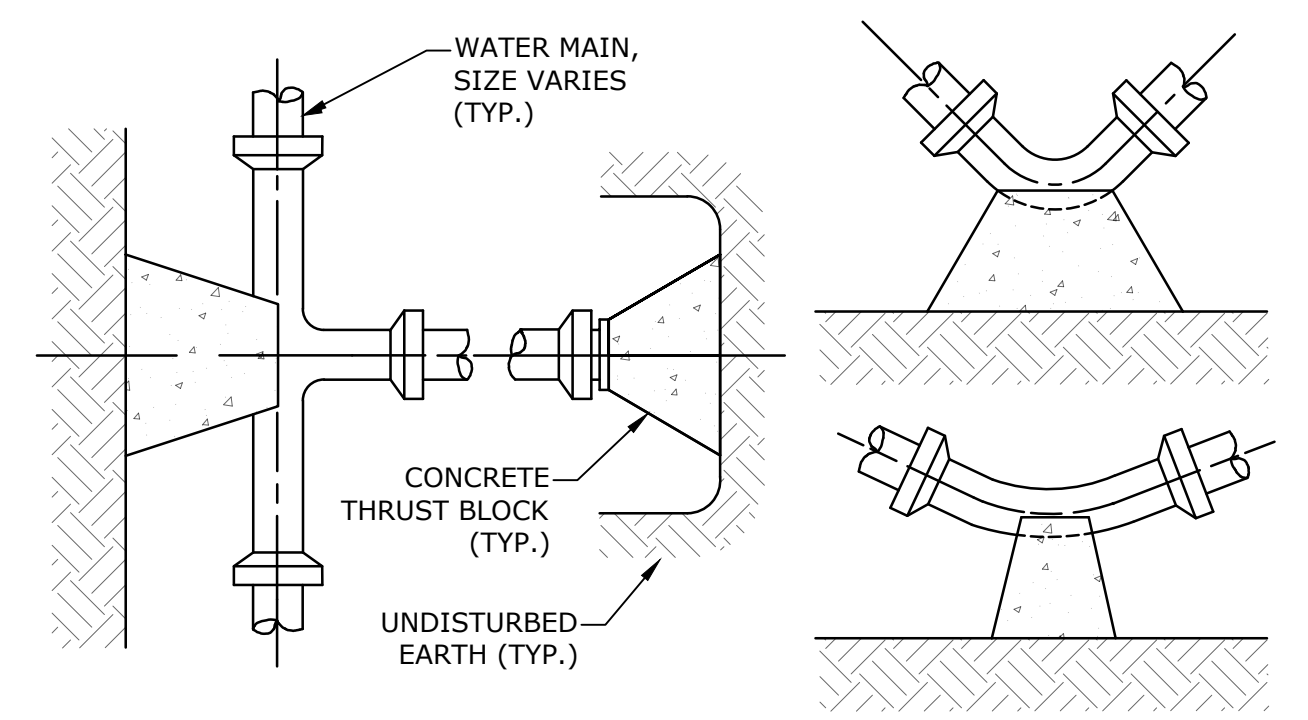


- NOTE:**
1. SAND BEDDING AND BACKFILL FOR FULL WIDTH OF THE TRENCH FROM 6" BELOW PIPE IN EARTH AND 12" BELOW PIPE IN ROCK UP TO 12" ABOVE TOP OF PIPE.
 2. GAS SHALL BE INSTALLED PER UNITIL STANDARDS. COORDINATE ALL INSTALLATIONS WITH UNITIL AND THE CITY OF PORTSMOUTH.

GAS TRENCH
NO SCALE



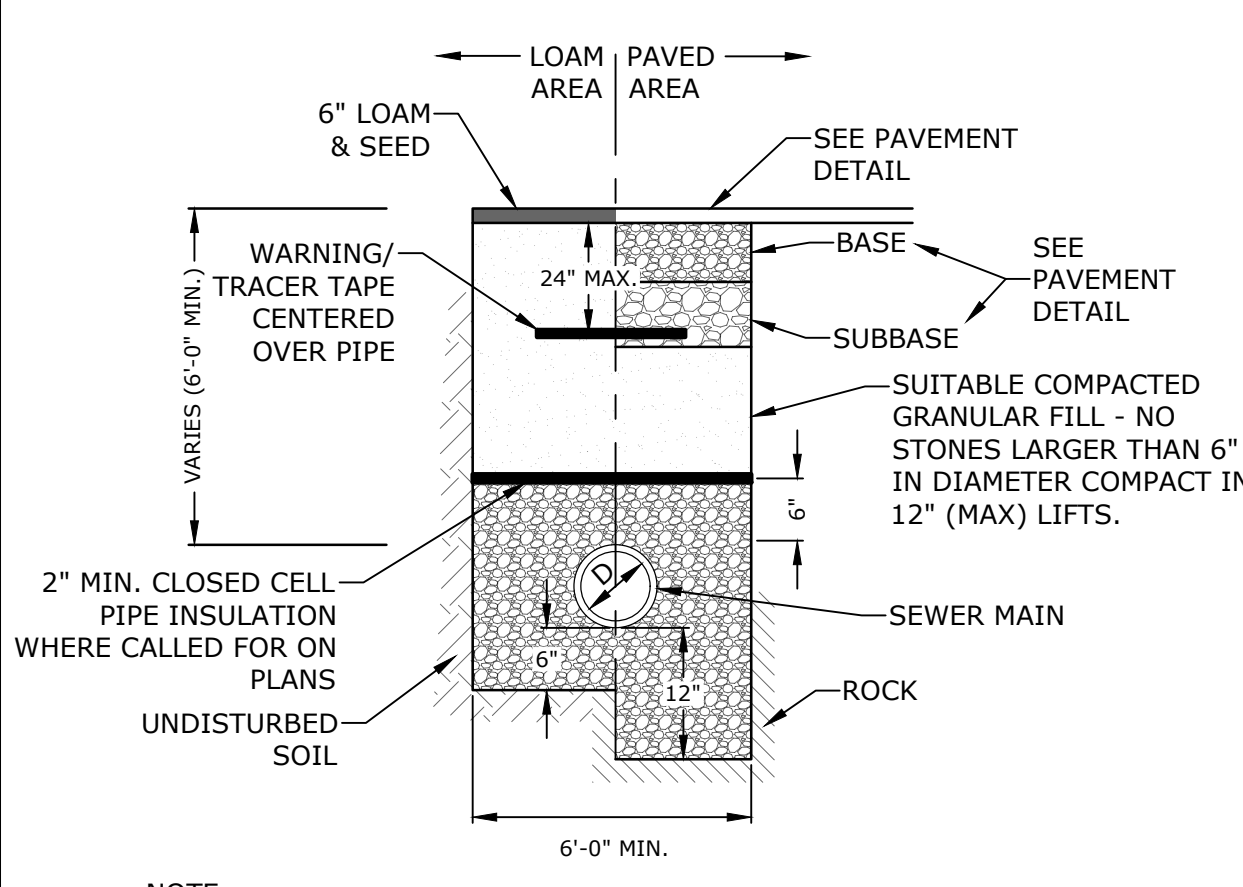
SEWER MANHOLE
NO SCALE



THRUST BLOCKING DETAIL
NO SCALE

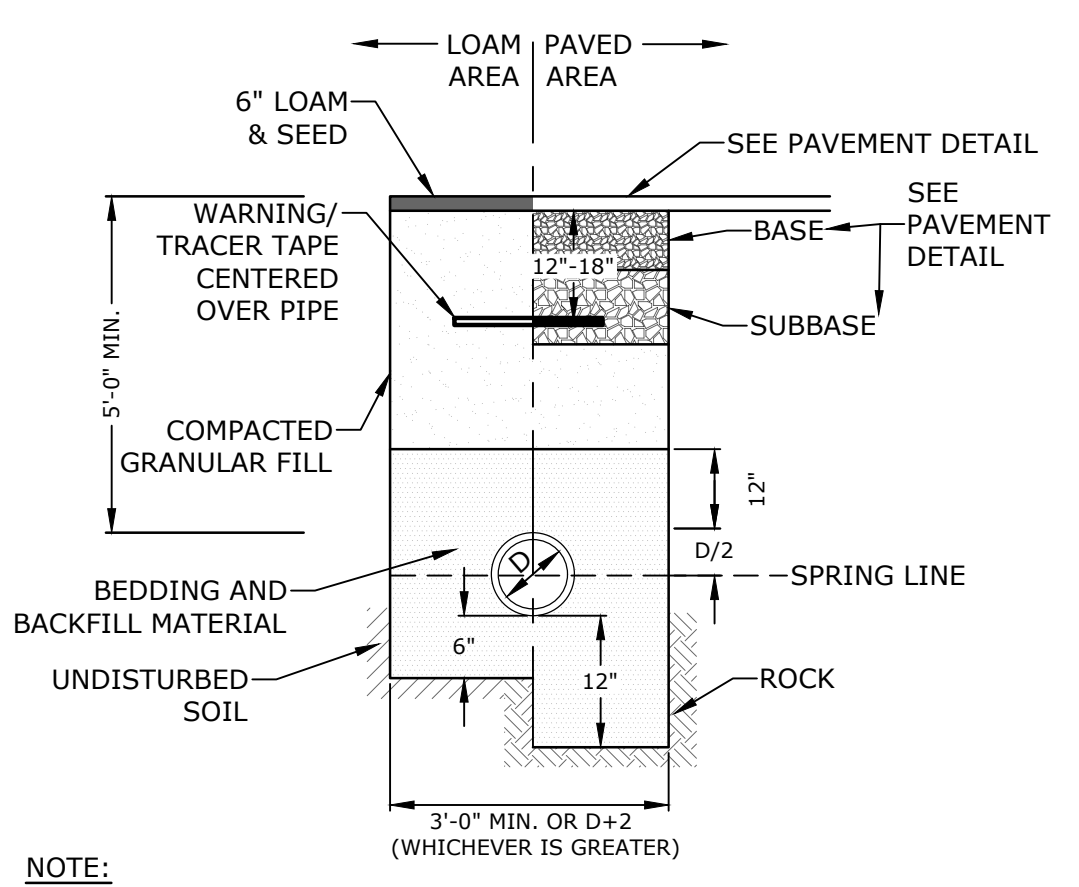
REACTION TYPE	PIPE SIZE			
	4"	6"	8"	12"
A 90°	0.89	2.19	3.82	11.14
B 180°	0.65	1.55	2.78	8.38
C 45°	0.48	1.19	2.12	6.02
D 22-1/2°	0.25	0.60	1.06	3.08
E 11-1/4°	0.13	0.30	0.54	1.54

- NOTES:**
1. POUR THRUST BLOCKS AGAINST UNDISTURBED MATERIAL, WHERE TRENCH WALL HAS BEEN DISTURBED, EXCAVATE LOOSE MATERIAL AND EXTEND THRUST BLOCK TO UNDISTURBED MATERIAL. NO JOINTS SHALL BE COVERED WITH CONCRETE.
 2. ON BENDS AND TEES, EXTEND THRUST BLOCKS FULL LENGTH OF FITTING.
 3. PLACE BOARD IN FRONT OF ALL PLUGS BEFORE POURING THRUST BLOCKS.
 4. WHERE M.J. PIPE IS USED, M.J. PLUG WITH RETAINER GLAND MAY BE SUBSTITUTED FOR END BLOCKINGS.
 5. INSTALLATION AND STANDARD DIMENSIONAL REQUIREMENTS SHALL BE WITH TOWN OF EXETER WATER DEPARTMENT STANDARDS.



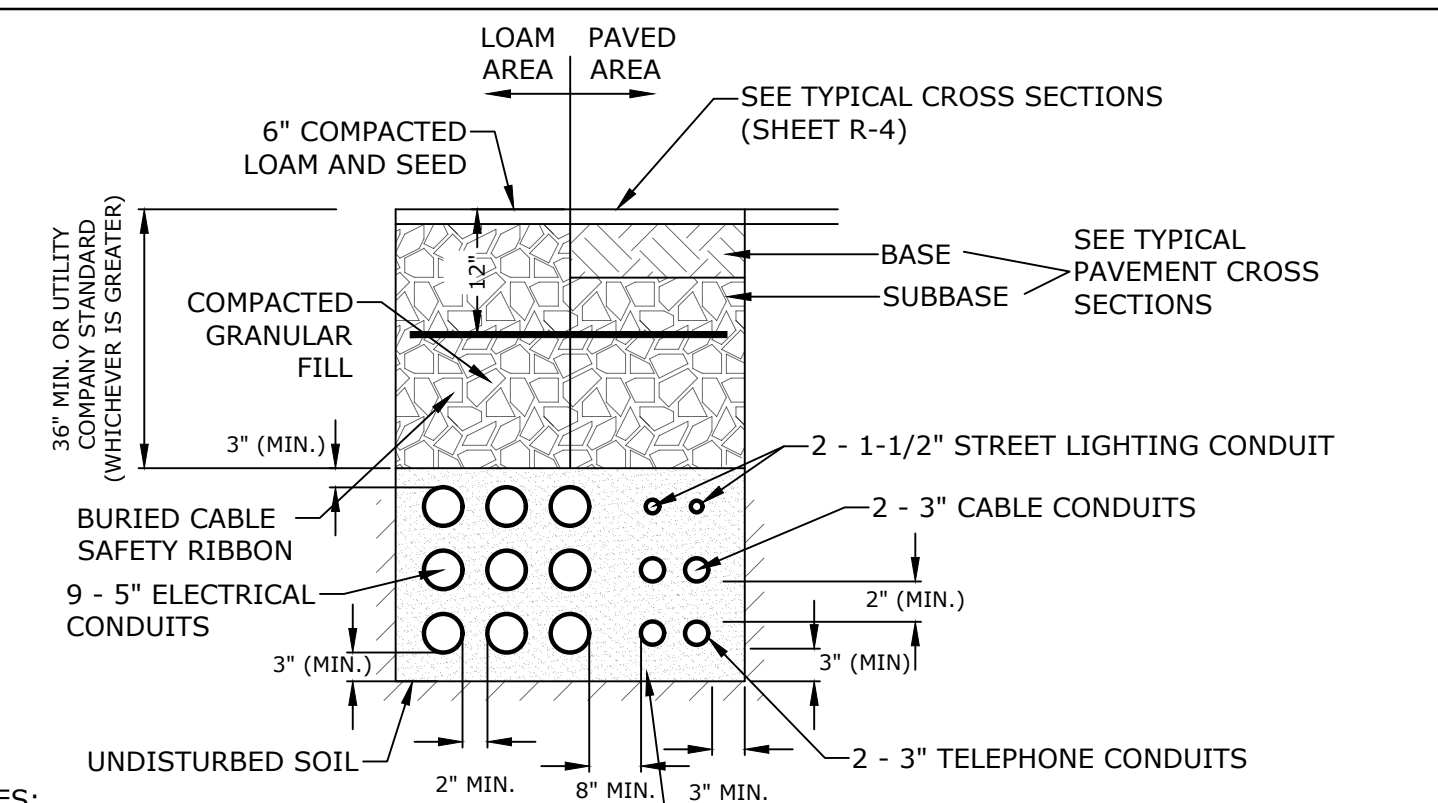
SEWER TRENCH
NO SCALE

- NOTE:**
1. COORDINATE ALL INSTALLATIONS WITH THE CITY OF PORTSMOUTH.



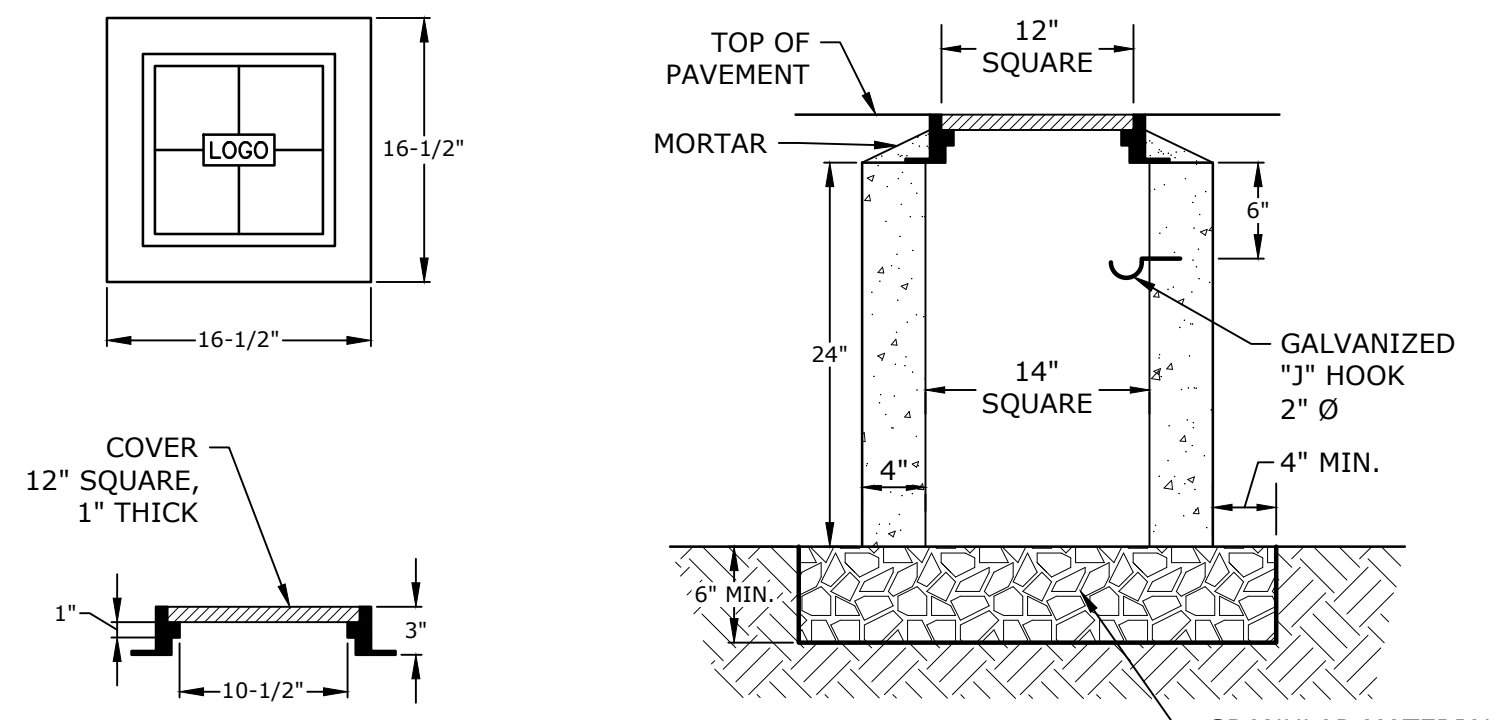
WATER TRENCH
NO SCALE

- NOTE:**
1. SAND BEDDING AND BACKFILL FOR FULL WIDTH OF THE TRENCH FROM 6" BELOW PIPE IN EARTH AND 12" BELOW PIPE IN ROCK UP TO 12" ABOVE TOP OF PIPE.
 2. WATER MAIN SHALL BE INSTALLED PER CITY OF PORTSMOUTH STANDARDS. COORDINATE ALL INSTALLATIONS WITH THE CITY OF PORTSMOUTH.



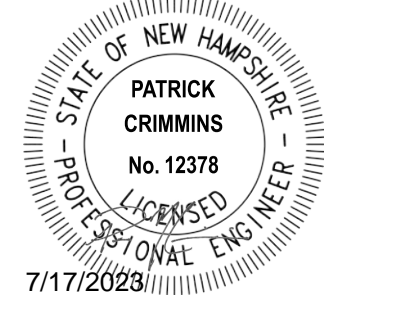
ELECTRICAL AND COMMUNICATION CONDUIT
NO SCALE

- NOTES:**
1. NUMBER, MATERIAL, AND SIZE OF UTILITY CONDUITS SHALL BE DETERMINED BY LOCAL UTILITY OR AS SHOWN ON ELECTRICAL DRAWINGS. CONTRACTOR TO PROVIDE ONE SPARE CONDUIT FOR EACH UTILITY TO BUILDING.
 2. DIMENSIONS SHOWN REPRESENT OWNERS MINIMUM REQUIREMENTS. ACTUAL DIMENSIONS MAY BE GREATER BASED ON UTILITY COMPANY STANDARDS, BUT SHALL NOT BE LESS THAN THOSE SHOWN.
 3. NO CONDUIT RUN SHALL EXCEED 360 DEGREES IN TOTAL BENDS.
 4. A SUITABLE PULLING STRING, CAPABLE OF 200 POUNDS OF PULL, MUST BE INSTALLED IN THE CONDUIT BEFORE UTILITY COMPANY IS NOTIFIED TO INSTALL CABLE. THE STRING SHOULD BE BLOWN INTO THE CONDUIT AFTER THE RUN IS ASSEMBLED TO AVOID BONDING THE STRING TO THE CONDUIT.
 5. UTILITY COMPANY MUST BE GIVEN THE OPPORTUNITY TO INSPECT THE CONDUIT PRIOR TO BACKFILL. THE CONTRACTOR IS RESPONSIBLE FOR ALL REPAIRS SHOULD THE UTILITY COMPANY BE UNABLE TO INSTALL ITS CABLE IN A SUITABLE MANNER.
 6. ALL CONDUIT INSTALLATIONS MUST CONFORM TO THE CURRENT EDITION OF THE NATIONAL ELECTRIC SAFETY CODE, STATE AND LOCAL CODES AND ORDINANCES, AND, WHERE APPLICABLE, THE NATIONAL ELECTRIC CODE.
 7. ALL 90° SWEEPS WILL BE MADE USING RIGID GALVANIZED STEEL. SWEEPS WITH A 36 TO 48 INCH RADIUS.
 8. SAND BEDDING TO BE REPLACED WITH CONCRETE ENCASEMENT WHERE COVER IS LESS THAN 3 FEET, WHEN LOCATED BELOW PAVEMENT, OR WHERE SHOWN ON THE UTILITIES PLAN. COORDINATE LIMITS OF CONCRETE ENCASEMENT WITH EVERSOURCE.



CONCRETE LIGHTING CONDUIT PULL BOX
NO SCALE

- NOTES:**
1. 14" X 14" CONCRETE PULL BOX, NHDOT ITEM 614.511



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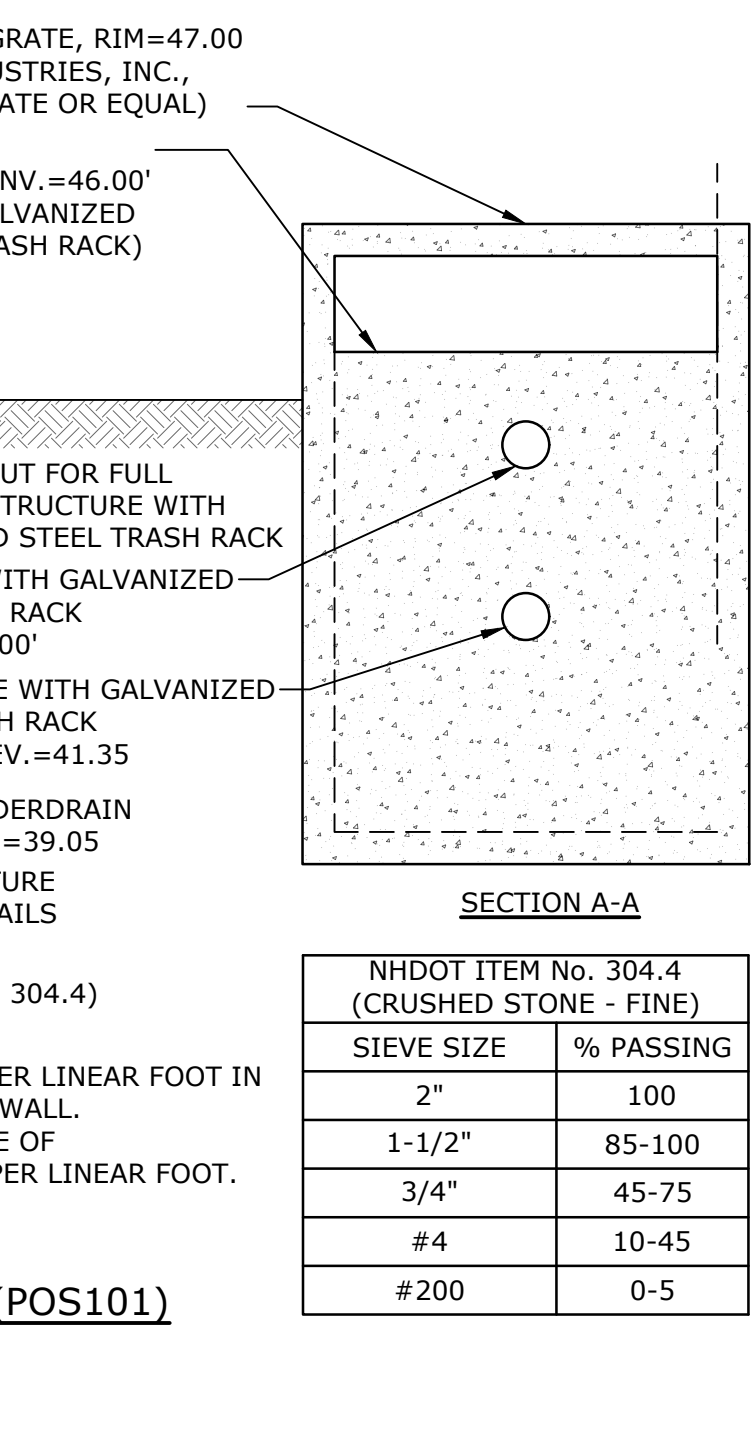
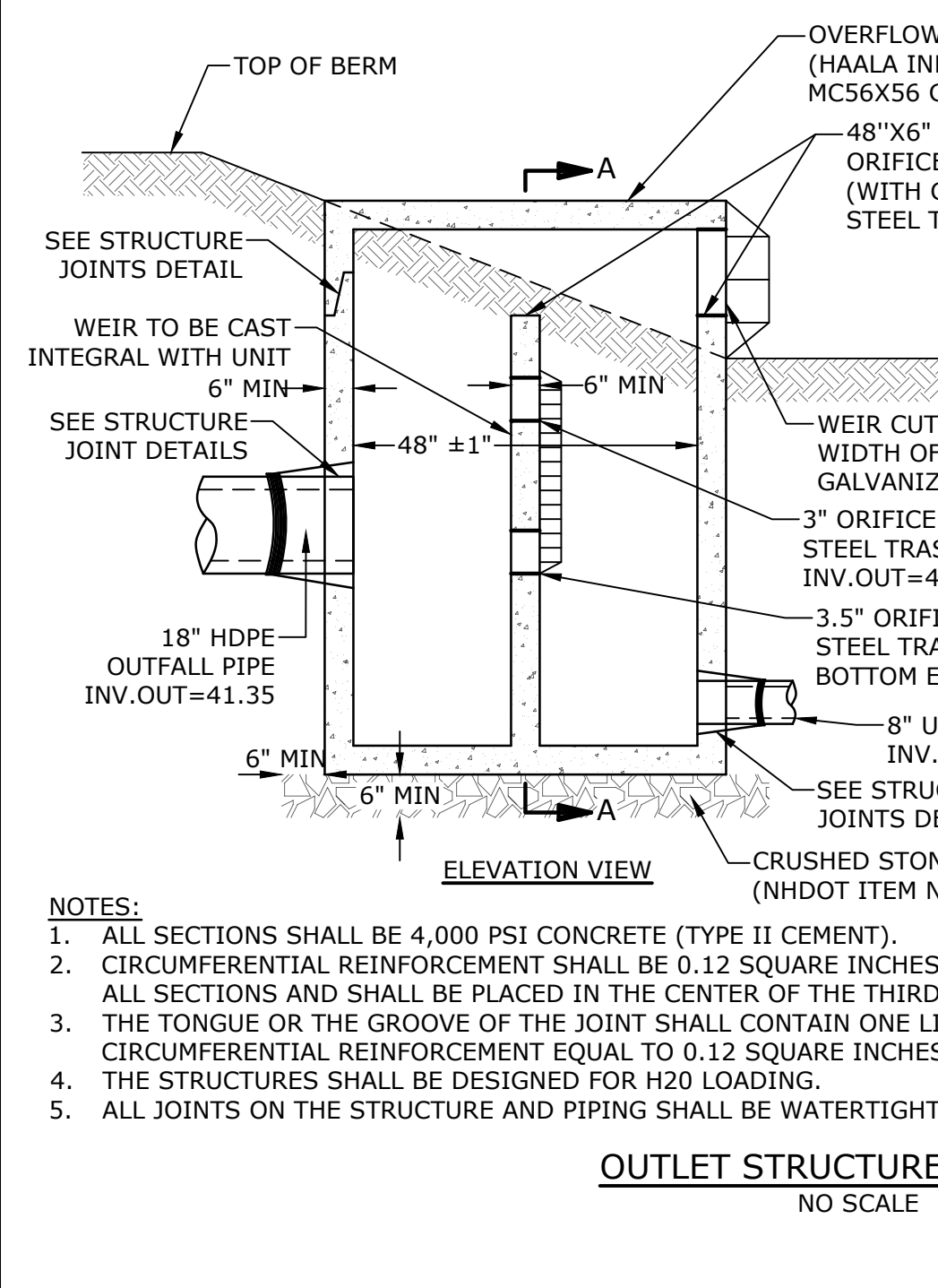
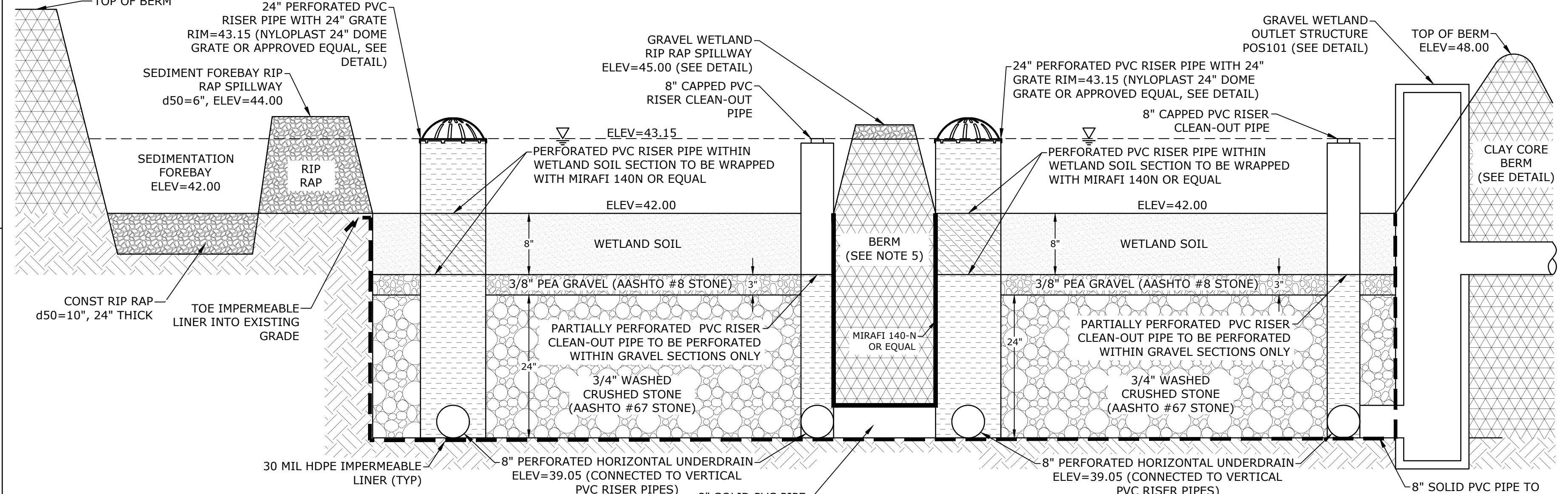
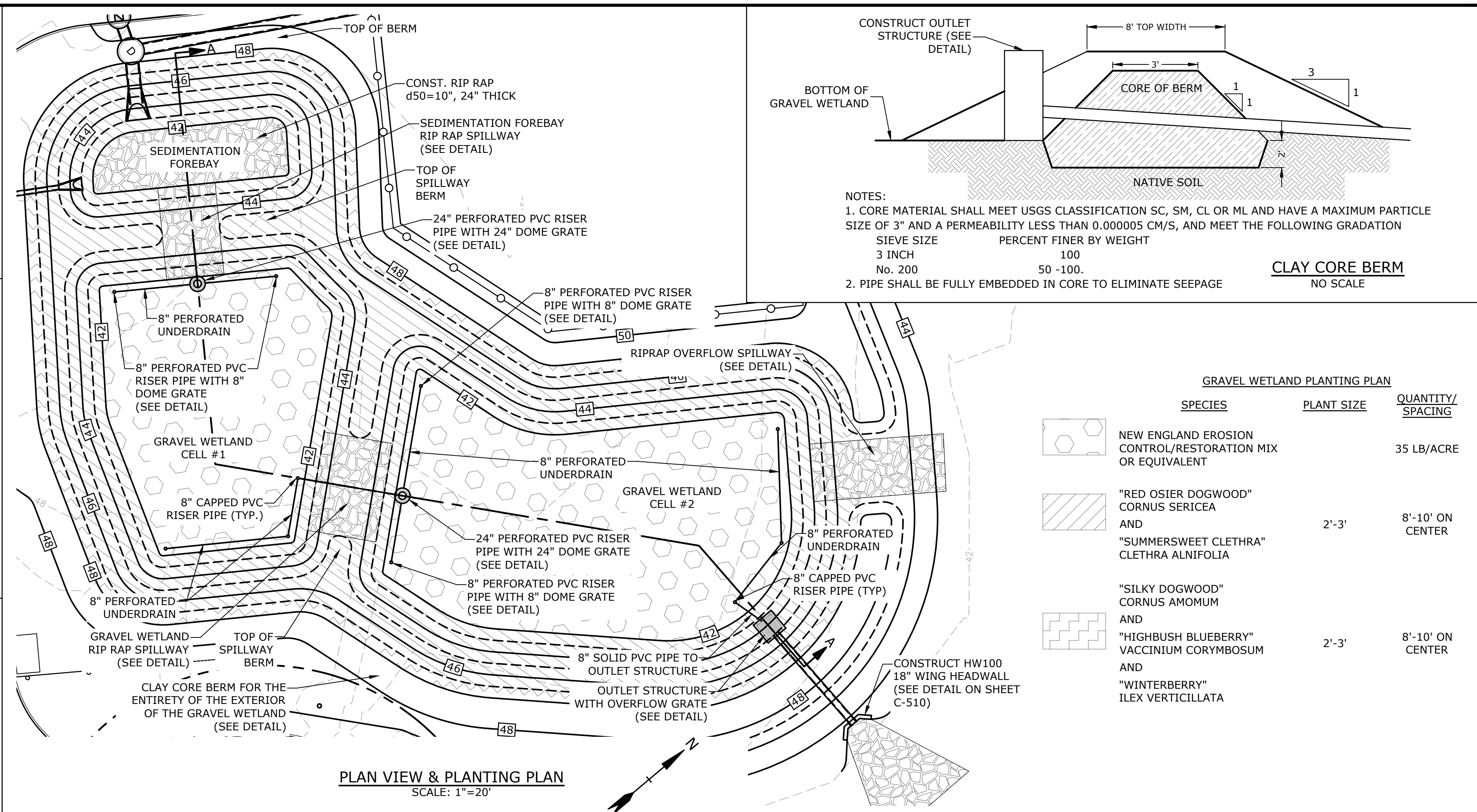
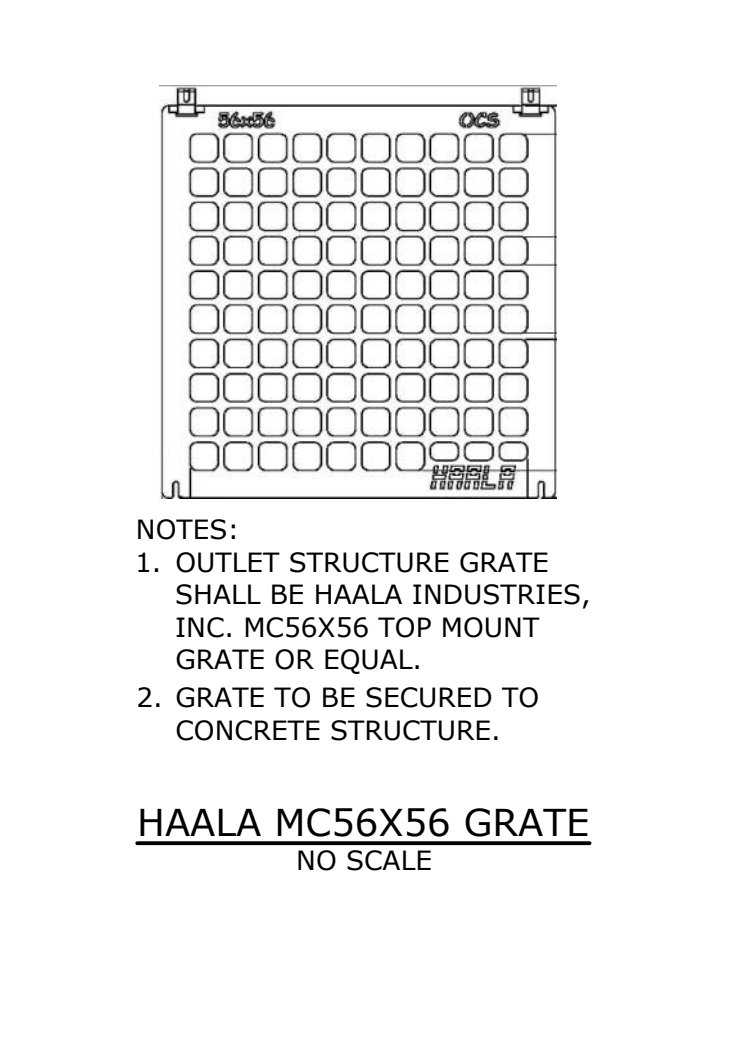
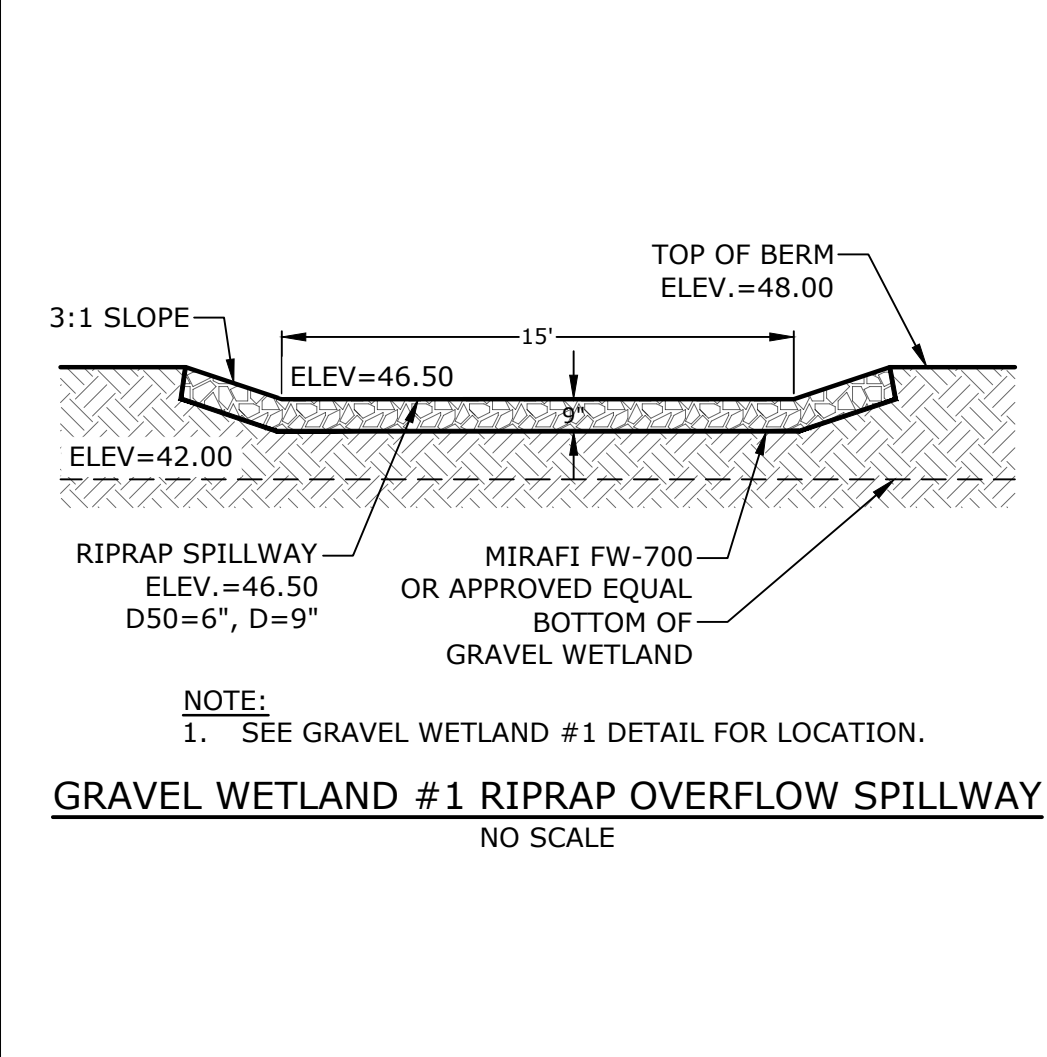
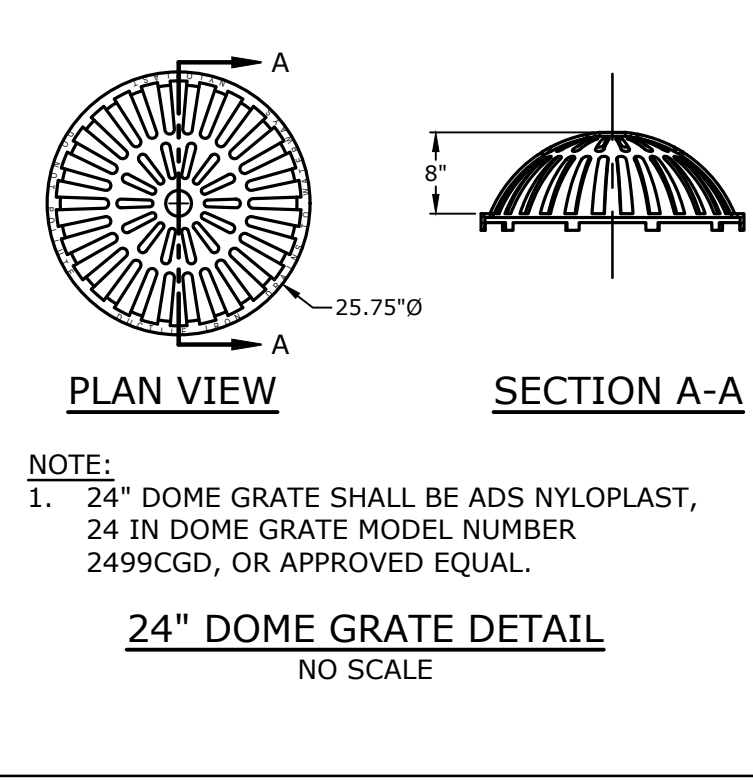
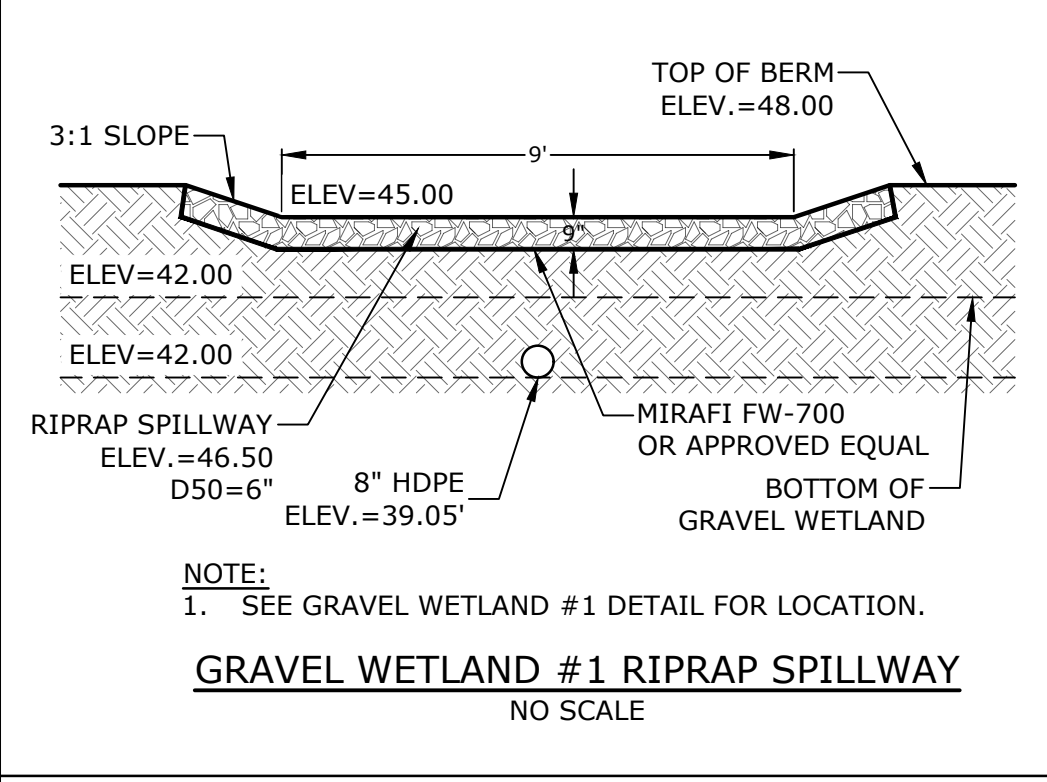
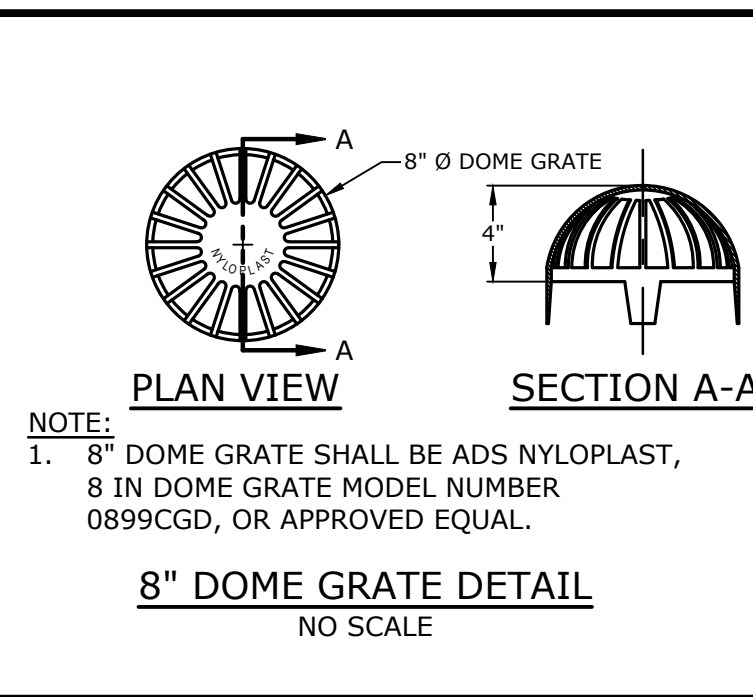
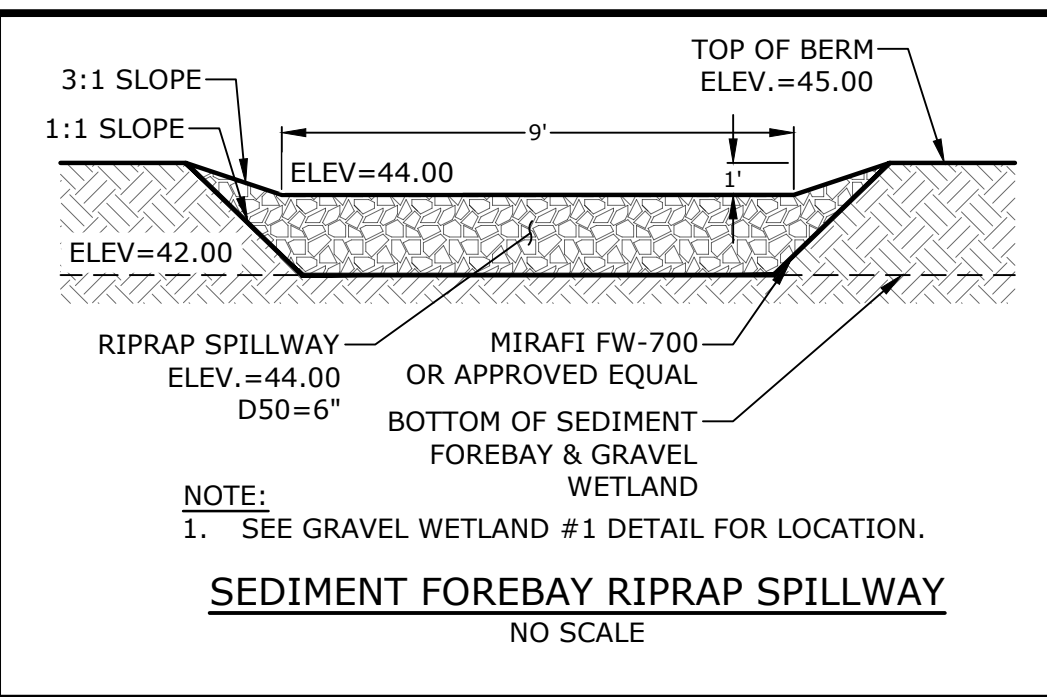
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DETAILS SHEET

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GRAVEL WETLAND INSPECTION / MAINTENANCE REQUIREMENTS

INSPECTION / MAINTENANCE	FREQUENCY	ACTION
MONITOR TO ENSURE THAT GRAVEL WETLAND FUNCTIONS EFFECTIVELY AFTER STORMS	FOUR (4) TIMES ANNUALLY (QUARTERLY) AND AFTER ANY RAINFALL EVENT EXCEEDING 2.5" IN A 24-HR PERIOD	- TRASH AND DEBRIS TO BE REMOVED - ANY REQUIRED MAINTENANCE SHALL BE ADDRESSED - INSPECT SOIL AND REPAIR ERODED AREAS, ESPECIALLY ON SLOPES. - CHECK INLETS, OUTLETS, AND OVERFLOW SPILLWAY FOR BLOCKAGE, STRUCTURAL INTEGRITY AND EVIDENCE OF EROSION.
INSPECT VEGETATION	ANNUALLY	- INSPECT THE CONDITION OF ALL GRAVEL WETLAND VEGETATION - PRUNE BACK OVERGROWTH - REPLACE DEAD VEGETATION - REMOVE ANY INVASIVE SPECIES - COORDINATE WITH UNH STORMWATER CENTER FOR FURTHER VEGETATION MANAGEMENT GUIDELINES
INSPECT DRAWDOWN TIME	ANNUALLY	- HIRE QUALIFIED PROFESSIONAL TO ASSESS THE CONDITION OF THE FACILITY TO DETERMINE MEASURES REQUIRED TO RESTORE THE FILTRATION FUNCTION, INCLUDING BUT NOT LIMITED TO REMOVAL OF ACCUMULATED SEDIMENTS OR RECONSTRUCTION OF THE FILTER.

NOTES:

- WETLAND SOIL SHALL BE A SANDY CLAY LOAM WITH A HYDRAULIC CONDUCTIVITY OF 0.1-0.01 FT/DAY. ORGANIC CONTENT SHALL BE GREATER THAN 15% BY VOLUME. CLAY CONTENT SHALL BE LESS THAN 15% BY VOLUME. CONTRACTOR MAY REUSE EXISTING ON-SITE WETLAND SOILS. TESTING MUST BE PERFORMED BY THE CONTRACTOR PRIOR TO SOIL REUSE TO DETERMINE IF THE EXISTING WETLAND SOILS MEET THE CRITERIA LISTED IN NOTE 1. IF THE EXISTING SOILS DO NOT MEET THE CRITERIA OF WETLAND SOILS AS DEFINED IN NOTE 1 THEY MAY NOT BE REUSED.
- PERFORATED PVC RISERS SHALL HAVE VERTICAL SLOTS CUT INTO PVC RISERS ABOVE GRADE MEASURING 3"x1/8".
- GRAVEL WETLAND SOIL SHALL BE SEEDDED WITH NEW ENGLAND EROSION CONTROL/RESTORATION MIX OR EQUIVALENT AT A RATE OF 35 LB/ACRE.
- BERM MATERIAL SHALL CONSIST OF NATIVE SOIL OR COMMON FILL.
- A PRE-INSTALL MEETING SHALL BE HELD WITH THE CONTRACTOR RESPONSIBLE FOR GRAVEL WETLAND CONSTRUCTION AND THE DESIGN ENGINEER.
- GRAVEL WETLAND TREATMENT CELLS SHALL BE LINED WITH AN IMPERMEABLE LINER.
- IT IS THE DESIGN ENGINEERS RECOMMENDATION THAT THE GRAVEL WETLAND BE CONSTRUCTED IN THE DRY TO ACHIEVE THE ANTICIPATED TREATMENT QUALITY STANDARDS.
- THE SLOPED SIDES OF THE GRAVEL WETLAND SHALL RECEIVE EROSION CONTROL MATTING. SEE DETAIL EROSION CONTROL BLANKET DETAIL.

AASHTO #8 STONE (#8 to 3/8")		AASHTO #67 STONE (#4 to 3/4")	
SIEVE SIZE	% PASSING	SIEVE SIZE	% PASSING
1/2"	100	1"	100
3/8"	85-100	3/4"	90-100
#4	10-30	3/8"	20-55
#8	0-10	#4	0-10
#16	0-5	#8	0-5

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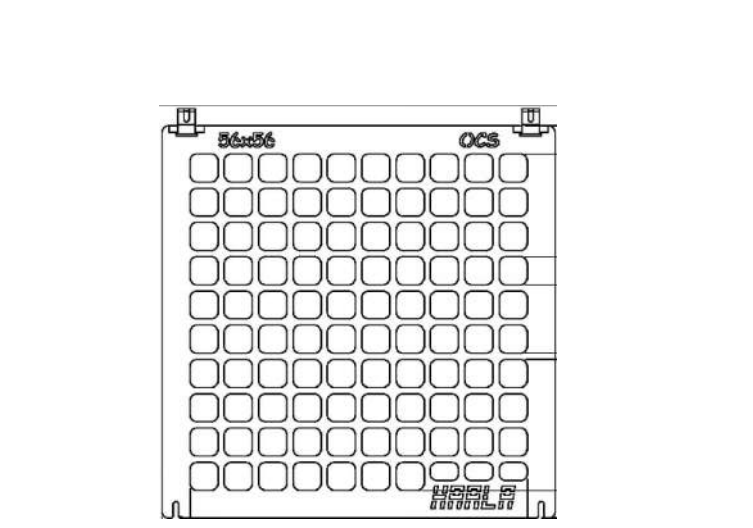
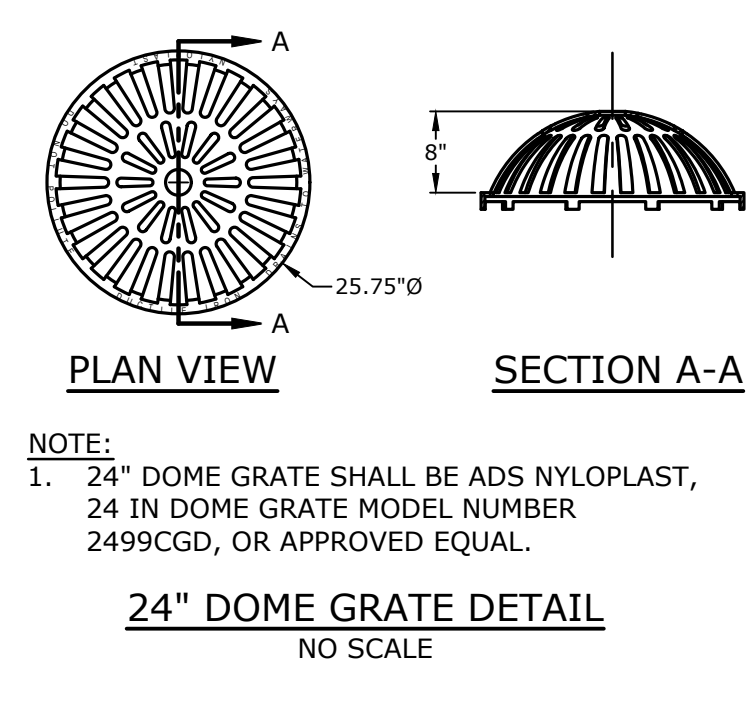
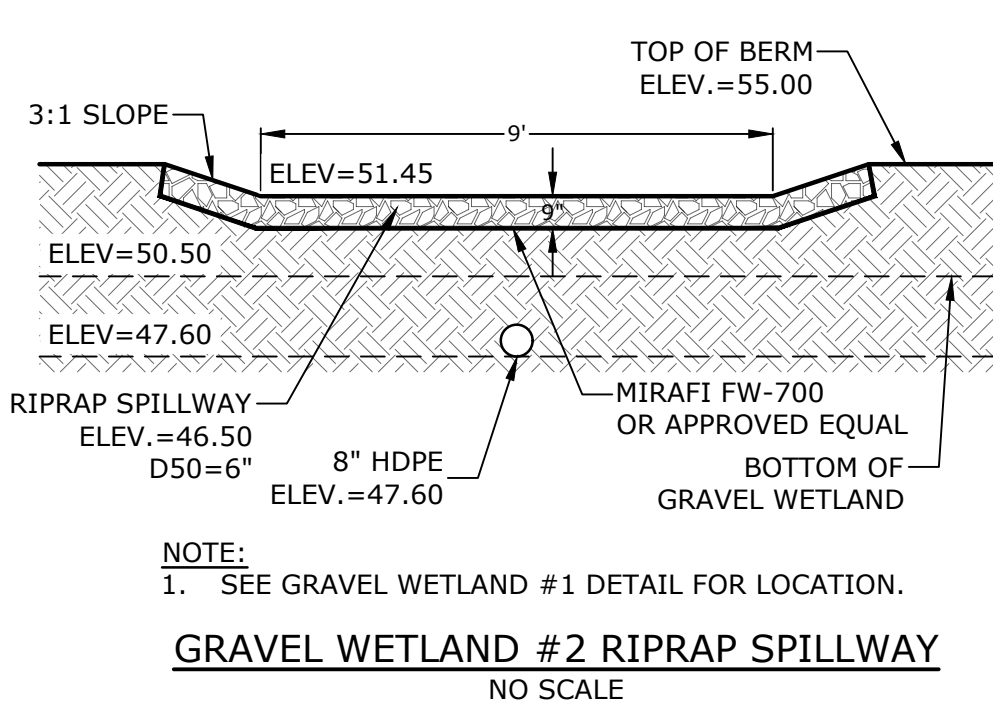
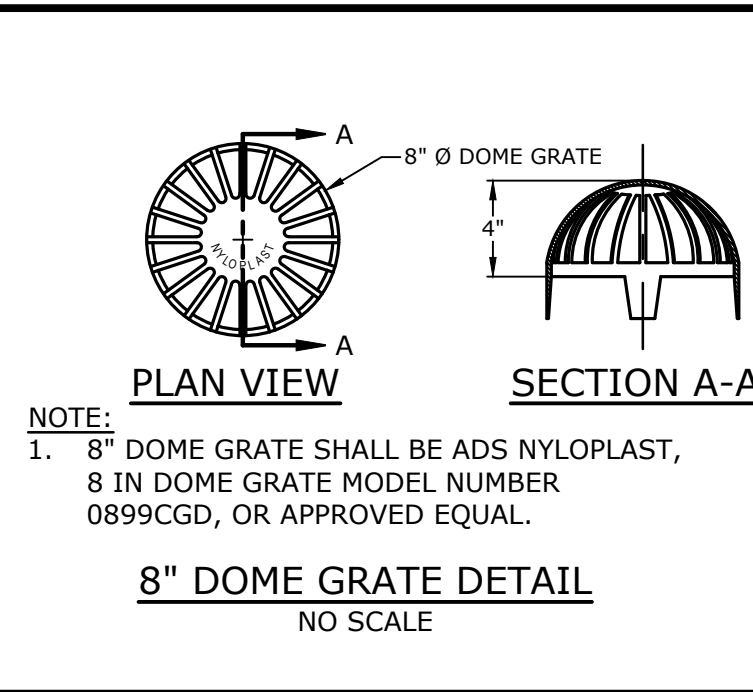
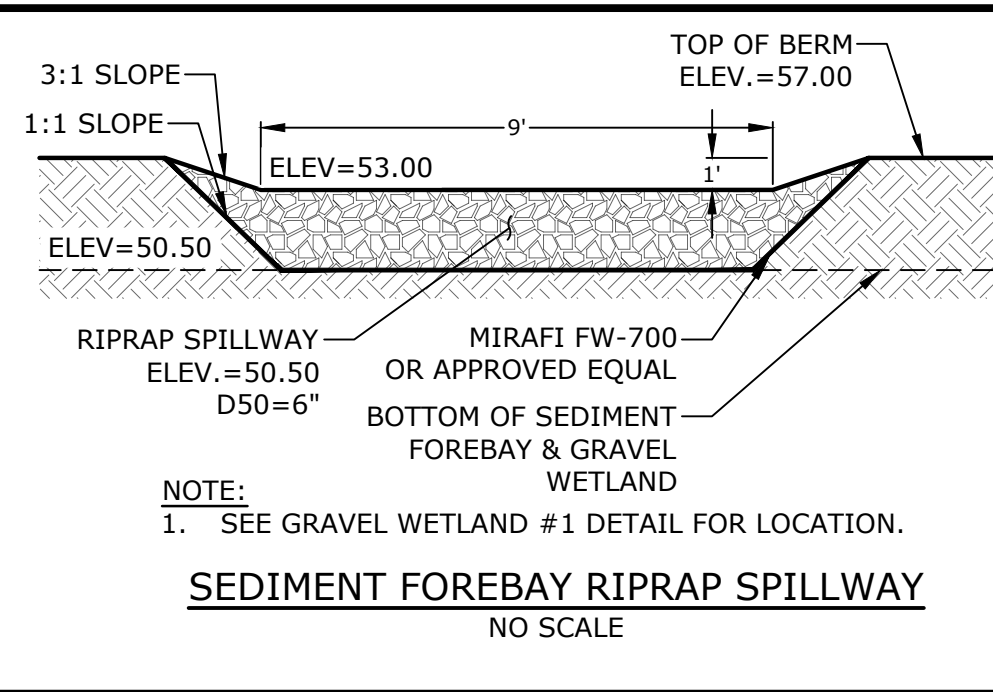
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APPROVED: PMC

DETAILS SHEETS

SCALE: AS SHOWN

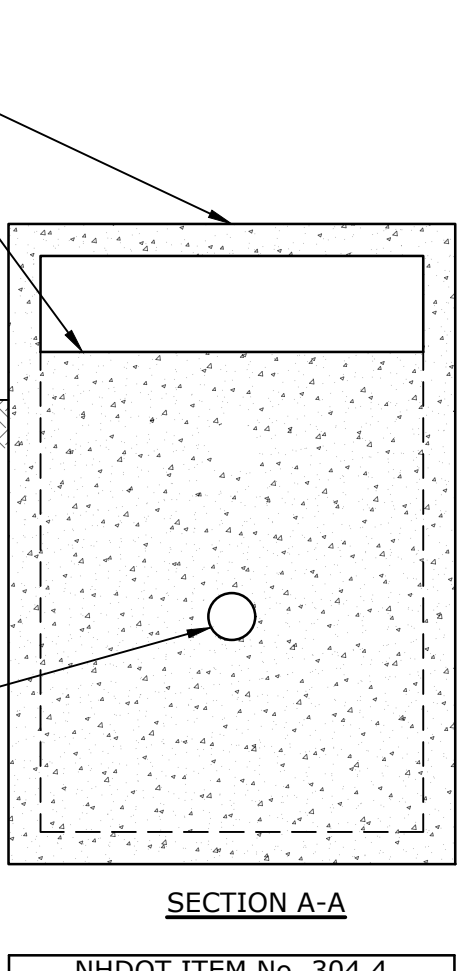
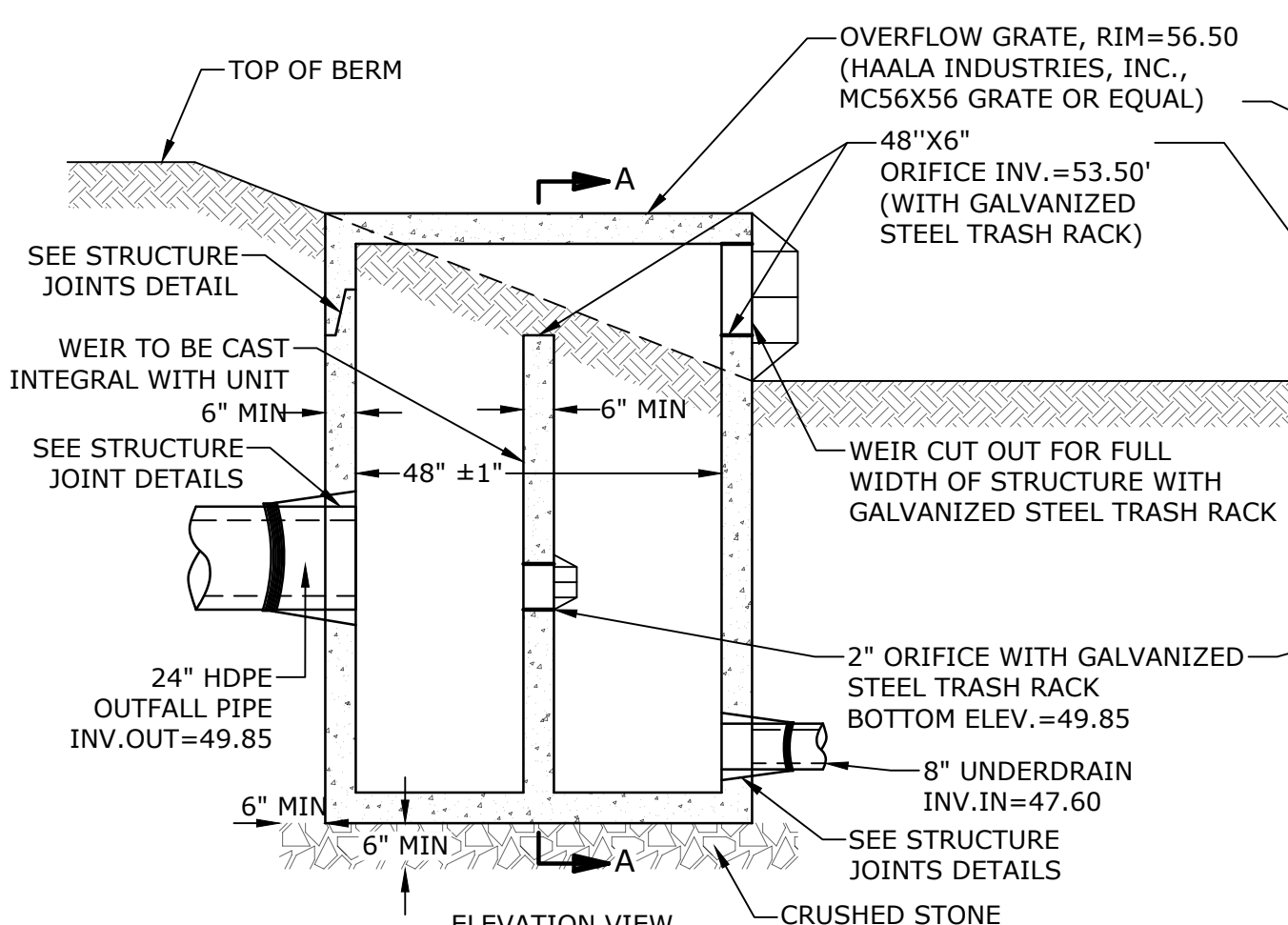
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NOTES:
1. OUTLET STRUCTURE GRATE SHALL BE HAALA INDUSTRIES, INC. MC56X56 TOP MOUNT GRATE OR EQUAL.
2. GRATE TO BE SECURED TO CONCRETE STRUCTURE.

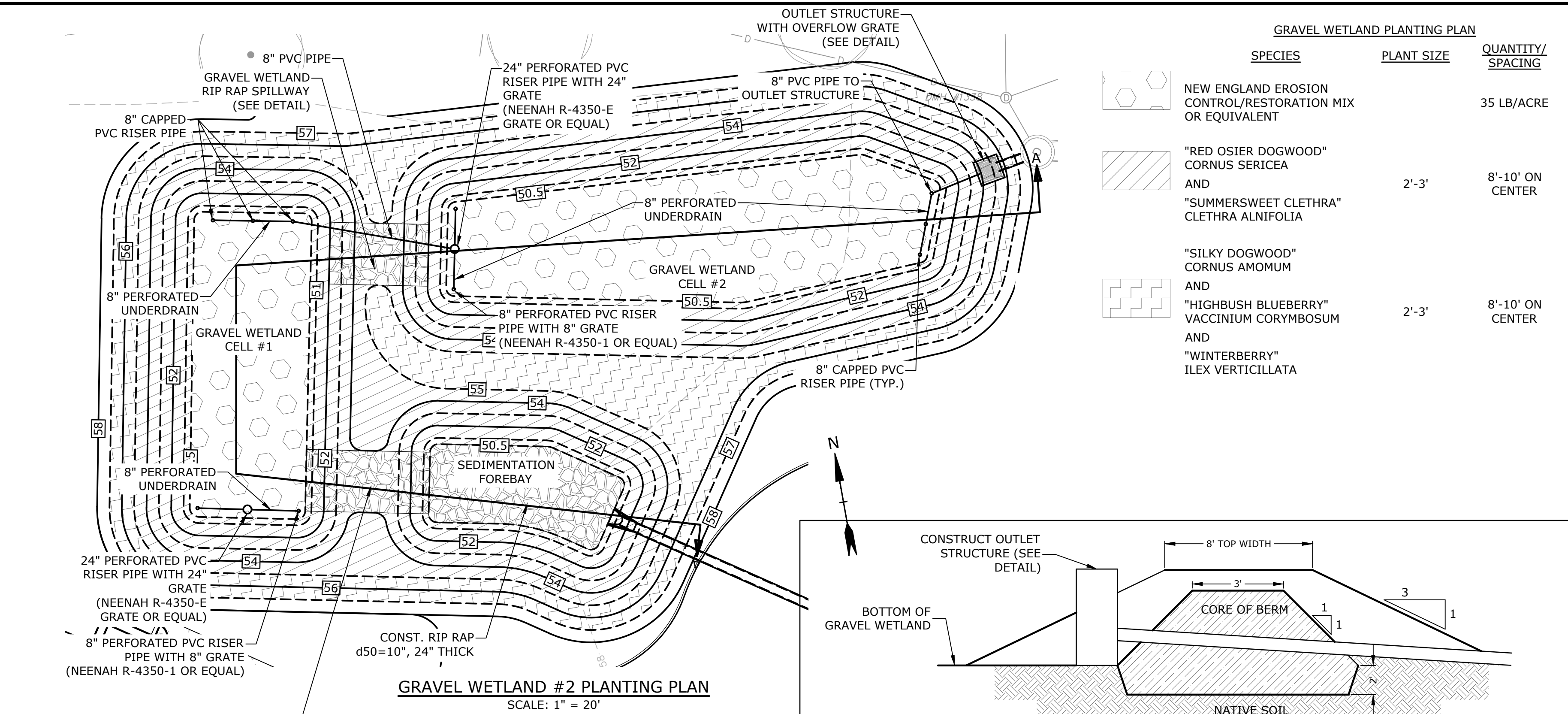
HAALA MC56X56 GRATE
NO SCALE



NOTES:
1. ALL SECTIONS SHALL BE 4,000 PSI CONCRETE (TYPE II CEMENT).
2. CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQUARE INCHES PER LINEAR FOOT IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER OF THE THIRDE WALL.
3. THE TONGUE OR THE GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQUARE INCHES PER LINEAR FOOT.
4. THE STRUCTURES SHALL BE DESIGNED FOR H2O LOADING.
5. ALL JOINTS ON THE STRUCTURE AND PIPING SHALL BE WATERTIGHT.

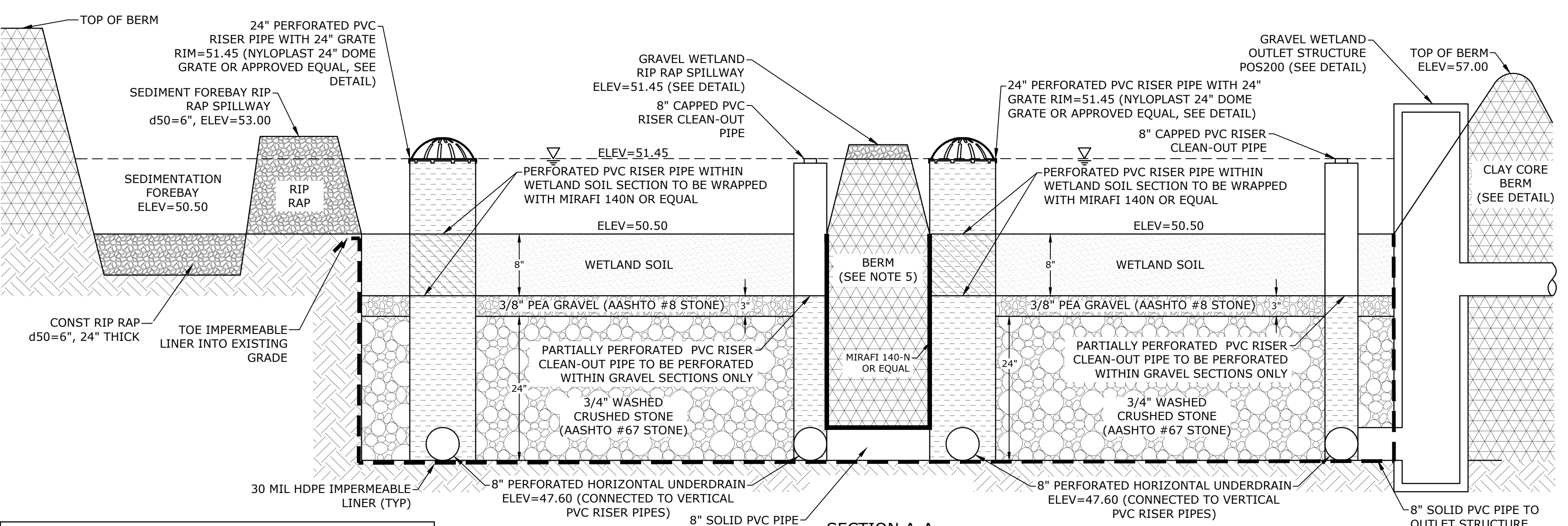
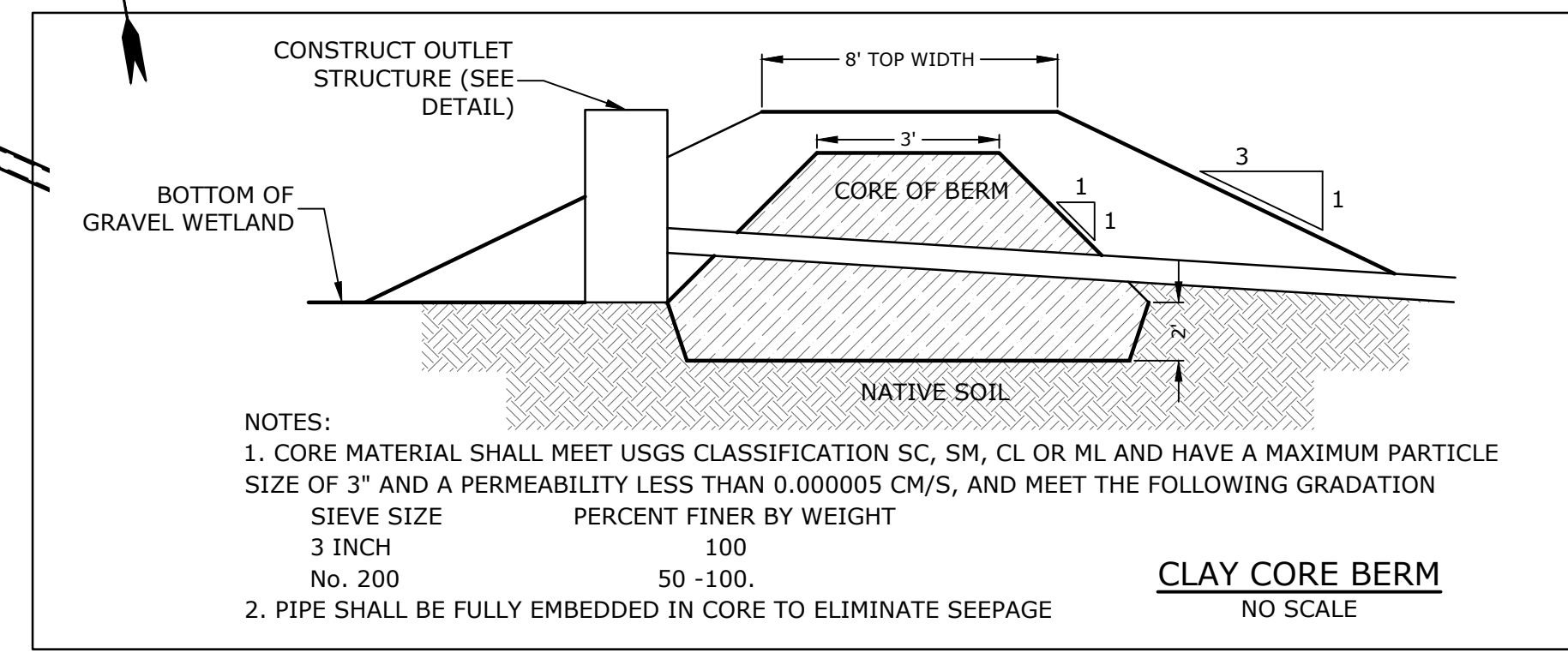
OUTLET STRUCTURE (POS200)
NO SCALE

NHDOT ITEM No. 304.4 (CRUSHED STONE - FINE)	
SIEVE SIZE	% PASSING
2"	100
1-1/2"	85-100
3/4"	45-75
#4	10-45
#200	0-5



GRAVEL WETLAND PLANTING PLAN

SPECIES	PLANT SIZE	QUANTITY/SPACING
NEW ENGLAND EROSION CONTROL/RESTORATION MIX OR EQUIVALENT		35 LB/ACRE
"RED OSIER DOGWOOD" CORNUS SERICEA AND "SUMMERSWEET CLETHRA" CLETHRA ALNIFOLIA	2'-3'	8'-10' ON CENTER
"SILKY DOGWOOD" CORNUS AMOMUM AND "Highbush Blueberry" VACCINIUM CORYMBOSUM AND "WINTERBERRY" ILEX VERTICILLATA	2'-3'	8'-10' ON CENTER



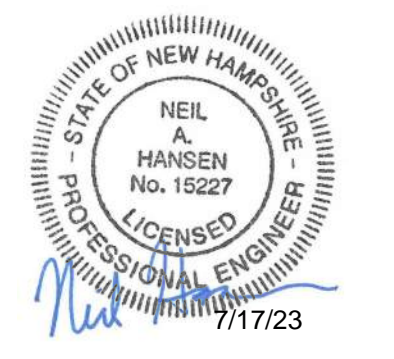
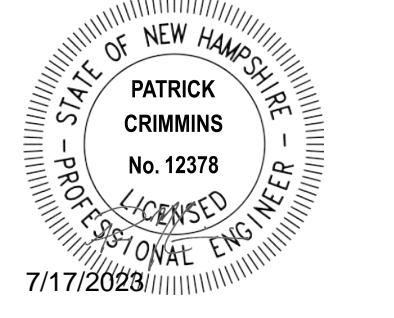
GRAVEL WETLAND INSPECTION / MAINTENANCE REQUIREMENTS

INSPECTION / MAINTENANCE	FREQUENCY	ACTION
MONITOR TO ENSURE THAT GRAVEL WETLAND FUNCTIONS EFFECTIVELY AFTER STORMS	FOUR (4) TIMES ANNUALLY (QUARTERLY) AND AFTER ANY RAINFALL EVENT EXCEEDING 2.5" IN A 24-HR PERIOD	- TRASH AND DEBRIS TO BE REMOVED - ANY REQUIRED MAINTENANCE SHALL BE ADDRESSED - INSPECT SOIL AND REPAIR ERODED AREAS, ESPECIALLY ON SLOPES. - CHECK INLETS, OUTLETS, AND OVERFLOW SPILLWAY FOR BLOCKAGE, STRUCTURAL INTEGRITY AND EVIDENCE OF EROSION.
INSPECT VEGETATION	ANNUALLY	- INSPECT THE CONDITION OF ALL GRAVEL WETLAND VEGETATION - PRUNE BACK OVERGROWTH - REPLACE DEAD VEGETATION - REMOVE ANY INVASIVE SPECIES - COORDINATE WITH UNH STORMWATER CENTER FOR FURTHER VEGETATION MANAGEMENT GUIDELINES
INSPECT DRAWDOWN TIME	ANNUALLY	- HIRE QUALIFIED PROFESSIONAL TO ASSESS THE CONDITION OF THE FACILITY TO DETERMINE MEASURES REQUIRED TO RESTORE THE FILTRATION FUNCTION, INCLUDING BUT NOT LIMITED TO REMOVAL OF ACCUMULATED SEDIMENTS OR RECONSTRUCTION OF THE FILTER.

NOTES:
1. WETLAND SOIL SHALL BE A SANDY CLAY LOAM WITH A HYDRAULIC CONDUCTIVITY OF 0.1-0.01 FT/DAY. ORGANIC CONTENT SHALL BE GREATER THAN 15% BY VOLUME. CLAY CONTENT SHALL BE LESS THAN 15% BY VOLUME. CONTRACTOR MAY REUSE EXISTING ON-SITE WETLAND SOILS. TESTING MUST BE PERFORMED BY THE CONTRACTOR PRIOR TO SOIL REUSE TO DETERMINE IF THE EXISTING WETLAND SOILS MEET THE CRITERIA LISTED IN NOTE 1. IF THE EXISTING SOILS DO NOT MEET THE CRITERIA OF WETLAND SOILS AS DEFINED IN NOTE 1 THEY MAY NOT BE REUSED.
2. PERFORATED PVC RISERS SHALL HAVE VERTICAL SLOTS CUT INTO PVC RISERS ABOVE GRADE MEASURING 3"x1/8".
3. GRAVEL WETLAND SOIL SHALL BE SEEDED WITH NEW ENGLAND EROSION CONTROL/RESTORATION MIX OR EQUIVALENT AT A RATE OF 35 LB/ACRE.
4. BERM MATERIAL SHALL CONSIST OF NATIVE SOIL OR COMMON FILL.
5. A PRE-INSTALL MEETING SHALL BE HELD WITH THE CONTRACTOR RESPONSIBLE FOR GRAVEL WETLAND CONSTRUCTION AND THE DESIGN ENGINEER.
6. GRAVEL WETLAND TREATMENT CELLS SHALL BE LINED WITH AN IMPERMEABLE LINER.
7. IT IS THE DESIGN ENGINEERS RECOMMENDATION THAT THE GRAVEL WETLAND BE CONSTRUCTED IN THE DRY TO ACHIEVE THE ANTICIPATED TREATMENT QUALITY STANDARDS.
8. THE SLOPED SIDES OF THE GRAVEL WETLAND SHALL RECEIVE EROSION CONTROL MATTING. SEE DETAIL EROSION CONTROL BLANKET DETAIL.

GRAVEL WETLAND #2
NO SCALE

AASHTO #8 STONE (#8 to 3/8")		AASHTO #67 STONE (#4 to 3/4")	
SIEVE SIZE	% PASSING	SIEVE SIZE	% PASSING
1/2"	100	1"	100
3/8"	85-100	3/4"	90-100
#4	10-30	3/8"	20-55
#8	0-10	#4	0-10
#16	0-5	#8	0-5



Proposed Industrial Development
Lonza Biologics

Portsmouth, New Hampshire

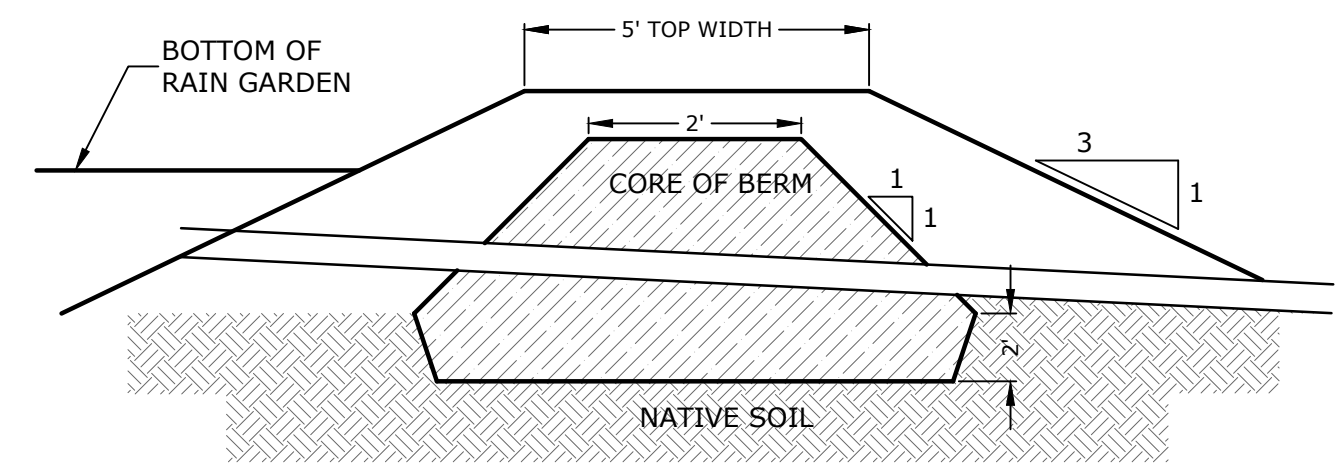
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K	5/5/2023	Phase 1B Issued for Bid
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F	11/6/2018	P.B. Submission

PROJECT NO: L-0700-013
DATE: 04/03/2018
FILE: L-0700-026-C-DTLS.dwg
DRAWN BY: CJK
CHECKED: NAH
APPROVED: PMC

DETAILS SHEETS

SCALE: AS SHOWN

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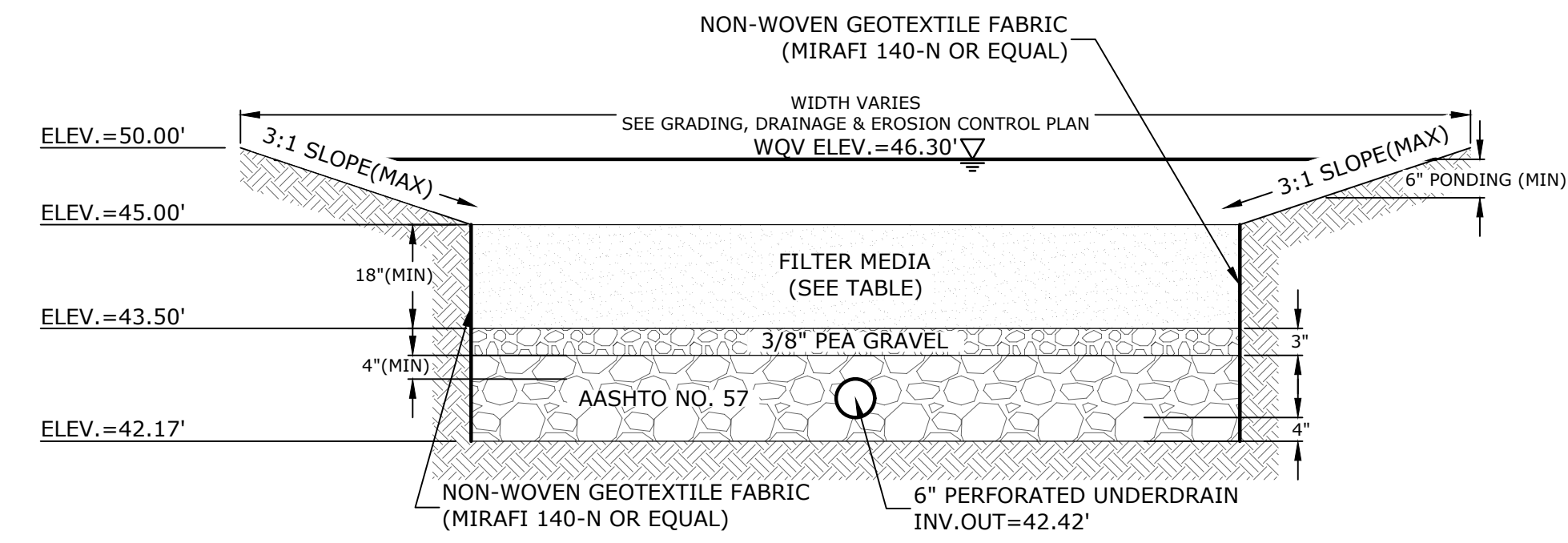


NOTES:
 1. CORE MATERIAL SHALL MEET USGS CLASSIFICATION SC, SM, CL OR ML AND HAVE A MAXIMUM PARTICLE SIZE OF 3" AND A PERMEABILITY LESS THAN 0.000005 CM/S, AND MEET THE FOLLOWING GRADATION

SIEVE SIZE	PERCENT FINER BY WEIGHT
3 INCH	100
No. 200	50 -100.

2. PIPE SHALL BE FULLY EMBEDDED IN CORE TO ELIMINATE SEEPAGE

CLAY CORE BERM
NO SCALE



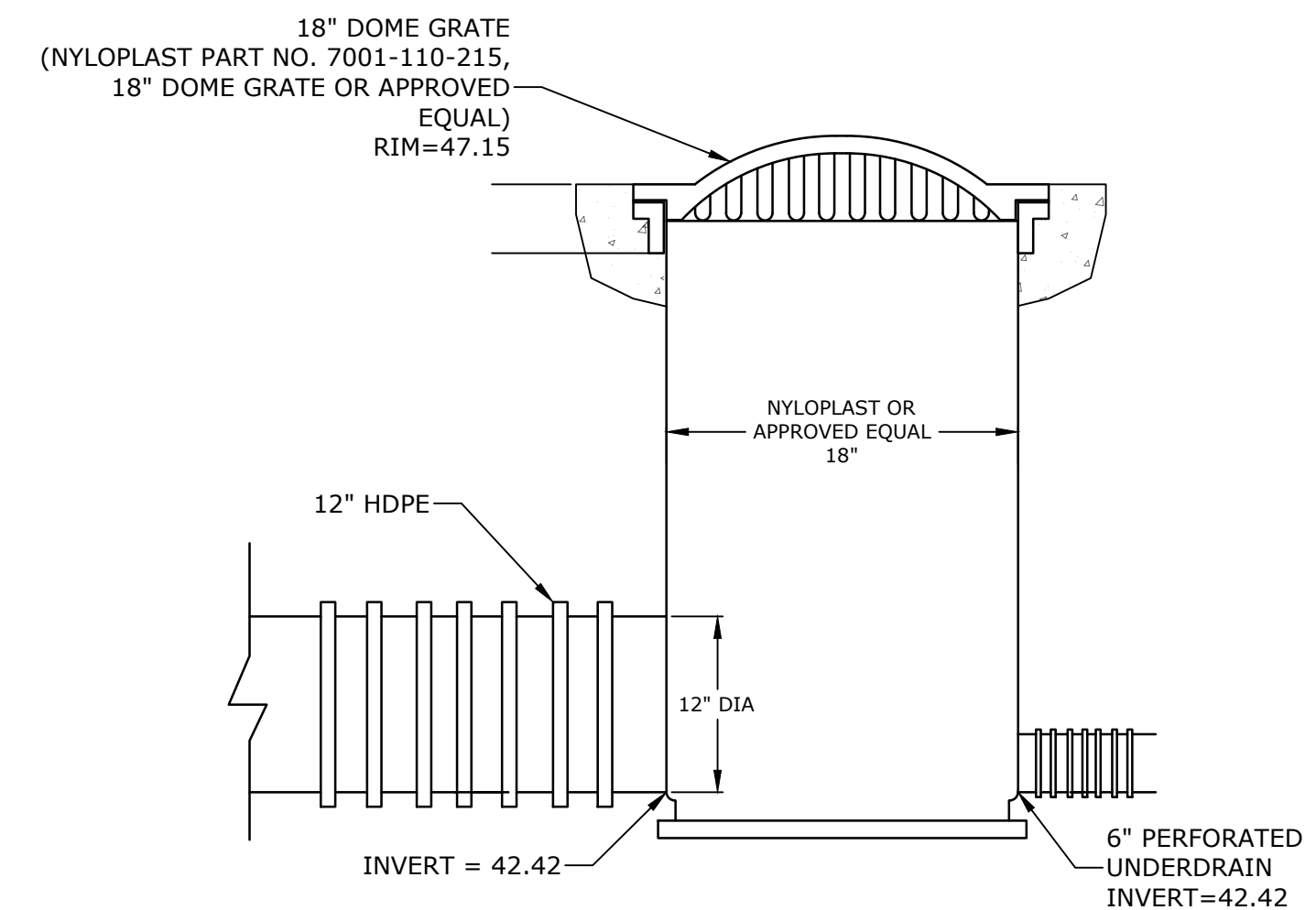
SECTION VIEW

FILTER MEDIA COMPOSITION:			
COMPONENT MATERIAL	PERCENT OF MIXTURE BY VOLUME	GRADATION OF MATERIAL SIEVE NO.	PERCENT PASSING
ASTM C-33 CONCRETE SAND	50-55	SEE NOTE #5	
LOAMY SAND TOPSOIL	20-30	200	15-25
MODERATELY FINE SHREDDED BARK OR WOOD FIBER MULCH	20-30	200	5 MAX.

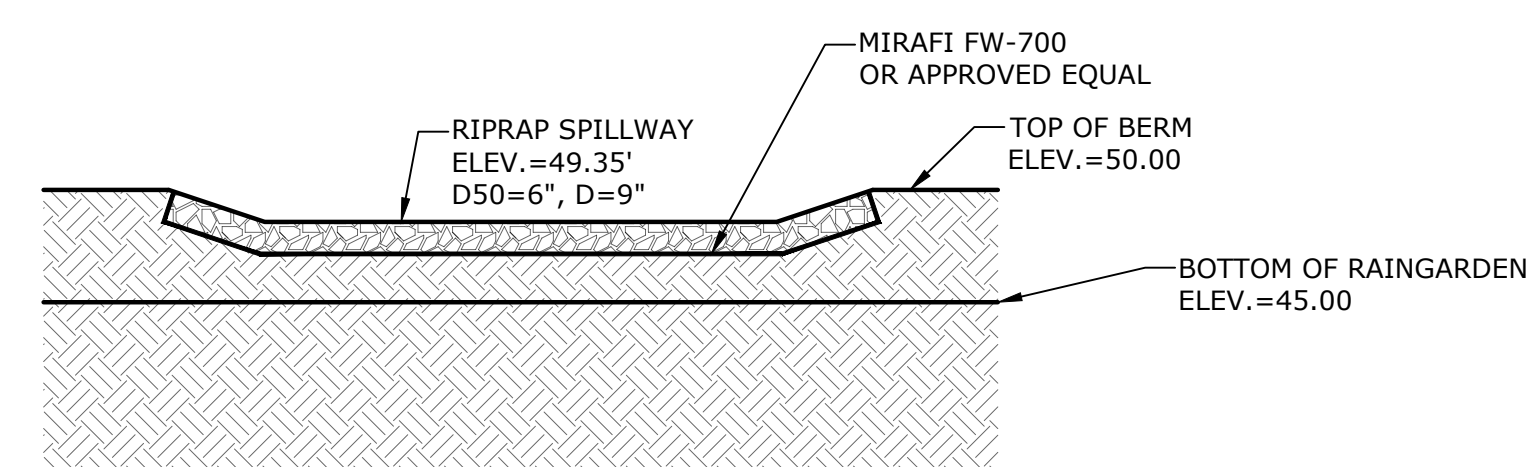
NOTES:
 1. RAIN GARDENS SHALL NOT BE PLACED INTO SERVICE UNTIL THE PRACTICE HAS BEEN PLANTED AND ITS CONTRIBUTING AREAS HAVE BEEN FULLY STABILIZED.
 2. DO NOT TRAFFIC EXPOSED SOIL SURFACES WITH CONSTRUCTION EQUIPMENT. CONTRACTOR SHALL KEEP ALL EXCAVATION EQUIPMENT OUTSIDE OF THE LIMIT OF THE RAIN GARDEN.
 3. SEE GRADING, DRAINAGE & EROSION CONTROL PLAN FOR LOCATIONS, LAYOUTS, AND ELEVATIONS.
 4. THE SAND PORTION OF THE FILTER MEDIA SHALL MEET THE FOLLOWING GRADATION (ASTM C-33):

SIEVE SIZE	PERCENT PASSING
3/8"	100
#4	95-100
#8	80-100
#16	50-85
#30	25-60
#50	5-30
#100	0-10

RAIN GARDEN
NO SCALE

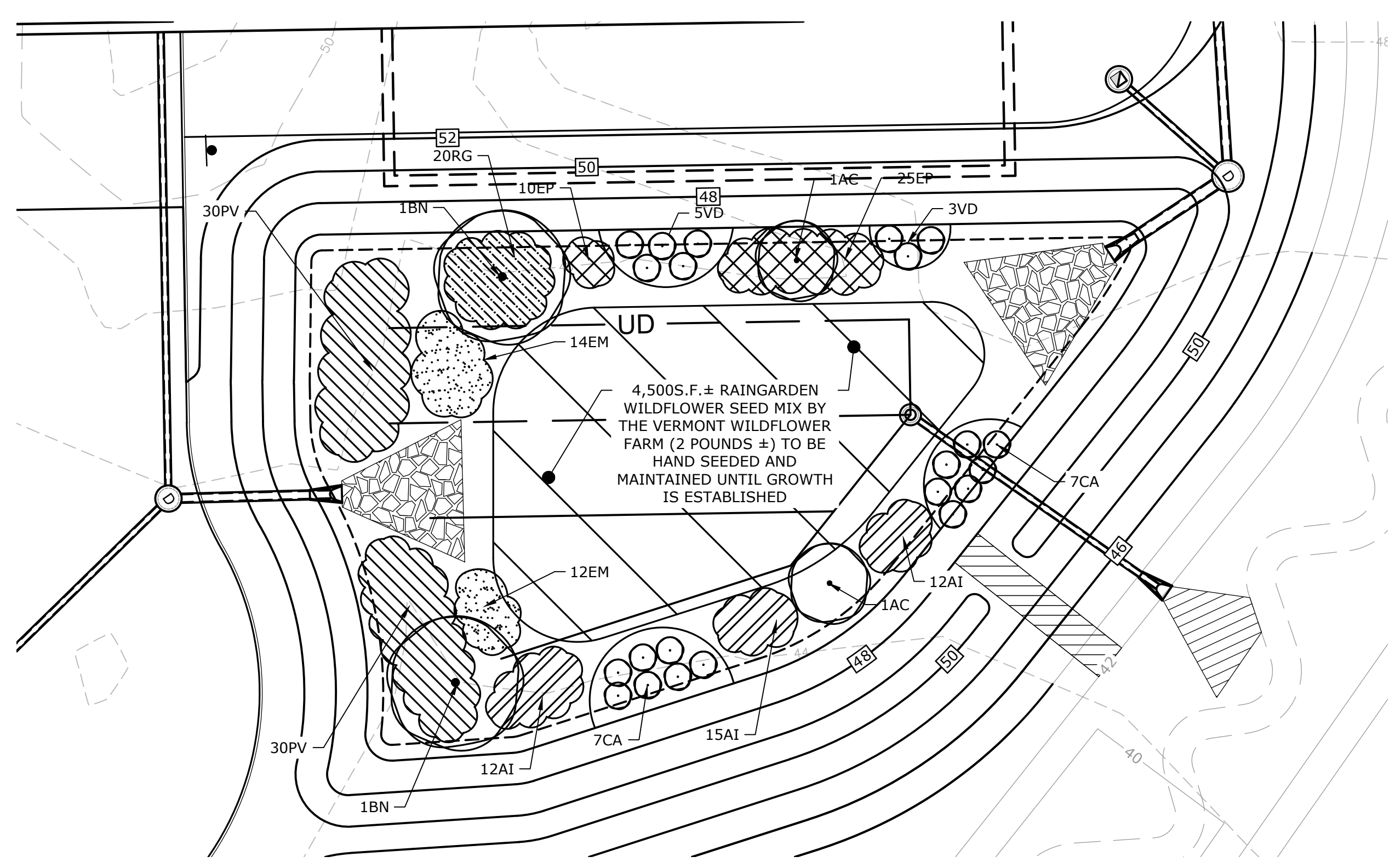


OUTLET STRUCTURE DETAIL (POS300)
NO SCALE



NOTE:
SEE GRADING, DRAINAGE & EROSION CONTROL PLANS, SHEET C-110, FOR LOCATIONS AND ELEVATIONS.

RIPRAP OVERFLOW SPILLWAY
NO SCALE



RAIN GARDEN PLANTING PLAN
SCALE: 1" = 20'

RAINGARDEN PLANT SCHEDULE				
CODE	BOTANICAL NAME	COMMON NAME	SIZE	REMARKS
TREES				
BN	BETULA NIGRA	RIVER BIRCH	12 - 14' HT	B & B (CLUMP)
AC	AMELANCHIER CANADENSIS	SHADBLow SERVICEBERRY	6 - 7' HT	B & B (CLUMP)
SHRUBS				
VD	VIBURNUM DENTATUM	ARROWWOOD VIBURNUM	5 GALLON	CONTAINER
CA	CLETHRA ALNIFOLIA	SUMMERSWEET CLETHRA	5 GALLON	CONTAINER
PERENNIALS				
PV	PANICUM VIRGATUM 'SHENANDOAH'	SHENANDOAH SWITCH GRASS	3 GALLON	CONTAINER
EM	EUPATORIUM MACULATUM	JOE PYE WEED	2 GALLON	CONTAINER
AI	ASCLEPIAS INCARNATA	MARSH MILKWEED	2 GALLON	CONTAINER
RG	RUDBECKIA 'GOLDSTURM'	GOLDSTURM BLACKEYED SUSAN	1 GALLON	CONTAINER
EP	ECHINACEA 'PURPUREA'	PURPLE CONEFLOWER	1 GALLON	CONTAINER

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Portsmouth, New Hampshire

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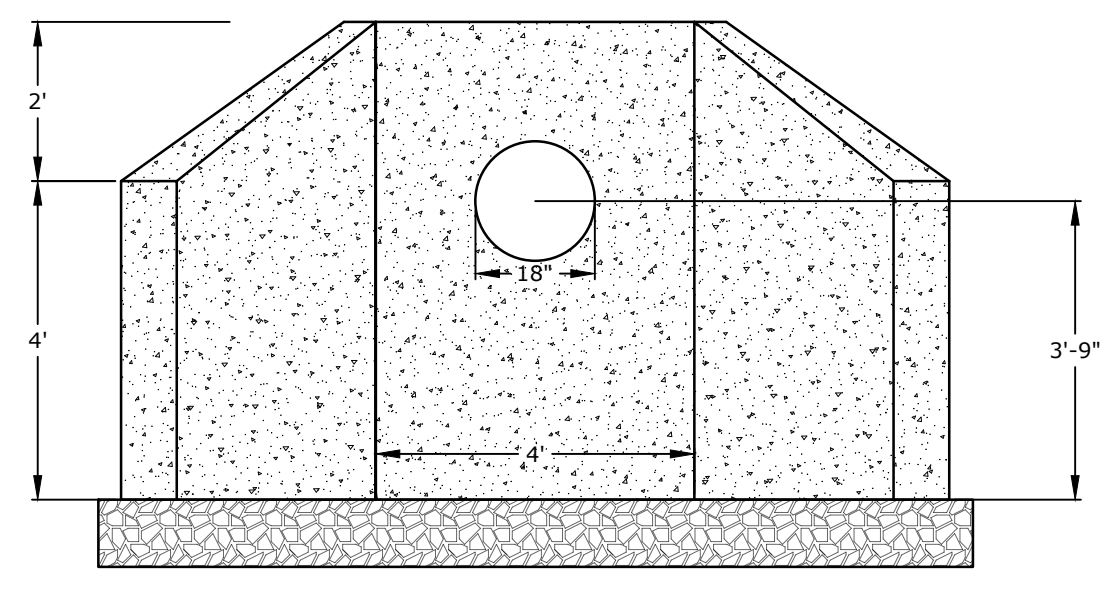
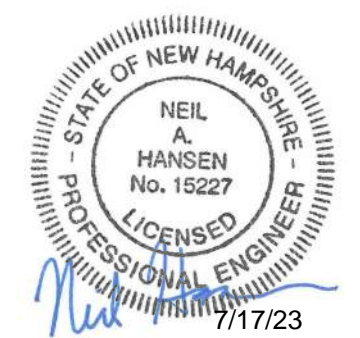
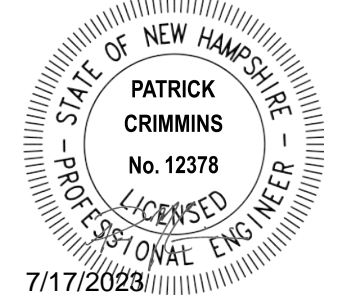
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DETAILS SHEETS

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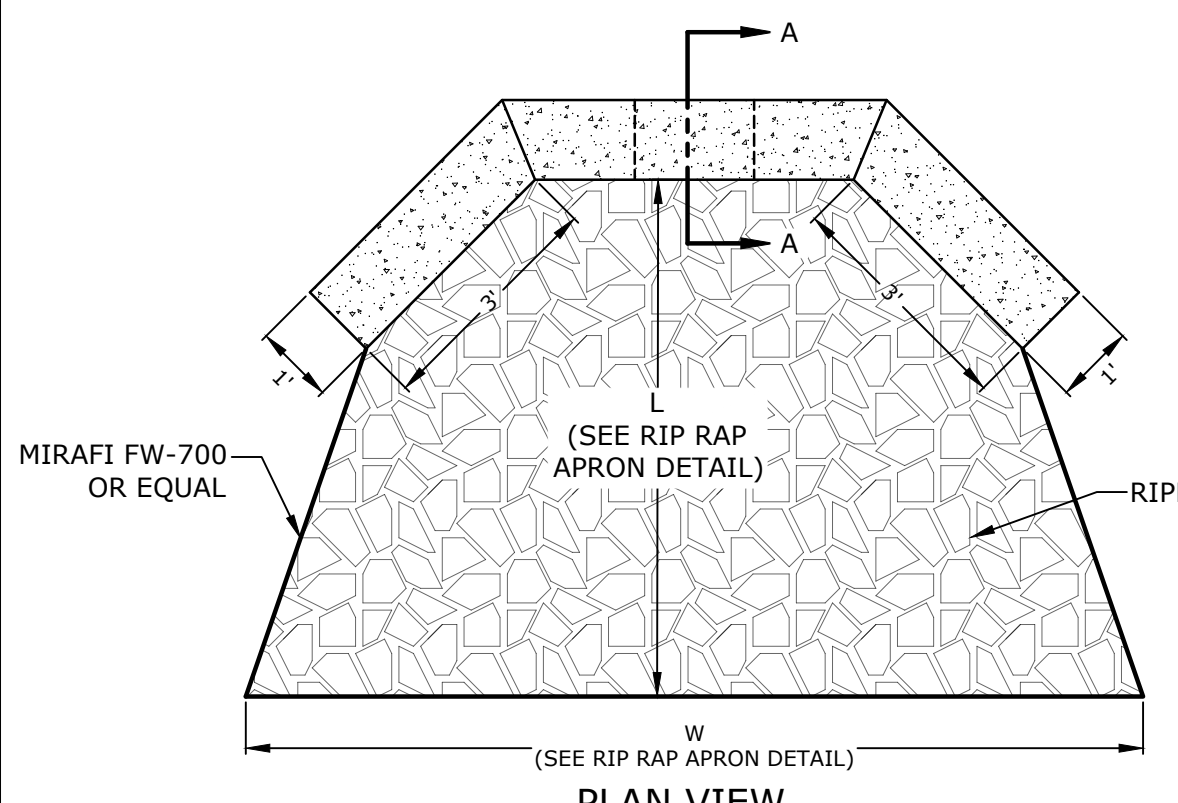
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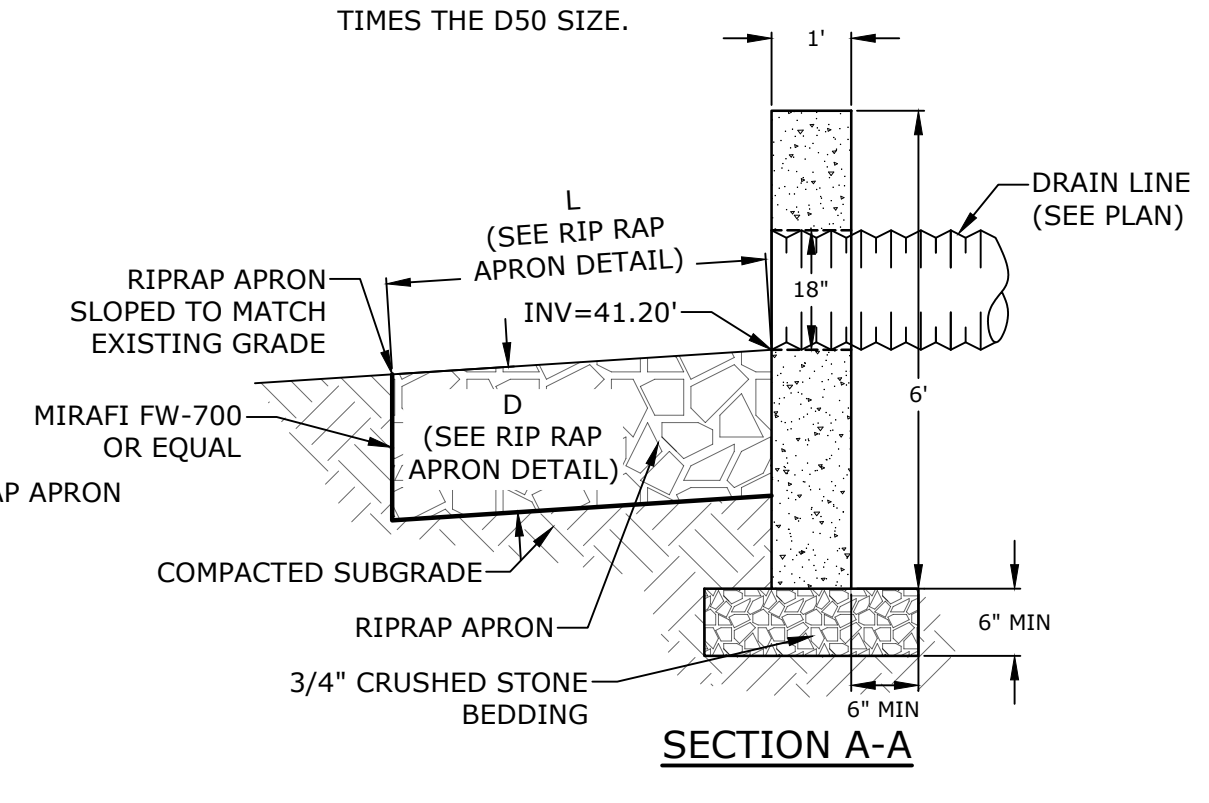
ELEVATION VIEW

- NOTES:**
1. HEADWALL SHALL BE 5,000 PSI CONCRETE.
 2. HEADWALL REINFORCEMENT SHALL BE 0.18 SQUARE INCHES PER LINEAR FOOT IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.
 3. SEE GRADING, DRAINAGE, & EROSION CONTROL PLAN FOR STONE SIZE AND APRON DIMENSIONS.
 4. STONE SHALL CONSIST OF SUB-ANGULAR FIELD STONE OR ROUGH UNHEWN QUARRY STONE OF APPROXIMATELY RECTANGULAR SHAPE. FLAT OR ROUND ROCKS ARE NOT ACCEPTABLE. THE STONE SHALL BE HARD AND OF SUCH QUALITY THAT IT WILL NOT DISINTEGRATE ON EXPOSURE TO WATER OR WEATHERING, BE CHEMICALLY STABLE AND IT SHALL BE SUITABLE IN ALL OTHER RESPECTS FOR THE PURPOSE INTENDED. THE BULK SPECIFIC GRAVITY (SATURATED SURFACE-DRY BASIS) OF THE INDIVIDUAL STONES SHALL BE AT LEAST 2.5.
 5. THE STONE SHALL BE COMPOSED OF A WELL-GRADED MIXTURE DOWN TO THE ONE-INCH SIZE PARTICLE SUCH THAT 50 PERCENT OF THE MIXTURE BY WEIGHT SHALL BE LARGER THAN THE D50 SIZE SPECIFIED. A WELL-GRADED MIXTURE IS DEFINED AS A MIXTURE COMPOSED PRIMARILY OF THE LARGER STONE SIZE BUT WITH A SUFFICIENT MIXTURE OF OTHER SIZES TO FILL THE PROGRESSIVELY SMALLER VOIDS BETWEEN THE STONES. THE DIAMETER OF THE LARGEST STONE SIZE IN SUCH A MIXTURE SHALL BE 1.5 TIMES THE D50 SIZE.

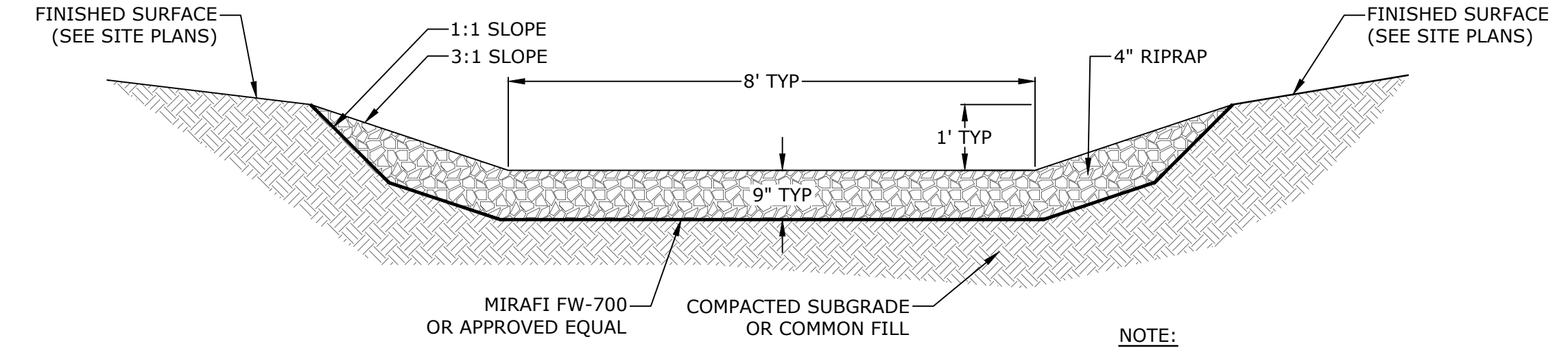


PLAN VIEW

PRECAST CONCRETE HEADWALL WITH WING WALLS (HW100)
NO SCALE

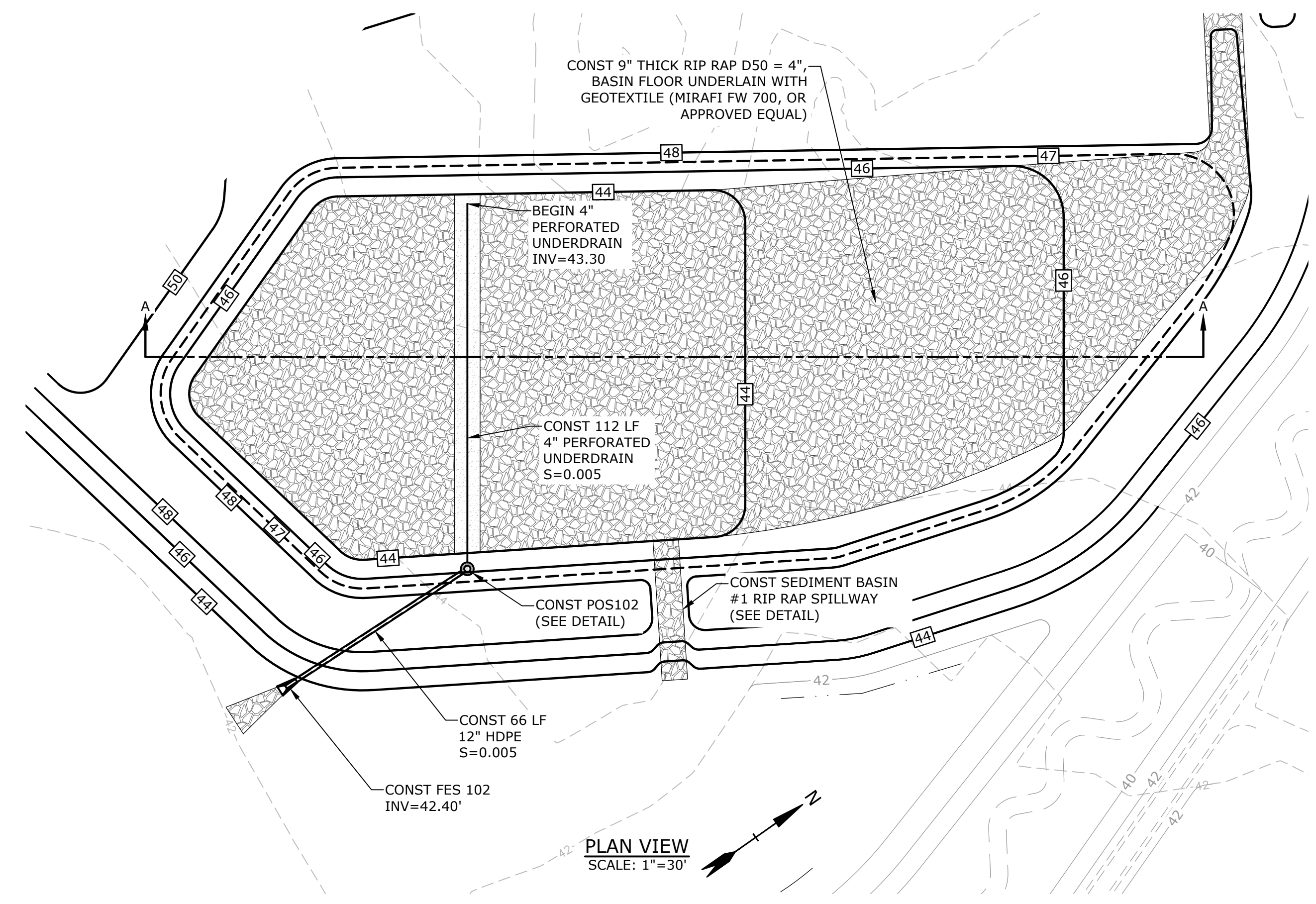


SECTION A-A

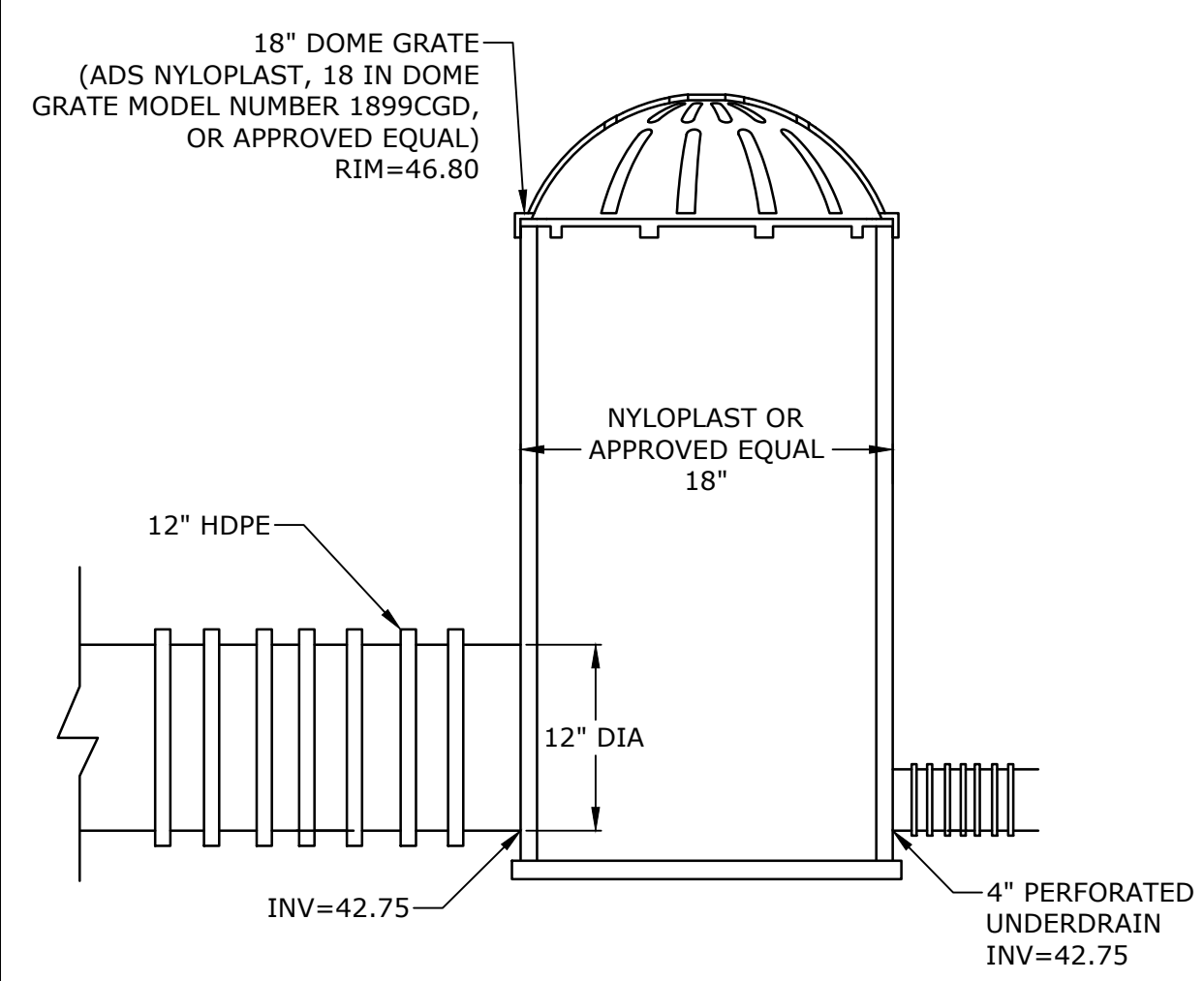


TEMPORARY CONVEYANCE SWALE
NO SCALE

- NOTE:**
1. CONTRACTOR TO INSTALL TEMPORARY CHECK DAMS AS NEEDED IN ACCORDANCE WITH NHDES REGULATIONS.

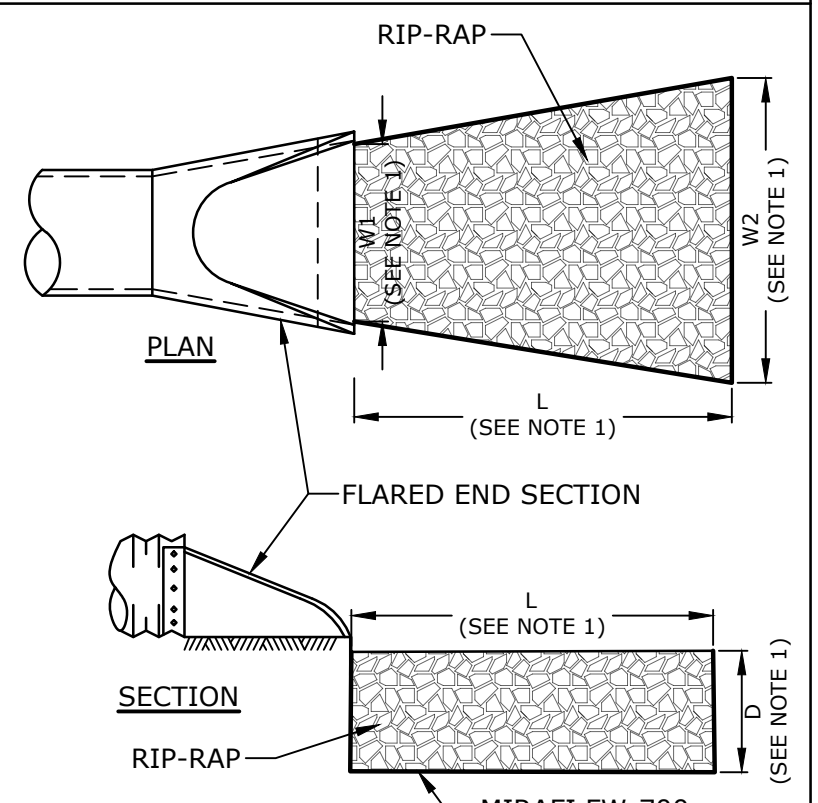


PLAN VIEW
SCALE: 1"=30'

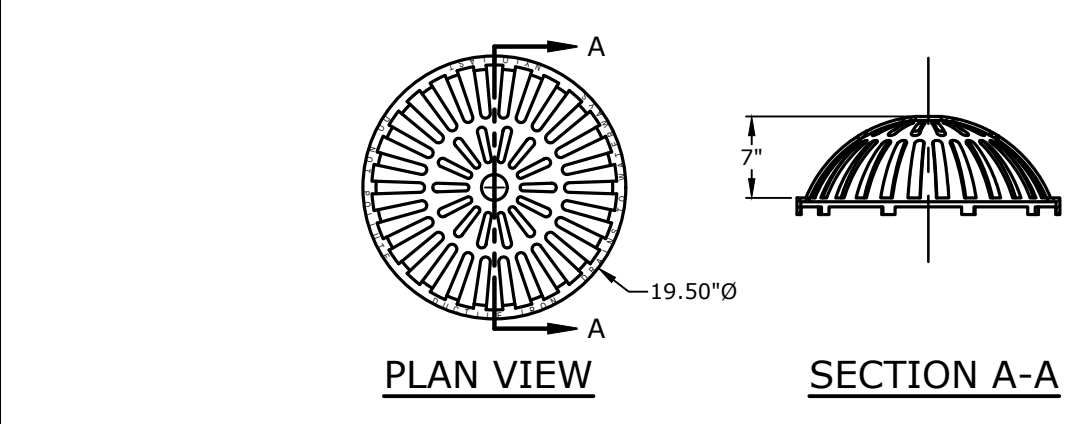


OUTLET STRUCTURE DETAIL (POS102)
NO SCALE

- NOTES:**
1. STONE SIZE AND MAT DIMENSIONS DETAILED ON PLANS.
 2. STONE SHALL CONSIST OF SUB-ANGULAR FIELD STONE OR ROUGH UNHEWN QUARRY STONE OF APPROXIMATELY RECTANGULAR SHAPE. FLAT OR ROUND ROCKS ARE NOT ACCEPTABLE. THE STONE SHALL BE HARD AND OF SUCH QUALITY THAT IT WILL NOT DISINTEGRATE ON EXPOSURE TO WATER OR WEATHERING, BE CHEMICALLY STABLE AND IT SHALL BE SUITABLE IN ALL OTHER RESPECTS FOR THE PURPOSE INTENDED. THE BULK SPECIFIC GRAVITY (SATURATED SURFACE-DRY BASIS) OF THE INDIVIDUAL STONES SHALL BE AT LEAST 2.5.
 3. THE STONE SHALL BE COMPOSED OF A WELL-GRADED MIXTURE DOWN TO THE ONE-INCH SIZE PARTICLE SUCH THAT 50 PERCENT OF THE MIXTURE BY WEIGHT SHALL BE LARGER THAN THE D50 SIZE SPECIFIED. A WELL-GRADED MIXTURE IS DEFINED AS A MIXTURE COMPOSED PRIMARILY OF THE LARGER STONE SIZE BUT WITH A SUFFICIENT MIXTURE OF OTHER SIZES TO FILL THE PROGRESSIVELY SMALLER VOIDS BETWEEN THE STONES. THE DIAMETER OF THE LARGEST STONE SIZE IN SUCH A MIXTURE SHALL BE 1.5 TIMES THE D50 SIZE.

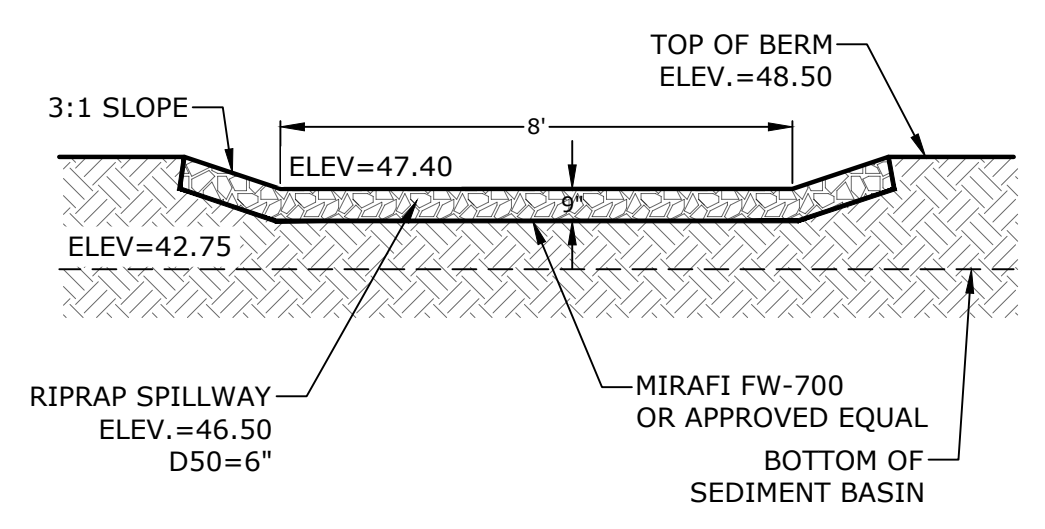


RIP-RAP APRON DETAIL
NO SCALE



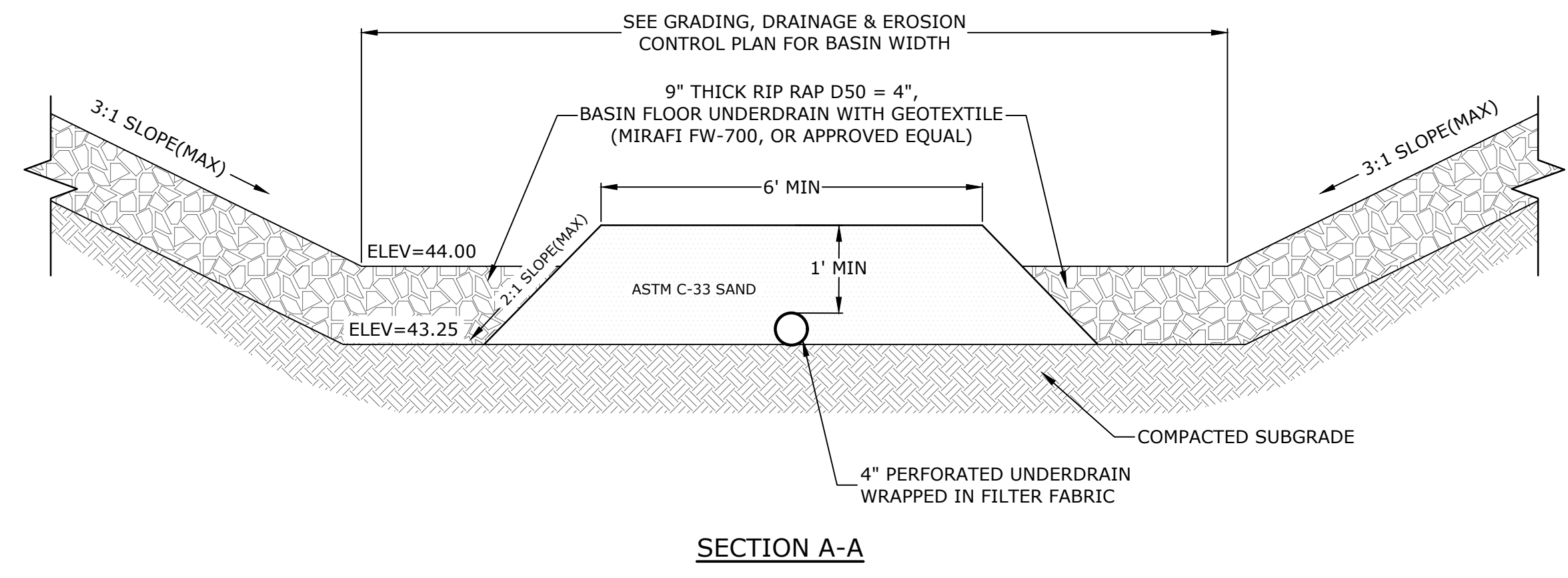
- NOTE:**
1. 18" DOME GRATE SHALL BE ADS NYLOPLAST, 18 IN DOME GRATE MODEL NUMBER 1899CGD, OR APPROVED EQUAL.

18" DOME GRATE DETAIL
NO SCALE



- NOTE:**
1. SEE SEDIMENT BASIN #1 DETAIL FOR LOCATION.

SEDIMENT BASIN #1 RIPRAP SPILLWAY
NO SCALE



SECTION A-A

- NOTES:**
1. UNDERDRAIN SAND SHALL BE ASTM C-33 CONCRETE SAND.
 2. 4" PERFORATED UNDERDRAIN SHALL BE ADS SB2 LEACH BED PIPE OR APPROVED EQUAL.

TEMPORARY SEDIMENT BASIN 1
NO SCALE

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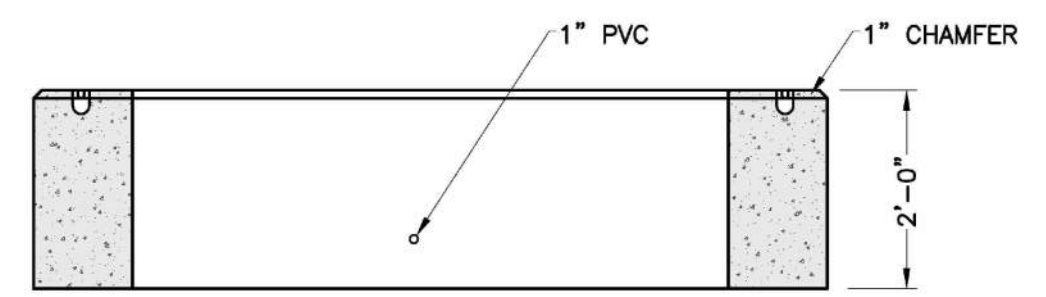
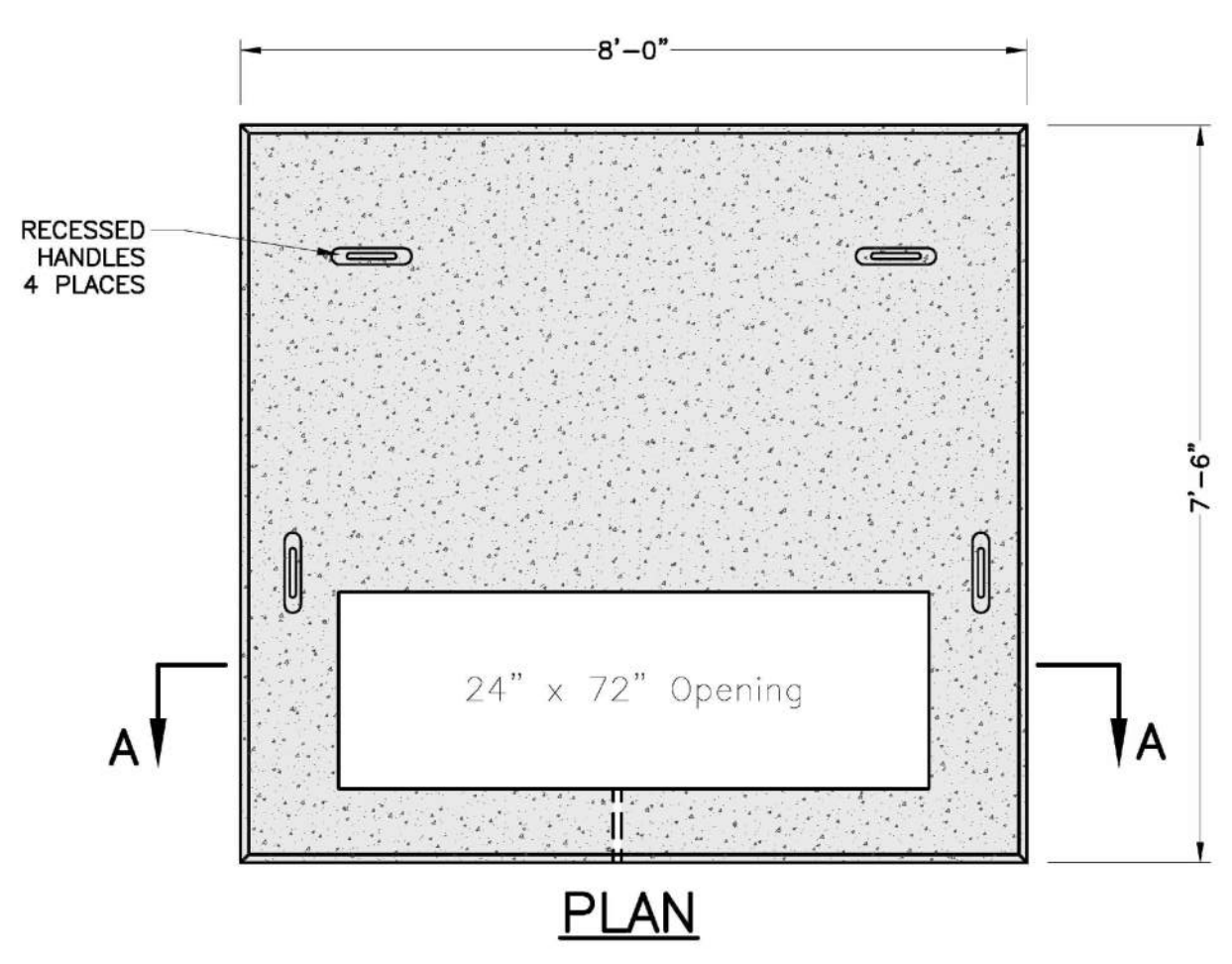
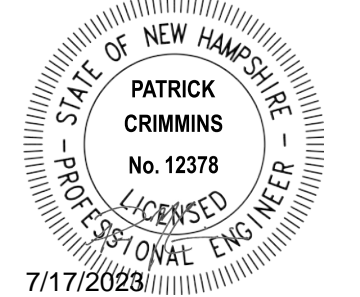
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APPROVED:	PMC

DETAILS SHEETS

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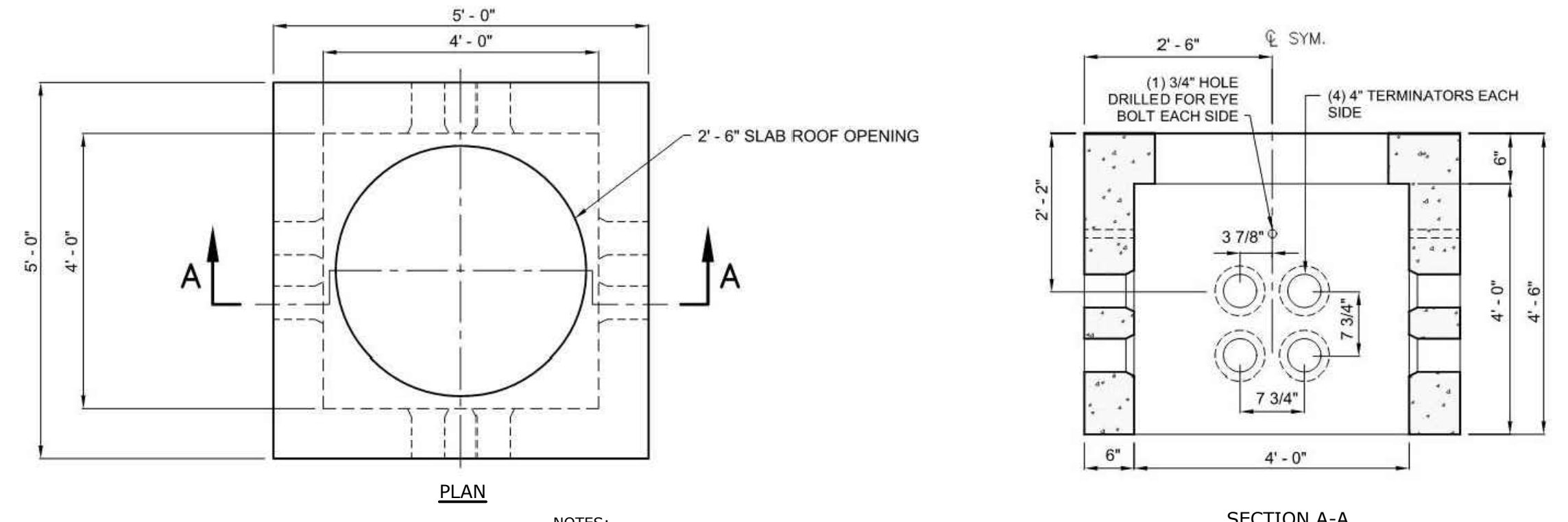
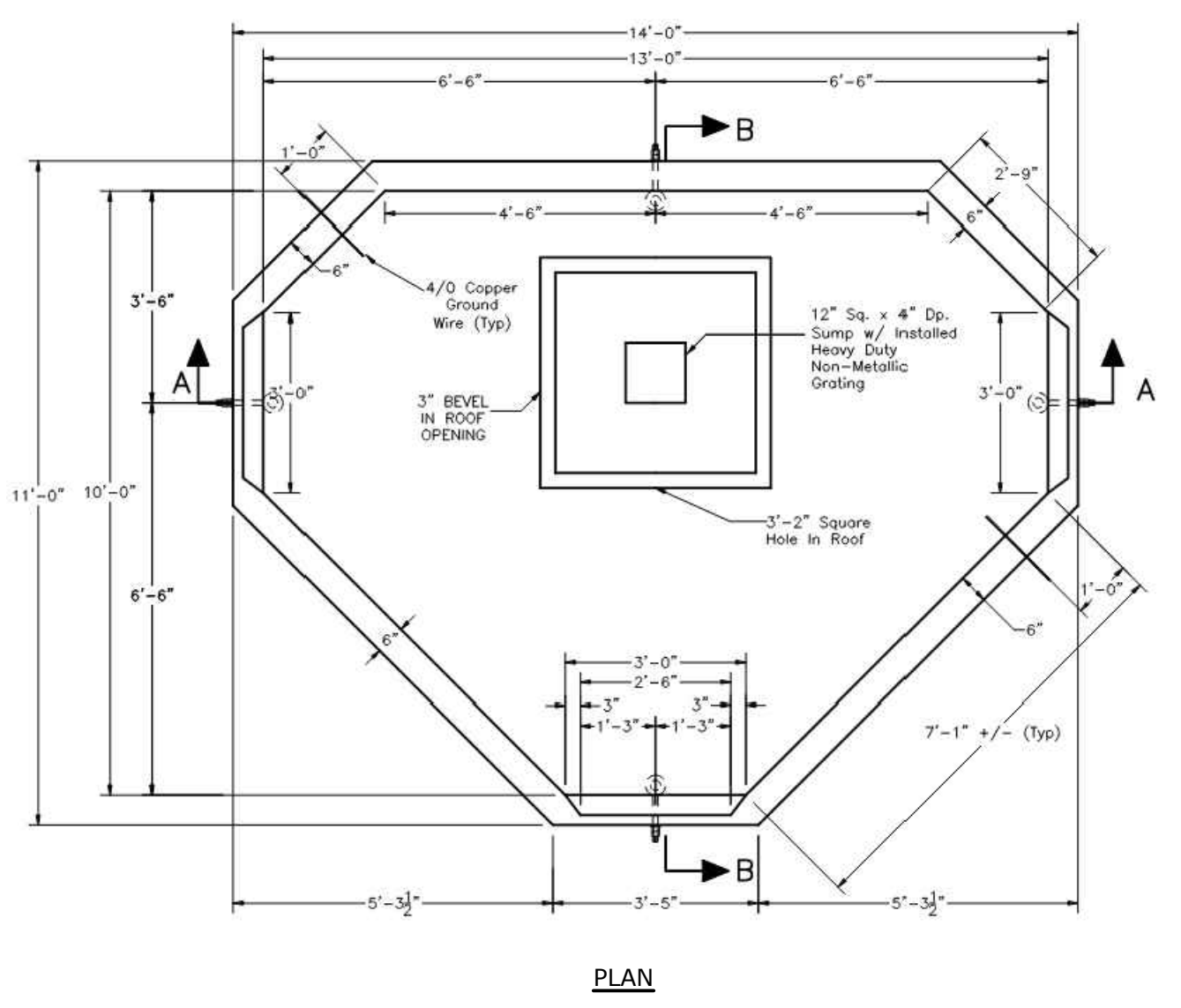
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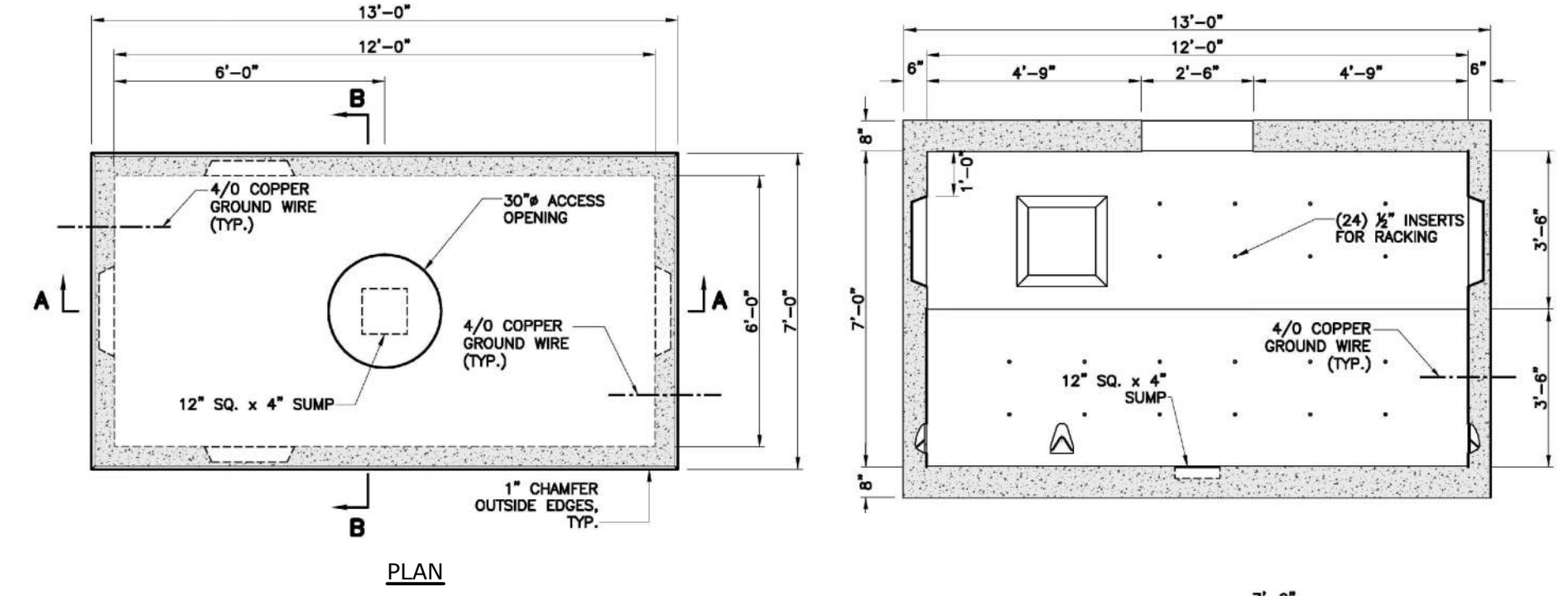
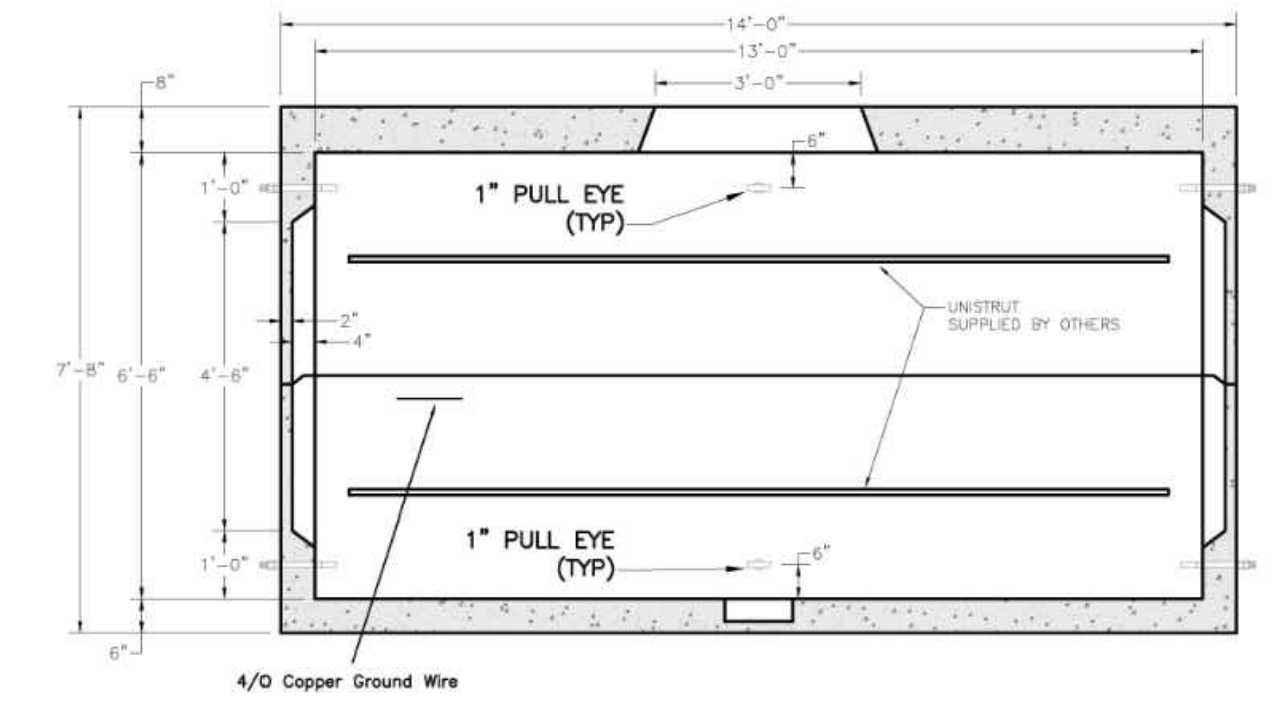
- NOTES:**
- DIMENSIONS SHOWN REPRESENT TYPICAL REQUIREMENTS. MANHOLE LOCATIONS AND REQUIREMENTS SHALL BE COORDINATED WITH EVERSOURCE PRIOR TO CONSTRUCTION.
 - CONCRETE MINIMUM STRENGTH - 4,000 PSI @ 28 DAYS
 - STEEL REINFORCEMENT - ASTM A615, GRADE 60
 - PAD MEETS OR EXCEEDS EVERSOURCE SPECIFICATIONS
 - TRANSFORMER PAD SHALL BE REVIEWED AND APPROVED BY EVERSOURCE PRIOR TO CONSTRUCTION.

TRANSFORMER PAD DETAIL
NO SCALE



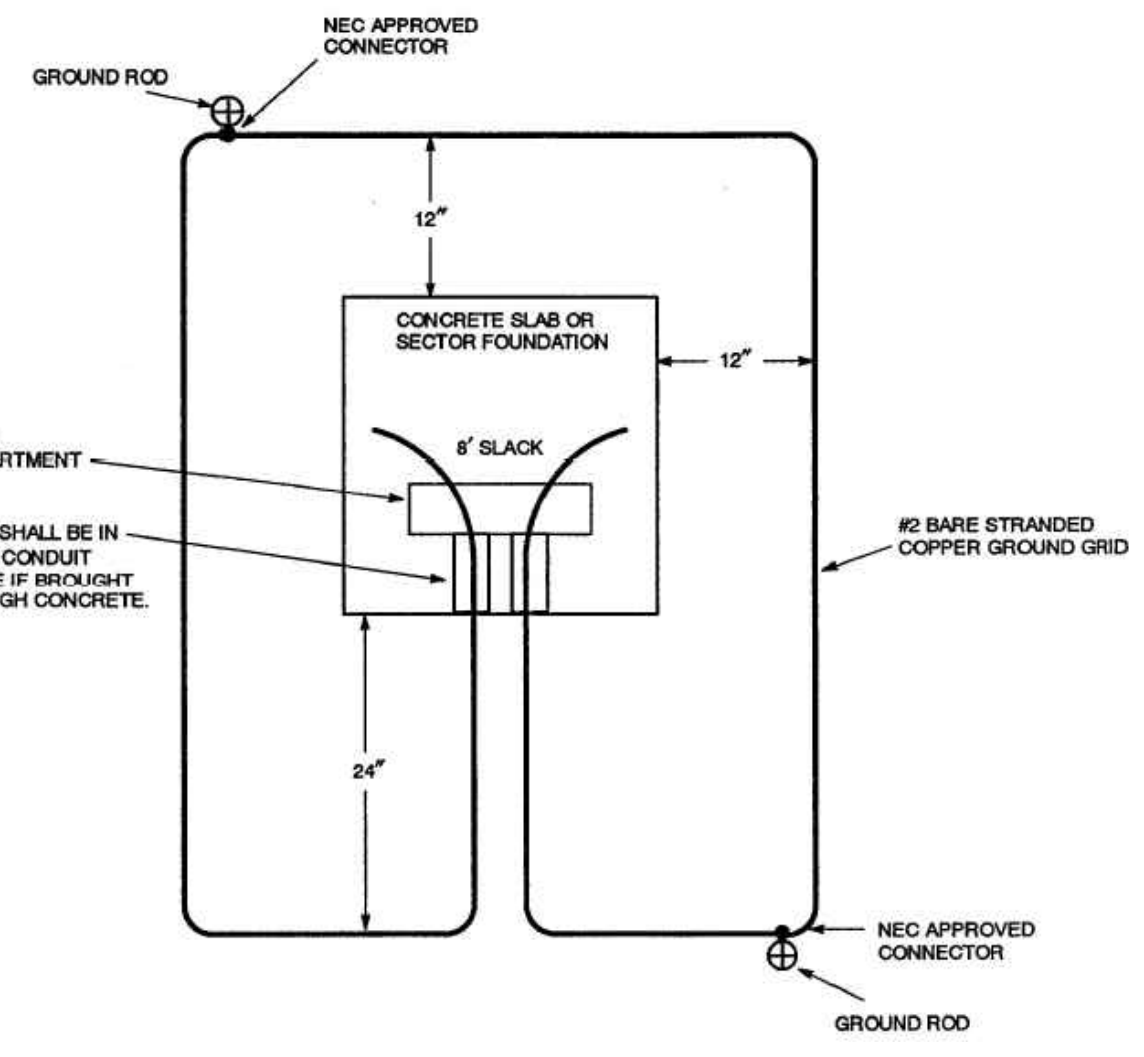
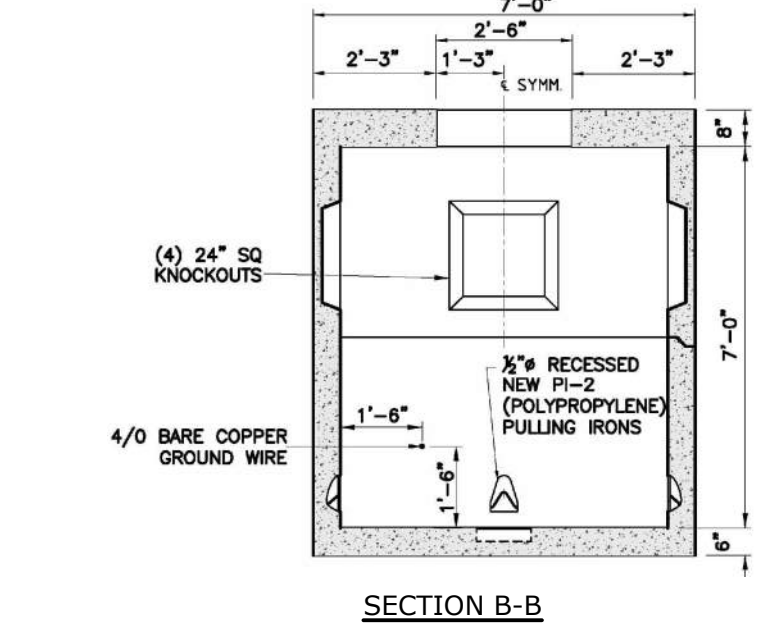
- NOTES:**
- DIMENSIONS SHOWN REPRESENT TYPICAL REQUIREMENTS. HAND HOLE LOCATIONS AND REQUIREMENTS SHALL BE COORDINATED WITH THE UTILITY COMPANY TO CONSTRUCTION.
 - CONCRETE MINIMUM STRENGTH - 5,000 PSI @ 28 DAYS
 - STEEL REINFORCEMENT - ASTM A615, GRADE 60
 - HAND HOLE SHALL BE REVIEWED AND APPROVED BY THE UTILITY COMPANY PRIOR TO CONSTRUCTION.

COMMUNICATIONS HAND HOLE DETAIL
NO SCALE



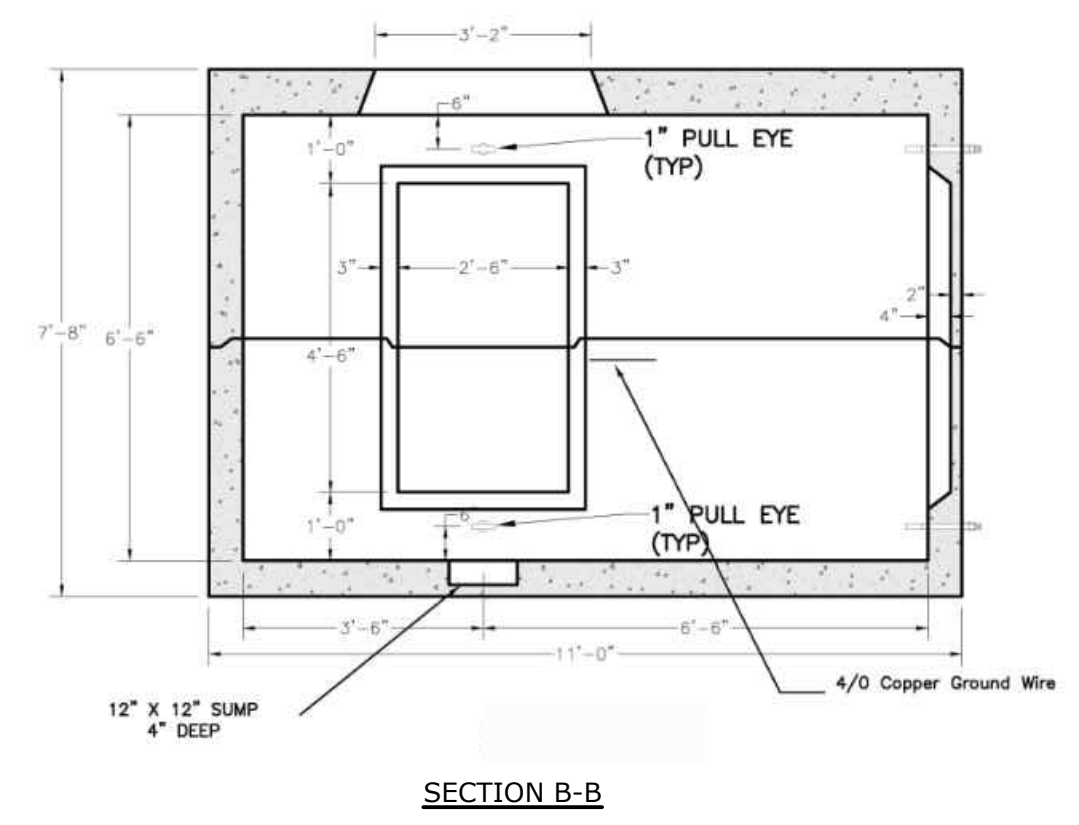
- NOTES:**
- DIMENSIONS SHOWN REPRESENT TYPICAL REQUIREMENTS. MANHOLE LOCATIONS AND REQUIREMENTS SHALL BE COORDINATED WITH EVERSOURCE PRIOR TO CONSTRUCTION.
 - CONCRETE MINIMUM STRENGTH - 5,000 PSI @ 28 DAYS
 - STEEL REINFORCEMENT - ASTM A615, GRADE 60
 - MINIMUM STEEL COVER - 1 INCH
 - DESIGN LOADING - AASHTO HS20-44
 - EXTERIOR COATING PROVIDED
 - ELECTRIC MANHOLE SHALL BE REVIEWED AND APPROVED BY EVERSOURCE PRIOR TO CONSTRUCTION.

TYPICAL ELECTRIC MANHOLE
NO SCALE



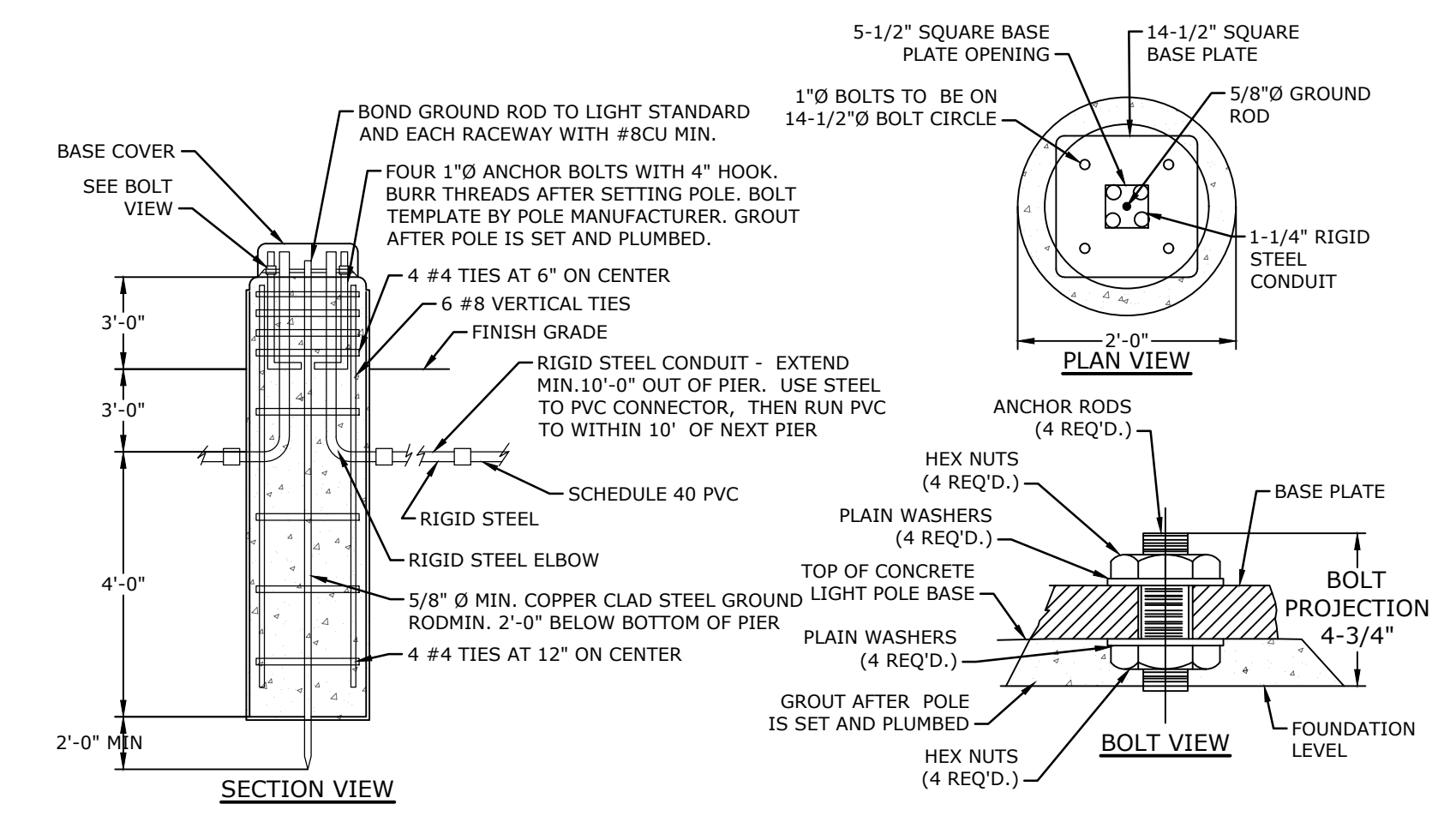
- NOTES:**
- THE GROUND GRID SHALL BE SUPPLIED AND INSTALLED BY THE CONTRACTOR AND IS TO BE BURIED AT LEAST 12 INCHES BELOW GRADE. EIGHT FEET OF EXTRA WIRE FOR EACH GROUND GRID LEG SHALL BE LEFT EXPOSED IN THE CABLE COMPARTMENT TO ALLOW FOR THE CONNECTION TO THE TRANSFORMER. THE TWO 8-FOOT GROUND RODS MAY BE EITHER GALVANIZED STEEL OR COPPERWELD AND THEY SHALL BE CONNECTED TO THE GRID WITH NEC APPROVED CONNECTORS.

TYPICAL PAD-MOUNTED EQUIPMENT GROUNDING GRID DETAIL
NO SCALE



- NOTES:**
- DIMENSIONS SHOWN REPRESENT TYPICAL REQUIREMENTS. MANHOLE LOCATIONS AND REQUIREMENTS SHALL BE COORDINATED WITH EVERSOURCE PRIOR TO CONSTRUCTION.
 - CONCRETE MINIMUM STRENGTH - 5,000 PSI @ 28 DAYS
 - STEEL REINFORCEMENT - ASTM A615, GRADE 60
 - MINIMUM STEEL COVER - 1 INCH
 - DESIGN LOADING - AASHTO HS20-44
 - EXTERIOR COATING PROVIDED
 - ELECTRIC MANHOLE SHALL BE REVIEWED AND APPROVED BY EVERSOURCE PRIOR TO CONSTRUCTION.

3-WAY ELECTRIC MANHOLE
NO SCALE



- NOTES:**
- PAINT BASE SAFETY YELLOW (UNLESS PROTECTED BY CURBED ISLAND).
 - CONCRETE TO BE CLASS A, 4000 PSI, AIR ENTRAINED STEEL TO BE 60 KSI
 - REFER TO ELECTRICAL PLANS FOR WIRING DETAILS.
 - LIGHT POLE BASE DETAIL FOR BIDDING PURPOSES ONLY. CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR APPROVAL, TO INCLUDE PERFORMANCE SPECIFICATIONS, CALCULATIONS AND NH LICENSED STRUCTURAL ENGINEER'S STAMP FOR LIGHT POLE FOUNDATION.

TYPICAL LIGHT POLE BASE
NO SCALE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

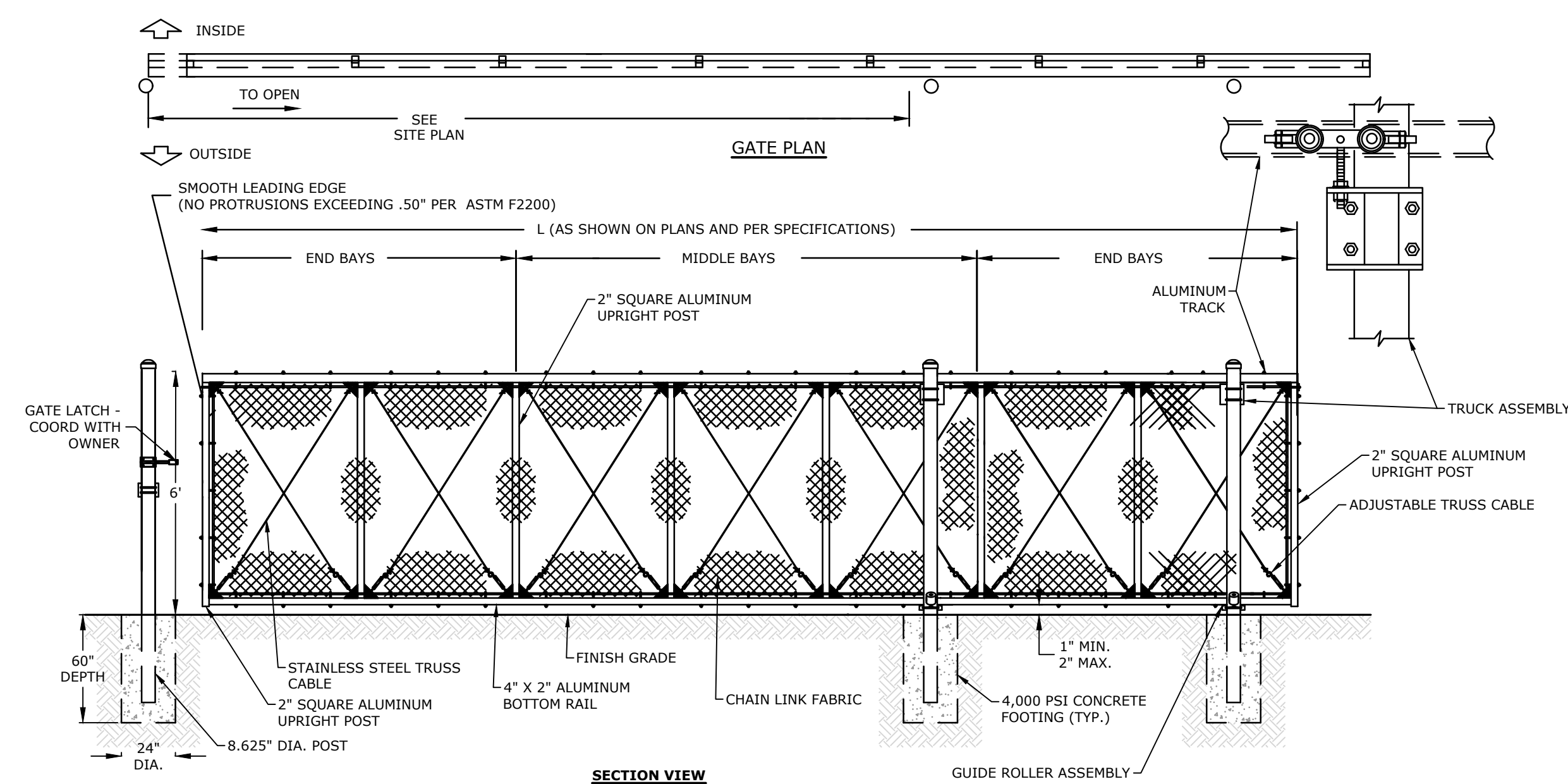
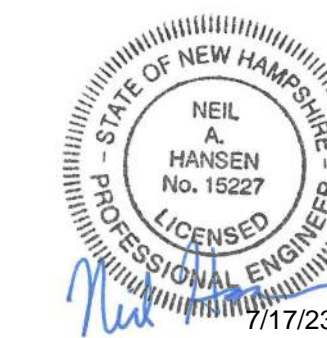
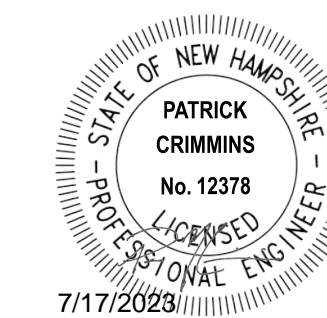
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F	11/6/2018	P.B. Submission

PROJECT NO: L-0700-013
 DATE: 04/03/2018
 FILE: L-0700-026-C-DTLS.dwg
 DRAWN BY: CIK
 CHECKED: NAH
 APPROVED: PMC

DETAILS SHEETS

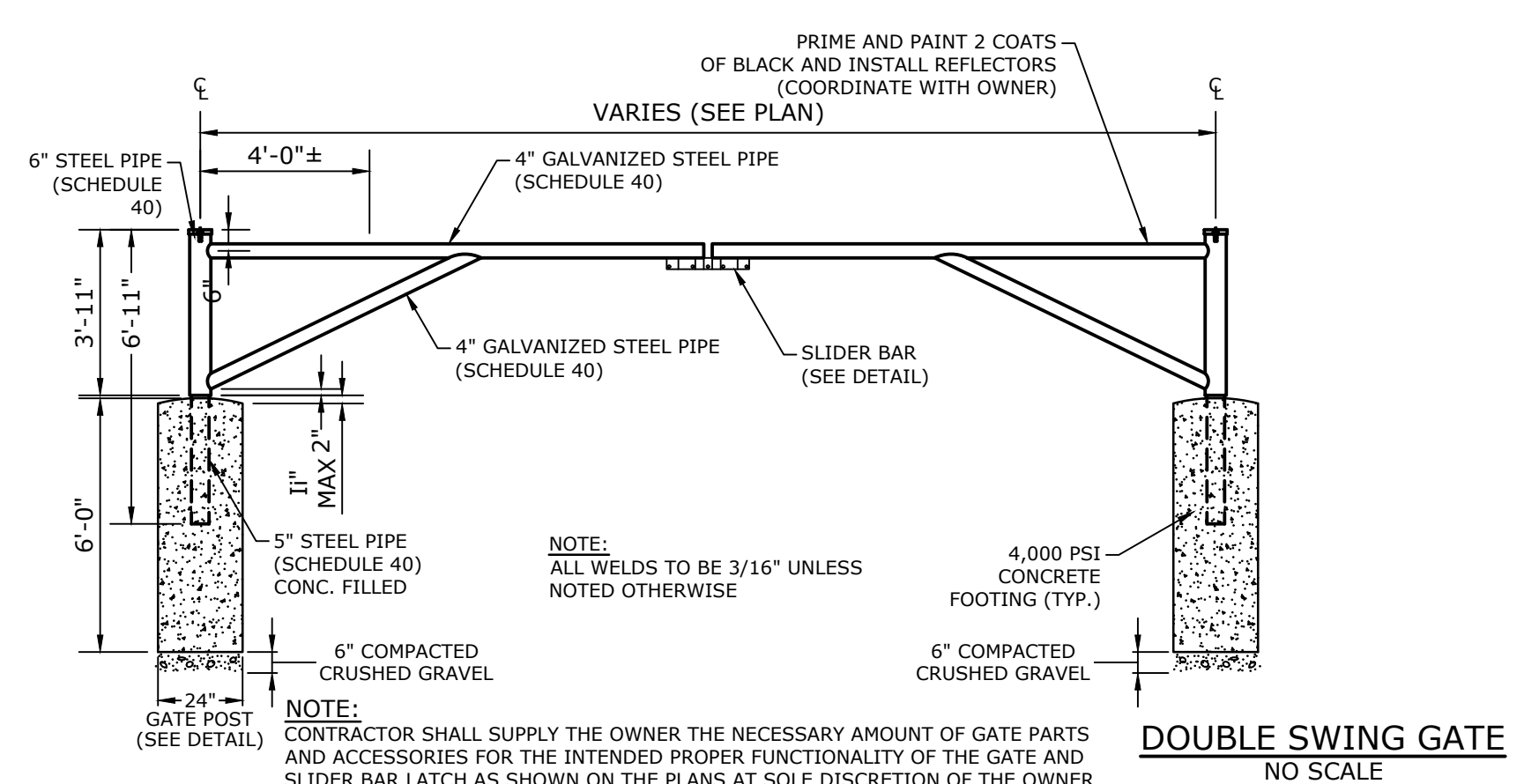
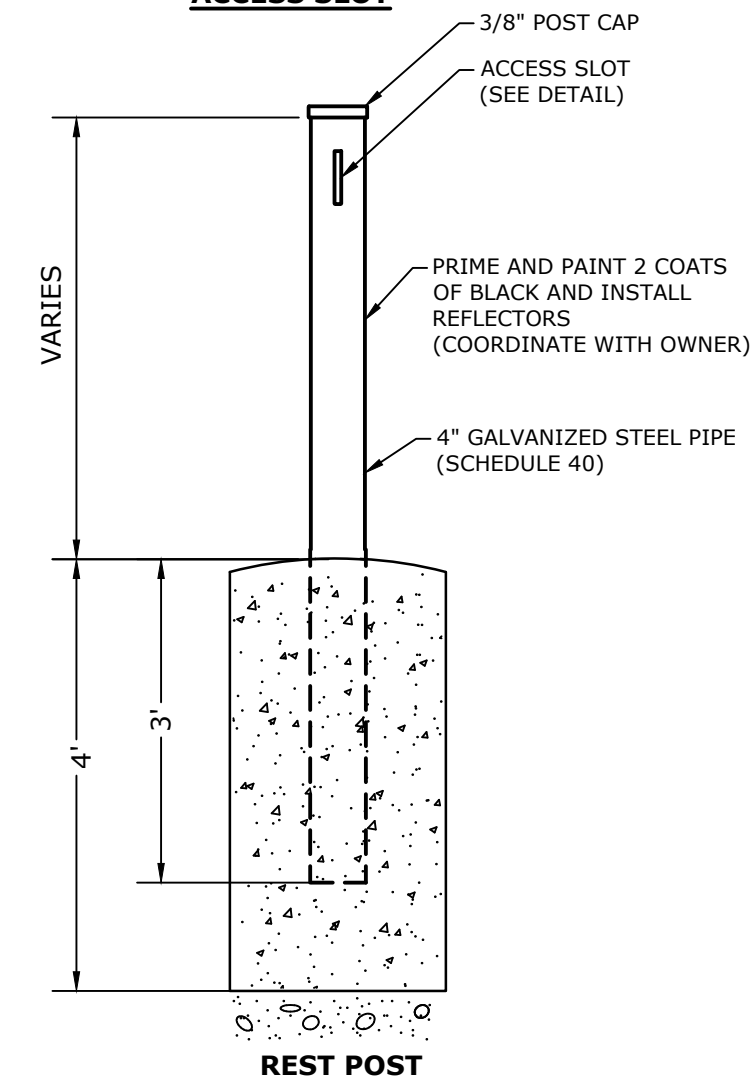
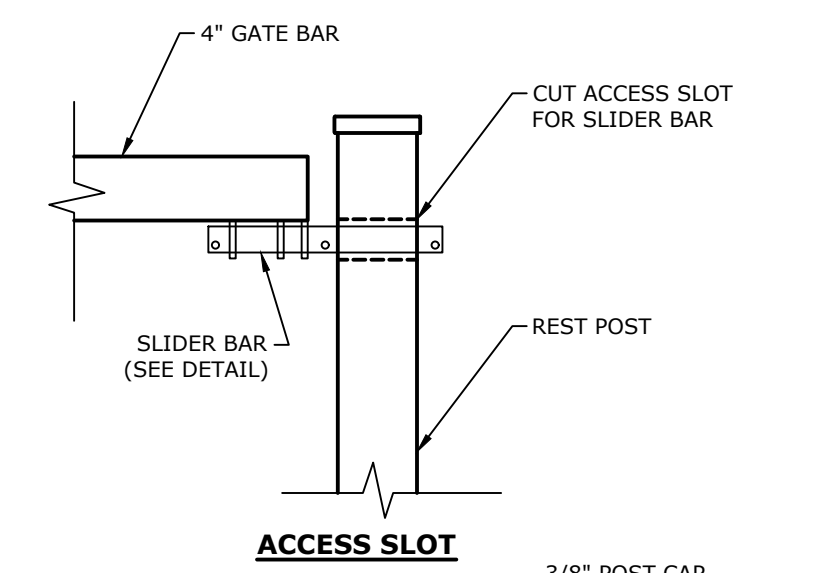
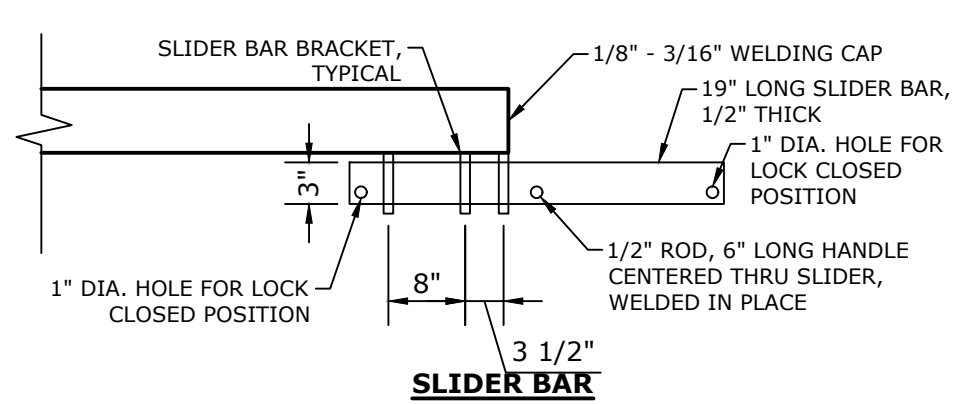
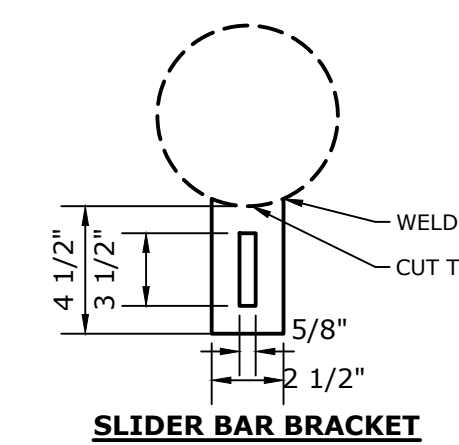
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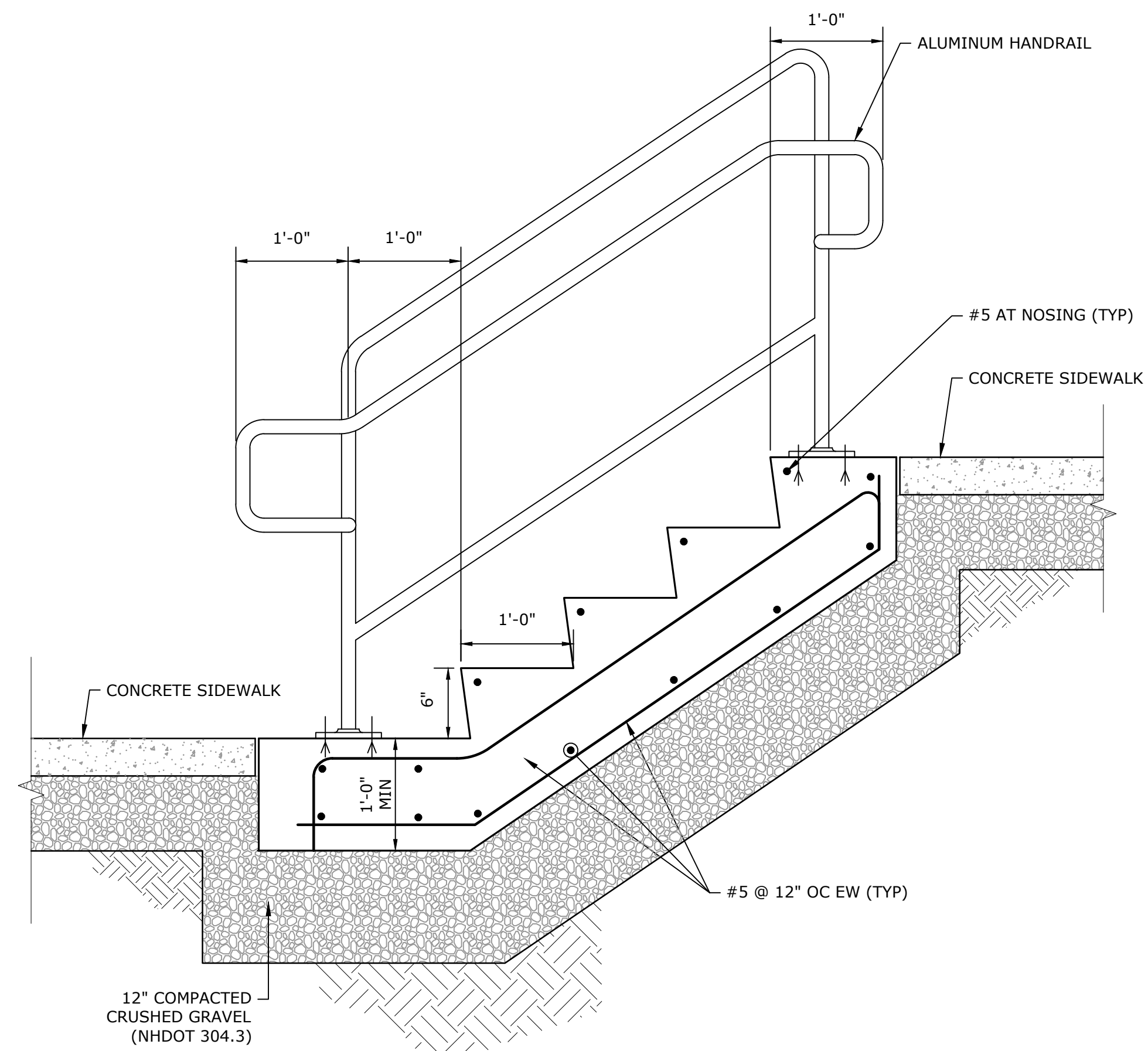


- NOTES:**
1. ALL GATE FRAMES SHALL BE A MINIMUM 1.90\"/>

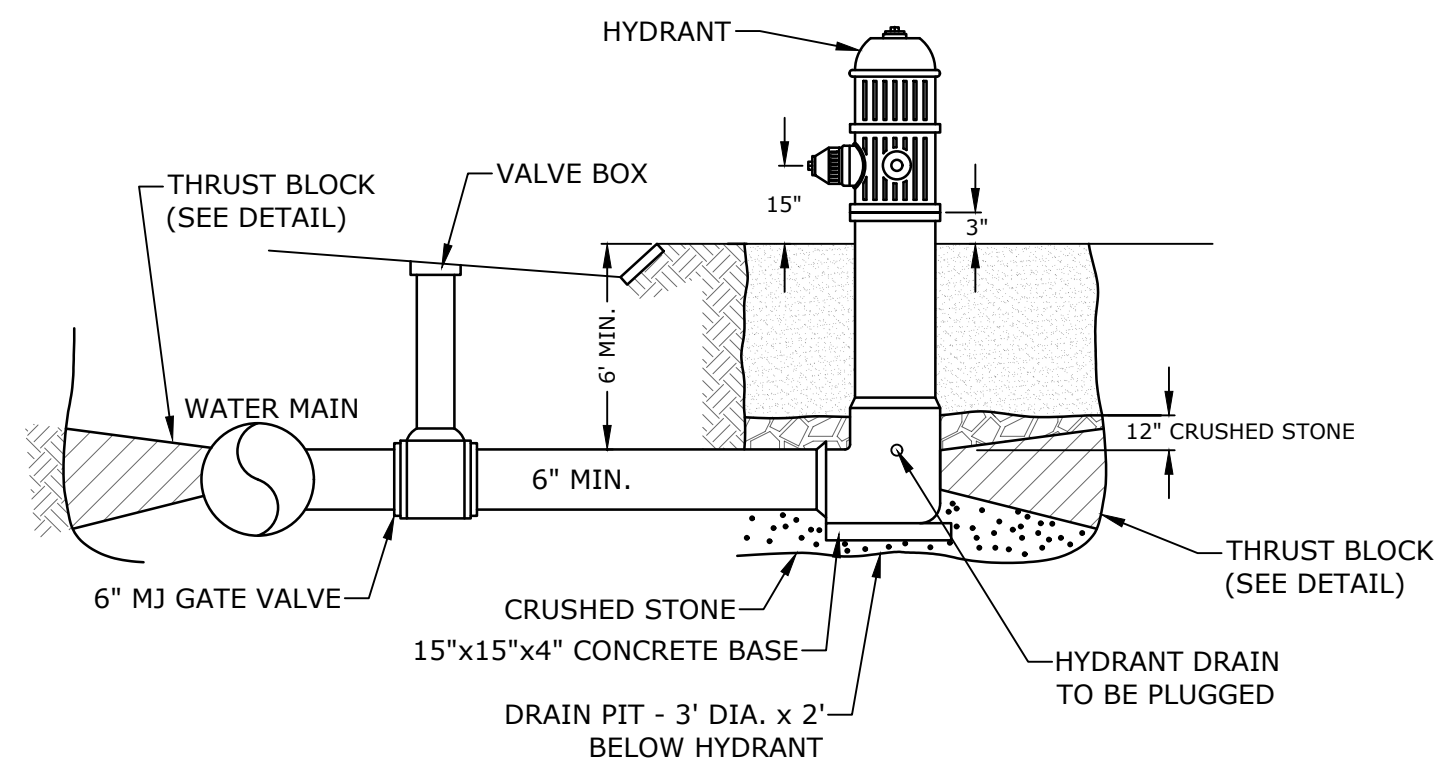
CANTILEVERED SLIDING GATE
NO SCALE



DOUBLE SWING GATE
NO SCALE



CONCRETE STAIRS AND HANDRAIL
NO SCALE



- NOTES:**
1. HYDRANT TO BE KENNEDY TYPE K-81, RIGHT OPEN (NO EQUAL). COORDINATE WITH CITY OF PORTSMOUTH WATER DEPARTMENT AND CITY OF PORTSMOUTH FIRE DEPARTMENT.
 2. PAINT HYDRANT IN ACCORDANCE WITH CITY STANDARD SPECIFICATIONS AFTER INSTALLATION AND TESTING.

FIRE HYDRANT
NO SCALE

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

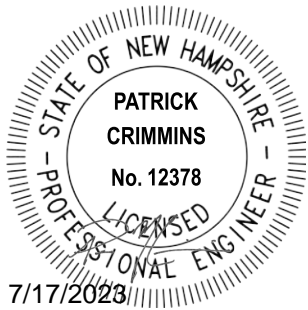
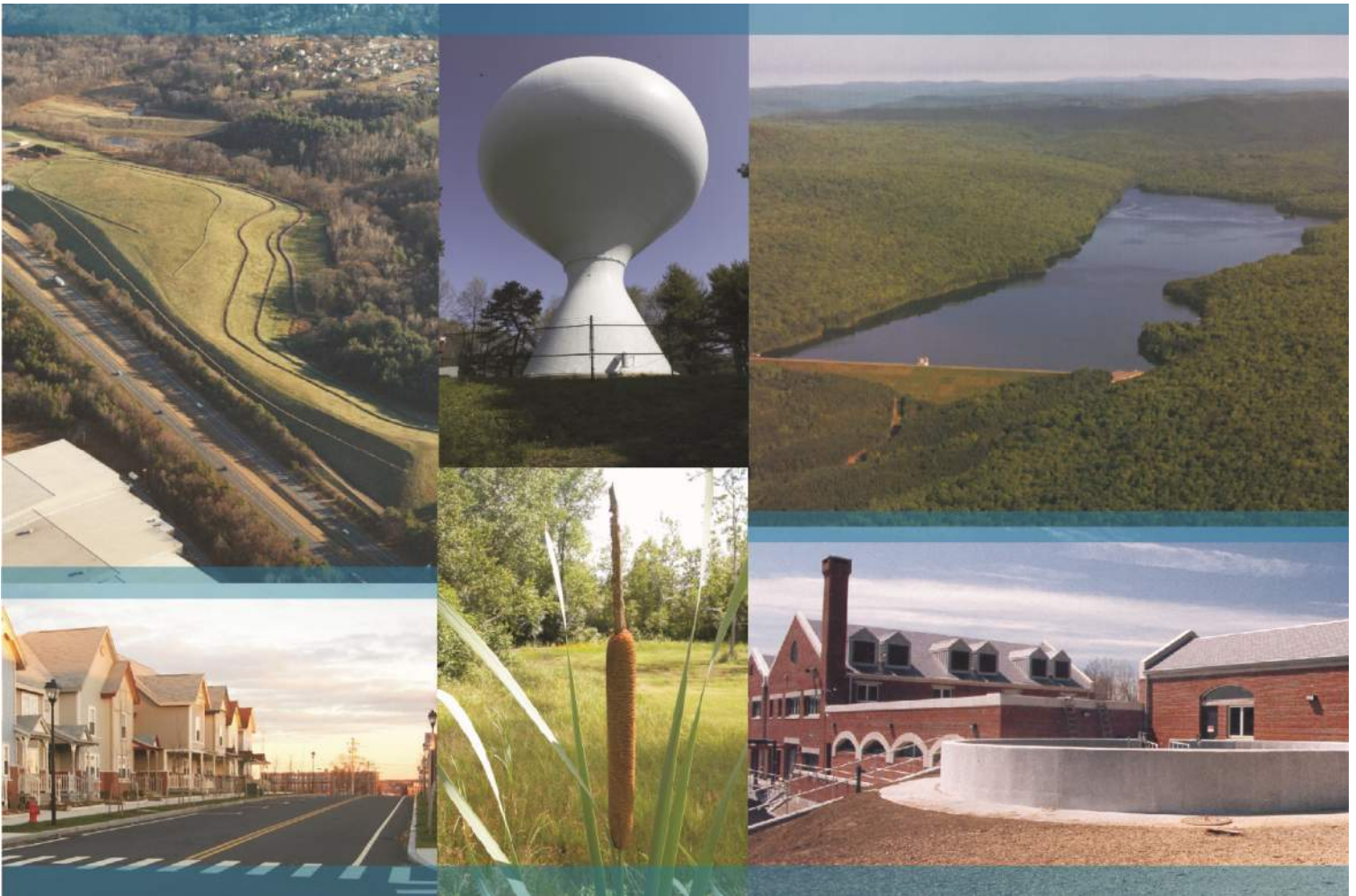
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MARK	DATE	DESCRIPTION
PROJECT NO:		L-0700-013
DATE:		04/03/2018
FILE:		L-0700-026-C-DTLS.dwg
DRAWN BY:		CJK
CHECKED:		NAH
APPROVED:		PMC

DETAILS SHEETS

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C-512

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Tighe&Bond

Iron Parcel Redevelopment
 70 & 80 Corporate Drive
 Portsmouth, New Hampshire

Drainage Analysis

Prepared For:

Lonza Biologics
101 International Drive
Portsmouth, New Hampshire

June 18, 2018
 Last Revised: July 17, 2023

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Appendices

A Civil Plans (Bound Separately)

B Extreme Precipitation Tables

C Soils Report and Boring Logs

D Full Size Watershed Plans

E BMP Worksheets

F Rip Rap Calculations

J:\L\L0700 Lonza Biologics Expansion was 1576F\026_Project Albacore\Report_Evaluations\Applications\City of Portsmouth\20230616 TAC Submission\Drainage\Working Files\L-0700-026_Drainage Analysis.docx

Section 1

Drainage Analysis

The proposed project is to expand Lonza Biologics facility to support its growing product development services to the pharmaceutical and biologic industries. The project is located on the vacant portion of Lonza's 46-acre parcel, referred to as the Iron Parcel, that once consisted of military housing and streets for Pease Air Force Base. The houses and roads were removed in the mid to late 1990's as part of the Civil Redevelopment Plan for Pease after the closure of the Air Force Base.

The total master plan build-out of the proposed industrial development is depicted in the enclosed Site Plan set. The master plan includes three (3) new buildings totaling approximately 800,000 square feet of gross floor area, a central utility building, and a new parking garage. The project's site improvements consist of drive aisles, sidewalks, fire lanes, utilities, lighting and landscaping. The site improvements will consist of new stormwater management systems that include two (2) gravel wetlands and one (1) rain garden. The project has already received an Alteration of Terrain Permit from the New Hampshire Department of Environmental Services (NHDES) for the stormwater management design.

This master plan will be constructed in phases. Full-buildout will take several years and must be completed in phases as Lonza identifies clients and fits out the buildings to meet their needs. The master plan has been broken out into three phases, Phase 1A, Phase 1B, and Phase 2. Currently, Phase 1A construction is nearing completion, and Phase 1B work will be breaking ground in mid-July 2023. Both Phase 1A and Phase 1B received site plan approvals in 2019, therefore the drainage analysis of those phases is not included in this analysis. The following summarizes the work completed during Phase 1A and to be completed during Phase 1B:

Phase 1A

- Construction of the stream
- Removal of the existing culvert
- Construction of the sidewalk and landscaping along Corporate Drive
- Completion of Soils Management Plan

Phase 1B

- Construction of building #1 shell
- Construction site improvements for building #1 such as drive aisles, fire lanes, utilities, lighting, sidewalks and stormwater management including Gravel Wetland #1
- Construction utility building shell
- Temporary gravel area for construction trailers, parking, and laydown in the approximate location of Proposed Building #3
- Intermittent grading between stream and Building #1
- Temporary sedimentation basins at locations of Gravel Wetland #2 and Rain Garden #1

Accordingly, this drainage analysis is submitted to analyze the Phase 2 and Master plan portions of the project in conjunction with the site plan review permitting of these phases. The stormwater design of the master plan has not changed from the 2019 approvals and the Alteration of Terrain Permit Approvals. Phase 2 of the project includes the internal fit-up of Building #1 and Central Utility Building, the construction of a temporary surface parking lot to support the employees of Building #1, the construction of Gravel Wetland #2, and their associated miscellaneous site improvements.

The pre-development conditions analyzed in this analysis are the 2018 pre-construction conditions. These pre-development conditions are the same pre-development conditions that were included in the drainage analysis for the 2018 site review permit application for Phase 1A, Phase 1B, and the Master Plan.

1.1 Calculation Methods

The design storms analyzed in this study are the 2-year, 10-year, 25-year and 50-year 24-hour duration storm events. The pre-development 1-year, 24-hour duration storm was also analyzed for channel protection requirements. The stormwater modeling system, HydroCAD 10.0 was utilized to predict the peak runoff rates from these storm events. The peak discharge rates were determined by analyzing Type III 24-hour storm events. The rainfall data for these storm events was obtained from the data published by the Northeast Regional Climate Center at Cornell University, with an additional 15% added factor of safety as required by Env-Wq 1503.08(I).

TABLE 1.1 – EXTREME PRECIPITATION ESTIMATES (NRCC)

YEAR	24-hr Estimate (inches)	+ 15% (inches)
1	2.65	3.05
2	3.20	3.68
10	4.85	5.58
25	6.15	7.07
50	7.36	8.46

Tailwater conditions in the inlet structure PDMH203 and at the outlet of the existing triple arch culverts into the road side swale on Goose Bay Drive have been included in these calculations to account for any surcharging that may occur due to the tailwater condition. These tailwater elevations were determined by Streamworks, PLLC as part of their overall watershed analysis.

The time of concentration was computed using the TR-55 Method, which provides a means of determining the time for an entire watershed to contribute runoff to a specific location via sheet flows, shallow concentrated flow, and channel flow. Runoff curve numbers were calculated by estimating the coverage areas and then summing the curve number for the coverage area as a percent of the entire watershed.

References:

1. HydroCAD Stormwater Modeling System, by HydroCAD Software Solutions LLC, Chocorua, New Hampshire.
2. New Hampshire Stormwater Management Manual, Volume 2, Post-Construction Best Management Practices Selection and Design, December 2008.
3. "Extreme Precipitation in New York & New England." Extreme Precipitation in New York & New England by Northeast Regional Climate Center (NRCC), 26 June 2012.

1.2 Pre-Development Conditions

In order to analyze the pre-development condition, the site has been divided into three watershed areas modeled at two points of analysis. These points of analysis and watersheds are depicted on the plan entitled "Pre-Development Watershed Plan", Sheet C-801.

Each of the points of analysis and their contributing watershed areas are described below:

Point of Analysis (PA1)

PRE 1.0 makes up almost the entire area to be developed. This area consists of the entire undeveloped parcel, as well as, a portion of Corporate Drive that drains onto the parcel via a closed drainage system. The pre-development conditions of the watershed was an undeveloped field area that with a portion of the site being used as a temporary construction parking area with associated stormwater management controls near the center of the parcel. Runoff from this area travels southeast via overland flow to Point of Analysis 1 located at the existing Hodgson Brook outlet headwall.

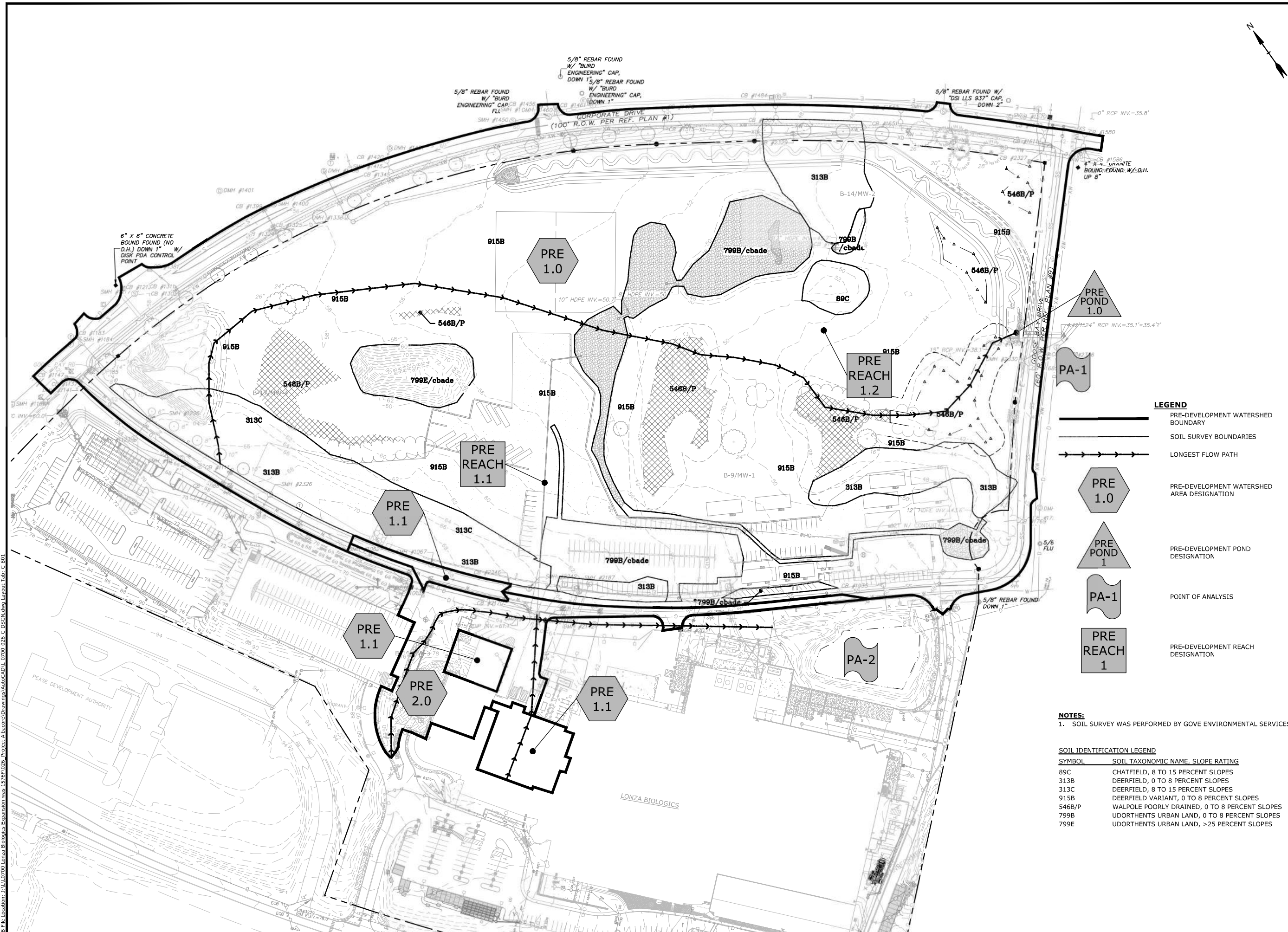
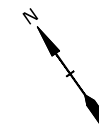
PRE 1.1 includes roof drain runoff from the existing Lonza facility located at 101 International Drive that is connected into the existing Hodgson Brook Culvert. There was also a small portion of Goose Bay Drive that enters this culvert.

The existing tailwater elevations for the road side swale along Goose Bay Drive were determined by Streamworks, PLLC as a part of their overall watershed analysis.

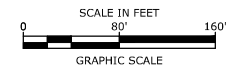
Point of Analysis (PA2)

PRE 2.0 is comprised mostly of runoff from Goose Bay Drive that is located between the undeveloped parcel and the existing Lonza facility. Runoff from this area travels via overland flow to the existing stormwater basin located at the existing Lonza facility. Point of Analysis 2 (PA2) is located at the existing basin.

1.2.1 Pre-Development Watershed Plan



- LEGEND**
- PRE-DEVELOPMENT WATERSHED BOUNDARY
 - SOIL SURVEY BOUNDARIES
 - LONGEST FLOW PATH
 - PRE-DEVELOPMENT WATERSHED AREA DESIGNATION
 - PRE-DEVELOPMENT POND DESIGNATION
 - POINT OF ANALYSIS
 - PRE-DEVELOPMENT REACH DESIGNATION



Proposed Industrial Development
Lonza Biologics
Portsmouth, New Hampshire

NOTES:
1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHENTS URBAN LAND, >25 PERCENT SLOPES

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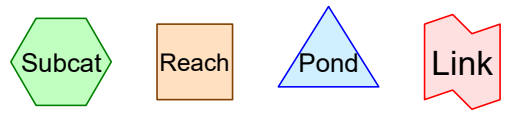
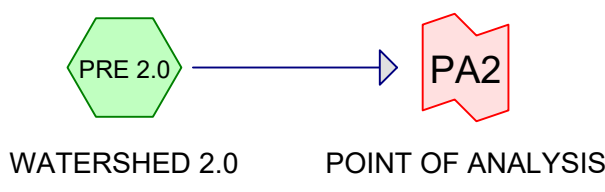
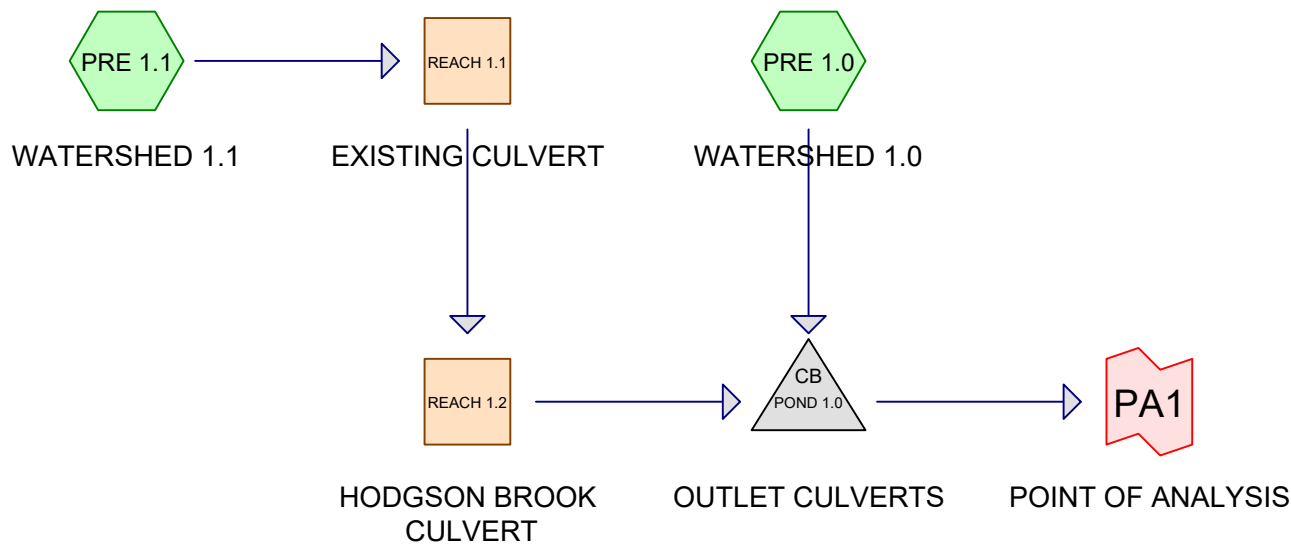
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PRE-DEVELOPMENT WATERSHED AREA PLAN

SCALE: AS SHOWN

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1.2.2 Pre-Development Calculations



Routing Diagram for L-0700-26 PRE
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L-0700-26 PRE

Prepared by Tighe & Bond

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Page 2

Area Listing (selected nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.736	74	>75% Grass cover, Good, HSG C (PRE 1.1, PRE 2.0)
2.274	91	Gravel roads, HSG D (PRE 1.0)
3.289	58	Meadow, non-grazed, HSG B (PRE 1.0)
19.420	71	Meadow, non-grazed, HSG C (PRE 1.0)
0.044	78	Meadow, non-grazed, HSG D (PRE 1.0)
3.668	98	Paved parking, HSG C (PRE 1.0, PRE 1.1, PRE 2.0)
0.758	98	Roofs, HSG C (PRE 1.1, PRE 2.0)
0.297	55	Woods, Good, HSG B (PRE 1.0)
1.123	70	Woods, Good, HSG C (PRE 1.0)
31.609	75	TOTAL AREA

L-0700-26 PRE

Prepared by Tighe & Bond

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Soil Listing (selected nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
3.586	HSG B	PRE 1.0
25.705	HSG C	PRE 1.0, PRE 1.1, PRE 2.0
2.318	HSG D	PRE 1.0
0.000	Other	
31.609		TOTAL AREA

L-0700-26 PRE

Type III 24-hr 2 Year Rainfall=3.68"

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Page 4

Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,727 sf 9.69% Impervious Runoff Depth>1.35"
Flow Length=1,805' Tc=34.4 min CN=74 Runoff=24.04 cfs 3.305 af

Subcatchment PRE 1.1: WATERSHED 1.1 Runoff Area=33,611 sf 90.29% Impervious Runoff Depth>3.22"
Flow Length=305' Tc=5.0 min CN=96 Runoff=2.71 cfs 0.207 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=67,564 sf 57.38% Impervious Runoff Depth>2.43"
Flow Length=872' Tc=5.0 min CN=88 Runoff=4.41 cfs 0.314 af

Reach REACH 1.1: EXISTING CULVERT Avg. Flow Depth=0.47' Max Vel=6.37 fps Inflow=2.71 cfs 0.207 af
15.0" Round Pipe n=0.012 L=515.0' S=0.0165 '/ Capacity=8.99 cfs Outflow=2.66 cfs 0.207 af

Reach REACH 1.2: HODGSON BROOK Avg. Flow Depth=0.34' Max Vel=4.72 fps Inflow=2.66 cfs 0.207 af
48.0" Round Pipe n=0.012 L=825.0' S=0.0112 '/ Capacity=164.33 cfs Outflow=2.46 cfs 0.207 af

Pond POND 1.0: OUTLET CULVERTS Peak Elev=38.24' Inflow=24.73 cfs 3.511 af
42.0" x 29.0", R=21.5"/66.1" Pipe Arch Culvert x 3.00 n=0.025 L=68.0' S=0.0044 '/ Outflow=24.86 cfs 3.511 af

Link PA1: POINT OF ANALYSIS Inflow=24.86 cfs 3.511 af
Primary=24.86 cfs 3.511 af

Link PA2: POINT OF ANALYSIS Inflow=4.41 cfs 0.314 af
Primary=4.41 cfs 0.314 af

Total Runoff Area = 31.609 ac Runoff Volume = 3.826 af Average Runoff Depth = 1.45"
86.00% Pervious = 27.184 ac 14.00% Impervious = 4.426 ac

L-0700-26 PRE

Prepared by Tighe & Bond

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Type III 24-hr 10 Year Rainfall=5.58"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,727 sf 9.69% Impervious Runoff Depth>2.81"
Flow Length=1,805' Tc=34.4 min CN=74 Runoff=51.44 cfs 6.869 af

Subcatchment PRE 1.1: WATERSHED 1.1 Runoff Area=33,611 sf 90.29% Impervious Runoff Depth>5.11"
Flow Length=305' Tc=5.0 min CN=96 Runoff=4.19 cfs 0.328 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=67,564 sf 57.38% Impervious Runoff Depth>4.22"
Flow Length=872' Tc=5.0 min CN=88 Runoff=7.49 cfs 0.545 af

Reach REACH 1.1: EXISTING CULVERT Avg. Flow Depth=0.59' Max Vel=7.16 fps Inflow=4.19 cfs 0.328 af
15.0" Round Pipe n=0.012 L=515.0' S=0.0165 '/' Capacity=8.99 cfs Outflow=4.12 cfs 0.328 af

Reach REACH 1.2: HODGSON BROOK Avg. Flow Depth=0.42' Max Vel=5.42 fps Inflow=4.12 cfs 0.328 af
48.0" Round Pipe n=0.012 L=825.0' S=0.0112 '/' Capacity=164.33 cfs Outflow=3.88 cfs 0.328 af

Pond POND 1.0: OUTLET CULVERTS Peak Elev=39.02' Inflow=52.53 cfs 7.196 af
42.0" x 29.0", R=21.5"/66.1" Pipe Arch Culvert x 3.00 n=0.025 L=68.0' S=0.0044 '/' Outflow=52.69 cfs 7.195 af

Link PA1: POINT OF ANALYSIS Inflow=52.69 cfs 7.195 af
Primary=52.69 cfs 7.195 af

Link PA2: POINT OF ANALYSIS Inflow=7.49 cfs 0.545 af
Primary=7.49 cfs 0.545 af

Total Runoff Area = 31.609 ac Runoff Volume = 7.742 af Average Runoff Depth = 2.94"
86.00% Pervious = 27.184 ac 14.00% Impervious = 4.426 ac

L-0700-26 PRE

Prepared by Tighe & Bond

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Type III 24-hr 10 Year Rainfall=5.58"

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Page 6

Summary for Subcatchment PRE 1.0: WATERSHED 1.0

Runoff = 51.44 cfs @ 12.49 hrs, Volume= 6.869 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
143,279	58	Meadow, non-grazed, HSG B
12,922	55	Woods, Good, HSG B
845,939	71	Meadow, non-grazed, HSG C
123,662	98	Paved parking, HSG C
48,932	70	Woods, Good, HSG C
1,932	78	Meadow, non-grazed, HSG D
99,061	91	Gravel roads, HSG D
1,275,727	74	Weighted Average
1,152,065		90.31% Pervious Area
123,662		9.69% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
6.9	100	0.0400	0.24		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
0.1	11	0.0400	1.40		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
1.0	70	0.0290	1.19		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
21.4	1,089	0.0147	0.85		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
1.6	120	0.0330	1.27		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
3.2	368	0.0160	1.90		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.2	47	0.0050	4.03	4.95	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.012 Concrete pipe, finished
34.4	1,805	Total			

Summary for Subcatchment PRE 1.1: WATERSHED 1.1

[49] Hint: Tc<2dt may require smaller dt

Runoff = 4.19 cfs @ 12.07 hrs, Volume= 0.328 af, Depth> 5.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

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Type III 24-hr 10 Year Rainfall=5.58"

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Area (sf)	CN	Description
22,865	98	Roofs, HSG C
3,263	74	>75% Grass cover, Good, HSG C
7,483	98	Paved parking, HSG C
33,611	96	Weighted Average
3,263		9.71% Pervious Area
30,348		90.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.0	100	0.0050	0.85		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
1.2	205	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
3.2	305	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment PRE 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

Runoff = 7.49 cfs @ 12.07 hrs, Volume= 0.545 af, Depth> 4.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
10,145	98	Roofs, HSG C
28,794	74	>75% Grass cover, Good, HSG C
28,625	98	Paved parking, HSG C
67,564	88	Weighted Average
28,794		42.62% Pervious Area
38,770		57.38% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.7	100	0.0650	2.36		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
1.5	320	0.0560	3.55		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.2	42	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Cast iron, coated
1.3	410	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013 Corrugated PE, smooth interior
3.7	872	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach REACH 1.1: EXISTING CULVERT

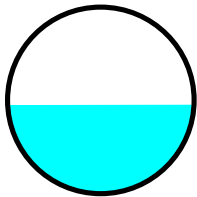
[52] Hint: Inlet/Outlet conditions not evaluated

Inflow Area = 0.772 ac, 90.29% Impervious, Inflow Depth > 5.11" for 10 Year event
Inflow = 4.19 cfs @ 12.07 hrs, Volume= 0.328 af
Outflow = 4.12 cfs @ 12.09 hrs, Volume= 0.328 af, Atten= 2%, Lag= 1.2 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity= 7.16 fps, Min. Travel Time= 1.2 min
Avg. Velocity = 2.41 fps, Avg. Travel Time= 3.6 min

Peak Storage= 296 cf @ 12.09 hrs
Average Depth at Peak Storage= 0.59'
Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 8.99 cfs

15.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 515.0' Slope= 0.0165 '/'
Inlet Invert= 53.60', Outlet Invert= 45.10'



Summary for Reach REACH 1.2: HODGSON BROOK CULVERT

[52] Hint: Inlet/Outlet conditions not evaluated

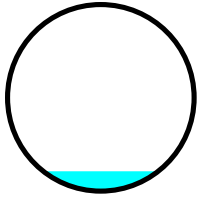
[61] Hint: Exceeded Reach REACH 1.1 outlet invert by 0.42' @ 12.10 hrs

Inflow Area = 0.772 ac, 90.29% Impervious, Inflow Depth > 5.10" for 10 Year event
Inflow = 4.12 cfs @ 12.09 hrs, Volume= 0.328 af
Outflow = 3.88 cfs @ 12.12 hrs, Volume= 0.328 af, Atten= 6%, Lag= 1.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Max. Velocity= 5.42 fps, Min. Travel Time= 2.5 min
Avg. Velocity = 1.85 fps, Avg. Travel Time= 7.4 min

Peak Storage= 588 cf @ 12.12 hrs
Average Depth at Peak Storage= 0.42'
Bank-Full Depth= 4.00' Flow Area= 12.6 sf, Capacity= 164.33 cfs

48.0" Round Pipe
n= 0.012 Concrete pipe, finished
Length= 825.0' Slope= 0.0112 '/'
Inlet Invert= 45.10', Outlet Invert= 35.90'



Summary for Pond POND 1.0: OUTLET CULVERTS

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=123)

[62] Hint: Exceeded Reach REACH 1.2 OUTLET depth by 2.89' @ 12.55 hrs

Inflow Area = 30.058 ac, 11.76% Impervious, Inflow Depth > 2.87" for 10 Year event
 Inflow = 52.53 cfs @ 12.48 hrs, Volume= 7.196 af
 Outflow = 52.69 cfs @ 12.47 hrs, Volume= 7.195 af, Atten= 0%, Lag= 0.0 min
 Primary = 52.69 cfs @ 12.47 hrs, Volume= 7.195 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 39.02' @ 12.47 hrs
 Flood Elev= 41.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	35.60'	42.0" W x 29.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 L= 68.0' CMP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 35.60' / 35.30' S= 0.0044 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 6.72 sf

Primary OutFlow Max=52.41 cfs @ 12.47 hrs HW=39.01' TW=38.65' (Dynamic Tailwater)
 ↳1=CMP_Arch_1/2 42x29 (Outlet Controls 52.41 cfs @ 2.60 fps)

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.0 by 3.05' @ 0.00 hrs (92.51 cfs 19.754 af)

Inflow Area = 30.058 ac, 11.76% Impervious, Inflow Depth > 2.87" for 10 Year event
 Inflow = 52.69 cfs @ 12.47 hrs, Volume= 7.195 af
 Primary = 52.69 cfs @ 12.47 hrs, Volume= 7.195 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet =
 38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area = 1.551 ac, 57.38% Impervious, Inflow Depth > 4.22" for 10 Year event
Inflow = 7.49 cfs @ 12.07 hrs, Volume= 0.545 af
Primary = 7.49 cfs @ 12.07 hrs, Volume= 0.545 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Type III 24-hr 25 Year Rainfall=7.07"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

SubcatchmentPRE 1.0: WATERSHED1.0 Runoff Area=1,275,727 sf 9.69% Impervious Runoff Depth>4.08"
Flow Length=1,805' Tc=34.4 min CN=74 Runoff=74.64 cfs 9.946 af

SubcatchmentPRE 1.1: WATERSHED1.1 Runoff Area=33,611 sf 90.29% Impervious Runoff Depth>6.59"
Flow Length=305' Tc=5.0 min CN=96 Runoff=5.34 cfs 0.424 af

SubcatchmentPRE 2.0: WATERSHED2.0 Runoff Area=67,564 sf 57.38% Impervious Runoff Depth>5.66"
Flow Length=872' Tc=5.0 min CN=88 Runoff=9.90 cfs 0.731 af

Reach REACH 1.1: EXISTING CULVERT Avg. Flow Depth=0.69' Max Vel=7.60 fps Inflow=5.34 cfs 0.424 af
15.0" Round Pipe n=0.012 L=515.0' S=0.0165 '/' Capacity=8.99 cfs Outflow=5.26 cfs 0.423 af

Reach REACH 1.2: HODGSON BROOK Avg. Flow Depth=0.48' Max Vel=5.85 fps Inflow=5.26 cfs 0.423 af
48.0" Round Pipe n=0.012 L=825.0' S=0.0112 '/' Capacity=164.33 cfs Outflow=4.99 cfs 0.423 af

Pond POND 1.0: OUTLET CULVERTS Peak Elev=39.52' Inflow=76.06 cfs 10.369 af
42.0" x 29.0", R=21.5"/66.1" Pipe Arch Culvert x 3.00 n=0.025 L=68.0' S=0.0044 '/' Outflow=76.06 cfs 10.369 af

Link PA1: POINT OF ANALYSIS Inflow=76.06 cfs 10.369 af
Primary=76.06 cfs 10.369 af

Link PA2: POINT OF ANALYSIS Inflow=9.90 cfs 0.731 af
Primary=9.90 cfs 0.731 af

Total Runoff Area = 31.609 ac Runoff Volume = 11.102 af Average Runoff Depth = 4.21"
86.00% Pervious = 27.184 ac 14.00% Impervious = 4.426 ac

L-0700-26 PRE

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Type III 24-hr 50 Year Rainfall=8.46"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment PRE 1.0: WATERSHED 1.0 Runoff Area=1,275,727 sf 9.69% Impervious Runoff Depth>5.30"
Flow Length=1,805' Tc=34.4 min CN=74 Runoff=96.90 cfs 12.947 af

Subcatchment PRE 1.1: WATERSHED 1.1 Runoff Area=33,611 sf 90.29% Impervious Runoff Depth>7.98"
Flow Length=305' Tc=5.0 min CN=96 Runoff=6.41 cfs 0.513 af

Subcatchment PRE 2.0: WATERSHED 2.0 Runoff Area=67,564 sf 57.38% Impervious Runoff Depth>7.01"
Flow Length=872' Tc=5.0 min CN=88 Runoff=12.13 cfs 0.907 af

Reach REACH 1.1: EXISTING CULVERT Avg. Flow Depth=0.77' Max Vel=7.92 fps Inflow=6.41 cfs 0.513 af
15.0" Round Pipe n=0.012 L=515.0' S=0.0165 '/' Capacity=8.99 cfs Outflow=6.32 cfs 0.513 af

Reach REACH 1.2: HODGSON BROOK Avg. Flow Depth=0.52' Max Vel=6.19 fps Inflow=6.32 cfs 0.513 af
48.0" Round Pipe n=0.012 L=825.0' S=0.0112 '/' Capacity=164.33 cfs Outflow=6.02 cfs 0.512 af

Pond POND 1.0: OUTLET CULVERTS Peak Elev=40.14' Inflow=98.61 cfs 13.459 af
42.0" x 29.0", R=21.5"/66.1" Pipe Arch Culvert x 3.00 n=0.025 L=68.0' S=0.0044 '/' Outflow=98.61 cfs 13.459 af

Link PA1: POINT OF ANALYSIS Inflow=98.61 cfs 13.459 af
Primary=98.61 cfs 13.459 af

Link PA2: POINT OF ANALYSIS Inflow=12.13 cfs 0.907 af
Primary=12.13 cfs 0.907 af

Total Runoff Area = 31.609 ac Runoff Volume = 14.366 af Average Runoff Depth = 5.45"
86.00% Pervious = 27.184 ac 14.00% Impervious = 4.426 ac

1.3 Post-Development Conditions

1.3.1 Master Post-Development Conditions

The post-development condition was analyzed by dividing the watersheds into six sub-catchment areas. Stormwater runoff from these sub-catchment areas flow to two gravel wetlands and one rain garden for treatment prior to discharging to the existing Hodgson Brook outlet. Flows from these sub-catchment areas are modeled at the same two points of analysis that were modeled in the pre-development analysis, PA1 and PA2. These points of analysis and sub-catchment areas are depicted on the plan entitled "Post-Development Watershed Plan", Sheet C-802.

Each of the points of analysis and their contributing watershed areas are described below:

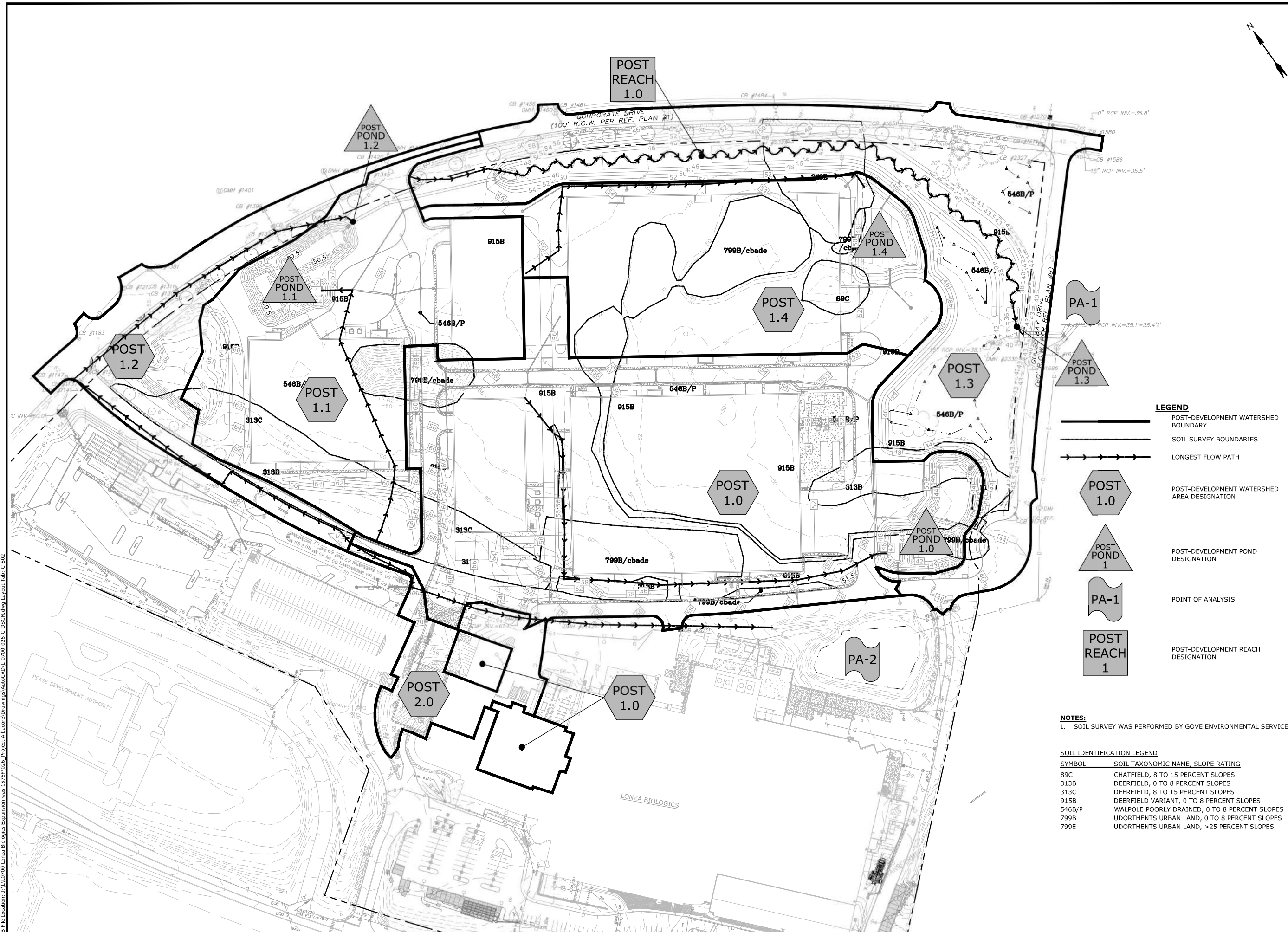
Point of Analysis (PA1)

Point of Analysis 1 (PA1) is located at the existing Hodgson Brook outlet headwall. For the purposes of this analysis, the area contributing to Point of Analysis 1 (PA1) has been divided into five sub-catchment areas (see plan C-802). Sub-catchments POST 1.0, POST 1.1, POST 1.2, POST 1.3 and POST 1.4 contribute to this point of analysis and consist of grass, paved parking lots, concrete sidewalks, and roof areas. Runoff generated in these sub-catchment areas is collected via one (1) rain garden and two (2) gravel wetlands which treat and discharge stormwater runoff either to infiltration or to PA1. Runoff from sub-catchments POST 1.0, 1.1 and 1.4 flow via overland flow to the closed drainage then flows via underground piping to one of the gravel wetlands or rain garden. Flows from sub-catchment POST 1.2 flows via overland flow to the Hodgson Brook restoration area (REACH 1.0) then flows via the brook until reach PA1. Runoff from POND 1.1 also flows via REACH 1.0 to PA1. LINK 1.0 has been added to the calculations between gravel wetland 2 (POND 1.1) and PDMH203 (POND 1.2) to account for the tailwater elevation in PDMH203 caused by the Hodgson Brook inflow to PDMH203. Tailwater elevations at the road side swale on Goose Bay Drive (PA1) have also been included in these calculations to account for any surcharging that may occur due to the tailwater condition. These tailwater elevations were determined by Streamworks, PLLC as part of their overall watershed analysis. Runoff from sub-catchment area POST 1.3 flows via overland flow to PA1. PA1 is shown on the Post-Development Watershed Plan (C-802).








Point of Analysis (PA2)

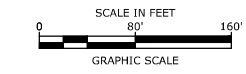
POST 2.0 is comprised mostly of runoff from Goose Bay Drive that is located between the undeveloped parcel and the existing Lonza facility. Runoff from this area travels via overland flow to the existing stormwater basin located at the existing Lonza facility. Point of Analysis 2 (PA2) is located at the existing basin.

1.3.1.1 Master Post-Development Watershed Plan



LEGEND

-  POST-DEVELOPMENT WATERSHED BOUNDARY
-  SOIL SURVEY BOUNDARIES
-  LONGEST FLOW PATH
-  POST 1.0
POST-DEVELOPMENT WATERSHED AREA DESIGNATION
-  POST POND 1
POST-DEVELOPMENT POND DESIGNATION
-  PA-1
POINT OF ANALYSIS
-  POST REACH 1
POST-DEVELOPMENT REACH DESIGNATION



NOTES:

1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHTENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHTENTS URBAN LAND, >25 PERCENT SLOPES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

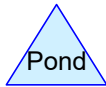
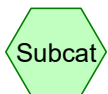
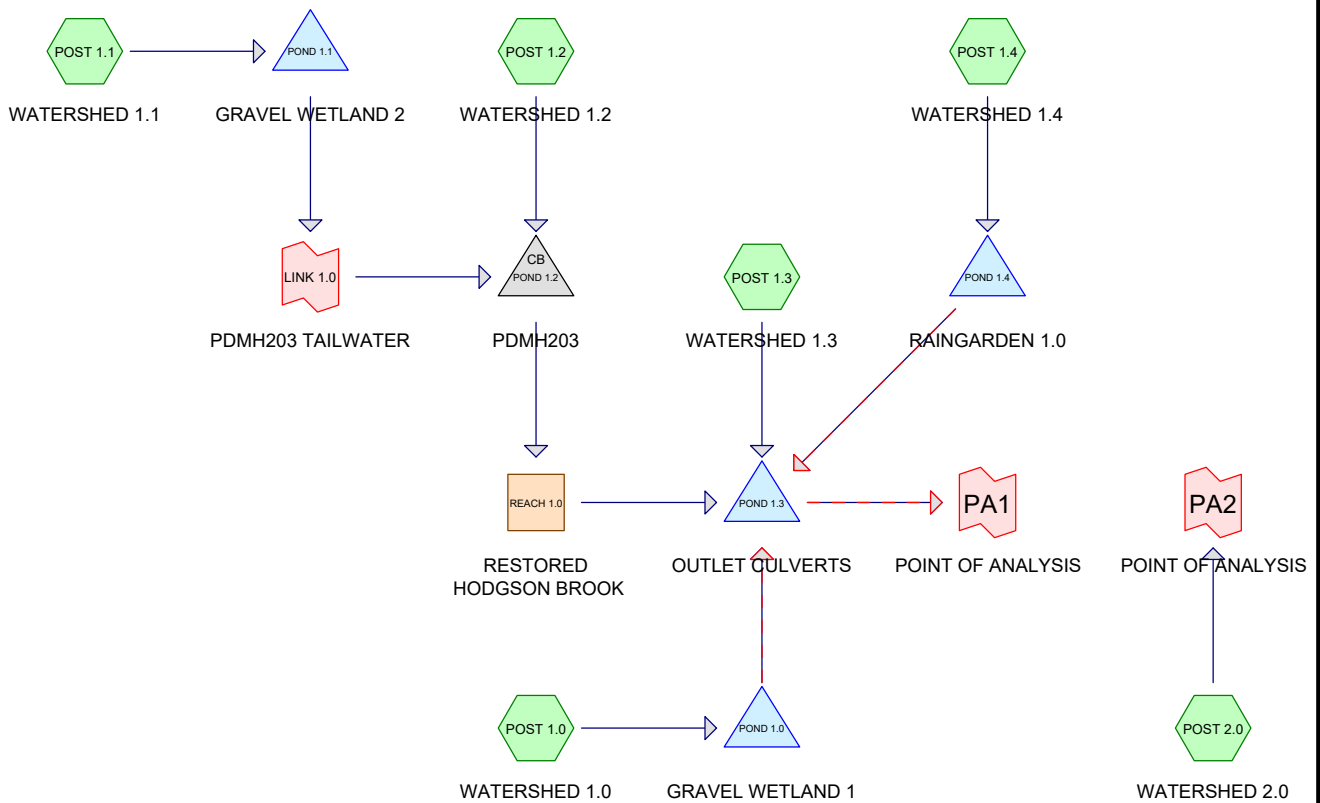
POST-DEVELOPMENT WATERSHED AREA PLAN

SCALE: AS SHOWN

C-802

Last Save Date: July 13, 2023 3:42 PM By: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
 P&E File Location: J:\L0700\Lonza Biologics Expansion.was 1576x026 Project\Subarea Drawings\AutoCAD\L-0700-026-C-DSGN.dwg Layout Tab: C-802

1.3.1.2 Master Post-Development Calculations



Routing Diagram for L-0700-26 POST
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L-0700-26 POST

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
1.776	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4)
6.801	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0)
0.436	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.323	58	Meadow, non-grazed, HSG B (POST 1.3)
3.143	71	Meadow, non-grazed, HSG C (POST 1.3)
0.799	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4)
7.546	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0)
0.146	98	Paved parking, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.688	98	Roofs, HSG B (POST 1.0, POST 1.1, POST 1.4)
8.166	98	Roofs, HSG C (POST 1.0, POST 1.1, POST 1.4, POST 2.0)
1.737	98	Roofs, HSG D (POST 1.0, POST 1.4)
0.049	76	Woods/grass comb., Fair, HSG C (POST 1.3)
31.609	87	TOTAL AREA

L-0700-26 POST

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

L-0700-26 POST

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Type III 24-hr 2 Year Rainfall=3.68"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=462,599 sf 72.19% Impervious Runoff Depth>2.71"
 Flow Length=933' Tc=11.4 min CN=91 Runoff=27.46 cfs 2.396 af

Subcatchment POST 1.1: WATERSHED Runoff Area=242,496 sf 58.73% Impervious Runoff Depth>2.25"
 Flow Length=750' Tc=10.3 min CN=86 Runoff=12.60 cfs 1.046 af

Subcatchment POST 1.2: WATERSHED Runoff Area=101,204 sf 62.15% Impervious Runoff Depth>2.43"
 Flow Length=1,191' Tc=6.4 min CN=88 Runoff=6.37 cfs 0.471 af

Subcatchment POST 1.3: WATERSHED Runoff Area=306,549 sf 22.64% Impervious Runoff Depth>1.55"
 Flow Length=1,525' Tc=45.9 min CN=77 Runoff=5.81 cfs 0.908 af

Subcatchment POST 1.4: WATERSHED Runoff Area=214,764 sf 85.05% Impervious Runoff Depth>3.01"
 Flow Length=717' Tc=7.5 min CN=94 Runoff=15.51 cfs 1.236 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf 80.99% Impervious Runoff Depth>2.91"
 Flow Length=758' Tc=5.0 min CN=93 Runoff=3.72 cfs 0.274 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.60' Max Vel=2.03 fps Inflow=6.37 cfs 0.617 af
 n=0.040 L=1,309.0' S=0.0092 '/ Capacity=2,720.29 cfs Outflow=4.54 cfs 0.608 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.16' Storage=70,734 cf Inflow=27.46 cfs 2.396 af
 Primary=1.57 cfs 1.041 af Secondary=0.00 cfs 0.000 af Outflow=1.57 cfs 1.041 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=53.90' Storage=39,230 cf Inflow=12.60 cfs 1.046 af
 Outflow=0.40 cfs 0.146 af

Pond POND 1.2: PDMH203 Peak Elev=50.33' Inflow=6.37 cfs 0.617 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/ Outflow=6.37 cfs 0.617 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,984 cf Inflow=9.25 cfs 3.255 af
 Primary=9.41 cfs 3.050 af Secondary=0.00 cfs 0.000 af Outflow=9.41 cfs 3.050 af

Pond POND 1.4: RAINGARDEN 1.0 Peak Elev=47.27' Storage=34,235 cf Inflow=15.51 cfs 1.236 af
 Primary=1.31 cfs 0.699 af Secondary=0.00 cfs 0.000 af Outflow=1.31 cfs 0.699 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=0.40 cfs 0.146 af
 Primary=0.40 cfs 0.146 af

Link PA1: POINT OF ANALYSIS Inflow=9.41 cfs 3.050 af
 Primary=9.41 cfs 3.050 af

Link PA2: POINT OF ANALYSIS Inflow=3.72 cfs 0.274 af
 Primary=3.72 cfs 0.274 af

Total Runoff Area = 31.609 ac Runoff Volume = 6.331 af Average Runoff Depth = 2.40"
39.63% Pervious = 12.527 ac 60.37% Impervious = 19.083 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=462,599 sf 72.19% Impervious Runoff Depth>4.54"
Flow Length=933' Tc=11.4 min CN=91 Runoff=44.88 cfs 4.017 af

Subcatchment POST 1.1: WATERSHED Runoff Area=242,496 sf 58.73% Impervious Runoff Depth>4.01"
Flow Length=750' Tc=10.3 min CN=86 Runoff=22.02 cfs 1.858 af

Subcatchment POST 1.2: WATERSHED Runoff Area=101,204 sf 62.15% Impervious Runoff Depth>4.22"
Flow Length=1,191' Tc=6.4 min CN=88 Runoff=10.81 cfs 0.817 af

Subcatchment POST 1.3: WATERSHED Runoff Area=306,549 sf 22.64% Impervious Runoff Depth>3.09"
Flow Length=1,525' Tc=45.9 min CN=77 Runoff=11.76 cfs 1.810 af

Subcatchment POST 1.4: WATERSHED Runoff Area=214,764 sf 85.05% Impervious Runoff Depth>4.88"
Flow Length=717' Tc=7.5 min CN=94 Runoff=24.45 cfs 2.004 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf 80.99% Impervious Runoff Depth>4.77"
Flow Length=758' Tc=5.0 min CN=93 Runoff=5.94 cfs 0.449 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.81' Max Vel=2.20 fps Inflow=10.81 cfs 1.367 af
n=0.040 L=1,309.0' S=0.0092 '/ Capacity=2,720.29 cfs Outflow=6.07 cfs 1.355 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.94' Storage=86,832 cf Inflow=44.88 cfs 4.017 af
Primary=7.09 cfs 2.106 af Secondary=11.63 cfs 0.435 af Outflow=18.72 cfs 2.541 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.08' Storage=57,197 cf Inflow=22.02 cfs 1.858 af
Outflow=1.76 cfs 0.550 af

Pond POND 1.2: PDMH203 Peak Elev=50.65' Inflow=10.81 cfs 1.367 af
48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/ Outflow=10.81 cfs 1.367 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.86' Storage=14,364 cf Inflow=40.12 cfs 7.107 af
Primary=39.92 cfs 6.819 af Secondary=0.00 cfs 0.000 af Outflow=39.92 cfs 6.819 af

Pond POND 1.4: RAINGARDEN 1.0 Peak Elev=48.07' Storage=45,635 cf Inflow=24.45 cfs 2.004 af
Primary=6.60 cfs 1.401 af Secondary=0.00 cfs 0.000 af Outflow=6.60 cfs 1.401 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=1.76 cfs 0.550 af
Primary=1.76 cfs 0.550 af

Link PA1: POINT OF ANALYSIS Inflow=39.92 cfs 6.819 af
Primary=39.92 cfs 6.819 af

Link PA2: POINT OF ANALYSIS Inflow=5.94 cfs 0.449 af
Primary=5.94 cfs 0.449 af

Total Runoff Area = 31.609 ac Runoff Volume = 10.955 af Average Runoff Depth = 4.16"
39.63% Pervious = 12.527 ac 60.37% Impervious = 19.083 ac

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Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 44.88 cfs @ 12.15 hrs, Volume= 4.017 af, Depth> 4.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
5,235	98	Roofs, HSG B
22,410	61	>75% Grass cover, Good, HSG B
19,146	98	Paved parking, HSG B
157,967	98	Roofs, HSG C
90,117	74	>75% Grass cover, Good, HSG C
114,873	98	Paved parking, HSG C
31,357	98	Roofs, HSG D
16,138	80	>75% Grass cover, Good, HSG D
5,356	98	Paved parking, HSG D
462,599	91	Weighted Average
128,665		27.81% Pervious Area
333,934		72.19% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	70	0.0150	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
0.2	32	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.1	19	0.0200	2.12		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.8	162	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
0.4	84	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.5	113	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013
1.2	299	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.4	94	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.1	46	0.0240	11.16	35.05	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
0.0	5	0.0800	7.16	0.98	Pipe Channel, 5.0" Round Area= 0.1 sf Perim= 1.3' r= 0.10' n= 0.013
0.0	9	0.0110	9.90	69.95	Pipe Channel,

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36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

n= 0.013

11.4 933 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff = 22.02 cfs @ 12.14 hrs, Volume= 1.858 af, Depth> 4.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
13,692	98	Roofs, HSG B
32,710	61	>75% Grass cover, Good, HSG B
2,729	98	Paved parking, HSG B
88,019	98	Roofs, HSG C
67,375	74	>75% Grass cover, Good, HSG C
37,971	98	Paved parking, HSG C
242,496	86	Weighted Average
100,085		41.27% Pervious Area
142,411		58.73% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.1	100	0.0380	0.24		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
1.2	163	0.0245	2.35		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
1.5	283	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.1	81	0.0240	9.21	16.27	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.4	123	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013

10.3 750 Total

Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 10.81 cfs @ 12.09 hrs, Volume= 0.817 af, Depth> 4.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

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Area (sf)	CN	Description
6,874	61	>75% Grass cover, Good, HSG B
4,785	98	Paved parking, HSG B
31,436	74	>75% Grass cover, Good, HSG C
58,109	98	Paved parking, HSG C
101,204	88	Weighted Average
38,310		37.85% Pervious Area
62,894		62.15% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.5	100	0.0100	1.12		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
1.0	153	0.0150	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.6	343	0.0050	3.47	2.73	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
0.1	13	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Corrugated PE, smooth interior
1.8	453	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013 Corrugated PE, smooth interior
0.4	129	0.0050	5.91	29.00	Pipe Channel, 30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63' n= 0.013 Corrugated PE, smooth interior
6.4	1,191	Total			

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.76 cfs @ 12.63 hrs, Volume= 1.810 af, Depth> 3.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
11,450	61	>75% Grass cover, Good, HSG B
14,068	58	Meadow, non-grazed, HSG B
908	98	Paved parking, HSG B
70,956	74	>75% Grass cover, Good, HSG C
136,905	71	Meadow, non-grazed, HSG C
2,120	76	Woods/grass comb., Fair, HSG C
68,005	98	Paved parking, HSG C
1,638	80	>75% Grass cover, Good, HSG D
499	98	Paved parking, HSG D
306,549	77	Weighted Average
237,137		77.36% Pervious Area
69,412		22.64% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.9	100	0.0130	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
1.1	52	0.0130	0.80		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2720	7.82		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
45.9	1,525	Total			

Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 24.45 cfs @ 12.10 hrs, Volume= 2.004 af, Depth> 4.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
11,051	98	Roofs, HSG B
3,902	61	>75% Grass cover, Good, HSG B
7,241	98	Paved parking, HSG B
86,748	98	Roofs, HSG C
26,995	74	>75% Grass cover, Good, HSG C
32,822	98	Paved parking, HSG C
44,300	98	Roofs, HSG D
1,206	80	>75% Grass cover, Good, HSG D
499	98	Paved parking, HSG D
214,764	94	Weighted Average
32,103		14.95% Pervious Area
182,661		85.05% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.9	40	0.0150	0.14		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
0.3	53	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.3	65	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
0.4	115	0.0100	4.54	3.56	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.7	140	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.9	275	0.0070	4.97	8.79	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013

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0.0	29	0.0550	13.94	24.63	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
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7.5	717	Total
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Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.94 cfs @ 12.07 hrs, Volume= 0.449 af, Depth> 4.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
22,995	98	Roofs, HSG C
9,368	74	>75% Grass cover, Good, HSG C
16,927	98	Paved parking, HSG C
49,290	93	Weighted Average
9,368		19.01% Pervious Area
39,922		80.99% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.2	100	0.0164	1.36		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
0.3	48	0.0164	2.60		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.3	130	0.0140	7.03	12.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.5	70	0.0250	2.37		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
1.3	410	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
3.6	758	Total,	Increased to minimum Tc = 5.0 min		

Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Area =	7.890 ac, 59.73% Impervious, Inflow Depth > 2.08" for 10 Year event
Inflow =	10.81 cfs @ 12.09 hrs, Volume= 1.367 af
Outflow =	6.07 cfs @ 12.81 hrs, Volume= 1.355 af, Atten= 44%, Lag= 42.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min

Avg. Velocity = 1.04 fps, Avg. Travel Time= 21.0 min

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Peak Storage= 6,364 cf @ 12.27 hrs
Average Depth at Peak Storage= 0.81'
Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals)
Constant n= 0.040 Winding stream, pools & shoals
Inlet Invert= 48.00', Outlet Invert= 36.00'



Offset (feet)	Elevation (feet)	Chan.Depth (feet)
0.00	12.00	0.00
18.00	6.00	6.00
30.25	6.00	6.00
31.75	5.25	6.75
34.25	5.25	6.75
35.75	6.00	6.00
48.00	6.00	6.00
66.00	12.00	0.00

Depth (feet)	End Area (sq-ft)	Perim. (feet)	Storage (cubic-feet)	Discharge (cfs)
0.00	0.0	2.5	0	0.00
0.75	3.0	30.4	3,927	2.28
6.75	291.0	68.3	380,919	2,720.29

Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device #4 rise exceeded

Inflow Area = 10.620 ac, 72.19% Impervious, Inflow Depth > 4.54" for 10 Year event
 Inflow = 44.88 cfs @ 12.15 hrs, Volume= 4.017 af
 Outflow = 18.72 cfs @ 12.45 hrs, Volume= 2.541 af, Atten= 58%, Lag= 18.0 min
 Primary = 7.09 cfs @ 12.45 hrs, Volume= 2.106 af
 Secondary = 11.63 cfs @ 12.45 hrs, Volume= 0.435 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 46.94' @ 12.45 hrs Surf.Area= 21,544 sf Storage= 86,832 cf
 Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

Plug-Flow detention time= 216.6 min calculated for 2.536 af (63% of inflow)
 Center-of-Mass det. time= 118.8 min (906.1 - 787.3)

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Volume	Invert	Avail.Storage	Storage Description
#1	39.05'	110,845 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.05	9,855	0.0	0	0
41.35	9,855	30.0	6,800	6,800
42.00	9,855	45.0	2,883	9,683
43.00	11,943	100.0	10,899	20,582
44.00	14,202	100.0	13,073	33,654
45.00	16,891	100.0	15,547	49,201
46.00	19,752	100.0	18,322	67,522
47.00	21,668	100.0	20,710	88,232
48.00	23,557	100.0	22,613	110,845

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	18.0" Round Culvert L= 30.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 41.35' / 41.20' S= 0.0050 ' S= 0.0050 ' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	41.35'	3.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	45.00'	3.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	46.00'	3.0' long x 0.50' rise Sharp-Crested Rectangular Weir 2 End Contraction(s) 4.0' Crest Height
#5	Device 1	47.00'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 Limited to weir flow at low heads
#6	Secondary	46.50'	15.0' long x 15.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=7.09 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 7.09 cfs of 18.71 cfs potential flow)
- ↑ 2=Orifice/Grate (Orifice Controls 0.75 cfs @ 11.23 fps)
- ↑ 3=Orifice/Grate (Orifice Controls 0.32 cfs @ 6.48 fps)
- ↑ 4=Sharp-Crested Rectangular Weir (Orifice Controls 6.02 cfs @ 4.15 fps)
- ↑ 5=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=11.59 cfs @ 12.45 hrs HW=46.93' TW=38.85' (Dynamic Tailwater)

- ↑ 6=Broad-Crested Rectangular Weir (Weir Controls 11.59 cfs @ 1.78 fps)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area = 5.567 ac, 58.73% Impervious, Inflow Depth > 4.01" for 10 Year event
 Inflow = 22.02 cfs @ 12.14 hrs, Volume= 1.858 af
 Outflow = 1.76 cfs @ 13.65 hrs, Volume= 0.550 af, Atten= 92%, Lag= 90.5 min
 Primary = 1.76 cfs @ 13.65 hrs, Volume= 0.550 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 55.08' @ 13.65 hrs Surf.Area= 16,909 sf Storage= 57,197 cf
 Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

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Plug-Flow detention time= 357.2 min calculated for 0.550 af (30% of inflow)
 Center-of-Mass det. time= 218.3 min (1,021.7 - 803.4)

Volume	Invert	Avail.Storage	Storage Description	
#1	47.55'	117,304 cf	Custom Stage Data (Prismatic) Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
47.55	6,269	0.0	0	0
49.85	6,269	30.0	4,326	4,326
50.50	6,269	45.0	1,834	6,159
51.00	7,199	100.0	3,367	9,526
52.00	9,187	100.0	8,193	17,719
53.00	11,345	100.0	10,266	27,985
54.00	13,814	100.0	12,580	40,565
55.00	16,645	100.0	15,230	55,794
56.00	19,805	100.0	18,225	74,019
58.00	23,480	100.0	43,285	117,304

Device	Routing	Invert	Outlet Devices
#1	Primary	49.85'	24.0" Round Culvert L= 12.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 49.85' / 49.45' S= 0.0333 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
#2	Device 1	49.85'	2.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	53.50'	4.0' long x 2.00' rise Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Device 1	56.50'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=1.76 cfs @ 13.65 hrs HW=55.08' TW=55.07' (Dynamic Tailwater)

- 1=Culvert (Inlet Controls 1.76 cfs @ 0.56 fps)
- 2=Orifice/Grate (Passes < 0.01 cfs potential flow)
- 3=Sharp-Crested Rectangular Weir (Passes < 3.33 cfs potential flow)
- 4=Orifice/Grate (Controls 0.00 cfs)

Summary for Pond POND 1.2: PDMH203

Inflow Area = 7.890 ac, 59.73% Impervious, Inflow Depth > 2.08" for 10 Year event
 Inflow = 10.81 cfs @ 12.09 hrs, Volume= 1.367 af
 Outflow = 10.81 cfs @ 12.09 hrs, Volume= 1.367 af, Atten= 0%, Lag= 0.0 min
 Primary = 10.81 cfs @ 12.09 hrs, Volume= 1.367 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 50.65' @ 12.09 hrs
 Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	48.0" Round Culvert L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/' Cc= 0.900

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Type III 24-hr 10 Year Rainfall=5.58"

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n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=10.64 cfs @ 12.09 hrs HW=50.64' TW=48.75' (Dynamic Tailwater)

↑1=Culvert (Inlet Controls 10.64 cfs @ 3.05 fps)

Summary for Pond POND 1.3: OUTLET CULVERTS

[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.50' @ 23.95 hrs

Inflow Area = 30.478 ac, 59.60% Impervious, Inflow Depth > 2.80" for 10 Year event
 Inflow = 40.12 cfs @ 12.47 hrs, Volume= 7.107 af
 Outflow = 39.92 cfs @ 12.50 hrs, Volume= 6.819 af, Atten= 0%, Lag= 1.8 min
 Primary = 39.92 cfs @ 12.50 hrs, Volume= 6.819 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 38.86' @ 12.50 hrs Surf.Area= 9,266 sf Storage= 14,364 cf
 Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 32.3 min calculated for 6.819 af (96% of inflow)
 Center-of-Mass det. time= 11.6 min (905.1 - 893.5)

Volume	Invert	Avail.Storage	Storage Description
#1	35.00'	236,017 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
35.00	960	0	0
36.00	1,428	1,194	1,194
38.00	5,418	6,846	8,040
40.00	14,354	19,772	27,812
42.00	66,884	81,238	109,050
43.00	92,707	79,796	188,846
43.50	95,977	47,171	236,017

Device	Routing	Invert	Outlet Devices
#1	Primary	35.60'	42.0" W x 29.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 L= 68.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 35.60' / 35.30' S= 0.0044 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 6.72 sf
#2	Secondary	43.00'	143.1 deg x 18.0' long x 0.50' rise Sharp-Crested Vee/Trap Weir Cv= 2.47 (C= 3.09)

Primary OutFlow Max=39.88 cfs @ 12.50 hrs HW=38.86' TW=38.65' (Dynamic Tailwater)

↑1=CMP_Arch_1/2 42x29 (Outlet Controls 39.88 cfs @ 1.98 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=35.00' TW=38.65' (Dynamic Tailwater)

↑2=Sharp-Crested Vee/Trap Weir(Controls 0.00 cfs)

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Summary for Pond POND 1.4: RAINGARDEN 1.0

Inflow Area = 4.930 ac, 85.05% Impervious, Inflow Depth > 4.88" for 10 Year event
 Inflow = 24.45 cfs @ 12.10 hrs, Volume= 2.004 af
 Outflow = 6.60 cfs @ 12.48 hrs, Volume= 1.401 af, Atten= 73%, Lag= 22.2 min
 Primary = 6.60 cfs @ 12.48 hrs, Volume= 1.401 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.07' @ 12.48 hrs Surf.Area= 14,774 sf Storage= 45,635 cf
 Flood Elev= 50.00' Surf.Area= 17,790 sf Storage= 77,050 cf

Plug-Flow detention time= 233.7 min calculated for 1.398 af (70% of inflow)
 Center-of-Mass det. time= 143.1 min (914.3 - 771.2)

Volume	Invert	Avail.Storage	Storage Description	
#1	42.17'	77,050 cf	Custom Stage Data (Prismatic) Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
42.17	10,418	0.0	0	0
43.50	10,418	40.0	5,542	5,542
45.00	10,418	10.0	1,563	7,105
46.00	11,745	100.0	11,082	18,187
48.00	14,664	100.0	26,409	44,596
50.00	17,790	100.0	32,454	77,050

Device	Routing	Invert	Outlet Devices
#1	Primary	42.42'	12.0" Round Culvert L= 48.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 42.42' / 42.20' S= 0.0046 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	42.42'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 2	45.00'	10.000 in/hr Exfiltration over Surface area above 45.00' Excluded Surface area = 10,418 sf
#4	Device 1	47.15'	13.2" x 13.2" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#5	Secondary	49.35'	7.0' long x 8.9' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 3.50 4.00 4.50 5.00 5.50 Coef. (English) 2.46 2.55 2.70 2.69 2.68 2.68 2.67 2.64 2.64 2.64 2.65 2.64 2.65 2.65 2.66 2.67 2.69

Primary OutFlow Max=6.59 cfs @ 12.48 hrs HW=48.07' TW=38.86' (Dynamic Tailwater)

- ↑ 1=Culvert (Passes 6.59 cfs of 6.77 cfs potential flow)
- ↑ 2=Orifice/Grate (Passes 1.01 cfs of 2.20 cfs potential flow)
- ↑ 3=Exfiltration (Exfiltration Controls 1.01 cfs)
- ↑ 4=Orifice/Grate (Orifice Controls 5.58 cfs @ 4.62 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=42.17' TW=35.00' (Dynamic Tailwater)

- ↑ 5=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 25.099 af)

Inflow Area = 5.567 ac, 58.73% Impervious, Inflow Depth > 1.19" for 10 Year event
Inflow = 1.76 cfs @ 13.65 hrs, Volume= 0.550 af
Primary = 1.76 cfs @ 13.65 hrs, Volume= 0.550 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25 Point manual elevation table, To= 0.00 hrs, dt= 1.00 hrs, feet =
55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07
55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07
55.07 55.07 55.07 55.07 55.07 55.07 55.07

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.65' @ 0.00 hrs (92.51 cfs 86.028 af)

Inflow Area = 30.478 ac, 59.60% Impervious, Inflow Depth > 2.69" for 10 Year event
Inflow = 39.92 cfs @ 12.50 hrs, Volume= 6.819 af
Primary = 39.92 cfs @ 12.50 hrs, Volume= 6.819 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet =
38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area = 1.132 ac, 80.99% Impervious, Inflow Depth > 4.77" for 10 Year event
Inflow = 5.94 cfs @ 12.07 hrs, Volume= 0.449 af
Primary = 5.94 cfs @ 12.07 hrs, Volume= 0.449 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Type III 24-hr 25 Year Rainfall=7.07"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=462,599 sf 72.19% Impervious Runoff Depth>6.00"
 Flow Length=933' Tc=11.4 min CN=91 Runoff=58.40 cfs 5.309 af

Subcatchment POST 1.1: WATERSHED Runoff Area=242,496 sf 58.73% Impervious Runoff Depth>5.43"
 Flow Length=750' Tc=10.3 min CN=86 Runoff=29.42 cfs 2.517 af

Subcatchment POST 1.2: WATERSHED Runoff Area=101,204 sf 62.15% Impervious Runoff Depth>5.66"
 Flow Length=1,191' Tc=6.4 min CN=88 Runoff=14.27 cfs 1.095 af

Subcatchment POST 1.3: WATERSHED Runoff Area=306,549 sf 22.64% Impervious Runoff Depth>4.39"
 Flow Length=1,525' Tc=45.9 min CN=77 Runoff=16.72 cfs 2.574 af

Subcatchment POST 1.4: WATERSHED Runoff Area=214,764 sf 85.05% Impervious Runoff Depth>6.35"
 Flow Length=717' Tc=7.5 min CN=94 Runoff=31.40 cfs 2.610 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf 80.99% Impervious Runoff Depth>6.24"
 Flow Length=758' Tc=5.0 min CN=93 Runoff=7.66 cfs 0.588 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.86' Max Vel=2.20 fps Inflow=14.27 cfs 2.076 af
 n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=7.67 cfs 2.061 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.21' Storage=92,932 cf Inflow=58.40 cfs 5.309 af
 Primary=19.23 cfs 2.787 af Secondary=24.16 cfs 0.988 af Outflow=43.41 cfs 3.776 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.71' Storage=68,356 cf Inflow=29.42 cfs 2.517 af
 Outflow=4.20 cfs 0.981 af

Pond POND 1.2: PDMH203 Peak Elev=50.86' Inflow=14.27 cfs 2.076 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=14.27 cfs 2.076 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.33' Storage=19,198 cf Inflow=67.56 cfs 10.378 af
 Primary=66.14 cfs 10.071 af Secondary=0.00 cfs 0.000 af Outflow=66.14 cfs 10.071 af

Pond POND 1.4: RAINGARDEN 1.0 Peak Elev=48.89' Storage=58,248 cf Inflow=31.40 cfs 2.610 af
 Primary=7.29 cfs 1.966 af Secondary=0.00 cfs 0.000 af Outflow=7.29 cfs 1.966 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=4.20 cfs 0.981 af
 Primary=4.20 cfs 0.981 af

Link PA1: POINT OF ANALYSIS Inflow=66.14 cfs 10.071 af
 Primary=66.14 cfs 10.071 af

Link PA2: POINT OF ANALYSIS Inflow=7.66 cfs 0.588 af
 Primary=7.66 cfs 0.588 af

Total Runoff Area = 31.609 ac Runoff Volume = 14.693 af Average Runoff Depth = 5.58"
39.63% Pervious = 12.527 ac 60.37% Impervious = 19.083 ac

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Type III 24-hr 50 Year Rainfall=8.46"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=462,599 sf 72.19% Impervious Runoff Depth>7.37"
 Flow Length=933' Tc=11.4 min CN=91 Runoff=70.91 cfs 6.521 af

Subcatchment POST 1.1: WATERSHED Runoff Area=242,496 sf 58.73% Impervious Runoff Depth>6.77"
 Flow Length=750' Tc=10.3 min CN=86 Runoff=36.28 cfs 3.140 af

Subcatchment POST 1.2: WATERSHED Runoff Area=101,204 sf 62.15% Impervious Runoff Depth>7.01"
 Flow Length=1,191' Tc=6.4 min CN=88 Runoff=17.48 cfs 1.358 af

Subcatchment POST 1.3: WATERSHED Runoff Area=306,549 sf 22.64% Impervious Runoff Depth>5.65"
 Flow Length=1,525' Tc=45.9 min CN=77 Runoff=21.42 cfs 3.313 af

Subcatchment POST 1.4: WATERSHED Runoff Area=214,764 sf 85.05% Impervious Runoff Depth>7.73"
 Flow Length=717' Tc=7.5 min CN=94 Runoff=37.84 cfs 3.177 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,290 sf 80.99% Impervious Runoff Depth>7.62"
 Flow Length=758' Tc=5.0 min CN=93 Runoff=9.25 cfs 0.718 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.90' Max Vel=2.19 fps Inflow=17.48 cfs 2.679 af
 n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=10.33 cfs 2.662 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.48' Storage=98,793 cf Inflow=70.91 cfs 6.521 af
 Primary=19.73 cfs 3.345 af Secondary=38.14 cfs 1.616 af Outflow=57.87 cfs 4.961 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.45' Storage=83,107 cf Inflow=36.28 cfs 3.140 af
 Outflow=6.58 cfs 1.321 af

Pond POND 1.2: PDMH203 Peak Elev=51.03' Inflow=17.48 cfs 2.679 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=17.48 cfs 2.679 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.77' Storage=24,643 cf Inflow=87.04 cfs 13.437 af
 Primary=83.35 cfs 13.109 af Secondary=0.00 cfs 0.000 af Outflow=83.35 cfs 13.109 af

Pond POND 1.4: RAINGARDEN 1.0 Peak Elev=49.56' Storage=69,290 cf Inflow=37.84 cfs 3.177 af
 Primary=7.69 cfs 2.462 af Secondary=1.60 cfs 0.039 af Outflow=9.29 cfs 2.500 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=6.58 cfs 1.321 af
 Primary=6.58 cfs 1.321 af

Link PA1: POINT OF ANALYSIS Inflow=83.35 cfs 13.109 af
 Primary=83.35 cfs 13.109 af

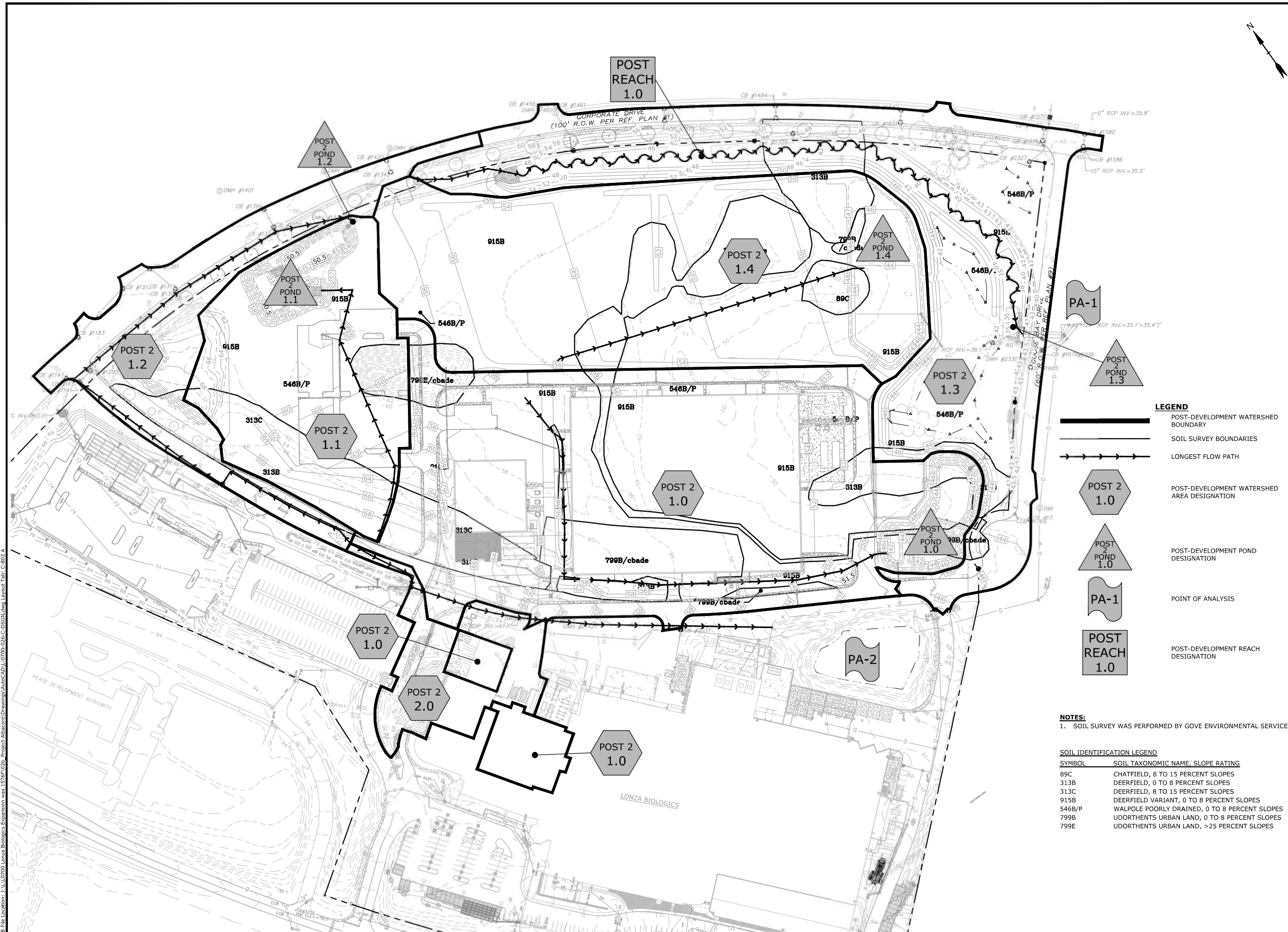
Link PA2: POINT OF ANALYSIS Inflow=9.25 cfs 0.718 af
 Primary=9.25 cfs 0.718 af

Total Runoff Area = 31.609 ac Runoff Volume = 18.227 af Average Runoff Depth = 6.92"
39.63% Pervious = 12.527 ac 60.37% Impervious = 19.083 ac

1.3.2 Phase 2 Post-Development Conditions

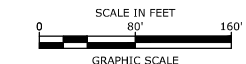
Phase 2 includes the fit up of Building #1's shell, central utility building, surface parking lot, temporary gravel construction laydown area, as well as the associated site improvement including drive aisles, utilities, lighting and sidewalks. The Phase 2 post-development condition was analyzed by dividing the watersheds into six sub-catchment areas. Stormwater runoff from these sub-catchment areas flow to either one of the two gravel wetlands, temporary sediment basin or the reconstructed Hodgson Brook prior to discharging to the existing Hodgson Brook outlet. Flows from these sub-catchment areas are modeled at the same two points of analysis that were modeled in the pre-development analysis, PA1 and PA2. These points of analysis and sub-catchment areas are depicted on the plan entitled "Phase 2 Post-Development Watershed Plan", Sheet C-802 A.

1.3.2.1 Phase 2 Post-Development Watershed Plan



LEGEND

- POST-DEVELOPMENT WATERSHED BOUNDARY
- SOIL SURVEY BOUNDARIES
- LONGEST FLOW PATH
- POST-DEVELOPMENT WATERSHED AREA DESIGNATION
- POST-DEVELOPMENT POND DESIGNATION
- POINT OF ANALYSIS
- POST-DEVELOPMENT REACH DESIGNATION



NOTES:

1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHTENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHTENTS URBAN LAND, >25 PERCENT SLOPES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

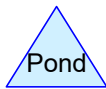
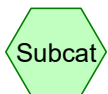
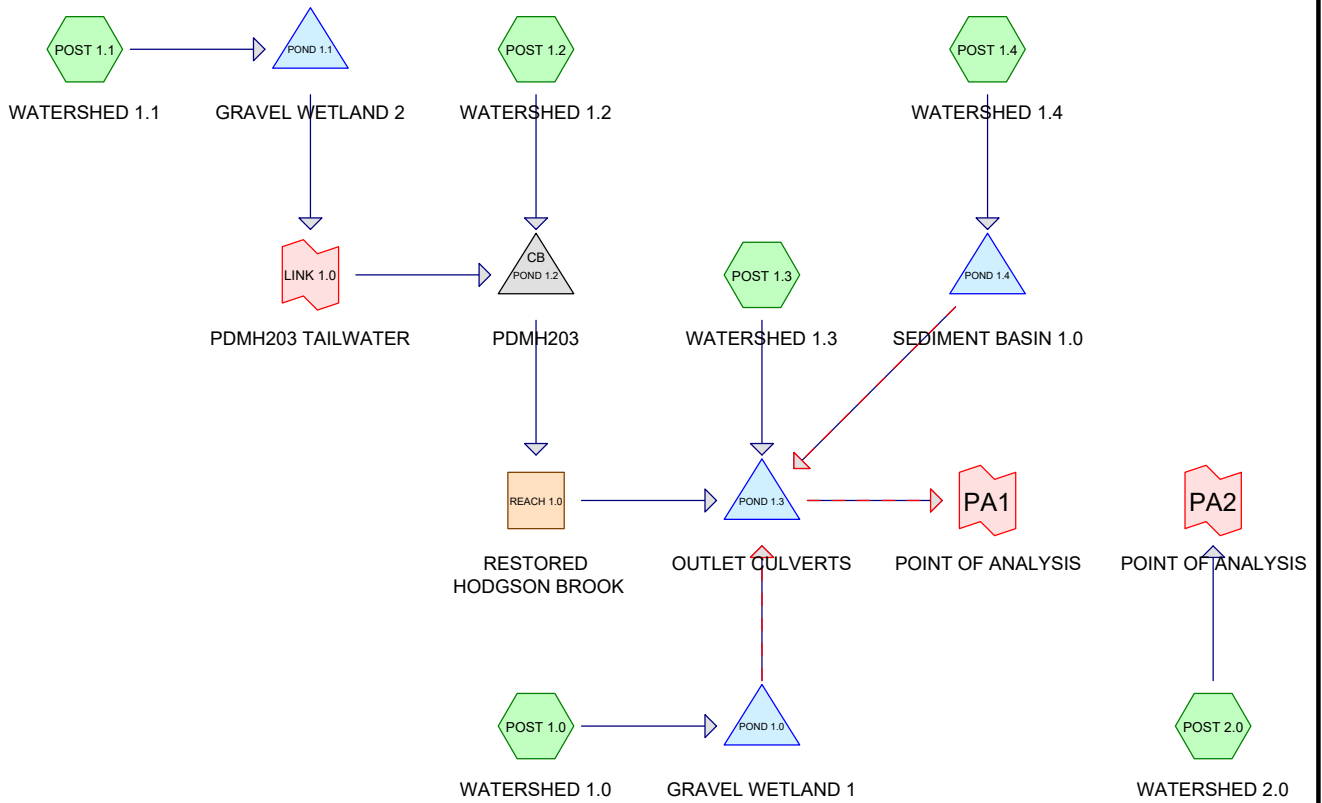
PHASE 2
POST-DEVELOPMENT
WATERSHED AREA PLAN

SCALE: AS SHOWN

C-802 A

Last Save Date: July 13, 2023 3:42 PM By: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzucik
 P&E File Location: J:\0700 Lonza Biologics Expansion\1576\026 - Project\Subarea Drawings\AutoCAD\0700-026-C-DSGN.dwg Layout Tab: C-802 A

1.3.2.2 Phase 2 Post-Development Calculations



Routing Diagram for L-0700-26 POST P2
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L-0700-26 POST P2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.312	61	>75% Grass cover, Good, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4)
13.558	74	>75% Grass cover, Good, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0)
1.467	80	>75% Grass cover, Good, HSG D (POST 1.0, POST 1.3, POST 1.4)
0.514	58	Meadow, non-grazed, HSG B (POST 1.3)
1.662	71	Meadow, non-grazed, HSG C (POST 1.3)
0.639	98	Paved parking, HSG B (POST 1.0, POST 1.1, POST 1.2, POST 1.3)
6.959	98	Paved parking, HSG C (POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0)
0.137	98	Paved parking, HSG D (POST 1.0, POST 1.3)
0.120	98	Roofs, HSG B (POST 1.0)
3.526	98	Roofs, HSG C (POST 1.0, POST 2.0)
0.714	98	Roofs, HSG D (POST 1.0)
31.609	82	TOTAL AREA

L-0700-26 POST P2

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
3.586	HSG B	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4
25.705	HSG C	POST 1.0, POST 1.1, POST 1.2, POST 1.3, POST 1.4, POST 2.0
2.318	HSG D	POST 1.0, POST 1.3, POST 1.4
0.000	Other	
31.609		TOTAL AREA

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Type III 24-hr 2 Year Rainfall=3.68"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>2.61"
 Flow Length=933' Tc=11.4 min CN=90 Runoff=25.38 cfs 2.201 af

Subcatchment POST 1.1: WATERSHED Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>1.63"
 Flow Length=464' Tc=8.3 min CN=78 Runoff=6.25 cfs 0.492 af

Subcatchment POST 1.2: WATERSHED Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>2.34"
 Flow Length=1,191' Tc=6.4 min CN=87 Runoff=6.94 cfs 0.511 af

Subcatchment POST 1.3: WATERSHED Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>1.62"
 Flow Length=1,525' Tc=45.9 min CN=78 Runoff=5.96 cfs 0.929 af

Subcatchment POST 1.4: WATERSHED 1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>1.36"
 Flow Length=585' Tc=13.5 min CN=74 Runoff=8.76 cfs 0.822 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>2.34"
 Flow Length=758' Tc=5.0 min CN=87 Runoff=3.10 cfs 0.221 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.63' Max Vel=2.08 fps Inflow=6.94 cfs 0.511 af
 n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=4.97 cfs 0.507 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.02' Storage=67,987 cf Inflow=25.38 cfs 2.201 af
 Primary=0.96 cfs 0.874 af Secondary=0.00 cfs 0.000 af Outflow=0.96 cfs 0.874 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=52.38' Storage=21,415 cf Inflow=6.25 cfs 0.492 af
 Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203 Peak Elev=50.38' Inflow=6.94 cfs 0.511 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=6.94 cfs 0.511 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.16' Storage=8,981 cf Inflow=9.25 cfs 3.060 af
 Primary=9.25 cfs 2.856 af Secondary=0.00 cfs 0.000 af Outflow=9.25 cfs 2.856 af

Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=44.62' Storage=21,007 cf Inflow=8.76 cfs 0.822 af
 Primary=0.51 cfs 0.751 af Secondary=0.00 cfs 0.000 af Outflow=0.51 cfs 0.751 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af
 Primary=0.00 cfs 0.000 af

Link PA1: POINT OF ANALYSIS Inflow=9.25 cfs 2.856 af
 Primary=9.25 cfs 2.856 af

Link PA2: POINT OF ANALYSIS Inflow=3.10 cfs 0.221 af
 Primary=3.10 cfs 0.221 af

Total Runoff Area = 31.609 ac Runoff Volume = 5.176 af Average Runoff Depth = 1.96"
61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>4.43"
Flow Length=933' Tc=11.4 min CN=90 Runoff=42.01 cfs 3.732 af

Subcatchment POST 1.1: WATERSHED Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>3.21"
Flow Length=464' Tc=8.3 min CN=78 Runoff=12.40 cfs 0.966 af

Subcatchment POST 1.2: WATERSHED Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>4.11"
Flow Length=1,191' Tc=6.4 min CN=87 Runoff=11.94 cfs 0.897 af

Subcatchment POST 1.3: WATERSHED Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>3.18"
Flow Length=1,525' Tc=45.9 min CN=78 Runoff=11.87 cfs 1.826 af

Subcatchment POST 1.4: WATERSHED 1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>2.83"
Flow Length=585' Tc=13.5 min CN=74 Runoff=18.77 cfs 1.708 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>4.11"
Flow Length=758' Tc=5.0 min CN=87 Runoff=5.36 cfs 0.388 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.82' Max Vel=2.20 fps Inflow=11.94 cfs 0.897 af
n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=6.12 cfs 0.891 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=46.78' Storage=83,438 cf Inflow=42.01 cfs 3.732 af
Primary=9.22 cfs 2.105 af Secondary=5.86 cfs 0.170 af Outflow=15.08 cfs 2.275 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=54.11' Storage=42,049 cf Inflow=12.40 cfs 0.966 af
Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203 Peak Elev=50.72' Inflow=11.94 cfs 0.897 af
48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=11.94 cfs 0.897 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=38.77' Storage=13,560 cf Inflow=31.34 cfs 5.942 af
Primary=31.22 cfs 5.655 af Secondary=0.00 cfs 0.000 af Outflow=31.22 cfs 5.655 af

Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=45.79' Storage=50,580 cf Inflow=18.77 cfs 1.708 af
Primary=0.68 cfs 0.950 af Secondary=0.00 cfs 0.000 af Outflow=0.68 cfs 0.950 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af
Primary=0.00 cfs 0.000 af

Link PA1: POINT OF ANALYSIS Inflow=31.22 cfs 5.655 af
Primary=31.22 cfs 5.655 af

Link PA2: POINT OF ANALYSIS Inflow=5.36 cfs 0.388 af
Primary=5.36 cfs 0.388 af

Total Runoff Area = 31.609 ac Runoff Volume = 9.517 af Average Runoff Depth = 3.61"
61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

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Summary for Subcatchment POST 1.0: WATERSHED 1.0

Runoff = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af, Depth> 4.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
5,235	98	Roofs, HSG B
29,148	61	>75% Grass cover, Good, HSG B
18,966	98	Paved parking, HSG B
143,455	98	Roofs, HSG C
82,022	74	>75% Grass cover, Good, HSG C
110,236	98	Paved parking, HSG C
31,119	98	Roofs, HSG D
14,671	80	>75% Grass cover, Good, HSG D
5,480	98	Paved parking, HSG D
440,332	90	Weighted Average
125,841		28.58% Pervious Area
314,491		71.42% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
7.7	70	0.0150	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
0.2	32	0.0200	2.87		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.1	19	0.0200	2.12		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.8	162	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013 Corrugated PE, smooth interior
0.4	84	0.0050	3.21	2.52	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.013
0.5	113	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013
1.2	299	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.4	94	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.1	46	0.0240	11.16	35.05	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
0.0	5	0.0800	7.16	0.98	Pipe Channel, 5.0" Round Area= 0.1 sf Perim= 1.3' r= 0.10' n= 0.013
0.0	9	0.0110	9.90	69.95	Pipe Channel,

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36.0" Round Area= 7.1 sf Perim= 9.4' r= 0.75'

n= 0.013

11.4 933 Total

Summary for Subcatchment POST 1.1: WATERSHED 1.1

Runoff = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af, Depth> 3.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
36,403	61	>75% Grass cover, Good, HSG B
3,210	98	Paved parking, HSG B
72,719	74	>75% Grass cover, Good, HSG C
45,096	98	Paved parking, HSG C
157,428	78	Weighted Average
109,122		69.32% Pervious Area
48,306		30.68% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.8	100	0.0625	0.29		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
2.2	312	0.0220	2.39		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps
0.3	33	0.0150	1.84		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.0	19	0.3300	8.62		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
8.3	464	Total			

Summary for Subcatchment POST 1.2: WATERSHED 1.2

Runoff = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
9,848	61	>75% Grass cover, Good, HSG B
4,784	98	Paved parking, HSG B
37,701	74	>75% Grass cover, Good, HSG C
61,646	98	Paved parking, HSG C
113,979	87	Weighted Average
47,549		41.72% Pervious Area
66,430		58.28% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.5	100	0.0100	1.12		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
1.0	153	0.0150	2.49		Shallow Concentrated Flow, Paved Kv= 20.3 fps
1.6	343	0.0050	3.47	2.73	Pipe Channel, 12.0" Round Area= 0.8 sf Perim= 3.1' r= 0.25' n= 0.012 Concrete pipe, finished
0.1	13	0.0050	3.72	4.57	Pipe Channel, 15.0" Round Area= 1.2 sf Perim= 3.9' r= 0.31' n= 0.013 Corrugated PE, smooth interior
1.8	453	0.0050	4.20	7.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013 Corrugated PE, smooth interior
0.4	129	0.0050	5.91	29.00	Pipe Channel, 30.0" Round Area= 4.9 sf Perim= 7.9' r= 0.63' n= 0.013 Corrugated PE, smooth interior
6.4	1,191	Total			

Summary for Subcatchment POST 1.3: WATERSHED 1.3

Runoff = 11.87 cfs @ 12.63 hrs, Volume= 1.826 af, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
1,830	61	>75% Grass cover, Good, HSG B
22,404	58	Meadow, non-grazed, HSG B
896	98	Paved parking, HSG B
131,991	74	>75% Grass cover, Good, HSG C
68,446	98	Paved parking, HSG C
72,396	71	Meadow, non-grazed, HSG C
1,638	80	>75% Grass cover, Good, HSG D
499	98	Paved parking, HSG D
300,100	78	Weighted Average
230,259		76.73% Pervious Area
69,841		23.27% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
10.9	100	0.0130	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
1.1	52	0.0130	0.80		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
0.1	27	0.2720	7.82		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
33.8	1,346	0.0090	0.66		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps
45.9	1,525	Total			

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Summary for Subcatchment POST 1.4: WATERSHED 1.4

Runoff = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af, Depth> 2.83"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
23,477	61	>75% Grass cover, Good, HSG B
243,330	74	>75% Grass cover, Good, HSG C
1,334	98	Paved parking, HSG C
47,586	80	>75% Grass cover, Good, HSG D
0	96	Gravel surface, HSG D
315,727	74	Weighted Average
314,393		99.58% Pervious Area
1,334		0.42% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8.4	100	0.0245	0.20		Sheet Flow, Grass: Short n= 0.150 P2= 3.68"
5.1	465	0.0103	1.52		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
0.0	20	0.3300	8.62		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
13.5	585	Total			

Summary for Subcatchment POST 2.0: WATERSHED 2.0

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.36 cfs @ 12.07 hrs, Volume= 0.388 af, Depth> 4.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
Type III 24-hr 10 Year Rainfall=5.58"

Area (sf)	CN	Description
10,145	98	Roofs, HSG C
22,815	74	>75% Grass cover, Good, HSG C
16,376	98	Paved parking, HSG C
49,336	87	Weighted Average
22,815		46.24% Pervious Area
26,521		53.76% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.2	100	0.0164	1.36		Sheet Flow, Smooth surfaces n= 0.011 P2= 3.68"
0.3	48	0.0164	2.60		Shallow Concentrated Flow, Paved Kv= 20.3 fps
0.3	130	0.0140	7.03	12.43	Pipe Channel, 18.0" Round Area= 1.8 sf Perim= 4.7' r= 0.38' n= 0.013
0.5	70	0.0250	2.37		Shallow Concentrated Flow, Grassed Waterway Kv= 15.0 fps
1.3	410	0.0050	5.09	16.00	Pipe Channel, 24.0" Round Area= 3.1 sf Perim= 6.3' r= 0.50' n= 0.013
3.6	758	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach REACH 1.0: RESTORED HODGSON BROOK

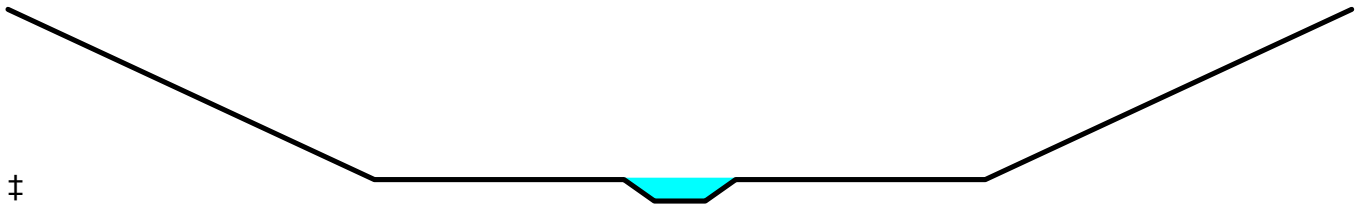
[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=2)

Inflow Area = 6.231 ac, 42.27% Impervious, Inflow Depth > 1.73" for 10 Year event
 Inflow = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af
 Outflow = 6.12 cfs @ 12.86 hrs, Volume= 0.891 af, Atten= 49%, Lag= 45.9 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Max. Velocity= 2.20 fps, Min. Travel Time= 9.9 min
 Avg. Velocity = 0.85 fps, Avg. Travel Time= 25.6 min

Peak Storage= 6,846 cf @ 12.27 hrs
 Average Depth at Peak Storage= 0.82'
 Bank-Full Depth= 6.75' Flow Area= 291.0 sf, Capacity= 2,720.29 cfs

Custom cross-section, Length= 1,309.0' Slope= 0.0092 '/' (101 Elevation Intervals)
 Constant n= 0.040 Winding stream, pools & shoals
 Inlet Invert= 48.00', Outlet Invert= 36.00'



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Offset (feet)	Elevation (feet)	Chan.Depth (feet)
0.00	12.00	0.00
18.00	6.00	6.00
30.25	6.00	6.00
31.75	5.25	6.75
34.25	5.25	6.75
35.75	6.00	6.00
48.00	6.00	6.00
66.00	12.00	0.00

Depth (feet)	End Area (sq-ft)	Perim. (feet)	Storage (cubic-feet)	Discharge (cfs)
0.00	0.0	2.5	0	0.00
0.75	3.0	30.4	3,927	2.28
6.75	291.0	68.3	380,919	2,720.29

Summary for Pond POND 1.0: GRAVEL WETLAND 1

[95] Warning: Outlet Device #4 rise exceeded

Inflow Area = 10.109 ac, 71.42% Impervious, Inflow Depth > 4.43" for 10 Year event
 Inflow = 42.01 cfs @ 12.16 hrs, Volume= 3.732 af
 Outflow = 15.08 cfs @ 12.50 hrs, Volume= 2.275 af, Atten= 64%, Lag= 20.8 min
 Primary = 9.22 cfs @ 12.50 hrs, Volume= 2.105 af
 Secondary = 5.86 cfs @ 12.50 hrs, Volume= 0.170 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 46.78' @ 12.50 hrs Surf.Area= 21,240 sf Storage= 83,438 cf
 Flood Elev= 48.00' Surf.Area= 23,557 sf Storage= 110,845 cf

Plug-Flow detention time= 226.3 min calculated for 2.275 af (61% of inflow)
 Center-of-Mass det. time= 125.2 min (916.2 - 791.0)

Volume	Invert	Avail.Storage	Storage Description	
#1	39.05'	110,845 cf	Custom Stage Data (Prismatic) Listed below (Recalc)	
Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.05	9,855	0.0	0	0
41.35	9,855	30.0	6,800	6,800
42.00	9,855	45.0	2,883	9,683
43.00	11,943	100.0	10,899	20,582
44.00	14,202	100.0	13,073	33,654
45.00	16,891	100.0	15,547	49,201
46.00	19,752	100.0	18,322	67,522
47.00	21,668	100.0	20,710	88,232
48.00	23,557	100.0	22,613	110,845

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Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	18.0" Round Culvert L= 30.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 41.35' / 41.20' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.77 sf
#2	Device 1	41.35'	3.5" Vert. Orifice/Grate C= 0.600
#3	Device 1	45.00'	3.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	46.00'	4.0' long x 0.50' rise Sharp-Crested Rectangular Weir 2 End Contraction(s) 0.5' Crest Height
#5	Device 1	47.00'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 Limited to weir flow at low heads
#6	Secondary	46.50'	15.0' long x 15.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=9.22 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

- 1=Culvert (Passes 9.22 cfs of 18.40 cfs potential flow)
- 2=Orifice/Grate (Orifice Controls 0.74 cfs @ 11.06 fps)
- 3=Orifice/Grate (Orifice Controls 0.30 cfs @ 6.19 fps)
- 4=Sharp-Crested Rectangular Weir (Orifice Controls 8.17 cfs @ 4.19 fps)
- 5=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=5.85 cfs @ 12.50 hrs HW=46.78' TW=38.77' (Dynamic Tailwater)

- 6=Broad-Crested Rectangular Weir (Weir Controls 5.85 cfs @ 1.41 fps)

Summary for Pond POND 1.1: GRAVEL WETLAND 2

Inflow Area = 3.614 ac, 30.68% Impervious, Inflow Depth > 3.21" for 10 Year event
 Inflow = 12.40 cfs @ 12.12 hrs, Volume= 0.966 af
 Outflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min
 Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 54.11' @ 24.00 hrs Surf.Area= 14,115 sf Storage= 42,049 cf
 Flood Elev= 57.00' Surf.Area= 21,643 sf Storage= 94,743 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)
 Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	Storage Description
#1	47.55'	117,304 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
47.55	6,269	0.0	0	0
49.85	6,269	30.0	4,326	4,326
50.50	6,269	45.0	1,834	6,159
51.00	7,199	100.0	3,367	9,526
52.00	9,187	100.0	8,193	17,719
53.00	11,345	100.0	10,266	27,985
54.00	13,814	100.0	12,580	40,565
55.00	16,645	100.0	15,230	55,794
56.00	19,805	100.0	18,225	74,019
58.00	23,480	100.0	43,285	117,304

Device	Routing	Invert	Outlet Devices
#1	Primary	49.85'	24.0" Round Culvert L= 12.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 49.85' / 49.45' S= 0.0333 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
#2	Device 1	49.85'	2.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	53.50'	4.0' long x 2.00' rise Sharp-Crested Rectangular Weir 2 End Contraction(s)
#4	Device 1	56.50'	4.0" x 4.0" Horiz. Orifice/Grate X 106.00 C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=47.55' TW=55.07' (Dynamic Tailwater)

- ↑ **1=Culvert** (Controls 0.00 cfs)
- ↑ **2=Orifice/Grate** (Controls 0.00 cfs)
- ↑ **3=Sharp-Crested Rectangular Weir** (Controls 0.00 cfs)
- ↑ **4=Orifice/Grate** (Controls 0.00 cfs)

Summary for Pond POND 1.2: PDMH203

Inflow Area = 6.231 ac, 42.27% Impervious, Inflow Depth > 1.73" for 10 Year event
 Inflow = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af
 Outflow = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af, Atten= 0%, Lag= 0.0 min
 Primary = 11.94 cfs @ 12.09 hrs, Volume= 0.897 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 50.72' @ 12.09 hrs
 Flood Elev= 57.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	49.35'	48.0" Round Culvert L= 269.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 49.35' / 48.00' S= 0.0050 '/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 12.57 sf

Primary OutFlow Max=11.76 cfs @ 12.09 hrs HW=50.71' TW=48.76' (Dynamic Tailwater)

- ↑ **1=Culvert** (Inlet Controls 11.76 cfs @ 3.13 fps)

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Type III 24-hr 10 Year Rainfall=5.58"

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Summary for Pond POND 1.3: OUTLET CULVERTS

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=12)

[62] Hint: Exceeded Reach REACH 1.0 OUTLET depth by 2.58' @ 23.95 hrs

Inflow Area = 30.477 ac, 37.69% Impervious, Inflow Depth > 2.34" for 10 Year event
 Inflow = 31.34 cfs @ 12.51 hrs, Volume= 5.942 af
 Outflow = 31.22 cfs @ 12.53 hrs, Volume= 5.655 af, Atten= 0%, Lag= 1.3 min
 Primary = 31.22 cfs @ 12.53 hrs, Volume= 5.655 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Peak Elev= 38.77' @ 12.53 hrs Surf.Area= 8,870 sf Storage= 13,560 cf
 Flood Elev= 43.50' Surf.Area= 95,977 sf Storage= 236,017 cf

Plug-Flow detention time= 56.2 min calculated for 5.642 af (95% of inflow)
 Center-of-Mass det. time= 29.8 min (900.3 - 870.4)

Volume	Invert	Avail.Storage	Storage Description
#1	35.00'	236,017 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
35.00	960	0	0
36.00	1,428	1,194	1,194
38.00	5,418	6,846	8,040
40.00	14,354	19,772	27,812
42.00	66,884	81,238	109,050
43.00	92,707	79,796	188,846
43.50	95,977	47,171	236,017

Device	Routing	Invert	Outlet Devices
#1	Primary	35.60'	42.0" W x 29.0" H, R=21.5"/66.1" Pipe Arch CMP_Arch_1/2 42x29 X 3.00 L= 68.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 35.60' / 35.30' S= 0.0044 '/' Cc= 0.900 n= 0.025 Corrugated metal, Flow Area= 6.72 sf
#2	Secondary	43.00'	143.1 deg x 18.0' long x 0.50' rise Sharp-Crested Vee/Trap Weir Cv= 2.47 (C= 3.09)

Primary OutFlow Max=31.11 cfs @ 12.53 hrs HW=38.77' TW=38.65' (Dynamic Tailwater)↑**1=CMP_Arch_1/2 42x29** (Outlet Controls 31.11 cfs @ 1.55 fps)**Secondary OutFlow** Max=0.00 cfs @ 0.00 hrs HW=35.04' TW=38.65' (Dynamic Tailwater)↑**2=Sharp-Crested Vee/Trap Weir** (Controls 0.00 cfs)

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Summary for Pond POND 1.4: SEDIMENT BASIN 1.0

Inflow Area = 7.248 ac, 0.42% Impervious, Inflow Depth > 2.83" for 10 Year event
 Inflow = 18.77 cfs @ 12.19 hrs, Volume= 1.708 af
 Outflow = 0.68 cfs @ 17.24 hrs, Volume= 0.950 af, Atten= 96%, Lag= 303.1 min
 Primary = 0.68 cfs @ 17.24 hrs, Volume= 0.950 af
 Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs
 Starting Elev= 44.15' Surf.Area= 18,132 sf Storage= 11,702 cf
 Peak Elev= 45.79' @ 17.24 hrs Surf.Area= 29,244 sf Storage= 50,580 cf (38,878 cf above start)
 Flood Elev= 48.50' Surf.Area= 38,802 sf Storage= 127,441 cf (115,739 cf above start)

Plug-Flow detention time= 356.9 min calculated for 0.681 af (40% of inflow)
 Center-of-Mass det. time= 9.2 min (846.8 - 837.5)

Volume	Invert	Avail.Storage	Storage Description
#1	43.00'	127,441 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
43.00	1,000	0	0
44.00	17,117	9,059	9,059
46.00	30,657	47,774	56,833
47.00	35,879	33,268	90,101
48.00	38,802	37,341	127,441

Device	Routing	Invert	Outlet Devices
#1	Primary	42.75'	12.0" Round Culvert L= 66.0' Ke= 0.500 Inlet / Outlet Invert= 42.75' / 42.40' S= 0.0053 '/' Cc= 0.900 n= 0.013, Flow Area= 0.79 sf
#2	Device 1	43.00'	4.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	46.80'	10.0" x 17.5" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#4	Secondary	47.40'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.10 Width (feet) 8.00 14.60

Primary OutFlow Max=0.68 cfs @ 17.24 hrs HW=45.79' TW=38.65' (Dynamic Tailwater)

↑ **1=Culvert** (Passes 0.68 cfs of 5.16 cfs potential flow)
 ↑ **2=Orifice/Grate** (Orifice Controls 0.68 cfs @ 7.80 fps)
 ↑ **3=Orifice/Grate** (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=44.15' TW=35.04' (Dynamic Tailwater)

↑ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Summary for Link LINK 1.0: PDMH203 TAILWATER

This link takes into account the tailwater condition in PDMH203 which the outlet of gravel wetland 2 connects. The purpose of this is to determine the effects of any surcharging caused by the tailwater of Hodgson Brook entering the structure. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.1 by 7.52' @ 0.00 hrs (23.95 cfs 41.618 af)

Inflow Area = 3.614 ac, 30.68% Impervious, Inflow Depth = 0.00" for 10 Year event
Inflow = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af
Primary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 25 Point manual elevation table, To= 0.00 hrs, dt= 1.00 hrs, feet =
55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07
55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07 55.07
55.07 55.07 55.07 55.07 55.07 55.07 55.07

Summary for Link PA1: POINT OF ANALYSIS

This link takes into account the tailwater condition in roadside swale along Goose Bay Drive which the existing culverts discharge into. These tailwater elevations were determined by Streamworks, PLLC as part of the overall watershed analysis they performed.

[80] Warning: Exceeded Pond POND 1.3 by 3.61' @ 0.00 hrs (92.51 cfs 60.023 af)

Inflow Area = 30.477 ac, 37.69% Impervious, Inflow Depth > 2.23" for 10 Year event
Inflow = 31.22 cfs @ 12.53 hrs, Volume= 5.655 af
Primary = 31.22 cfs @ 12.53 hrs, Volume= 5.655 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

10 Year 2 Point manual elevation table, To= 0.00 hrs, dt= 24.00 hrs, feet =
38.65 38.65

Summary for Link PA2: POINT OF ANALYSIS

Inflow Area = 1.133 ac, 53.76% Impervious, Inflow Depth > 4.11" for 10 Year event
Inflow = 5.36 cfs @ 12.07 hrs, Volume= 0.388 af
Primary = 5.36 cfs @ 12.07 hrs, Volume= 0.388 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs

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Type III 24-hr 25 Year Rainfall=7.07"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>5.88"
 Flow Length=933' Tc=11.4 min CN=90 Runoff=54.93 cfs 4.956 af

Subcatchment POST 1.1: WATERSHED Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>4.53"
 Flow Length=464' Tc=8.3 min CN=78 Runoff=17.44 cfs 1.365 af

Subcatchment POST 1.2: WATERSHED Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>5.54"
 Flow Length=1,191' Tc=6.4 min CN=87 Runoff=15.85 cfs 1.209 af

Subcatchment POST 1.3: WATERSHED Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>4.50"
 Flow Length=1,525' Tc=45.9 min CN=78 Runoff=16.75 cfs 2.583 af

Subcatchment POST 1.4: WATERSHED 1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>4.09"
 Flow Length=585' Tc=13.5 min CN=74 Runoff=27.23 cfs 2.472 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>5.54"
 Flow Length=758' Tc=5.0 min CN=87 Runoff=7.12 cfs 0.523 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.87' Max Vel=2.22 fps Inflow=15.85 cfs 1.209 af
 n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=8.65 cfs 1.202 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.10' Storage=90,424 cf Inflow=54.93 cfs 4.956 af
 Primary=19.03 cfs 2.766 af Secondary=18.86 cfs 0.671 af Outflow=37.88 cfs 3.437 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=55.22' Storage=59,446 cf Inflow=17.44 cfs 1.365 af
 Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203 Peak Elev=50.94' Inflow=15.85 cfs 1.209 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=15.85 cfs 1.209 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.17' Storage=17,433 cf Inflow=57.33 cfs 8.292 af
 Primary=56.26 cfs 7.985 af Secondary=0.00 cfs 0.000 af Outflow=56.26 cfs 7.985 af

Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=46.65' Storage=77,792 cf Inflow=27.23 cfs 2.472 af
 Primary=0.78 cfs 1.070 af Secondary=0.00 cfs 0.000 af Outflow=0.78 cfs 1.070 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af
 Primary=0.00 cfs 0.000 af

Link PA1: POINT OF ANALYSIS Inflow=56.26 cfs 7.985 af
 Primary=56.26 cfs 7.985 af

Link PA2: POINT OF ANALYSIS Inflow=7.12 cfs 0.523 af
 Primary=7.12 cfs 0.523 af

Total Runoff Area = 31.609 ac Runoff Volume = 13.108 af Average Runoff Depth = 4.98"
61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

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Type III 24-hr 50 Year Rainfall=8.46"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points
 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
 Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment POST 1.0: WATERSHED Runoff Area=440,332 sf 71.42% Impervious Runoff Depth>7.25"
 Flow Length=933' Tc=11.4 min CN=90 Runoff=66.89 cfs 6.105 af

Subcatchment POST 1.1: WATERSHED Runoff Area=157,428 sf 30.68% Impervious Runoff Depth>5.81"
 Flow Length=464' Tc=8.3 min CN=78 Runoff=22.21 cfs 1.750 af

Subcatchment POST 1.2: WATERSHED Runoff Area=113,979 sf 58.28% Impervious Runoff Depth>6.89"
 Flow Length=1,191' Tc=6.4 min CN=87 Runoff=19.47 cfs 1.503 af

Subcatchment POST 1.3: WATERSHED Runoff Area=300,100 sf 23.27% Impervious Runoff Depth>5.77"
 Flow Length=1,525' Tc=45.9 min CN=78 Runoff=21.37 cfs 3.312 af

Subcatchment POST 1.4: WATERSHED 1.4 Runoff Area=315,727 sf 0.42% Impervious Runoff Depth>5.33"
 Flow Length=585' Tc=13.5 min CN=74 Runoff=35.32 cfs 3.218 af

Subcatchment POST 2.0: WATERSHED 2.0 Runoff Area=49,336 sf 53.76% Impervious Runoff Depth>6.89"
 Flow Length=758' Tc=5.0 min CN=87 Runoff=8.76 cfs 0.651 af

Reach REACH 1.0: RESTORED Avg. Flow Depth=0.92' Max Vel=2.24 fps Inflow=19.47 cfs 1.503 af
 n=0.040 L=1,309.0' S=0.0092 '/' Capacity=2,720.29 cfs Outflow=11.76 cfs 1.495 af

Pond POND 1.0: GRAVEL WETLAND 1 Peak Elev=47.39' Storage=96,897 cf Inflow=66.89 cfs 6.105 af
 Primary=19.58 cfs 3.347 af Secondary=33.37 cfs 1.209 af Outflow=52.94 cfs 4.556 af

Pond POND 1.1: GRAVEL WETLAND 2 Peak Elev=56.11' Storage=76,209 cf Inflow=22.21 cfs 1.750 af
 Outflow=0.00 cfs 0.000 af

Pond POND 1.2: PDMH203 Peak Elev=51.13' Inflow=19.47 cfs 1.503 af
 48.0" Round Culvert n=0.013 L=269.0' S=0.0050 '/' Outflow=19.47 cfs 1.503 af

Pond POND 1.3: OUTLET CULVERTS Peak Elev=39.58' Storage=22,150 cf Inflow=76.91 cfs 10.982 af
 Primary=74.09 cfs 10.655 af Secondary=0.00 cfs 0.000 af Outflow=74.09 cfs 10.655 af

Pond POND 1.4: SEDIMENT BASIN 1.0 Peak Elev=47.02' Storage=90,878 cf Inflow=35.32 cfs 3.218 af
 Primary=2.39 cfs 1.619 af Secondary=0.00 cfs 0.000 af Outflow=2.39 cfs 1.619 af

Link LINK 1.0: PDMH203 TAILWATER Inflow=0.00 cfs 0.000 af
 Primary=0.00 cfs 0.000 af

Link PA1: POINT OF ANALYSIS Inflow=74.09 cfs 10.655 af
 Primary=74.09 cfs 10.655 af

Link PA2: POINT OF ANALYSIS Inflow=8.76 cfs 0.651 af
 Primary=8.76 cfs 0.651 af

Total Runoff Area = 31.609 ac Runoff Volume = 16.539 af Average Runoff Depth = 6.28"
61.73% Pervious = 19.513 ac 38.27% Impervious = 12.096 ac

1.4 Peak Rate Comparisons

The following table summarizes and compares the pre- and post-development peak runoff rates for the 2-year, 10-year, 25-year and 50-year storm events at each point of analysis. The pre-development 1-year storm event is also included for channel protection requirements.

Point of Analysis	Phase	Pre 1-Year Storm (cfs)	Pre/Post 2-Year Storm (cfs)	Pre/Post 10-Year Storm (cfs)	Pre/Post 25-Year Storm (cfs)	Pre/Post 50-Year Storm (cfs)
PA1	2	16.58	24.86/ 9.25	52.70/ 31.22	76.06/ 56.26	98.56/ 74.09
	Master	16.58	24.89/ 9.41	52.70/ 39.92	76.06/ 66.14	98.56/ 83.35
PA2	2	3.38	4.41/ 3.10	7.49/ 5.36	9.90/ 7.12	12.13/ 8.76
	Master	3.38	4.41/ 3.72	7.49/ 5.94	9.90/ 7.66	12.13/ 9.25

The Peak Runoff Control Requirements of Env-Wq 1507.06 are required to be met for the point of analysis. As shown in Table 1.4 the Post-Development flows are decreased from the Pre-Development flows for PA1 and PA2.

1.5 Mitigation Description

1.5.1 Mitigation Calculations

The proposed project area has been evaluated to treat the required water quality flow (WQF) per the requirements of Env-Wq 1500. These calculations have been provided in Appendix E of this report. The water quality volumes (WQV) have been provided below outlets.

1.5.2 Pre-Treatment Methods for Protecting Water Quality

Pre-treatment for the two (2) proposed gravel wetlands is provided by a sediment forebay. Pre-treatment for the raingarden consists of deep sump catchbasins.

BMP	Total Suspended Solids	Total Nitrogen	Total Phosphorus
Sediment Forebay ¹	TBA	TBA	TBA
Deep Sump Catch Basin w/Hood ¹	15%	85%	5%

1. Pollutant removal efficiencies from NH Stormwater Manual Volume 2, Appendix B.

1.5.3 Treatment Methods for Protecting Water Quality

Treatment for the increased impervious area comes from one rain gardens/bio-retention basins and two gravel wetlands.

The BMP Worksheets for each treatment practice have been included in Appendix E of this report.

Table 1.6 – Pollutant Removal Efficiencies			
BMP	Total Suspended Solids	Total Nitrogen	Total Phosphorus
Rain Garden/Bio-Retention Basin ¹	90%	65%	65%
Gravel Wetland ¹	95%	85%	64%

1. Pollutant removal efficiencies from NH Stormwater Manual Volume 2, Appendix B.

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APPENDIX A
(Bound Separately)

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APPENDIX B

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing	Yes
State	New Hampshire
Location	
Longitude	70.802 degrees West
Latitude	43.085 degrees North
Elevation	0 feet
Date/Time	Tue, 06 Feb 2018 11:48:23 -0500

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.81	1.04	1yr	0.70	0.98	1.21	1.56	2.02	2.65	2.91	1yr	2.35	2.79	3.20	3.92	4.52	1yr
2yr	0.32	0.49	0.62	0.81	1.02	1.30	2yr	0.88	1.18	1.51	1.93	2.48	3.20	3.55	2yr	2.83	3.42	3.92	4.66	5.30	2yr
5yr	0.37	0.58	0.72	0.97	1.24	1.60	5yr	1.07	1.46	1.88	2.42	3.13	4.05	4.56	5yr	3.59	4.38	5.01	5.91	6.67	5yr
10yr	0.41	0.64	0.81	1.11	1.44	1.87	10yr	1.24	1.71	2.21	2.87	3.73	4.85	5.50	10yr	4.29	5.29	6.04	7.07	7.94	10yr
25yr	0.47	0.75	0.96	1.32	1.75	2.31	25yr	1.51	2.12	2.75	3.60	4.71	6.15	7.06	25yr	5.44	6.79	7.74	8.97	10.01	25yr
50yr	0.53	0.85	1.09	1.52	2.04	2.72	50yr	1.76	2.50	3.25	4.28	5.62	7.36	8.54	50yr	6.51	8.21	9.34	10.75	11.93	50yr
100yr	0.60	0.96	1.24	1.75	2.38	3.20	100yr	2.05	2.95	3.84	5.09	6.71	8.82	10.33	100yr	7.80	9.93	11.28	12.88	14.23	100yr
200yr	0.66	1.08	1.40	2.01	2.78	3.78	200yr	2.40	3.47	4.55	6.06	8.02	10.57	12.49	200yr	9.35	12.01	13.62	15.45	16.97	200yr
500yr	0.78	1.29	1.68	2.43	3.41	4.68	500yr	2.94	4.32	5.67	7.61	10.13	13.43	16.07	500yr	11.89	15.46	17.47	19.64	21.43	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.73	0.89	1yr	0.63	0.87	0.92	1.31	1.66	2.23	2.50	1yr	1.97	2.41	2.83	3.17	3.88	1yr
2yr	0.31	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.36	1.82	2.34	3.05	3.44	2yr	2.70	3.31	3.81	4.53	5.05	2yr
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.13	2.74	3.78	4.18	5yr	3.34	4.02	4.69	5.51	6.22	5yr
10yr	0.38	0.59	0.73	1.02	1.32	1.60	10yr	1.14	1.56	1.81	2.41	3.08	4.36	4.86	10yr	3.86	4.67	5.42	6.39	7.18	10yr
25yr	0.44	0.67	0.83	1.18	1.56	1.90	25yr	1.34	1.86	2.10	2.78	3.57	4.69	5.90	25yr	4.15	5.67	6.63	7.78	8.67	25yr
50yr	0.48	0.73	0.91	1.31	1.76	2.17	50yr	1.52	2.12	2.35	3.11	3.98	5.30	6.82	50yr	4.69	6.56	7.71	9.02	10.00	50yr
100yr	0.53	0.81	1.01	1.46	2.01	2.47	100yr	1.73	2.42	2.63	3.46	4.41	5.95	7.88	100yr	5.27	7.58	8.97	10.48	11.53	100yr
200yr	0.59	0.89	1.13	1.63	2.28	2.82	200yr	1.96	2.76	2.93	3.85	4.88	6.67	9.10	200yr	5.90	8.75	10.43	12.19	13.33	200yr
500yr	0.69	1.02	1.31	1.91	2.71	3.37	500yr	2.34	3.30	3.40	4.41	5.58	7.75	11.02	500yr	6.86	10.59	12.73	14.91	16.12	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.28	0.44	0.53	0.72	0.88	1.08	1yr	0.76	1.06	1.25	1.75	2.21	2.99	3.13	1yr	2.65	3.01	3.57	4.36	5.02	1yr
2yr	0.33	0.52	0.63	0.86	1.06	1.26	2yr	0.91	1.23	1.48	1.96	2.51	3.41	3.68	2yr	3.02	3.53	4.06	4.81	5.61	2yr
5yr	0.40	0.61	0.76	1.04	1.33	1.61	5yr	1.15	1.57	1.88	2.53	3.24	4.32	4.92	5yr	3.82	4.73	5.34	6.33	7.11	5yr
10yr	0.46	0.71	0.88	1.23	1.59	1.96	10yr	1.38	1.92	2.27	3.09	3.93	5.31	6.15	10yr	4.70	5.91	6.74	7.78	8.68	10yr
25yr	0.57	0.87	1.08	1.54	2.02	2.54	25yr	1.74	2.48	2.93	4.04	5.09	7.73	8.25	25yr	6.84	7.94	9.02	10.25	11.33	25yr
50yr	0.66	1.01	1.25	1.80	2.42	3.09	50yr	2.09	3.02	3.56	4.96	6.23	9.67	10.34	50yr	8.56	9.94	11.25	12.61	13.86	50yr
100yr	0.77	1.17	1.47	2.12	2.91	3.75	100yr	2.51	3.67	4.33	6.10	7.63	12.09	12.94	100yr	10.70	12.45	14.03	15.54	16.96	100yr
200yr	0.90	1.36	1.72	2.50	3.48	4.57	200yr	3.00	4.47	5.28	7.50	9.34	15.15	16.23	200yr	13.41	15.60	17.53	19.14	20.77	200yr
500yr	1.12	1.66	2.14	3.11	4.42	5.91	500yr	3.81	5.78	6.84	9.88	12.24	20.44	21.88	500yr	18.09	21.04	23.53	25.23	27.17	500yr



Coastal and Great Bay Region Precipitation Increase		
	24-hr Storm Event (in.)	24-hr Storm Event + 15% (in.)
1 Year	2.65	3.05
2 Year	3.20	3.68
10 Year	4.85	5.58
25 Year	6.15	7.07
50 Year	7.36	8.46
100 Year	8.82	10.14

Tighe&Bond

APPENDIX C

Project/Site Information

**Proposed Industrial Development
101 International Drive
Portsmouth, NH**

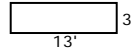
Test Pit No. **TP-1**
 Page No. 1 of 1
 File No. L-0700-013
 Checked By: D. Brogan

T&B Rep. M. Trovato Contractor New England Boring Contractors Date 03/21/18
 Operator Ben Cross Ground Elev. ± 48'
 Weather 30 Degrees - Cloudy Make Kubota Model KX080 Time Started 7:50
 Capacity 0.3 yd³ Reach 15.1 ft. Time Completed 9:05

Depth	Soil Description	Sample No.	PID Reading (ppm)	Excav. Effort	Boulder Count/Class	Note No.
0'	Dark brown fine to coarse SAND and fine to coarse GRAVEL, little Silt (FILL)	0.5'	0.0	D	5-10%/A	1
1'	Brown, fine to coarse SAND and fine to coarse GRAVEL, some Silt, trace Brick, Wood, Clay Pipe (FILL)	S-1		E	5-10%/A	
2'				E	5-10%/A	
3'				E	5-10%/A	
4'	Grayish-brown, fine to coarse SAND and SILT, with thin seems of Silty Clay (FILL)	S-2	0.0	E	5%/A	
5'				E	5%/A	
6'	Grayish-brown, fine to medium SAND, some Silty Clay, some fine to coarse Gravel	S-3		E	5%/A	
7'				M	5%/A	
8'				M	5%/A	2
9'	Bottom of exploration at 8.5 feet due to bedrock refusal					
10'						
11'						
12'						
13'						
14'						
15'						
16'						

Notes:

- 1) Frost layer observed to be approximately 6-inches thick.
- 2) Groundwater observed to infiltrate test pit at approximately 8.5 feet.

Test Pit Plan  Volume = _____ cu. yd.	Boulder Class Letter Designation: A, B, C Size Range Classification: 6" - 17", 18" - 36", 36" +	Proportions Used TRACE (TR.) 0 - 10% LITTLE (LI.) 10 - 20% SOME (SO.) 20 - 35% AND 35 - 50%	Abbreviations F = Fine M = Medium C = Coarse V = Very F/M = Fine to medium F/C = Fine to coarse GR = Gray BN = Brown YEL = Yellow	GROUNDWATER (X) Encountered () Not Encountered Elapsed Time to Reading (Hours) 0.25 Depth to Ground-water 8.5'

Project/Site Information

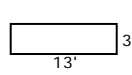
**Proposed Industrial Development
101 International Drive
Portsmouth, NH**

Test Pit No. **TP-6**
 Page No. 1 of 1
 File No. L-0700-013
 Checked By: D. Brogan

T&B Rep. M. Trovato Contractor New England Boring Contractors Date 03/21/18
 Operator Ben Cross Ground Elev. ± 44'
 Weather 36 Degrees - Cloudy Make Kubota Model KX080 Time Started 13:55
 Capacity 0.3 yd³ Reach 15.1 ft. Time Completed 14:35

Depth	Soil Description	Sample No.	PID Reading (ppm)	Excav. Effort	Boulder Count/Class	Note No.
0'	Dark brown, fine to coarse SAND and SILT, little fine to coarse Gravel, trace Brick, Wood (FILL)			E	5%/A	
1'				E	5%/A-B	
2'	Light gray, Silty CLAY, trace Wood (FILL)			E	5%/A	
3'				E	5%/A	
4'				E	5%/A	
5'				E	5%/A	1
6'	Light gray, Silty CLAY, trace fine to coarse Gravel			E	0%	
7'				E	0%	
8'	Bottom of exploration at 7.5 feet due to bedrock refusal					
9'						
10'						
11'						
12'						
13'						
14'						
15'						
16'						

Notes:
 1) Groundwater observed to infiltrate test pit sidewalls at approximately 5 feet below grade.

Test Pit Plan  Volume = _____ cu. yd.	Boulder Class Letter Designation: A, B, C Size Range Classification: 6" - 17", 18" - 36", 36" + Excavation Effort E-----Easy, M-----Moderate, D-----Difficult	Proportions Used TRACE (TR.) 0 - 10% LITTLE (LI.) 10 - 20% SOME (SO.) 20 - 35% AND 35 - 50%	Abbreviations F = Fine, M = Medium, C = Coarse, V = Very F/M = Fine to medium, F/C = Fine to coarse GR = Gray, BN = Brown, YEL = Yellow	GROUNDWATER (X) Encountered, () Not Encountered Elapsed Time to Reading (Hours): 0.25 Depth to Ground-water: 5'

Project/Site Information

**Proposed Industrial Development
101 International Drive
Portsmouth, NH**

Test Pit No.	TP-17
Page No.	1 of 1
File No.	L-0700-013
Checked By:	D. Brogan

T&B Rep.	<u>M. Trovato</u>	Contractor	<u>New England Boring Contractors</u>	Date	<u>03/23/18</u>
Weather	<u>36 Degrees - Sunny</u>	Operator	<u>Ben Cross</u>	Ground Elev.	<u>± 57'</u>
		Make	<u>Kubota</u> Model <u>KX080</u>	Time Started	<u>9:10</u>
		Capacity	<u>0.3 yd³</u> Reach <u>15.1 ft.</u>	Time Completed	<u>10:00</u>

Depth	Soil Description	Sample No.	PID Reading (ppm)	Excav. Effort	Boulder Count/Class	Note No.
0'	Brown, fine to coarse SAND, some fine to coarse Gravel, some Silt, trace Clay Pipe, Trash (FILL)		0.0	E	5%/A	
1'				E	5%/A	
2'	Gray, fine to medium SAND and SILT	S-1	0.0	E	5%/A	
3'				E	0%	1
4'	Gray, Silty CLAY	S-2		E	0%	
5'				E	0%	
6'				E	5%/A	
7'	Grayish-brown, fine to medium SAND and SILT	S-3	0.0	E	0%	
8'				E	0%	
9'				E	0%	
10'				E	0%	
11'	Bottom of exploration at 11 feet					
12'						
13'						
14'						
15'						
16'						

Notes:

1) 4-inch metal pipe encountered at approximately 3 feet below grade running perpendicular with test pit.

<p>Test Pit Plan</p> <p>Volume = _____ cu. yd.</p>	<p>Boulder Class</p> <table border="1"> <tr> <th>Letter Designation</th> <th>Size Range Classification</th> </tr> <tr> <td>A</td> <td>6" - 17"</td> </tr> <tr> <td>B</td> <td>18" - 36"</td> </tr> <tr> <td>C</td> <td>36" +</td> </tr> </table> <p>Excavation Effort</p> <table border="1"> <tr> <td>E-----Easy</td> </tr> <tr> <td>M-----Moderate</td> </tr> <tr> <td>D-----Difficult</td> </tr> </table>	Letter Designation	Size Range Classification	A	6" - 17"	B	18" - 36"	C	36" +	E-----Easy	M-----Moderate	D-----Difficult	<p>Proportions Used</p> <table border="1"> <tr> <td>TRACE (TR.)</td> <td>0 - 10%</td> </tr> <tr> <td>LITTLE (LI.)</td> <td>10 - 20%</td> </tr> <tr> <td>SOME (SO.)</td> <td>20 - 35%</td> </tr> <tr> <td>AND</td> <td>35 - 50%</td> </tr> </table>	TRACE (TR.)	0 - 10%	LITTLE (LI.)	10 - 20%	SOME (SO.)	20 - 35%	AND	35 - 50%	<p>Abbreviations</p> <p>F = Fine M = Medium C = Coarse V = Very F/M = Fine to medium F/C = Fine to coarse GR = Gray BN = Brown YEL = Yellow</p>	<p>GROUNDWATER</p> <p>() Encountered (X) Not Encountered</p> <table border="1"> <tr> <th>Elapsed Time to Reading (Hours)</th> <th>Depth to Ground-water</th> </tr> <tr> <td> </td> <td> </td> </tr> </table>	Elapsed Time to Reading (Hours)	Depth to Ground-water		
	Letter Designation	Size Range Classification																									
A	6" - 17"																										
B	18" - 36"																										
C	36" +																										
E-----Easy																											
M-----Moderate																											
D-----Difficult																											
TRACE (TR.)	0 - 10%																										
LITTLE (LI.)	10 - 20%																										
SOME (SO.)	20 - 35%																										
AND	35 - 50%																										
Elapsed Time to Reading (Hours)	Depth to Ground-water																										

Project/Site Information

**Proposed Industrial Development
101 International Drive
Portsmouth, NH**

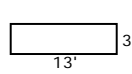
Test Pit No.	TP-18
Page No.	1 of 1
File No.	L-0700-013
Checked By:	D. Brogan

T&B Rep.	<u>M. Trovato</u>	Contractor	<u>New England Boring Contractors</u>	Date	<u>03/23/18</u>
Weather	<u>38 Degrees - Sunny</u>	Operator	<u>Ben Cross</u>	Ground Elev.	<u>± 59'</u>
		Make	<u>Kubota</u> Model <u>KX080</u>	Time Started	<u>10:10</u>
		Capacity	<u>0.3 yd³</u> Reach <u>15.1 ft.</u>	Time Completed	<u>11:15</u>

Depth	Soil Description	Sample No.	PID Reading (ppm)	Excav. Effort	Boulder Count/Class	Note No.
0'	Brown, fine to coarse SAND and fine to coarse GRAVEL, some Silt, trace Trash, Clay Pipe, Brick (FILL)			E	5-10%/A	1
1'						
2'	Light brown, fine to coarse SAND, some Silt, little fine to coarse Gravel, trace Brick (FILL)			E	10%/A	
3'						
4'						
5'	Brown, fine to coarse SAND, some Silt, little fine to coarse Gravel (FILL)	S-1		E	10-15%/A	
6'						
7'						
8'						
9'	Light brown, fine to coarse SAND, some fine to coarse Gravel, little Silt	S-2		E	10%/A	
10'						
11'						
11'	WEATHERED ROCK					
12'	Bottom of exploration at 11.4 feet			M	10%/A	2
13'						
14'						
15'						
16'						

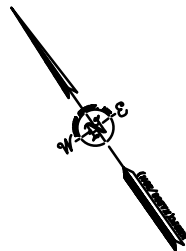
Notes:

- 1) Metal pipe encountered at approximately 1 foot below grade.
- 2) Groundwater observed to infiltrate test pit at approximately 11 feet below grade.

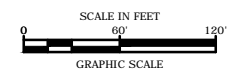
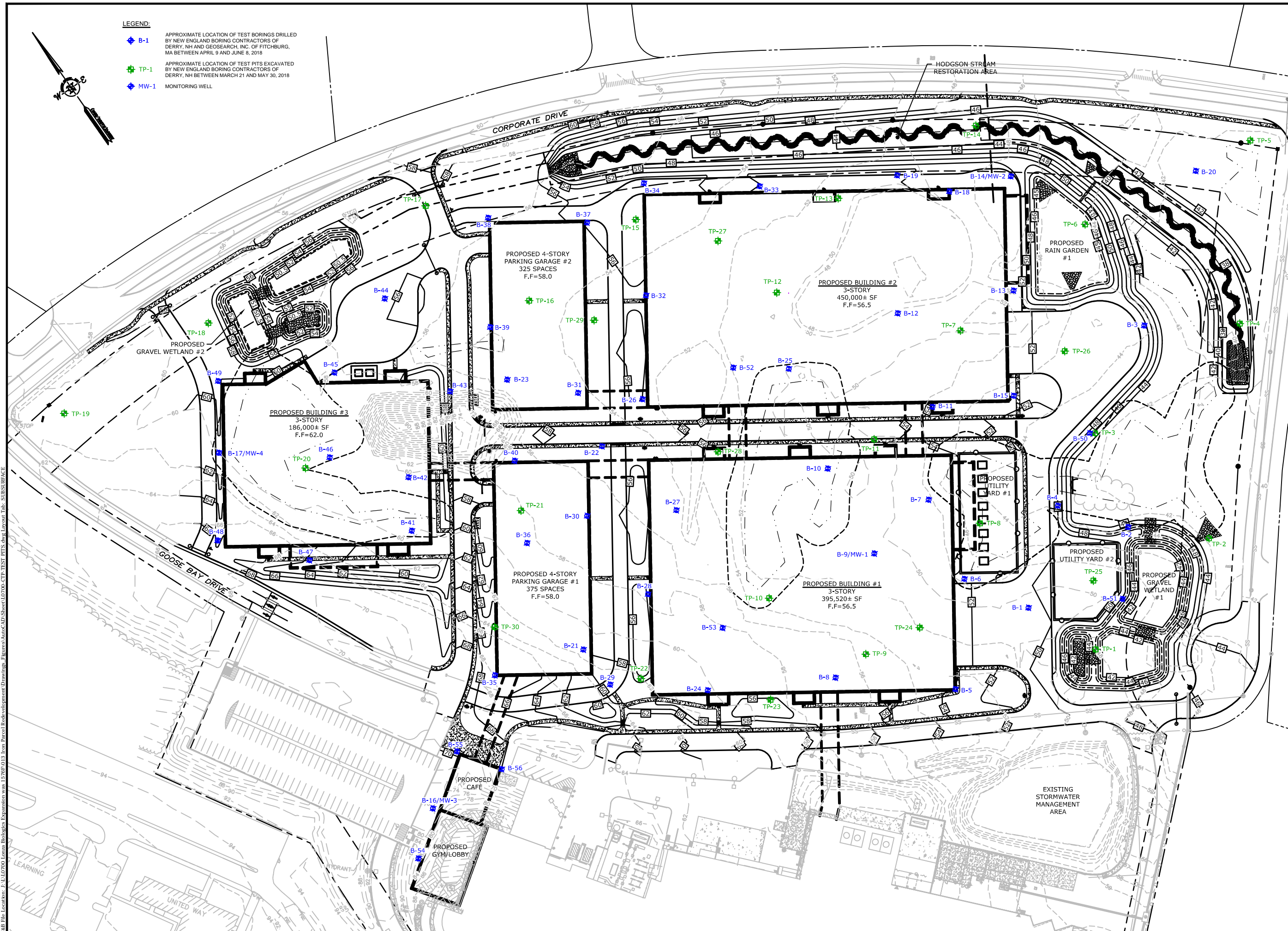
Test Pit Plan  Volume = _____ cu. yd.	Boulder Class Letter Designation: A, B, C Size Range Classification: 6" - 17", 18" - 36", 36" +	Proportions Used TRACE (TR.) 0 - 10% LITTLE (LI.) 10 - 20% SOME (SO.) 20 - 35% AND 35 - 50%	Abbreviations F = Fine M = Medium C = Coarse V = Very F/M = Fine to medium F/C = Fine to coarse GR = Gray BN = Brown YEL = Yellow	GROUNDWATER (X) Encountered () Not Encountered Elapsed Time to Reading (Hours): 0.25 Depth to Ground-water: 11'
	Excavation Effort: E-----Easy, M-----Moderate, D-----Difficult			

LEGEND:

- ◆ B-1 APPROXIMATE LOCATION OF TEST BORINGS DRILLED BY NEW ENGLAND BORING CONTRACTORS OF DERRY, NH AND GEOSURCH, INC. OF FITCHBURG, MA BETWEEN APRIL 9 AND JUNE 8, 2018
- + TP-1 APPROXIMATE LOCATION OF TEST PITS EXCAVATED BY NEW ENGLAND BORING CONTRACTORS OF DERRY, NH BETWEEN MARCH 21 AND MAY 30, 2018
- ◆ MW-1 MONITORING WELL



Last Save Date: August 2, 2018 3:22 PM By: BIL
 Plot Date: Tuesday, August 21, 2018 Plotted By: Neil A. Hansen
 File Location: J:\L0700\Lonza Biologics Expansion.wa 15781-013 from Parcel Redevelopment Drawings - Figures\AutoCAD\Sheet\L0700-CTP-TEST PITS.dwg Layout Tab: SUBSURFACE



Proposed Industrial Development
Lonza Biologics

Portsmouth,
New Hampshire

July 19, 2018

MARK	DATE	DESCRIPTION
PROJECT NO:	L-0700-13	
DATE:	07/19/2018	
FILE:	L0700-CTP-TEST PITS.dwg	
DRAWN BY:	BIL	
CHECKED:	DRB	
APPROVED:	DRB	

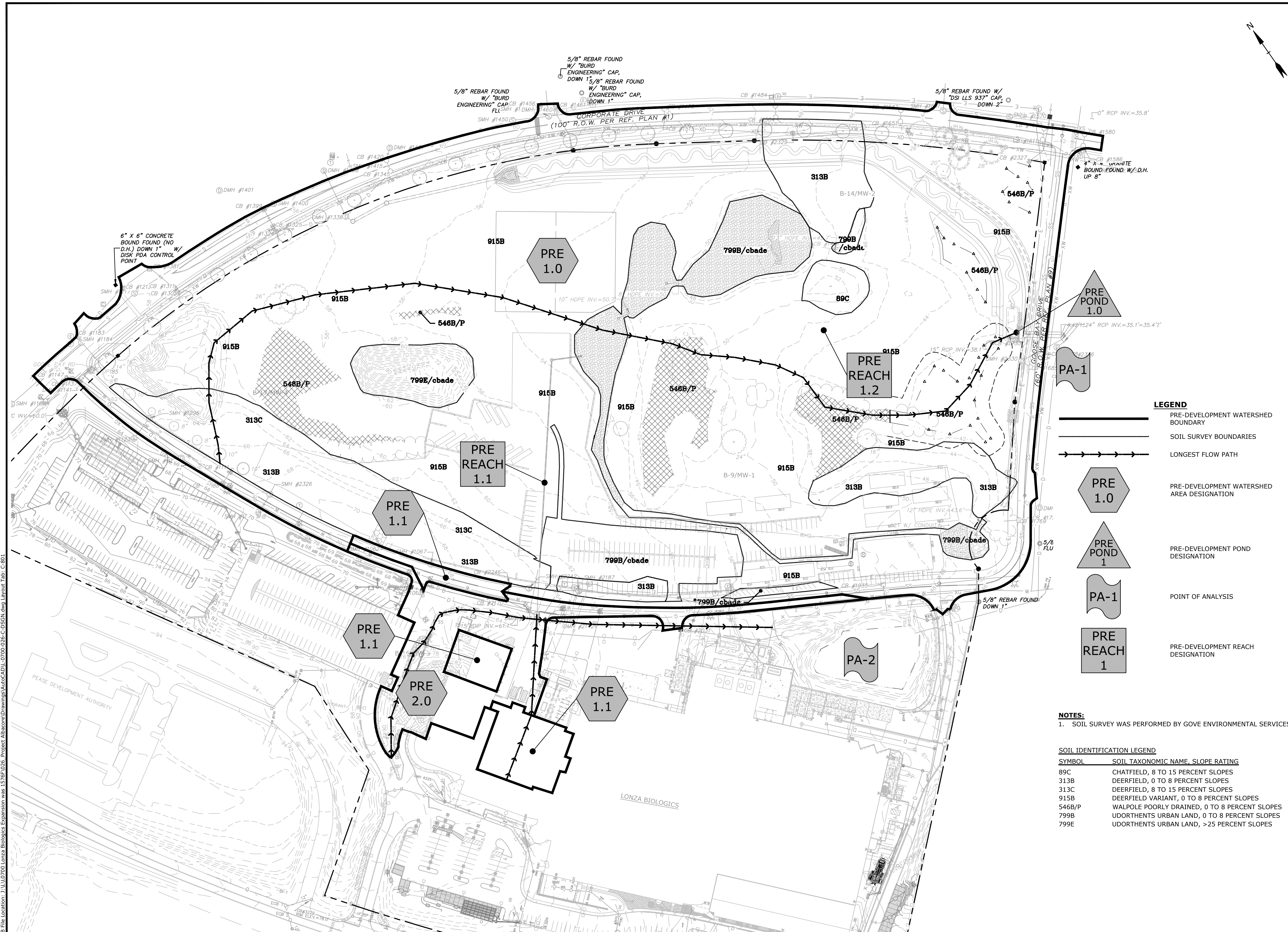
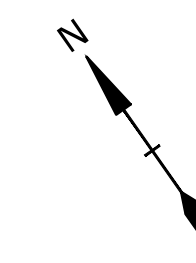
SUBSURFACE EXPLORATION PLAN

SCALE: AS SHOWN

FIGURE 2

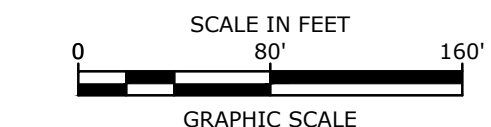
Tighe&Bond

APPENDIX D



LEGEND

- PRE-DEVELOPMENT WATERSHED BOUNDARY
- SOIL SURVEY BOUNDARIES
- LONGEST FLOW PATH
- PRE-DEVELOPMENT WATERSHED AREA DESIGNATION
- PRE-DEVELOPMENT POND DESIGNATION
- POINT OF ANALYSIS
- PRE-DEVELOPMENT REACH DESIGNATION



NOTES:

1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHTENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHTENTS URBAN LAND, >25 PERCENT SLOPES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

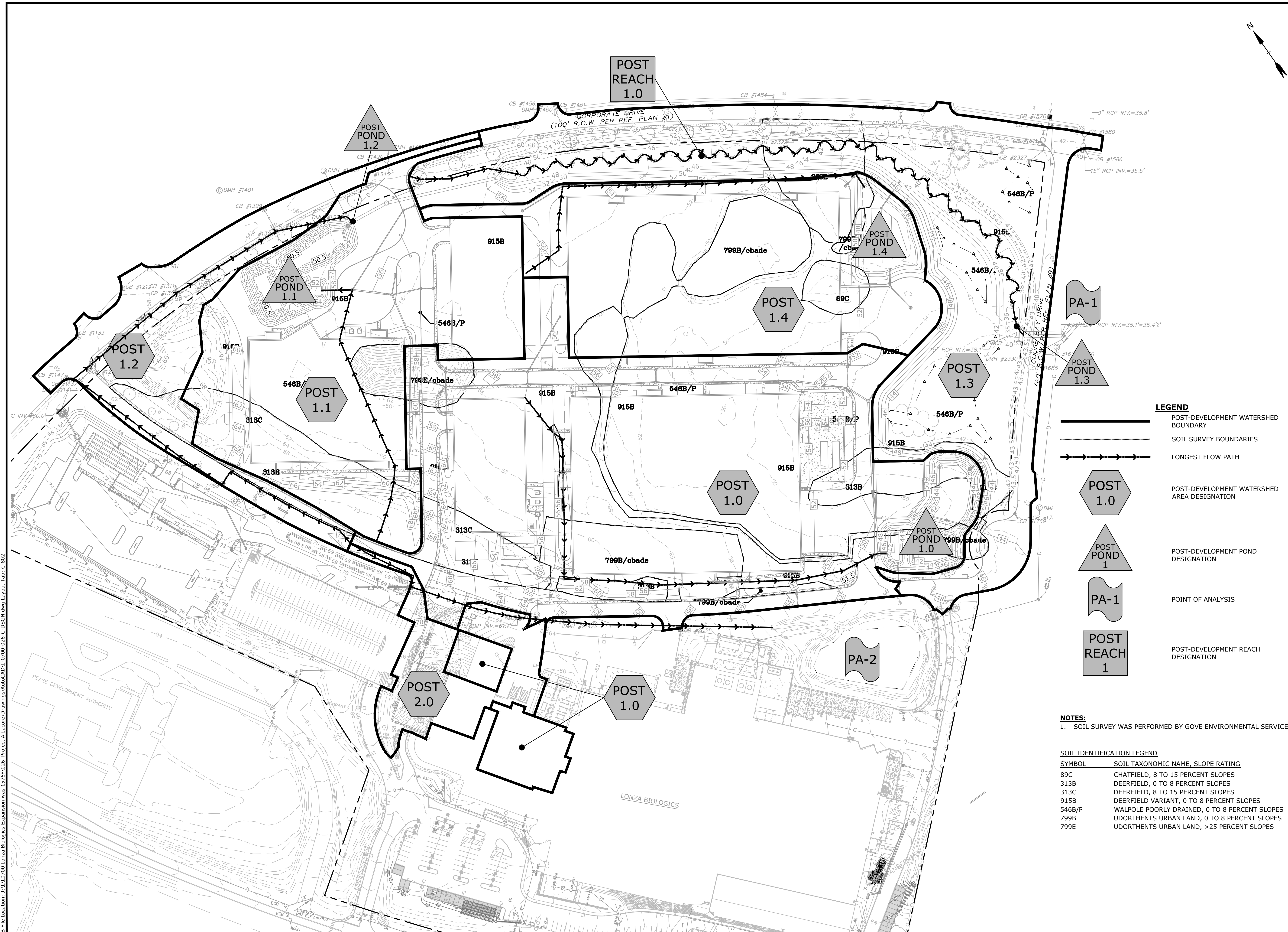
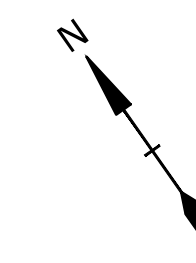
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DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

PRE-DEVELOPMENT WATERSHED AREA PLAN








SCALE: AS SHOWN

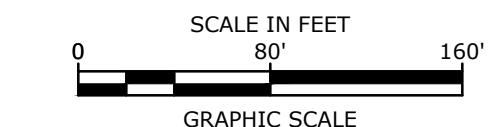
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 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
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LEGEND

-  POST-DEVELOPMENT WATERSHED BOUNDARY
-  SOIL SURVEY BOUNDARIES
-  LONGEST FLOW PATH
-  POST 1.0
POST-DEVELOPMENT WATERSHED AREA DESIGNATION
-  POST POND 1
POST-DEVELOPMENT POND DESIGNATION
-  PA-1
POINT OF ANALYSIS
-  POST REACH 1
POST-DEVELOPMENT REACH DESIGNATION



NOTES:

1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHENTS URBAN LAND, >25 PERCENT SLOPES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

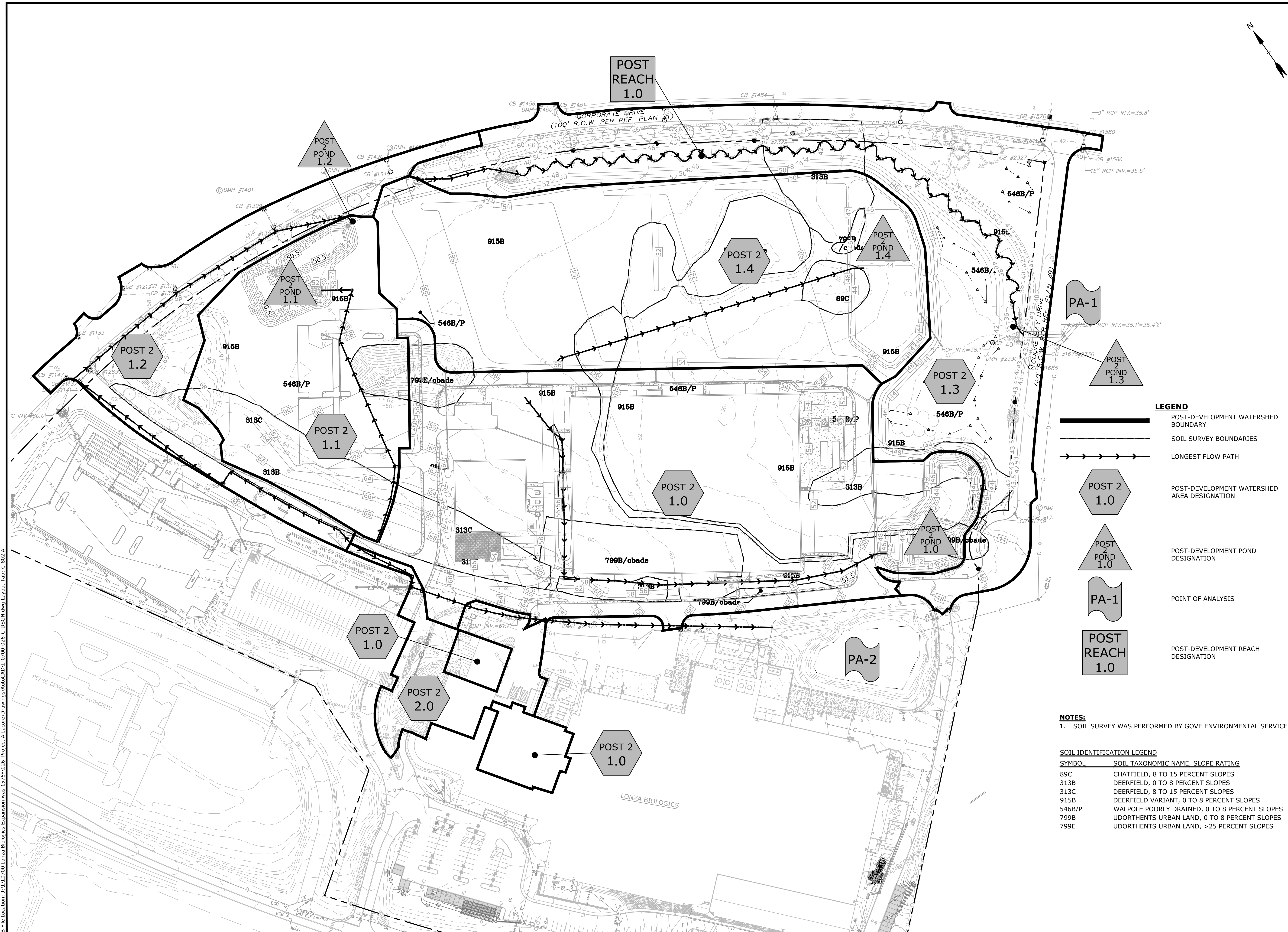
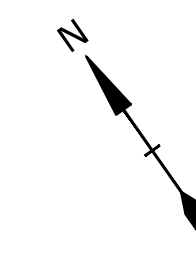
PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

POST-DEVELOPMENT WATERSHED AREA PLAN

SCALE: AS SHOWN

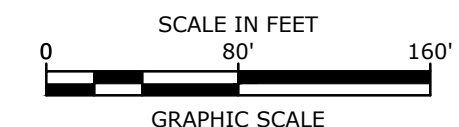
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LEGEND

- POST-DEVELOPMENT WATERSHED BOUNDARY
- SOIL SURVEY BOUNDARIES
- LONGEST FLOW PATH
- POST-DEVELOPMENT WATERSHED AREA DESIGNATION
- POST-DEVELOPMENT POND DESIGNATION
- POINT OF ANALYSIS
- POST-DEVELOPMENT REACH DESIGNATION



NOTES:
1. SOIL SURVEY WAS PERFORMED BY GOVE ENVIRONMENTAL SERVICES.

SOIL IDENTIFICATION LEGEND

SYMBOL	SOIL TAXONOMIC NAME, SLOPE RATING
89C	CHATFIELD, 8 TO 15 PERCENT SLOPES
313B	DEERFIELD, 0 TO 8 PERCENT SLOPES
313C	DEERFIELD, 8 TO 15 PERCENT SLOPES
915B	DEERFIELD VARIANT, 0 TO 8 PERCENT SLOPES
546B/P	WALPOLE POORLY DRAINED, 0 TO 8 PERCENT SLOPES
799B	UDORTHENTS URBAN LAND, 0 TO 8 PERCENT SLOPES
799E	UDORTHENTS URBAN LAND, >25 PERCENT SLOPES

Proposed Industrial Development

Lonza Biologics

Portsmouth, New Hampshire

MARK	DATE	DESCRIPTION
L	7/17/2023	Amended Site Plan Review
K	5/5/2023	Phase 1B Issued for Bid
J	3/15/2023	Phase 1B Issued for Preliminary Pricing
I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission

PROJECT NO:	L-0700-013
DATE:	04/03/2018
FILE:	L-0700-026-C-DSGN.dwg
DRAWN BY:	CJK
CHECKED:	NAH
APPROVED:	PMC

PHASE 2
POST-DEVELOPMENT
WATERSHED AREA PLAN
SCALE: AS SHOWN

C-802 A

Last Save Date: July 13, 2023 3:42 PM BY: CKRZCUIK
 Plot Date: Thursday, July 13, 2023 Plotted By: Colter Krzcuik
 P&E File Location: J:\110720 Lonza Biologics Expansion.was 12762.026 Project Abstract\Drawings\AutoCAD\0700-026-C-DSGN.dwg Layout Tab: C-802 A

Tighe&Bond

APPENDIX E



GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland 1 (POND 1.0)

Enter the node name in the drainage analysis if applicable.

10.62	ac	A = Area draining to the practice	
7.66	ac	A _i = Impervious area draining to the practice	
0.72	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.70	unitless	R _v = Runoff coefficient = 0.05 + (0.9 x I)	
7.43	ac-in	WQV = 1" x R _v x A	
26,953	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
2,695	cf	10% x WQV (check calc for sediment forebay)	
12,129	cf	45% x WQV (check calc for gravel wetland treatment bay volume)	
3,205	cf	V _{SED} = Sediment forebay volume	≥ 10%WQV
14,269	cf	V _{TB1} = Volume of treatment bay 1 ¹	≥ 45%WQV
20,912	cf	V _{TB2} = Volume of treatment bay 2 ¹	≥ 45%WQV
0.62	cfs	2Q _{avg} = 2* WQV / 24 hrs * (1hr / 3600 sec) ⁴	
44.23	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
0.53	cfs	Q _{WQV} = Discharge at the E _{WQV} (attach stage-discharge table)	< 2Q _{avg}
28.25	hours	T _{ED} = Drawdown time of extended detention = 2WQV/Q _{WQV}	≥ 24-hrs
3.00	:1	Pond side slopes	≥ 3:1
39.50	ft	Elevation of SHWT	
37.50	ft	SHWT - 2 feet	
41.35	ft	E _{pp} = Elevation of the permanent pool (elevation of lowest orifice) ³	≤ E _{SHWT} - 2 ft
85.00	ft	Length of the flow path between the inlet and outlet in each cell	≥ 15 ft
Trash Rack		What mechanism is proposed to prevent the outlet structure from clogging (applicable for orifices/weirs with a dimension of ≤6")?	
47.48	ft	Peak elevation of the 50-year storm event (E ₅₀)	
48.00	ft	Berm elevation of the pond	
YES		E ₅₀ ≤ the berm elevation?	← yes
Qualified professional that developed the planting plan Name, Profession:			

1. Volume stored above the wetland soil and below the high flow by-pass.
2. To ensure orifice is sized so that WQV is released at a relatively stable rate.
3. 4" to 8" below the wetland soil. If lowest orifice is higher than (SHWT - 2 feet), and saturated hydraulic conductivity (Ksat) is greater than 0.015 in/hr, the system must be lined.

Designer's Notes:

L-0700-26 POST

Prepared by Tighe & Bond

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Type III 24-hr 1" Storm Rainfall=1.00"

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Stage-Area-Storage for Pond POND 1.0: GRAVEL WETLAND 1

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
39.05	9,855	0	44.25	14,874	37,289
39.15	9,855	296	44.35	15,143	38,789
39.25	9,855	591	44.45	15,412	40,317
39.35	9,855	887	44.55	15,681	41,872
39.45	9,855	1,183	44.65	15,950	43,453
39.55	9,855	1,478	44.75	16,219	45,062
39.65	9,855	1,774	44.85	16,488	46,697
39.75	9,855	2,070	44.95	16,757	48,359
39.85	9,855	2,365	45.05	17,034	50,049
39.95	9,855	2,661	45.15	17,320	51,766
40.05	9,855	2,957	45.25	17,606	53,513
40.15	9,855	3,252	45.35	17,892	55,288
40.25	9,855	3,548	45.45	18,178	57,091
40.35	9,855	3,843	45.55	18,465	58,923
40.45	9,855	4,139	45.65	18,751	60,784
40.55	9,855	4,435	45.75	19,037	62,673
40.65	9,855	4,730	45.85	19,323	64,591
40.75	9,855	5,026	45.95	19,609	66,538
40.85	9,855	5,322	46.05	19,848	68,512
40.95	9,855	5,617	46.15	20,039	70,506
41.05	9,855	5,913	46.25	20,231	72,520
41.15	9,855	6,209	46.35	20,423	74,553
41.25	9,855	6,504	46.45	20,614	76,604
41.35	9,855	6,800	46.55	20,806	78,675
41.45	9,855	7,243	46.65	20,997	80,766
41.55	9,855	7,687	46.75	21,189	82,875
41.65	9,855	8,130	46.85	21,381	85,003
41.75	9,855	8,574	46.95	21,572	87,151
41.85	9,855	9,017	47.05	21,762	89,318
41.95	9,855	9,461	47.15	21,951	91,503
42.05	9,959	10,178	47.25	22,140	93,708
42.15	10,168	11,184	47.35	22,329	95,932
42.25	10,377	12,212	47.45	22,518	98,174
42.35	10,586	13,260	47.55	22,707	100,435
42.45	10,795	14,329	47.65	22,896	102,715
42.55	11,003	15,419	47.75	23,085	105,014
42.65	11,212	16,529	47.85	23,274	107,332
42.75	11,421	17,661	47.95	23,463	109,669
42.85	11,630	18,814			
42.95	11,839	19,987			
43.05	12,056	21,182			
43.15	12,282	22,398			
43.25	12,508	23,638			
43.35	12,734	24,900			
43.45	12,960	26,185			
43.55	13,185	27,492			
43.65	13,411	28,822			
43.75	13,637	30,174			
43.85	13,863	31,549			
43.95	14,089	32,947			
44.05	14,336	34,367			
44.15	14,605	35,815			

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Type III 24-hr 1" Storm Rainfall=1.00"

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Stage-Discharge for Pond POND 1.0: GRAVEL WETLAND 1

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
39.05	0.00	0.00	0.00	44.25	0.53	0.53	0.00
39.15	0.00	0.00	0.00	44.35	0.54	0.54	0.00
39.25	0.00	0.00	0.00	44.45	0.55	0.55	0.00
39.35	0.00	0.00	0.00	44.55	0.56	0.56	0.00
39.45	0.00	0.00	0.00	44.65	0.57	0.57	0.00
39.55	0.00	0.00	0.00	44.75	0.58	0.58	0.00
39.65	0.00	0.00	0.00	44.85	0.59	0.59	0.00
39.75	0.00	0.00	0.00	44.95	0.60	0.60	0.00
39.85	0.00	0.00	0.00	45.05	0.61	0.61	0.00
39.95	0.00	0.00	0.00	45.15	0.66	0.66	0.00
40.05	0.00	0.00	0.00	45.25	0.71	0.71	0.00
40.15	0.00	0.00	0.00	45.35	0.74	0.74	0.00
40.25	0.00	0.00	0.00	45.45	0.77	0.77	0.00
40.35	0.00	0.00	0.00	45.55	0.80	0.80	0.00
40.45	0.00	0.00	0.00	45.65	0.83	0.83	0.00
40.55	0.00	0.00	0.00	45.75	0.85	0.85	0.00
40.65	0.00	0.00	0.00	45.85	0.87	0.87	0.00
40.75	0.00	0.00	0.00	45.95	0.89	0.89	0.00
40.85	0.00	0.00	0.00	46.05	1.02	1.02	0.00
40.95	0.00	0.00	0.00	46.15	1.50	1.50	0.00
41.05	0.00	0.00	0.00	46.25	2.17	2.17	0.00
41.15	0.00	0.00	0.00	46.35	2.98	2.98	0.00
41.25	0.00	0.00	0.00	46.45	3.90	3.90	0.00
41.35	0.00	0.00	0.00	46.55	5.28	4.83	0.45
41.45	0.02	0.02	0.00	46.65	7.86	5.53	2.34
41.55	0.07	0.07	0.00	46.75	11.16	6.13	5.03
41.65	0.13	0.13	0.00	46.85	15.04	6.66	8.37
41.75	0.16	0.16	0.00	46.95	19.39	7.16	12.23
41.85	0.19	0.19	0.00	47.05	29.31	12.79	16.52
41.95	0.22	0.22	0.00	47.15	40.23	19.12	21.11
42.05	0.24	0.24	0.00	47.25	45.18	19.31	25.87
42.15	0.26	0.26	0.00	47.35	50.50	19.50	31.00
42.25	0.28	0.28	0.00	47.45	56.24	19.68	36.56
42.35	0.30	0.30	0.00	47.55	62.35	19.86	42.49
42.45	0.31	0.31	0.00	47.65	68.84	20.05	48.79
42.55	0.33	0.33	0.00	47.75	75.57	20.23	55.34
42.65	0.35	0.35	0.00	47.85	82.52	20.40	62.11
42.75	0.36	0.36	0.00	47.95	89.66	20.58	69.08
42.85	0.37	0.37	0.00				
42.95	0.39	0.39	0.00				
43.05	0.40	0.40	0.00				
43.15	0.41	0.41	0.00				
43.25	0.43	0.43	0.00				
43.35	0.44	0.44	0.00				
43.45	0.45	0.45	0.00				
43.55	0.46	0.46	0.00				
43.65	0.47	0.47	0.00				
43.75	0.48	0.48	0.00				
43.85	0.49	0.49	0.00				
43.95	0.50	0.50	0.00				
44.05	0.51	0.51	0.00				
44.15	0.52	0.52	0.00				



GRAVEL WETLAND DESIGN CRITERIA (Env-Wq 1508.05)

Type/Node Name: Gravel Wetland 2 (POND 1.1)

Enter the node name in the drainage analysis if applicable.

5.57	ac	A = Area draining to the practice	
3.27	ac	A_i = Impervious area draining to the practice	
0.59	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.58	unitless	R_v = Runoff coefficient = $0.05 + (0.9 \times I)$	
3.22	ac-in	$WQV = 1'' \times R_v \times A$	
11,694	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
1,169	cf	10% x WQV (check calc for sediment forebay)	
5,262	cf	45% x WQV (check calc for gravel wetland treatment bay volume)	
3,510	cf	V_{SED} = Sediment forebay volume	≥ 10%WQV
11,448	cf	V_{TB1} = Volume of treatment bay 1 ¹	≥ 45%WQV
17,112	cf	V_{TB2} = Volume of treatment bay 2 ¹	≥ 45%WQV
0.27	cfs	$2Q_{avg} = 2 * WQV / 24 \text{ hrs} * (1\text{hr} / 3600 \text{ sec})$ ⁴	
52.03	ft	E_{WQV} = Elevation of WQV (attach stage-storage table)	
0.13	cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	< $2Q_{avg}$
49.97	hours	T_{ED} = Drawdown time of extended detention = $2WQV/Q_{WQV}$	≥ 24-hrs
3.00	:1	Pond side slopes	≥ 3:1
46.00	ft	Elevation of SHWT	
44.00	ft	SHWT - 2 feet	
49.85	ft	E_{pp} = Elevation of the permanent pool (elevation of lowest orifice) ³	≤ $E_{SHWT} - 2 \text{ ft}$
105.00	ft	Length of the flow path between the inlet and outlet in each cell	≥ 15 ft
	Trash Rack	What mechanism is proposed to prevent the outlet structure from clogging (applicable for orifices/weirs with a dimension of ≤6")?	
56.45	ft	Peak elevation of the 50-year storm event (E_{50})	
57.00	ft	Berm elevation of the pond	
YES		$E_{50} \leq$ the berm elevation?	← yes
Qualified professional that developed the planting plan			
Name, Profession:			

1. Volume stored above the wetland soil and below the high flow by-pass.
2. To ensure orifice is sized so that WQV is released at a relatively stable rate.
3. 4" to 8" below the wetland soil. If lowest orifice is higher than (SHWT - 2 feet), and saturated hydraulic conductivity (K_{sat}) is greater than 0.015 in/hr, the system must be lined.

Designer's Notes:

L-0700-26 POST

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Type III 24-hr 1" Storm Rainfall=1.00"

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Stage-Area-Storage for Pond POND 1.1: GRAVEL WETLAND 2

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
47.55	6,269	0	55.35	17,751	61,814
47.70	6,269	282	55.50	18,225	64,512
47.85	6,269	564	55.65	18,699	67,281
48.00	6,269	846	55.80	19,173	70,121
48.15	6,269	1,128	55.95	19,647	73,033
48.30	6,269	1,411	56.10	19,989	76,009
48.45	6,269	1,693	56.25	20,264	79,028
48.60	6,269	1,975	56.40	20,540	82,088
48.75	6,269	2,257	56.55	20,816	85,190
48.90	6,269	2,539	56.70	21,091	88,333
49.05	6,269	2,821	56.85	21,367	91,517
49.20	6,269	3,103	57.00	21,643	94,743
49.35	6,269	3,385	57.15	21,918	98,010
49.50	6,269	3,667	57.30	22,194	101,318
49.65	6,269	3,949	57.45	22,469	104,668
49.80	6,269	4,232	57.60	22,745	108,059
49.95	6,269	4,608	57.75	23,021	111,492
50.10	6,269	5,031	57.90	23,296	114,965
50.25	6,269	5,454			
50.40	6,269	5,877			
50.55	6,362	6,475			
50.70	6,641	7,450			
50.85	6,920	8,467			
51.00	7,199	9,526			
51.15	7,497	10,629			
51.30	7,795	11,775			
51.45	8,094	12,967			
51.60	8,392	14,204			
51.75	8,690	15,485			
51.90	8,988	16,811			
52.05	9,295	18,181			
52.20	9,619	19,600			
52.35	9,942	21,067			
52.50	10,266	22,583			
52.65	10,590	24,147			
52.80	10,913	25,759			
52.95	11,237	27,421			
53.10	11,592	29,132			
53.25	11,962	30,899			
53.40	12,333	32,721			
53.55	12,703	34,598			
53.70	13,073	36,532			
53.85	13,444	38,520			
54.00	13,814	40,565			
54.15	14,239	42,669			
54.30	14,663	44,836			
54.45	15,088	47,068			
54.60	15,513	49,363			
54.75	15,937	51,722			
54.90	16,362	54,144			
55.05	16,803	56,630			
55.20	17,277	59,186			

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Stage-Discharge for Pond POND 1.1: GRAVEL WETLAND 2

Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)	Elevation (feet)	Primary (cfs)
47.55	0.00	50.67	0.04	53.79	2.20	56.91	37.24
47.61	0.00	50.73	0.04	53.85	2.85	56.97	37.42
47.67	0.00	50.79	0.05	53.91	3.56	57.03	37.60
47.73	0.00	50.85	0.06	53.97	4.31	57.09	37.79
47.79	0.00	50.91	0.06	54.03	5.11	57.15	37.97
47.85	0.00	50.97	0.07	54.09	5.95	57.21	38.15
47.91	0.00	51.03	0.07	54.15	6.83	57.27	38.33
47.97	0.00	51.09	0.08	54.21	7.75	57.33	38.51
48.03	0.00	51.15	0.08	54.27	8.70	57.39	38.68
48.09	0.00	51.21	0.09	54.33	9.68	57.45	38.86
48.15	0.00	51.27	0.09	54.39	10.70	57.51	39.04
48.21	0.00	51.33	0.09	54.45	11.74	57.57	39.21
48.27	0.00	51.39	0.10	54.51	12.82	57.63	39.39
48.33	0.00	51.45	0.10	54.57	13.91	57.69	39.56
48.39	0.00	51.51	0.10	54.63	15.04	57.75	39.73
48.45	0.00	51.57	0.11	54.69	16.18	57.81	39.91
48.51	0.00	51.63	0.11	54.75	17.35	57.87	40.08
48.57	0.00	51.69	0.11	54.81	18.54	57.93	40.25
48.63	0.00	51.75	0.12	54.87	19.76	57.99	40.42
48.69	0.00	51.81	0.12	54.93	20.99		
48.75	0.00	51.87	0.12	54.99	22.24		
48.81	0.00	51.93	0.12	55.05	23.51		
48.87	0.00	51.99	0.13	55.11	24.79		
48.93	0.00	52.05	0.13	55.17	26.10		
48.99	0.00	52.11	0.13	55.23	27.42		
49.05	0.00	52.17	0.13	55.29	28.75		
49.11	0.00	52.23	0.14	55.35	30.10		
49.17	0.00	52.29	0.14	55.41	31.46		
49.23	0.00	52.35	0.14	55.47	32.51		
49.29	0.00	52.41	0.14	55.53	32.72		
49.35	0.00	52.47	0.15	55.59	32.93		
49.41	0.00	52.53	0.15	55.65	33.14		
49.47	0.00	52.59	0.15	55.71	33.35		
49.53	0.00	52.65	0.15	55.77	33.55		
49.59	0.00	52.71	0.15	55.83	33.76		
49.65	0.00	52.77	0.16	55.89	33.96		
49.71	0.00	52.83	0.16	55.95	34.16		
49.77	0.00	52.89	0.16	56.01	34.36		
49.83	0.00	52.95	0.16	56.07	34.56		
49.89	0.00	53.01	0.16	56.13	34.76		
49.95	0.00	53.07	0.17	56.19	34.96		
50.01	0.00	53.13	0.17	56.25	35.15		
50.07	0.00	53.19	0.17	56.31	35.35		
50.13	0.00	53.25	0.17	56.37	35.54		
50.19	0.00	53.31	0.17	56.43	35.73		
50.25	0.00	53.37	0.18	56.49	35.92		
50.31	0.00	53.43	0.18	56.55	36.11		
50.37	0.00	53.49	0.18	56.61	36.30		
50.43	0.00	53.55	0.33	56.67	36.49		
50.49	0.00	53.61	0.66	56.73	36.68		
50.55	0.00	53.67	1.09	56.79	36.87		
50.61	0.03	53.73	1.61	56.85	37.05		



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name: _____

Rain Garden 1.0 (POND 1.4)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.07(a).	
4.93	ac	A = Area draining to the practice	
4.19	ac	A _i = Impervious area draining to the practice	
0.85	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.81	unitless	R _v = Runoff coefficient = 0.05 + (0.9 x I)	
4.02	ac-in	WQV = 1" x R _v x A	
14,584	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
3,646	cf	25% x WQV (check calc for sediment forebay volume)	
10,938	cf	75% x WQV (check calc for surface sand filter volume)	
Deep Sump		Method of Pretreatment? (not required for clean or roof runoff)	
	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
Calculate time to drain if system IS NOT underdrained:			
10,418	sf	A _{SA} = Surface area of the practice	
0.30	iph	K _{sat} _{DESIGN} = Design infiltration rate ¹	
		If K _{sat} (prior to factor of safety) is < 0.50 iph, has an underdrain been provided? (Use the calculations below)	
Yes	Yes/No		
56.0	hours	T _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	≤ 72-hrs
Calculate time to drain if system IS underdrained:			
46.31	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
0.41	cfs	Q _{WQV} = Discharge at the E _{WQV} (attach stage-discharge table)	
19.76	hours	T _{DRAIN} = Drain time = 2WQV/Q _{WQV}	≤ 72-hrs
43.50	feet	E _{FC} = Elevation of the bottom of the filter course material ²	
42.42	feet	E _{UD} = Invert elevation of the underdrain (UD), if applicable	
39.00	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test pit)	
36.50	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test pit)	
1.08	feet	D _{FC to UD} = Depth to UD from the bottom of the filter course	≥ 1'
7.00	feet	D _{FC to ROCK} = Depth to bedrock from the bottom of the filter course	≥ 1'
4.50	feet	D _{FC to SHWT} = Depth to SHWT from the bottom of the filter course	≥ 1'
49.56	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
50.00	ft	Elevation of the top of the practice	
YES		50 peak elevation ≤ Elevation of the top of the practice	← yes
If a surface sand filter or underground sand filter is proposed:			
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	
	Yes/No	Access grate provided?	← yes

If a bioretention area is proposed:

YES	ac	Drainage Area no larger than 5 ac?	← yes
25,499	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
18.0	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	C-509	Note what sheet in the plan set contains the filter course specification	
3.0	:1	Pond side slopes	> 3:1
Sheet	C-509	Note what sheet in the plan set contains the planting plans and surface cover	

If porous pavement is proposed:

		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A _{SA} = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (see spec)

1. Rate of the limiting layer (either the filter course or the underlying soil). $K_{sat_{design}}$ includes factor of safety. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
2. See lines 34, 40 and 48 for required depths of filter media.
3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet structure, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:

L-0700-26 POST

Prepared by Tighe & Bond

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Type III 24-hr 1" Storm Rainfall=1.00"

Printed 6/5/2023

Stage-Area-Storage for Pond POND 1.4: RAINGARDEN 1.0

Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)	Elevation (feet)	Surface (sq-ft)	Storage (cubic-feet)
42.17	10,418	0	47.37	13,745	35,647
42.27	10,418	417	47.47	13,890	37,029
42.37	10,418	833	47.57	14,036	38,425
42.47	10,418	1,250	47.67	14,182	39,836
42.57	10,418	1,667	47.77	14,328	41,261
42.67	10,418	2,084	47.87	14,474	42,702
42.77	10,418	2,500	47.97	14,620	44,156
42.87	10,418	2,917	48.07	14,773	45,626
42.97	10,418	3,334	48.17	14,930	47,111
43.07	10,418	3,750	48.27	15,086	48,612
43.17	10,418	4,167	48.37	15,242	50,128
43.27	10,418	4,584	48.47	15,399	51,660
43.37	10,418	5,001	48.57	15,555	53,208
43.47	10,418	5,417	48.67	15,711	54,771
43.57	10,418	5,615	48.77	15,868	56,350
43.67	10,418	5,719	48.87	16,024	57,945
43.77	10,418	5,824	48.97	16,180	59,555
43.87	10,418	5,928	49.07	16,336	61,181
43.97	10,418	6,032	49.17	16,493	62,822
44.07	10,418	6,136	49.27	16,649	64,479
44.17	10,418	6,240	49.37	16,805	66,152
44.27	10,418	6,345	49.47	16,962	67,840
44.37	10,418	6,449	49.57	17,118	69,544
44.47	10,418	6,553	49.67	17,274	71,264
44.57	10,418	6,657	49.77	17,431	72,999
44.67	10,418	6,761	49.87	17,587	74,750
44.77	10,418	6,865	49.97	17,743	76,517
44.87	10,418	6,970			
44.97	10,418	7,074			
45.07	10,511	7,838			
45.17	10,644	8,895			
45.27	10,776	9,966			
45.37	10,909	11,051			
45.47	11,042	12,148			
45.57	11,174	13,259			
45.67	11,307	14,383			
45.77	11,440	15,520			
45.87	11,572	16,671			
45.97	11,705	17,835			
46.07	11,847	19,012			
46.17	11,993	20,204			
46.27	12,139	21,411			
46.37	12,285	22,632			
46.47	12,431	23,868			
46.57	12,577	25,118			
46.67	12,723	26,383			
46.77	12,869	27,663			
46.87	13,015	28,957			
46.97	13,161	30,266			
47.07	13,307	31,589			
47.17	13,453	32,927			
47.27	13,599	34,280			

L-0700-26 POST

Prepared by Tighe & Bond

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Type III 24-hr 1" Storm Rainfall=1.00"

Printed 6/5/2023

Stage-Discharge for Pond POND 1.4: RAINGARDEN 1.0

Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)	Elevation (feet)	Discharge (cfs)	Primary (cfs)	Secondary (cfs)
42.17	0.00	0.00	0.00	47.37	2.25	2.25	0.00
42.27	0.00	0.00	0.00	47.47	3.41	3.41	0.00
42.37	0.00	0.00	0.00	47.57	4.61	4.61	0.00
42.47	0.00	0.00	0.00	47.67	5.07	5.07	0.00
42.57	0.00	0.00	0.00	47.77	5.49	5.49	0.00
42.67	0.00	0.00	0.00	47.87	5.88	5.88	0.00
42.77	0.00	0.00	0.00	47.97	6.25	6.25	0.00
42.87	0.00	0.00	0.00	48.07	6.60	6.60	0.00
42.97	0.00	0.00	0.00	48.17	6.84	6.84	0.00
43.07	0.00	0.00	0.00	48.27	6.91	6.91	0.00
43.17	0.00	0.00	0.00	48.37	6.97	6.97	0.00
43.27	0.00	0.00	0.00	48.47	7.03	7.03	0.00
43.37	0.00	0.00	0.00	48.57	7.10	7.10	0.00
43.47	0.00	0.00	0.00	48.67	7.16	7.16	0.00
43.57	0.00	0.00	0.00	48.77	7.22	7.22	0.00
43.67	0.00	0.00	0.00	48.87	7.28	7.28	0.00
43.77	0.00	0.00	0.00	48.97	7.34	7.34	0.00
43.87	0.00	0.00	0.00	49.07	7.40	7.40	0.00
43.97	0.00	0.00	0.00	49.17	7.46	7.46	0.00
44.07	0.00	0.00	0.00	49.27	7.52	7.52	0.00
44.17	0.00	0.00	0.00	49.37	7.63	7.58	0.05
44.27	0.00	0.00	0.00	49.47	8.36	7.64	0.72
44.37	0.00	0.00	0.00	49.57	9.48	7.70	1.78
44.47	0.00	0.00	0.00	49.67	10.94	7.76	3.19
44.57	0.00	0.00	0.00	49.77	12.70	7.81	4.89
44.67	0.00	0.00	0.00	49.87	14.80	7.87	6.93
44.77	0.00	0.00	0.00	49.97	17.15	7.93	9.22
44.87	0.00	0.00	0.00				
44.97	0.00	0.00	0.00				
45.07	0.02	0.02	0.00				
45.17	0.05	0.05	0.00				
45.27	0.08	0.08	0.00				
45.37	0.11	0.11	0.00				
45.47	0.14	0.14	0.00				
45.57	0.18	0.18	0.00				
45.67	0.21	0.21	0.00				
45.77	0.24	0.24	0.00				
45.87	0.27	0.27	0.00				
45.97	0.30	0.30	0.00				
46.07	0.33	0.33	0.00				
46.17	0.36	0.36	0.00				
46.27	0.40	0.40	0.00				
46.37	0.43	0.43	0.00				
46.47	0.47	0.47	0.00				
46.57	0.50	0.50	0.00				
46.67	0.53	0.53	0.00				
46.77	0.57	0.57	0.00				
46.87	0.60	0.60	0.00				
46.97	0.63	0.63	0.00				
47.07	0.67	0.67	0.00				
47.17	0.74	0.74	0.00				
47.27	1.33	1.33	0.00				

Tighe&Bond

APPENDIX F

Tighe & Bond

Engineers | Environmental Specialists

Project: Lonza Biologics
 Location: Portsmouth, NH
 T&B #: L-0700-026
 Calculations By: CJK
 Checked By: NAH
 Date: 6/5/2023

APRON DESIGN

Terms: HW100

length of apron (ft.) L_a
 discharge from pipe (cfs) Q (25 YR STORM EVENT)
 pipe dia. or channel width (ft.) Do
 tailwater depth (ft.) T_w
 width of apron (at outlet)(ft) $W1$
 width of apron (downstream)(ft) $W2$
 median stone diameter (ft.) d_{50}

Equations Used:		
Length of Apron (L_a)		
when $T_w < .5 * Do$	$L_a = \frac{1.8(Q)}{Do^{(3/2)}} + 7Do$	
when $T_w \geq .5 * Do$	$L_a = \frac{3(Q)}{Do^{(3/2)}} + 7Do$	
Width of Apron ($W1$)	$W1 = 3Do$	
Width of Apron ($W2$)		
when $T_w < .5 * Do$	$W2 = 3Do + La$	
when $T_w \geq .5 * Do$	$W2 = 3Do + 0.4La$	
Median Diameter	$d_{50} = \frac{0.02 * Q^{(1.3)}}{(T_w * Do)}$	
Input:		
Q (cfs)	19.23	cfs
Do (ft.)	1.50	ft
T_w (ft.)	0.60	ft
Output:		
Width of Apron ($W1$)	5	ft.
Width of Apron ($W2$)	34	ft.
Length of Apron (L_a)	29	ft.
Median Diameter	1.04	ft.
Riprap min. depth	2.33	ft.

Tighe & Bond

Engineers | Environmental Specialists

Project: Lonza Biologics
 Location: Portsmouth, NH
 T&B #: L-0700-026
 Calculations By: CJK
 Checked By: NAH
 Date: 6/5/2023

APRON DESIGN

Terms: FES300

length of apron (ft.) L_a
 discharge from pipe (cfs) Q (25 YR STORM EVENT)
 pipe dia. or channel width (ft.) Do
 tailwater depth (ft.) T_w
 width of apron (at outlet)(ft) $W1$
 width of apron (downstream)(ft) $W2$
 median stone diameter (ft.) d_{50}

Equations Used:

Length of Apron (L_a)
 when $T_w < .5 * Do$ $L_a = \frac{1.8(Q)}{Do^{(3/2)}} + 7Do$
 when $T_w \geq .5 * Do$ $L_a = \frac{3(Q)}{Do^{(3/2)}} + 7Do$
 Width of Apron ($W1$)
 $W1 = 3Do$
 Width of Apron ($W2$)
 when $T_w < .5 * Do$ $W2 = 3Do + La$
 when $T_w \geq .5 * Do$ $W2 = 3Do + 0.4La$
 Median Diameter $d_{50} = \frac{0.02 * Q^{(1.3)}}{(T_w * Do)}$

<u>Input:</u>			
Q (cfs)	12.67	cfs	
Do (ft.)	1.50	ft	
T_w (ft.)	0.60	ft	
<u>Output:</u>			
Width of Apron ($W1$)	5	ft.	
Width of Apron ($W2$)	27	ft.	
Length of Apron (L_a)	23	ft.	
Median Diameter	0.60	ft.	
Riprap min. depth	1.36	ft.	

Tighe & Bond

Engineers | Environmental Specialists

Project: Lonza Biologics
 Location: Portsmouth, NH
 T&B #: L-0700-026
 Calculations By: CJK
 Checked By: NAH
 Date: 6/5/2023

APRON DESIGN

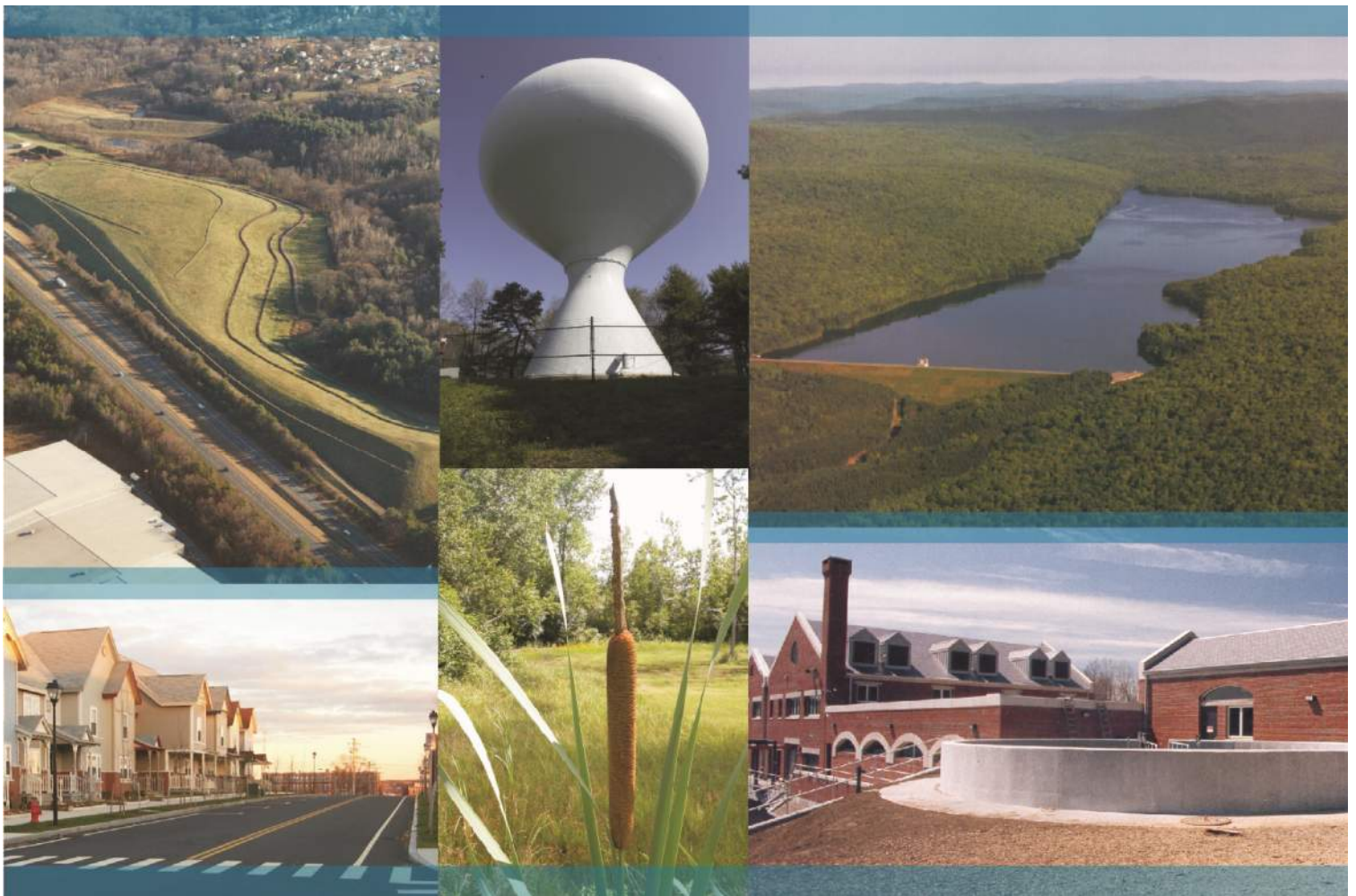
Terms: FES301

length of apron (ft.) L_a
 discharge from pipe (cfs) Q (25 YR STORM EVENT)
 pipe dia. or channel width (ft.) Do
 tailwater depth (ft.) T_w
 width of apron (at outlet)(ft) $W1$
 width of apron (downstream)(ft) $W2$
 median stone diameter (ft.) d_{50}

Equations Used:

Length of Apron (L_a)
 when $T_w < .5 * Do$ $L_a = \frac{1.8(Q)}{Do^{(3/2)}} + 7Do$
 when $T_w \geq .5 * Do$ $L_a = \frac{3(Q)}{Do^{(3/2)}} + 7Do$
 Width of Apron ($W1$)
 $W1 = 3Do$
 Width of Apron ($W2$)
 when $T_w < .5 * Do$ $W2 = 3Do + La$
 when $T_w \geq .5 * Do$ $W2 = 3Do + 0.4La$
 Median Diameter $d_{50} = \frac{0.02 * Q^{(1.3)}}{(T_w * Do)}$

<u>Input:</u>			
Q (cfs)	13.54	cfs	
Do (ft.)	2.00	ft	
T_w (ft.)	0.80	ft	
<u>Output:</u>			
Width of Apron ($W1$)	6	ft.	
Width of Apron ($W2$)	29	ft.	
Length of Apron (L_a)	23	ft.	
Median Diameter	0.50	ft.	
Riprap min. depth	1.13	ft.	



Tighe&Bond

Iron Parcel Redevelopment
70 & 80 Corporate Drive
Portsmouth, New Hampshire

Operations & Maintenance Manual

Prepared For:

Lonza Biologics
101 International Drive
Portsmouth, New Hampshire

June 18, 2018
Last Revised: July 17, 2023

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Section 1

Long-Term Operation & Maintenance Plan

It is the intent of this Operation and Maintenance Plan to identify the areas of this site that need special attention and consideration, as well as implementing a plan to assure routine maintenance. By identifying the areas of concern as well as implementing a frequent and routine maintenance schedule the site will maintain a high quality stormwater runoff.

1.1 Contact/Responsible Party

Lonza Biologics
101 International Drive
Portsmouth, NH 03801

(Note: The contact information for the Contact/Responsible Party shall be kept current. If ownership changes, the Operation and Maintenance Plan must be transferred to the new party.)

1.2 Maintenance Items

Maintenance of the following items shall be recorded:

- Litter/Debris Removal
- Landscaping
- Catchbasin Cleaning
- Pavement Sweeping
- Gravel Wetland Maintenance
- Rain Garden Maintenance
- Stream Maintenance

The following maintenance items and schedule represent the minimum action required. Periodic site inspections shall be conducted, and all measures must be maintained in effective operating condition. The following items shall be observed during site inspection and maintenance:

- Inspect vegetated areas, particularly slopes and embankments for areas of erosion. Replant and restore as necessary
- Inspect catch basins for sediment buildup
- Inspect site for trash and debris

1.3 Overall Site Operation & Maintenance Schedule

Overall Site Operation and Maintenance Schedule		
Maintenance Item	Frequency of Maintenance	Operation
Litter/Debris Removal - Trash and debris to be removed including long the full length of the stream.	Weekly	Management Company
Pavement Sweeping - Sweep impervious areas to remove sand and litter.	Annually	Parking Lot Sweeper
Sediment Forebay - Trash and debris to be removed including at check dam. - Embankment to be mowed. - Any required maintenance shall be addressed. - Inspect sediment accumulation and clean as needed.	Periodically (At least two (2) times annually)	Management Company
Gravel wetland - Trash and debris to be removed including at outlet structure. - Embankment to be mowed. - Any required maintenance shall be addressed.	Periodically (At least two (2) times annually)	Management Company
Rain Gardens/Infiltration Basin - Trash and debris to be removed. - Any required maintenance shall be addressed.	Two (2) times annually and after any rainfall event exceeding 2.5" in a 24-hr period	Management Company
Rip Rap Aprons - Trash and debris to be removed. - Any required maintenance shall be addressed.	Annually	Management Company
Catch Basin (CB) Cleaning - CB to be cleaned of solids and oils.	Annually	Vacuum Truck

Landscaping - Landscaped islands to be maintained and mulched.	Maintained as required and mulched each Spring	Management Company
---	--	--------------------

Sediment Forebay Inspection/Maintenance Requirements		
Inspection/ Maintenance	Frequency	Action
Monitor Sediment Accumulation	Annually	- Install and maintain a staff gage or other measuring devise, to indicate depth of sediment accumulation and level at which clean-out is required
Visual inspection	Annually	- Remove trash and debris as needed - Remove any woody vegetation - Inspect and repair embankments - Inspect check dam
Mowing	Periodically (At least two (2) times annually)	- Embankments shall be mowed

Gravel Wetland Inspection/Maintenance Requirements		
Inspection/ Maintenance	Frequency	Action
Inspect inlets and outlets to ensure good condition and no evidence of deterioration. Check to see if high-flow bypass is functioning.	Annually, more frequently in the first year of operation	Repair or replace any damaged structural parts, inlets and outlets. Clear or remove debris or restrictions.
Check for internal erosion, evidence of short circuiting, and animal burrows.	Annually, more frequently in the first year of operation	Soil erosion from short-circuiting or animal boroughs should be repaired when they occur.
Monitor to ensure that Gravel Wetland functions effectively after storms	Four (4) times annually (quarterly) and after any rainfall event exceeding 2.5" in a 24-hr period	- Trash and debris to be removed - Any required maintenance shall be addressed

Inspect Vegetation	Annually	<ul style="list-style-type: none"> - Inspect the condition of all gravel wetland vegetation -Vegetation should cover >75% of the system and should be reseeded and cared for as needed. - Prune back overgrowth - Replace dead vegetation - Remove any invasive species -Coordinate with UNH Stormwater Center for further vegetation management guidelines
Cut and remove vegetation from the Gravel Wetland System and forebay in order to maintain nitrogen removal performance.	Once every 3 years	<ul style="list-style-type: none"> - The vegetation should be cut and removed from the system to prevent nitrogen from cycling back into the system.
Inspect Drawdown Time - The system shall drawdown between 24 and 48-hours following a rainfall event.	Annually, more frequently in the first year of operation	<ul style="list-style-type: none"> - Hire qualified professional to assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.

Additional Gravel Wetland Operation and Maintenance Requirements:

- **1st Year Post-Construction:** Inspection frequency shall be after every storm in the first year following construction.
- Inspect to be certain system drains within 24 - 48 hours (within the design period, but also not so quickly as to minimize stormwater treatment).
- Watering plants as necessary during the first growing season.
- Re-vegetating poorly established areas as necessary.
- Treating diseased vegetation as necessary.
- Inspect soil and repair eroded areas, especially on slopes, at a minimum quarterly.
- Check inlets, outlets, and overflow spillway for blockage, structural integrity and evidence of erosion.

Cleaning Criteria for Gravel Wetland Treatment Cells: Sediment shall be removed from the gravel wetland surface when it accumulates to a depth of several inches (>10 cm) across the wetland surface. Materials shall be removed with rakes rather than heavy construction equipment to avoid compaction of the gravel wetland surface. Heavy equipment may be used if the equipment is located outside the gravel wetland, while a backhoe shovel reaches inside the gravel wetland to remove sediment. Removed sediments shall be dewatered (if necessary) and disposed of in accordance with all local, state and federal requirements. Removal of vegetation within the gravel wetland shall occur every three (3) growing seasons, or the end of the summer of the third year. This is to prevent decay and release of nutrients from accumulated biomass.

Rain Garden Inspection/Maintenance Requirements		
Inspection/ Maintenance	Frequency	Action
Monitor to ensure that Rain Gardens function effectively after storms	Two (2) times annually and after any rainfall event exceeding 2.5" in a 24-hr period	<ul style="list-style-type: none"> - Trash and debris to be removed - Any required maintenance shall be addressed
Inspect Vegetation	Annually	<ul style="list-style-type: none"> - Inspect the condition of all Rain Garden vegetation - Prune back overgrowth - Replace dead vegetation - Remove any invasive species
Inspect Drawdown Time - The system shall drawdown within 48-hours following a rainfall event.	Annually	<ul style="list-style-type: none"> - Assess the condition of the facility to determine measures required to restore the filtration function, including but not limited to removal of accumulated sediments or reconstruction of the filter.

Rip Rap Inspection/Maintenance Requirements		
Inspection/ Maintenance	Frequency	Action
Visual Inspection	Annually	<ul style="list-style-type: none"> - Visually inspect for damage and deterioration - Repair damages immediately

Stream Inspection/Maintenance Requirements		
Inspection/ Maintenance	Frequency	Action
Visual Inspection	Annually	<ul style="list-style-type: none"> - Visually inspect for damage and deterioration - Repair damages immediately
Litter/Debris Removal - Trash and debris to be removed including long	Weekly	Management Company

the full length of the stream.		
--------------------------------	--	--

Stream Restoration Operation and Maintenance Requirements:

Stream restoration operation and maintenance requirements are detailed in the Stream Restoration report prepared by Streamworks PLLC, and in the NHDES Hodgson Brook Watershed Management Plan.

1.3.1 Disposal Requirements

Disposal of debris, trash, sediment and other waste material should be done at suitable disposal/recycling sites and in compliance with all applicable local, state and federal waste regulations.

1.4 Snow & Ice Management for Standard Asphalt and Walkways

Snow storage areas shall be located such that no direct untreated discharges are possible to receiving waters from the storage site (snow storage areas have been shown on the Site Plan). Salt storage areas shall be covered or located such that no direct untreated discharges are possible to receiving waters from the storage site. Salt and sand shall be used to the minimum extent practical (refer to the attached for de-icing application rate guideline from the New Hampshire Stormwater Management Manual, Volume 2,).

Deicing Application Rate Guidelines

24' of pavement (typical two-lane road)

These rates are not fixed values, but rather the middle of a range to be selected and adjusted by an agency according to its local conditions and experience.

Pavement Temp. (°F) and Trend (↑↓)	Weather Condition	Maintenance Actions	Pounds per two-lane mile			
			Salt Prewetted / Pretreated with Salt Brine	Salt Prewetted / Pretreated with Other Blends	Dry Salt*	Winter Sand (abrasives)
> 30° ↑	Snow	Plow, treat intersections only	80	70	100*	Not recommended
	Freezing Rain	Apply Chemical	80 - 160	70 - 140	100 - 200*	Not recommended
30° ↓	Snow	Plow and apply chemical	80 - 160	70 - 140	100 - 200*	Not recommended
	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
25° - 30° ↑	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
	Freezing Rain	Apply Chemical	150 - 200	130 - 180	180 - 240*	Not recommended
25° - 30° ↓	Snow	Plow and apply chemical	120 - 160	100 - 140	150 - 200*	Not recommended
	Freezing Rain	Apply Chemical	160 - 240	140 - 210	200 - 300*	400
20° - 25° ↑	Snow or Freezing Rain	Plow and apply chemical	160 - 240	140 - 210	200 - 300*	400
20° - 25° ↓	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15° - 20° ↑	Snow	Plow and apply chemical	200 - 280	175 - 250	250 - 350*	Not recommended
	Freezing Rain	Apply Chemical	240 - 320	210 - 280	300 - 400*	400
15° - 20° ↓	Snow or Freezing Rain	Plow and apply chemical	240 - 320	210 - 280	300 - 400*	500 for freezing rain
0° - 15° ↑↓	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	300 - 400	Not recommended	500 - 750 spot treatment as needed
< 0°	Snow	Plow, treat with blends, sand hazardous areas	Not recommended	400 - 600**	Not recommended	500 - 750 spot treatment as needed

* Dry salt is not recommended. It is likely to blow off the road before it melts ice.

** A blend of 6 - 8 gal/ton MgCl₂ or CaCl₂ added to NaCl can melt ice as low as -10°.

Anti-icing Route Data Form				
Truck Station:				
Date:				
Air Temperature	Pavement Temperature	Relative Humidity	Dew Point	Sky
Reason for applying:				
Route:				
Chemical:				
Application Time:				
Application Amount:				
Observation (first day):				
Observation (after event):				
Observation (before next application):				
Name:				

Section 2

Chloride Management Plan

Winter Operational Guidelines

The following Chloride Management Plan is for the Lonza Biologics – Iron Parcel Redevelopment in Portsmouth, New Hampshire. The Plan includes operational guidelines including: winter operator certification requirements, weather monitoring, equipment calibration requirements, mechanical removal, and salt usage evaluation and monitoring. Due to the evolving nature of chloride management efforts, the Chlorides Management Plan will be reviewed annually, in advance of the winter season, to reflect the current management standards.

2.1 Background Information

The Lonza Biologics – Iron Parcel Redevelopment located within the Upper Hodgson Brook Watershed in Newington and Portsmouth, New Hampshire. The Upper Hodgson Brook is identified as a chloride-impaired waterbody.

2.2 Operational Guidelines – Chloride Management

All Lonza Biologics private contractors engaged at the Lonza Biologics premises for the purposes of winter operational snow removal and surface maintenance, are responsible for assisting in meeting compliance for the following protocols. Lonza Biologics private contractors are expected to minimize the effects of the use of de-icing, anti-icing and pretreatment materials by adhering to the strict guidelines outlined below.

The Lonza Biologics winter operational de-icing, anti-icing and pretreatment materials will adhere to the following protocols:

2.2.1 Winter Operator Certification Requirements

All private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance must be current UNHT2 Green SnowPro Certified operators or equivalent and will use only pre-approved methods for spreading abrasives on private roadways and parking lots. All private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance shall provide to Lonza Biologics management two copies of the annual UNHT2 Green SnowPro certificate or equivalent for each operator utilized on the Lonza Biologics premises. The annual UNHT2 Green SnowPro certificate or equivalent for each operator will be available on file in the Lonza Biologics Facilities Management office and be present in the vehicle/carrier at all times.

2.2.2 Improved Weather Monitoring

Lonza Biologics will coordinate weather information for use by winter maintenance contractors. This information in conjunction with site specific air/ground surface temperature monitoring will ensure that private contractors engaged at the Lonza Biologics premises for the purpose of winter operational

snow removal and surface maintenance will make more informed decisions as to when and to what extent de-icing, anti-icing and pretreatment materials are applied to private roadways, sidewalks, and parking lots.

2.2.3 Equipment Calibration Requirements

All equipment utilized on the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance will conform to the following calibration requirements.

2.2.3.1 Annual Calibration Requirements

All private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance shall provide two copies of the annual calibration report for each piece of equipment utilized on the Lonza Biologics premises. Each calibration report shall include the vehicle/carrier VIN number and the serial numbers for each component including, but not limited to, spreader control units, salt aggregate spreader equipment, brining/pre-wetting equipment, ground speed orientation unit, and air/ground surface temperature monitor. Annual calibration reports will be available on file in the Lonza Biologics Facilities Management office and be present in the vehicle/carrier at all times.

Prior to each use, each vehicle/carrier operator will perform a systems check to verify that unit settings remain within the guidelines established by the Lonza Biologics Management Team in order to accurately dispense material. All private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance will be subject to spot inspections by members of the Lonza Biologics Management Team to ensure that each vehicle/carrier is operating in a manner consistent with the guidelines set herein or State and Municipal regulations. All units will be recalibrated, and the updated calibration reports will be provided each time repairs or maintenance procedures affect the hydraulic system of the vehicle/carrier.

2.2.4 Increased Mechanical Removal Capabilities

All private contractors engaged at the Lonza Biologics premises will endeavor to use mechanical removal means on a more frequent basis for roadways, parking lots and sidewalks. Dedicating more manpower and equipment to increase snow removal frequencies prevents the buildup of snow and the corresponding need for de-icing, anti-icing and pretreatment materials. Shortened maintenance routes, with shorter service intervals, will be used to stay ahead of snowfall. Minimized snow and ice packing will reduce the need for abrasives, salt aggregates, and/or brining solution to restore surfaces back to bare surface states after winter precipitation events.

After storm events the Lonza Biologics management team will be responsible for having the streets swept to recapture un-melted de-icing materials, when practical.

2.3 Salt Usage Evaluation and Monitoring

All private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance shall provide two copies of a storm report, which includes detailed information regarding treatment areas and the use of de-icing, anti-icing and pretreatment materials applied for the removal of snow and surface maintenance on the Lonza Biologics premises. Lonza Biologics will maintain copies of Summary Documents, including copies of the Storm Reports, operator certifications, equipment used for roadway and sidewalk winter maintenance, calibration reports and amount of de-icing materials used.

2.4 Summary

The above-described methodologies are incorporated into the Lonza Biologics Operational Manual and are to be used to qualify and retain all private contractors engaged at the Lonza Biologics premises for the purpose of winter operational snow removal and surface maintenance. This section of the Manual, is intended to be an adaptive management document that is modified as required based on experience gained from past practices and technological advancements that reflect chloride BMP standards. All Lonza Biologics employees directly involved with winter operational activities are required to review this document and the current standard Best Management Practices published by the UNH Technology Transfer (T2) program annually. All Lonza Biologics employees directly involved with winter operational activities, and all private contractors engaged at the Lonza Biologics premises for the purposes of winter operational snow removal and surface maintenance, must be current UNHT2 Green SnowPro Certified operators or equivalent and undergo the necessary requirements to maintain this certification annually.

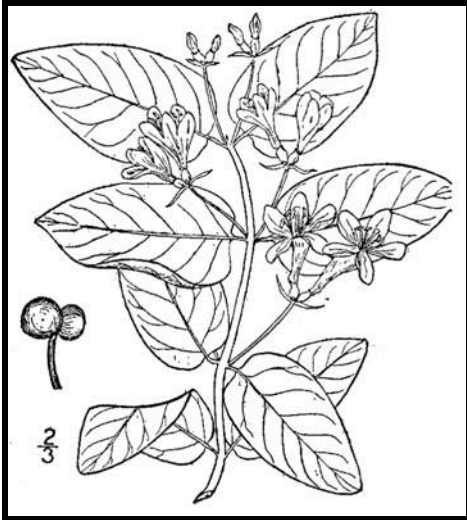
Section 3

Invasive Species

With respect to a particular ecosystem, any species, including its seeds, eggs, spores, or other biological material capable of propagating that species, that is not native to that ecosystem is classified as an invasive species. Refer to the following fact sheet prepared by the University of New Hampshire Cooperative Extension entitled Methods for Disposing Non-Native Invasive Plants for recommended methods to dispose of invasive plant species.



Prepared by the Invasives Species Outreach Group, volunteers interested in helping people control invasive plants. Assistance provided by the Piscataquog Land Conservancy and the NH Invasives Species Committee. Edited by Karen Bennett, Extension Forestry Professor and Specialist.



Tatarian honeysuckle
Lonicera tatarica

USDA-NRCS PLANTS Database / Britton, N.L., and A. Brown. 1913. *An illustrated flora of the northern United States, Canada and the British Possessions*. Vol. 3: 282.

Non-native invasive plants crowd out natives in natural and managed landscapes. They cost taxpayers billions of dollars each year from lost agricultural and forest crops, decreased biodiversity, impacts to natural resources and the environment, and the cost to control and eradicate them.

Invasive plants grow well even in less than desirable conditions such as sandy soils along roadsides, shaded wooded areas, and in wetlands. In ideal conditions, they grow and spread even faster. There are many ways to remove these non-native invasives, but once removed, care is needed to dispose the removed plant material so the plants don't grow where disposed.

Knowing how a particular plant reproduces indicates its method of spread and helps determine

the appropriate disposal method. Most are spread by seed and are dispersed by wind, water, animals, or people. Some reproduce by vegetative means from pieces of stems or roots forming new plants. Others spread through both seed and vegetative means.

Because movement and disposal of viable plant parts is restricted (see NH Regulations), viable invasive parts can't be brought to most transfer stations in the state. Check with your transfer station to see if there is an approved, designated area for invasives disposal. This fact sheet gives recommendations for rendering plant parts non-viable.

Control of invasives is beyond the scope of this fact sheet. For information about control visit www.nhinvasives.org or contact your UNH Cooperative Extension office.

New Hampshire Regulations

Prohibited invasive species shall only be disposed of in a manner that renders them nonliving and nonviable. (Agr. 3802.04)

No person shall collect, transport, import, export, move, buy, sell, distribute, propagate or transplant any living and viable portion of any plant species, which includes all of their cultivars and varieties, listed in Table 3800.1 of the New Hampshire prohibited invasive species list. (Agr 3802.01)

How and When to Dispose of Invasives?

To prevent seed from spreading remove invasive plants before seeds are set (produced). Some plants continue to grow, flower and set seed even after pulling or cutting. Seeds can remain viable in the ground for many years. If the plant has flowers or seeds, place the flowers and seeds in a heavy plastic bag “head first” at the weeding site and transport to the disposal site. The following are general descriptions of disposal methods. See the chart for recommendations by species.

Burning: Large woody branches and trunks can be used as firewood or burned in piles. For outside burning, a written fire permit from the local forest fire warden is required unless the ground is covered in snow. Brush larger than 5 inches in diameter can't be burned. Invasive plants with easily airborne seeds like black swallow-wort with mature seed pods (indicated by their brown color) shouldn't be burned as the seeds may disperse by the hot air created by the fire.

Bagging (solarization): Use this technique with softer-tissue plants. Use heavy black or clear plastic bags (contractor grade), making sure that no parts of the plants poke through. Allow the bags to sit in the sun for several weeks and on dark pavement for the best effect.

Tarping and Drying: Pile material on a sheet of plastic and cover with a tarp, fastening the tarp to the ground and monitoring it for escapes. Let the material dry for several weeks, or until it is clearly nonviable.

Chipping: Use this method for woody plants that don't reproduce vegetatively.

Burying: This is risky, but can be done with watchful diligence. Lay thick plastic in a deep pit before placing the cut up plant material in the hole. Place the material away from the edge of the plastic before covering it with more heavy plastic. Eliminate as much air as possible and toss in soil to weight down the material in the pit. Note that the top of the buried material should be at least three feet underground. Japanese knotweed should be at least 5 feet underground!

Drowning: Fill a large barrel with water and place soft-tissue plants in the water. Check after a few weeks and look for rotted plant material (roots, stems, leaves, flowers). Well-rotted plant material may be composted. A word of caution- seeds may still be viable after using this method. Do this before seeds are set. This method isn't used often. Be prepared for an awful stink!

Composting: Invasive plants can take root in compost. Don't compost any invasives unless you know there is no viable (living) plant material left. Use one of the above techniques (bagging, tarping, drying, chipping, or drowning) to render the plants nonviable before composting. Closely examine the plant before composting and avoid composting seeds.






Japanese knotweed
Polygonum cuspidatum
USDA-NRCS PLANTS Database /
Britton, N.L., and A. Brown. 1913. *An illustrated flora of the northern United States, Canada and the British Possessions*. Vol. 1: 676.

Be diligent looking for seedlings for years in areas where removal and disposal took place.

Suggested Disposal Methods for Non-Native Invasive Plants

This table provides information concerning the disposal of removed invasive plant material. If the infestation is treated with herbicide and left in place, these guidelines don't apply. Don't bring invasives to a local transfer station, unless there is a designated area for their disposal, or they have been rendered non-viable. This listing includes wetland and upland plants from the New Hampshire Prohibited Invasive Species List. The disposal of aquatic plants isn't addressed.

Woody Plants	Method of Reproducing	Methods of Disposal
Norway maple <i>(Acer platanoides)</i> European barberry <i>(Berberis vulgaris)</i> Japanese barberry <i>(Berberis thunbergii)</i> autumn olive <i>(Elaeagnus umbellata)</i> burning bush <i>(Euonymus alatus)</i> Morrow's honeysuckle <i>(Lonicera morrowii)</i> Tatarian honeysuckle <i>(Lonicera tatarica)</i> showy bush honeysuckle <i>(Lonicera x bella)</i> common buckthorn <i>(Rhamnus cathartica)</i> glossy buckthorn <i>(Frangula alnus)</i>	Fruit and Seeds 	<p>Prior to fruit/seed ripening</p> <p>Seedlings and small plants</p> <ul style="list-style-type: none"> ▪ Pull or cut and leave on site with roots exposed. No special care needed. <p>Larger plants</p> <ul style="list-style-type: none"> ▪ Use as firewood. ▪ Make a brush pile. ▪ Chip. ▪ Burn. <hr/> <p>After fruit/seed is ripe</p> <p>Don't remove from site.</p> <ul style="list-style-type: none"> ▪ Burn. ▪ Make a covered brush pile. ▪ Chip once all fruit has dropped from branches. ▪ Leave resulting chips on site and monitor.
oriental bittersweet <i>(Celastrus orbiculatus)</i> multiflora rose <i>(Rosa multiflora)</i>	Fruits, Seeds, Plant Fragments 	<p>Prior to fruit/seed ripening</p> <p>Seedlings and small plants</p> <ul style="list-style-type: none"> ▪ Pull or cut and leave on site with roots exposed. No special care needed. <p>Larger plants</p> <ul style="list-style-type: none"> ▪ Make a brush pile. ▪ Burn. <hr/> <p>After fruit/seed is ripe</p> <p>Don't remove from site.</p> <ul style="list-style-type: none"> ▪ Burn. ▪ Make a covered brush pile. ▪ Chip – only after material has fully dried (1 year) and all fruit has dropped from branches. Leave resulting chips on site and monitor.

Non-Woody Plants	Method of Reproducing	Methods of Disposal
<p>garlic mustard (<i>Alliaria petiolata</i>)</p> <p>spotted knapweed (<i>Centaurea maculosa</i>)</p> <ul style="list-style-type: none"> ▪ Sap of related knapweed can cause skin irritation and tumors. Wear gloves when handling. <p>black swallow-wort (<i>Cynanchum nigrum</i>)</p> <ul style="list-style-type: none"> ▪ May cause skin rash. Wear gloves and long sleeves when handling. <p>pale swallow-wort (<i>Cynanchum rossicum</i>)</p> <p>giant hogweed (<i>Heracleum mantegazzianum</i>)</p> <ul style="list-style-type: none"> ▪ Can cause major skin rash. Wear gloves and long sleeves when handling. <p>dame's rocket (<i>Hesperis matronalis</i>)</p> <p>perennial pepperweed (<i>Lepidium latifolium</i>)</p> <p>purple loosestrife (<i>Lythrum salicaria</i>)</p> <p>Japanese stilt grass (<i>Microstegium vimineum</i>)</p> <p>mile-a-minute weed (<i>Polygonum perfoliatum</i>)</p>	<p>Fruits and Seeds</p> 	<p>Prior to flowering</p> <p>Depends on scale of infestation</p> <p>Small infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and leave on site with roots exposed. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and pile. (You can pile onto or cover with plastic sheeting). ▪ Monitor. Remove any re-sprouting material. <hr/> <p>During and following flowering</p> <p>Do nothing until the following year or remove flowering heads and bag and let rot.</p> <p>Small infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and leave on site with roots exposed. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and pile remaining material. (You can pile onto plastic or cover with plastic sheeting). ▪ Monitor. Remove any re-sprouting material.
<p>common reed (<i>Phragmites australis</i>)</p> <p>Japanese knotweed (<i>Polygonum cuspidatum</i>)</p> <p>Bohemian knotweed (<i>Polygonum x bohemicum</i>)</p>	<p>Fruits, Seeds, Plant Fragments</p> <p>Primary means of spread in these species is by plant parts. Although all care should be given to preventing the dispersal of seed during control activities, the presence of seed doesn't materially influence disposal activities.</p>	<p>Small infestation</p> <ul style="list-style-type: none"> ▪ Bag all plant material and let rot. ▪ Never pile and use resulting material as compost. ▪ Burn. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Remove material to unsuitable habitat (dry, hot and sunny or dry and shaded location) and scatter or pile. ▪ Monitor and remove any sprouting material. ▪ Pile, let dry, and burn.

January 2010

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Managing Invasive Plants

Methods of Control

by Christopher Mattrick

They're out there. The problem of invasive plants is as close as your own backyard.

Maybe a favorite dogwood tree is struggling in the clutches of an Oriental bittersweet vine. Clawlike canes of multiflora rose are scratching at the side of your house. That handsome burning bush you planted few years ago has become a whole clump in practically no time ... but what happened to the azalea that used to grow right next to it?

If you think controlling or managing invasive plants on your property is a daunting task, you're not alone. Though this topic is getting lots of attention from federal, state, and local government agencies, as well as the media, the basic question for most homeowners is simply, "How do I get rid of the invasive plants in my own landscape?" Fortunately, the best place to begin to tackle this complex issue is in our own backyards and on local conservation lands. We hope the information provided here will help you take back your yard. We won't kid you—there's some work involved, but the payoff in beauty, wildlife habitat, and peace of mind makes it all worthwhile.

PLAN OF ATTACK

Three broad categories cover most invasive plant control: mechanical, chemical, and biological. Mechanical control means physically removing plants from the environment



Spraying chemicals to control invasive plants.

through cutting or pulling. Chemical control uses herbicides to kill plants and inhibit regrowth. Techniques and chemicals used will vary depending on the species. Biological controls use plant diseases or insect predators, typically from the targeted species' home range. Several techniques may be effective in controlling a single species, but there is usually one preferred method—the one that is most resource efficient with minimal impact on non-target species and the environment.

MECHANICAL CONTROL METHODS

Mechanical treatments are usually the first ones to look at when evaluating an invasive plant removal project. These procedures do not require special licensing or introduce chemicals into the environment. They do require permits in some situations, such as wetland zones. [See sidebar on page 23.] Mechanical removal is highly labor intensive and creates a significant amount of site disturbance, which can lead to rapid reinvasion if not handled properly.

Pulling and digging

Many herbaceous plants and some woody species (up to about one inch in diameter), if present in limited quantities, can be pulled out or dug up. It's important to remove as much of the root system as possible; even a small portion can restart the infestation. Pull plants by hand or use a digging fork, as shovels can shear off portions of the root system, allowing for regrowth. To remove larger woody stems (up to about three inches in diameter), use a Weed Wrench™, Root Jack, or Root Talon. These tools, available from several manufacturers, are designed to remove the aboveground portion of the plant as well as the entire root system. It's easiest to undertake this type of control in the spring or early summer when soils are moist and plants come out more easily.



Using tools to remove woody stems.



Volunteers hand pulling invasive plants.

Suffocation

Try suffocating small seedlings and herbaceous plants. Place double or triple layers of thick UV-stabilized plastic sheeting, either clear or black (personally I like clear), over the infestation and secure the plastic with stakes or weights. Make sure the plastic extends at least five feet past the edge of infestation on all sides. Leave the plastic in place for at least two years. This technique will kill everything beneath the plastic—invasive and non-invasive plants alike. Once the plastic is removed, sow a cover crop such as annual rye to prevent new invasions.

Cutting or mowing

This technique is best suited for locations you can visit and treat often. To be effective, you will need to mow or cut infested areas three or four times a year for up to five years. The goal is to interrupt the plant's ability to photosynthesize by removing as much leafy material as possible. Cut the plants at ground level and remove all resulting debris from the site. With this treatment, the infestation may actually appear to get worse at first, so you will need to be as persistent as the invasive plants themselves. Each time you cut the plants back, the root system gets slightly larger, but must also rely on its energy reserves to push up new growth. Eventually, you will exhaust these reserves and the plants will die. This may take many years, so you have to remain committed to this process once you start; otherwise the treatment can backfire, making the problem worse.

CHEMICAL CONTROL METHODS

Herbicides are among the most effective and resource-efficient tools to treat invasive species. Most of the commonly known invasive plants can be treated using only two herbicides—glyphosate (the active ingredient in Roundup™ and Rodeo™) and triclopyr (the active ingredient in Brush-B-Gone™ and Garlon™). Glyphosate is non-selective, meaning it kills everything it contacts. Triclopyr is selective and does not injure monocots (grasses, orchids, lilies, etc.). Please read labels and follow directions precisely for both environmental and personal safety. These are relatively benign herbicides, but improperly used they can still cause both short- and long-term health and environmental problems. Special aquatic formulations are required when working in wetland zones. You are required to have a state-issued pesticide applicator license when applying these chemicals on land you do not own. To learn more about the pesticide regulations in your state, visit or call your state's pesticide control division, usually part of the state's Department of Agriculture. In wetland areas, additional permits are usually required by the Wetlands Protection Act. [See sidebar on page 23.]

Foliar applications

When problems are on a small scale, this type of treatment is usually applied with a backpack sprayer or even a small handheld spray bottle. It is an excellent way to treat large monocultures of herbaceous plants, or to spot-treat individual plants that are difficult to remove mechanically, such as goutweed, swallowwort, or purple loosestrife. It is also an effective treatment for some woody species, such as Japanese barberry, multiflora rose, Japanese honeysuckle, and Oriental bittersweet that grow in dense masses or large numbers over many acres. The herbicide mixture should contain no more than five percent of the active ingredient, but it is important to follow the instructions on the product label. This treatment is most effective when the plants are actively growing, ideally when they are flowering or beginning to form fruit. It has been shown that plants are often more susceptible to this type of treatment if the existing stems are cut off and the regrowth is treated. This is especially true for Japanese knotweed. The target plants should be thoroughly wetted with the herbicide on a day when there is no rain in the forecast for the next 24 to 48 hours.

Cut stem treatments

There are several different types of cut stem treatments, but here we will review only the one most commonly used. All treatments of this type require a higher concentration of the active ingredient than is used in foliar applications. A 25 to 35 percent solution of the active ingredient should be used for cut stem treatments, but read and follow all label instructions. In most cases, the appropriate herbicide is glyphosate, except for Oriental bittersweet, on which triclopyr should be used. This treatment can be used on all woody stems, as well as phragmites and Japanese knotweed.

For woody stems, treatments are most effective when applied in the late summer and autumn—between late August and November. Stems should be cut close to the ground, but not so close that you will lose track of them. Apply herbicide directly to the cut surface as soon as possible after cutting. Delaying the application will reduce the effectiveness of the treatment. The herbicide can be applied with a sponge, paintbrush, or spray bottle.



Cut stem treatment tools.

For phragmites and Japanese knotweed, treatment is the same, but the timing and equipment are different. Plants should be treated anytime from mid-July through September, but the hottest, most humid days of the summer are best

for this method. Cut the stems halfway between two leaf nodes at a comfortable height. Inject (or squirt) herbicide into the exposed hollow stem. All stems in an infestation should be treated. A wash bottle is the most effective application tool, but you can also use an eyedropper, spray bottle, or one of the recently developed high-tech injection systems.

It is helpful to mix a dye in with the herbicide solution. The dye will stain the treated surface and mark the areas that have been treated, preventing unnecessary reapplication. You can buy a specially formulated herbicide dye, or use food coloring or laundry dye.

There is not enough space in this article to describe all the possible ways to control invasive plants. You can find other treatments, along with more details on the above-described methods, and species-specific recommendations on The Nature Conservancy Web site (tncweeds.ucdavis.edu). An upcoming posting on the Invasive Plant Atlas of New England (www.ipane.org) and the New England Wild Flower Society (www.newfs.org) Web sites will also provide further details.



Hollow stem injection tools.

Biological controls—still on the horizon

Biological controls are moving into the forefront of control methodology, but currently the only widely available and applied biocontrol relates to purple loosestrife. More information on purple loosestrife and other biological control projects can be found at www.invasiveplants.net.

DISPOSAL OF INVASIVE PLANTS

Proper disposal of removed invasive plant material is critical to the control process. Leftover plant material can cause new infestations or reinfest the existing project area. There are many appropriate ways to dispose of invasive plant debris. I've listed them here in order of preference.

- 1. Burn it**—Make a brush pile and burn the material following local safety regulations and restrictions, or haul it to your town's landfill and place it in their burn pile.
- 2. Pile it**—Make a pile of the woody debris. This technique will provide shelter for wildlife as well.
- 3. Compost it**—Place all your herbaceous invasive plant debris in a pile and process as compost. Watch the pile closely for resprouts and remove as necessary. Do not use the resulting compost in your garden. The pile is for invasive plants only.



Injecting herbicide into the hollow stem of phragmites.

4. Dry it/cook it—Place woody debris out on your driveway or any asphalt surface and let it dry out for a month. Place herbaceous material in a doubled-up black trash bag and let it cook in the sun for one month. At the end of the month, the material should be non-viable and you can dump it or dispose of it with the trash. The method assumes there is no viable seed mixed in with the removed material.

Care should be taken in the disposal of all invasive plants, but several species need extra attention. These are the ones that have the ability to sprout vigorously from plant fragments and should ideally be burned or dried prior to disposal: Oriental bittersweet, multiflora rose, Japanese honeysuckle, phragmites, and Japanese knotweed.

Christopher Mattrick is the former Senior Conservation Programs Manager for New England Wild Flower Society, where he managed conservation volunteer and invasive and rare plant management programs. Today, Chris and his family work and play in the White Mountains of New Hampshire, where he is the Forest Botanist and Invasive Species Coordinator for the White Mountain National Forest.



Controlling Invasive Plants in Wetlands

Special concerns; special precautions

Control of invasive plants in or around wetlands or bodies of water requires a unique set of considerations. Removal projects in wetland zones can be legal and effective if handled appropriately. In many cases, herbicides may be the least disruptive tools with which to remove invasive plants. You will need a state-issued pesticide license to apply herbicide on someone else's property, but all projects in wetland or aquatic systems fall under the jurisdiction of the Wetlands Protection Act and therefore require a permit. *Yes, even hand-pulling that colony of glossy buckthorn plants from your own swampland requires a permit.* Getting a permit for legal removal is fairly painless if you plan your project carefully.

1. Investigate and understand the required permits and learn how to obtain them. The entity charged with the enforcement of the Wetlands Protection Act varies from state to state. For more information in your state, contact:

ME: Department of Environmental Protection
www.state.me.us/dep/blwq/docstand/nrapage.htm

NH: Department of Environmental Services
www.des.state.nh.us/wetlands/

VT: Department of Environmental Conservation
www.anr.state.vt.us/dec/waterq/permits/htm/pm_cud.htm

MA: Consult your local town conservation commission

RI: Department of Environmental Management
www.dem.ri.gov/programs/benviron/water/permits/fresh/index.htm

CT: Consult your local town Inland Wetland and Conservation Commission

2. Consult an individual or organization with experience in this area. Firsthand experience in conducting projects in wetland zones and navigating the permitting process is priceless. Most states have wetland scientist societies whose members are experienced in working in wetlands and navigating the regulations affecting them. A simple Web search will reveal the contact point for these societies. Additionally, most environmental consulting firms and some nonprofit organizations have skills in this area.

3. Develop a well-written and thorough project plan. You are more likely to be successful in obtaining a permit for your project if you submit a project plan along with your permit application. The plan should include the reasons for the project, your objectives in completing the project, how you plan to reach those objectives, and how you will monitor the outcome.

4. Ensure that the herbicides you plan to use are approved for aquatic use. Experts consider most herbicides harmful to water quality or aquatic organisms, but rate some formulations as safe for aquatic use. Do the research and select an approved herbicide, and then closely follow the instructions on the label.

5. If you are unsure—research, study, and most of all, ask for help. Follow the rules. The damage caused to aquatic systems by the use of an inappropriate herbicide or the misapplication of an appropriate herbicide not only damages the environment, but also may reduce public support for safe, well-planned projects.

Section 4

Annual Updates and Log Requirements

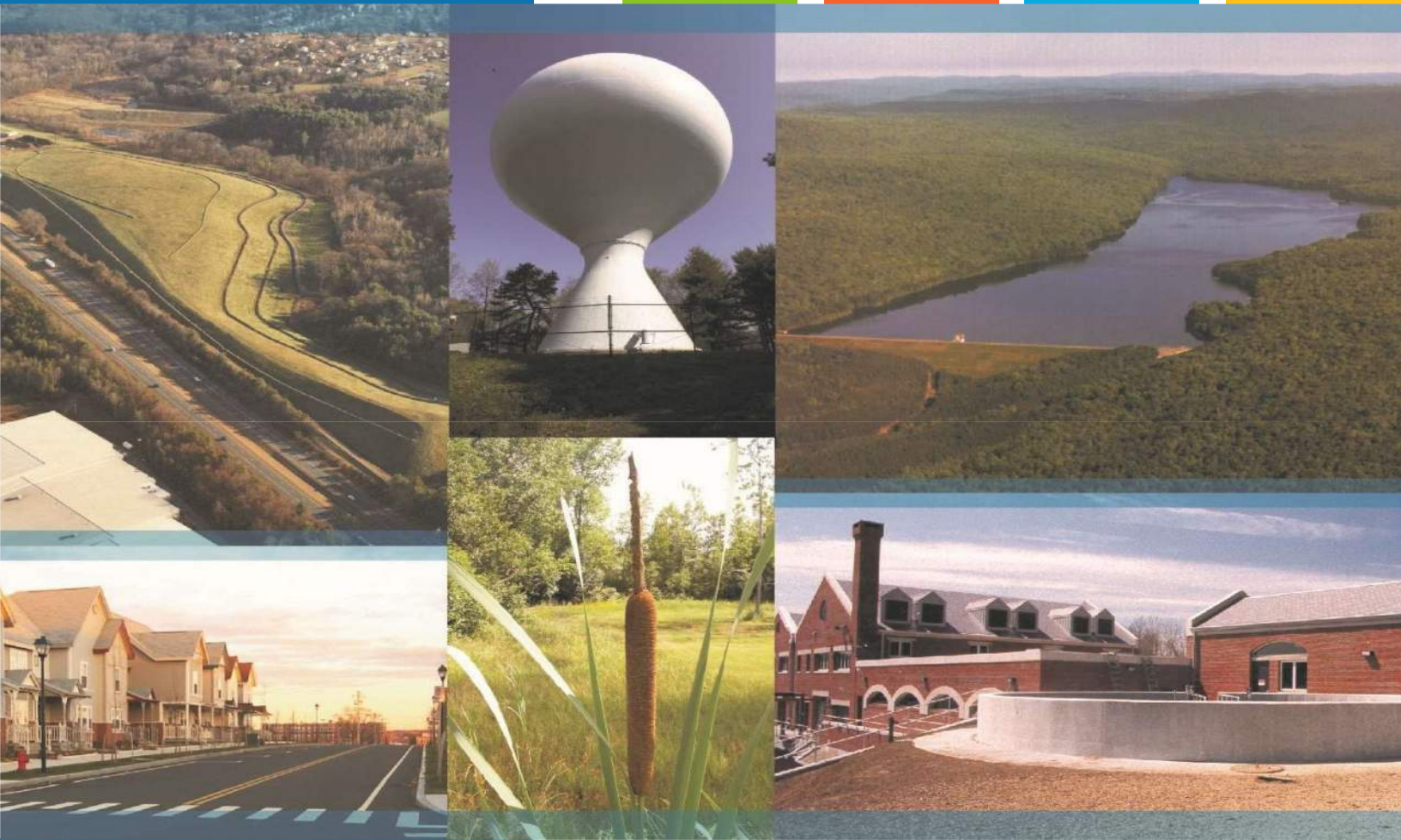
The Owner and/or Contact/Responsible Party shall review this Operation and Maintenance Plan once per year for its effectiveness and adjust the plan and deed as necessary.

A log of all preventative and corrective measures for the stormwater system shall be kept on-site and be made available upon request by any public entity with administrative, health environmental or safety authority over the site including NHDES.

Copies of the Stormwater Maintenance report shall be submitted to the Pease Development Authority on an annual basis.

Stormwater Management Report						
Project Name		Lonza – Iron Parcel				
BMP Description	Date of Inspection	Inspector	BMP Installed and Operating Properly?	Cleaning / Corrective Action Needed	Date of Cleaning / Repair	Performed By
			<input type="checkbox"/> Yes <input type="checkbox"/> No			
			<input type="checkbox"/> Yes <input type="checkbox"/> No			
			<input type="checkbox"/> Yes <input type="checkbox"/> No			
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			<input type="checkbox"/> Yes <input type="checkbox"/> No			

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Lonza Biologics Industrial Development

TRAFFIC IMPACT ASSESSMENT

Lonza Biologics

June 1, 2023

Last Revised: July 17, 2023

Tighe&Bond

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Section 1

Introduction

This Traffic Impact Assessment (TIA) evaluates the potential traffic impact of the proposed Lonza Biologics industrial development, located along Corporate Drive and Goose Bay Drive within the Pease International Tradeport in Portsmouth, NH. The TIA is based in part on the previous *Lonza Biologics Proposed Industrial Development Traffic Evaluation*, dated April 3, 2018, completed by Tighe & Bond. This updated TIA addresses the City of Portsmouth Planning Department Site Plan Application Conditions of Approval, dated January 18, 2019, to expand the Traffic Analysis study area as stated in Condition 2.10 for subsequent phases of development for the Lonza site. This revised TIA has been prepared in accordance with NHDOT and industry standards. The Project Site is bounded by Corporate Drive to the north, and Goose Bay Drive to the west, south and east. The site is surrounded by industrial, manufacturing, medical, and office land uses, consistent with the Tradeport as a whole. The Site location is shown in Figure 1.

The existing Lonza facility currently includes 900,000+/- square feet (SF) of building space including manufacturing, research and development, office, and ancillary services with 780+/- parking spaces. The Applicant plans to construct three buildings totaling approximately 800,000+/- square foot (SF) of industrial space with 700 additional parking spaces contained in one garage. The proposed buildings will be located on currently vacant land on the north side of Goose Bay Drive. Primary access to the site will be provided via a new driveway on Goose Bay Drive opposite the existing parking garage entrance. A new curb cut is also proposed on Corporate Drive, approximately 400 feet east of Redhook Way; however, this driveway will be gated in the near-term, but is expected to be used for deliveries to the proposed Building 3 once the full build-out is complete. Roadway improvements as part of the project include the closure of Goose Bay Drive to through traffic approximately 125 feet southwest of the Corporate Center driveway, and conversion of a portion of Goose Bay Drive from a public road to be merged with the Lonza parcel. The proposed Site Plan Layout is enclosed in Appendix I. Proposed Building 1 is expected to be complete and occupied in 2025; however, for the purposes of this study, the full build-out of the site is assumed to be in 2025.

Based on the analyses conducted herein, it is the professional opinion of Tighe & Bond that while the adjustment of collected volumes to an assumed pre-pandemic condition and the addition of background growth on a 12-year horizon to the 2035 design year results in undesirable LOS at some area intersections, the traffic expected to be generated by the proposed industrial development has a negligible effect on traffic operations within the study area.

Section 2

Existing Conditions

The Project Site is bounded by Corporate Drive to north and east, and Goose Bay Drive to the south and west. The following sections describe the roadways and intersections included within the study area.

2.1 Roadways

2.1.1 Corporate Drive

Corporate Drive is a local road maintained by the City of Portsmouth. The roadway runs between International Drive and loops back around to Durham Street/ International Drive to the south. The roadway is generally 28 feet wide with a two-lane cross section and narrow shoulders. Beginning at the intersection with International Drive, the roadway cross section is four lanes with westbound dedicated left, through, and right lanes, and a single eastbound travel lane. An eastbound left-turn lane is provided at Redhook Way. Narrow 2-foot striped shoulders are present between International Drive and approximately 500 feet east of Redhook Way. The shoulders to the east of this section are not striped, providing a wide approximately 14-foot travel lane. The roadway transitions to a three-lane cross section in the vicinity of Grafton Road where an eastbound dedicated left-turn lane and westbound dedicated right-turn lane are provided.

A 5-foot sidewalk is provided on both sides of the roadway between International Drive and Redhook Way. Sidewalk is provided along at least one side of the roadway except for a short 350-foot gap between Redhook Way and the Wentworth-Douglas Hospital Outpatient Center driveway and a second 300-foot gap between Ashland Road and the 273 Corporate Drive north driveway. The posted speed limit on Corporate Drive is 35 mph.

2.1.2 Goose Bay Drive

Goose Bay Drive is a local road maintained by the City of Portsmouth. The roadway intersects International Drive 180 feet west of Redhook Way at the west end and 775 feet west of Rye Street at the east end. One travel lane is provided in each direction along the entire roadway. No sidewalks are provided except for a short 200-foot section along the south side of the roadway along the Lonza property. There is no posted speed on the roadway.

2.1.3 International Drive

International Drive is a major collector road and is maintained by the City of Portsmouth. The roadway runs north to south between Pease Boulevard and New Hampshire Avenue/ Corporate Drive. A two-lane cross section is provided between New Hampshire Avenue/ Corporate Drive and Manchester Square/ Corporate Drive. At the intersection with Manchester Square/ Corporate Drive, the roadway opens to a four-lane cross section with northbound dedicated left turn lane, through lane, and shared through/ right lane and a single southbound travel lane. A five-lane cross section (three northbound, two southbound) is provided north of Corporate Drive approaching Pease Boulevard. The posted speed is 35 mph in both directions.

Sidewalk is provided on both sides of the roadway between Pease Boulevard and Corporate Drive and the west side of the roadway only between Corporate Drive and New Hampshire Avenue.

2.1.4 Pease Boulevard

Pease Boulevard is classified as an urban major collector and is maintained by the City of Portsmouth. The roadway is located north of the site location and runs primarily in the east-west direction connecting US Route 4 On/Off Ramps to the east and Pease Air National Guard Base to the west. Between Arboretum Drive/New Hampshire Avenue and International Drive, the Pease Boulevard cross section varies. Pease Boulevard at Arboretum/New Hampshire Avenue starts as a three-lane roadway (two westbound, one eastbound) with 11-foot travel lanes and narrow shoulders. The single eastbound travel lane widens to two lanes approaching International Drive, with two 11-foot travel lanes in each direction and narrow shoulders, a dedicated eastbound left turn lane, and two westbound left turn lanes. Pease Boulevard widens to a five-lane section eastbound with four 11-foot wide through lanes and a right-turn lane to the US Route 4 southbound on-ramp, with the four travel lanes aligning with two left turn lanes and two through lanes at the US Route 4 northbound ramps. Four 11-foot travel lanes are also carried westbound under the US Route 4 overpass, with two left turn lanes to the southbound on-ramp and two through lanes. The roadway continues west of US Route 4 as Gosling Road.

A five-foot sidewalk is provided on both sides of Pease Boulevard between Arboretum Drive/New Hampshire Avenue and International Drive, with a 10-foot buffered multi-use path provided on the north side of the roadway between International Drive and the US Route 4 southbound off-ramp. A 6-foot sidewalk is provided on the north side of Pease Boulevard between the US Route 4 ramps. The speed limit is posted at 35 mph in both directions.

2.1.5 Grafton Road

Grafton Road is classified as an urban major collector and maintained by the City of Portsmouth. The roadway runs in a northeast to southwest alignment connecting Corporate Drive to the northeast and Route 33 (Greenland Road) to the southwest. Grafton Road is typically a two-lane roadway with 12-foot travel lanes, widening to provide a two-lane approach with separate left and right turn lanes at its northeastern termini at Corporate Drive and its southern termini at Route 33. Shoulder lane widths vary along the roadway. Narrow shoulder widths are found near the Aviation Avenue intersection which gradually increases to 3-foot shoulders on the west side of the roadway and 5-foot shoulder on the east side of the roadway. Near Pease Golf Course Driveway/Park & Ride Driveway, the shoulder lane width increases to 10 feet on the east side of the roadway. Between Pease Golf Course Driveway/Park & Ride Driveway and Route 33, the shoulder width on both sides of the roadway is 10 feet which reduces to 3 feet on the west side of the roadway with no marked shoulder on the east at Route 33 intersection. A 10-foot buffered multi-use path is provided on the northwest side of the roadway. The speed limit is posted at 35 mph in both directions.

2.1.6 Route 33 (Greenland Road)

Route 33 (Greenland Road) is classified as an urban minor arterial and maintained by the State of New Hampshire. The roadway runs primarily in the east to west direction connecting Route 151 (Portsmouth Avenue) and the Town of Greenland to the west of the study area and US Route 1 (Lafayette Road) to the east of the study area. Between the I-

95 Southbound ramps and Grafton Road, Route 33 is a four-lane divided roadway with 11-foot travel lanes and 8-foot-wide shoulders on both sides of the roadway. Route 33 continues as an undivided four-lane roadway east of Grafton Road, with 11-foot travel lanes and 8-foot shoulders. Shoulder widths are narrower where dedicated turn lanes are provided at Grafton Road and at the I-95 Northbound ramps. No pedestrian accommodations are provided east of Grafton Road, with a speed limit of 35 mph.

2.2 Study Area Intersections

2.2.1 Gosling Road at US Route 4 Northbound Ramps

Gosling Road intersects the US Route 4 Northbound Ramps to the east of the US Route 4 (Spaulding Turnpike) overpass at a signalized intersection, with the Northbound off-ramp approaching from the south and the Northbound on-ramp departing to the north. The Gosling Road eastbound approach provides four lanes, with two left-turn lanes and two through travel lanes. The Gosling Road westbound approach consists of three lanes, with two through lanes and one shared through/right-turn lane. The left-most westbound through lane aligns with a left-turn lane at the downstream southbound ramp intersection. The northbound off-ramp approach provides four lanes, with two left-turn lanes and two right-turn lanes. Left turn movements from Gosling Road eastbound and from the northbound off-ramp are controlled with exclusive signal phases. The northbound on-ramp provides two lanes departing the intersection. As previously described, a sidewalk is provided on the north side of Gosling Road through the intersection, with a crosswalk across the northbound on-ramp. A concurrent pedestrian traffic signal phase is provided for this crosswalk. Marked edge lines are provided on all approaches with a 1-to-2-foot offset from the curb or edge of roadway.

2.2.2 Pease Boulevard at US Route 4 Southbound Ramps

Pease Boulevard intersects the US Route 4 Southbound Ramps to the west of the US Route 4 (Spaulding Turnpike) overpass at a signalized intersection, with the Southbound off-ramp approaching from the north and the Southbound on-ramp departing to the south. The Pease Boulevard westbound approach provides four lanes, with two left-turn lanes and two through travel lanes. The Pease Boulevard eastbound approach consists of five lanes, with four through lanes and one exclusive right-turn lane. The two left-most eastbound through lanes align with the left-turn lanes at the downstream northbound ramp intersection. The southbound off-ramp approach provides four lanes, with two left-turn lanes and two right-turn lanes. Left turn movements from Pease Boulevard westbound and from the southbound off-ramp are controlled with exclusive signal phases. The southbound on-ramp provides two lanes departing the intersection. As previously described, a sidewalk is provided on the north side of Pease Boulevard through the intersection, with a crosswalk across the southbound off-ramp. A concurrent pedestrian traffic signal phase is provided for this crosswalk. Marked edge lines are provided on all approaches with a 1-to-2-foot offset from the curb or edge of roadway.

2.2.3 Pease Boulevard at International Drive

International Drive intersects Pease Boulevard from the north and south to form a 4-way, signalized intersection. Pease Boulevard is median divided, with the eastbound approach providing an exclusive left-turn lane and two through travel lanes, while the westbound approach provides two left-turn lanes and two through lanes. The north leg of International Drive is median divided and provides a wide, unmarked southbound approach, which is of adequate width to accommodate two vehicles side-by-side.

International Drive northbound provides one shared left/through lane and two channelized right turn lanes under signal control. Sidewalks are provided on both sides of Pease Boulevard west of the intersection, on both sides of International Drive to the south, on the west side of International Drive to the north, and on the north side of Pease Boulevard to the east. Crosswalks are provided across all four approaches and across the channelized northbound right-turn lanes, and concurrent pedestrian traffic signal phases are provided. Marked edge lines are provided on Pease Boulevard, with a 1-to-2-foot offset from the curb or edge of roadway. Variable width shoulders are provided on International Drive south of the intersection, ranging from 2 to 8 feet.

2.2.4 International Drive at Corporate Drive and Manchester Square

Corporate Drive and Manchester Square intersect International Drive from the east and west, respectively to form a 4-way unsignalized intersection under all-way stop control. The northbound approach provides a dedicated left-turn lane, through lane, and shared through/ right lane while the southbound approach provides dedicated left-turn, through, and right-turn lane. The westbound approach provides a dedicated left-turn, through, and right-turn lane, while the eastbound approach provides a dedicated left-turn lane and through/ right lane. Edge lines are present on the north, east, and west legs of the intersection. Crosswalks are provided across all four legs of the intersection.

2.2.5 Corporate Drive at Goose Bay Drive (West JCT)

Goose Bay Drive intersects Corporate Drive from the south to form a 3-way, T-intersection. Goose Bay Drive provides a single general purpose travel lane. A single dedicated eastbound left-turn from Corporate Drive begins west of Goose Bay Drive, which provides access to the Residence Inn just east of the intersection and to Cisco Brewers via Red Hook Way. Edge lines are provided on all approaches. A crosswalk is provided across Goose Bay Drive.

2.2.6 Corporate Drive at Redhook Way

Redhook Way intersects Corporate Drive from the north to form a 3-way, T-intersection. A dedicated left-turn lane and through lane are provided on the eastbound approach while a single general-purpose lane is provided on the westbound and southbound approaches. A crosswalk is provided on the west leg of the intersection. Edge lines are provided on the east and west approaches.

2.2.7 Corporate Drive at Goose Bay Drive (East JCT)

Goose Bay Drive intersects Corporate Drive from the west to form a 3-way, T-intersection. A single general-purpose travel lane is provided on all approaches. There are no marked shoulders on the intersection approaches. A crosswalk is provided across the south leg of the intersection, which provides connection between sidewalk segments on the east side of Corporate Drive north of the intersection and on the west side of Corporate Drive south of the intersection.

2.2.8 New Hampshire Avenue and Corporate Drive at Durham Street and International Drive

New Hampshire Avenue and Corporate Drive form the north and south legs, respectively, of a 4-way unsignalized intersection, with Durham Street approaching from the west and International Drive approaching from the east under stop control. All approaches provide single general-purpose lanes, with no marked shoulders. Sidewalks are provided on the north side of Durham Street and International Drive, on the east side of New Hampshire

Avenue, and on both sides of Corporate Drive. Crosswalks are provided across the north and west legs of the intersection.

2.2.9 Corporate Drive at Grafton Road

Grafton Road intersects Corporate Drive from the southwest under stop control at a 3-way, T-intersection. Corporate Drive southbound provides a through travel lane and a right-turn lane, while Corporate Drive northbound provides a left-turn lane and a through lane. Grafton Road widens at its approach to Corporate Drive to provide separate left and right turn lanes. No shoulders or edge lines are present. Sidewalks are provided on the south side of Grafton Road and on the east side of Corporate Drive, with a crosswalk across the south leg of the intersection.

2.2.10 Grafton Road at I-95 Southbound Off-Ramp

I-95 Southbound Exit 3A includes a direct off-ramp to Grafton Road. Grafton Road is median divided in the vicinity of the off-ramp, prohibiting left turns to Grafton Road southbound. The ramp provides a single-lane approach under stop control, while Grafton Road provides a single lane northbound through the intersection.

2.2.11 Grafton Road at Route 33 (Greenland Road)

Grafton Road intersects Route 33 (Greenland Road) from the north to form a 3-way, T-type, signalized intersection. Grafton Road southbound has a two-lane approach with exclusive left and right turn lanes. Route 33 eastbound provides an exclusive left-turn lane and two through lanes, while the westbound approach provides two through lanes and a right-turn lane. The north and west legs of the intersection are median divided. The multi-use path along the west side of Grafton Road continues adjacent to the intersection, turning towards the west and continuing on the north side of Route 33; however, no connection to the intersection is provided and no crosswalks or other pedestrian accommodations are provided. A narrow 2-foot shoulder is provided on the Grafton Road approach, with 7-to-10-foot shoulders provided on Route 33.

2.2.12 Minor Driveway Intersections

There are six additional intersections at minor driveways that are included in the study area:

- International Drive at Pease Development Authority Driveway (south location)
- International Drive at Lonza Biologics Driveway (north location)
- International Drive at Lonza Biologics Driveway (south location)
- Goose Bay Drive at Lonza Biologics Parking Garage Entrance
- Goose Bay Drive at Lonza Biologics Driveway (south location)
- Goose Bay Drive at Corporate Center Driveway

Each of these intersections provides a single general-purpose lane on all approaches. No crosswalks are provided except for the International Drive at Lonza Biologics driveway which provides a crosswalk on the north leg of the intersection.

2.3 Traffic Volumes

Turning movement counts (TMC) were collected at the study area intersections on both February 17, 2022 and March 7, 2023 during the weekday morning (7:00 AM to 9:00 AM) and weekday afternoon peak periods (4:00 PM to 6:00 PM). Automatic traffic recorder (ATR) data was collected on Pease Boulevard, just west of the US Route 4 southbound ramps during a 48-hour period from Tuesday thru Wednesday in March 2023. The ATR location was strategically chosen to align with the NHDOT Count Station (LOC ID 82379024) to serve as a basis for comparison of existing traffic volumes to recent NHDOT traffic volumes and to traffic counts collected in 2022 to determine if adjustments to traffic volumes should be made. The historical traffic volumes on Pease Boulevard at this location are presented below in Table 1 below.

TABLE 1

Pease Boulevard Historical Traffic Volumes

Year	Peak Hour Traffic Volumes			Source
	AADT	AM Peak	PM Peak	
2015	21,000	2,160	2,272	NHDOT (October) ¹
2016	21,420	Not Available		NHDOT Growth Estimate ²
2017	21,848	Not Available		NHDOT Growth Estimate ²
2018	20,100	1,835	2,052	NHDOT July ³
2019	20,341	Not Available		NHDOT Growth Estimate ²
2020	17,168	Not Available		NHDOT Growth Estimate ²
2021	15,807	1,212	1,558	NHDOT (August)
2022	17,175	1,211	1,428	Tighe & Bond February 2022 ATR ⁴
2023	18,485	1,551	1,783	Tighe & Bond March 2023 ATR ⁴

¹Peak Hour Traffic Volumes Adjusted based on 2017 Seasonal Adjustment Factor to Peak

²Based on NHDOT Yearly Growth Rates

³Peak Hour Traffic Volumes Adjusted based on 2018 Seasonal Adjustment Factor to Peak

⁴Total Daily Traffic and Peak Hour Traffic Volumes Adjusted based on 2019 Seasonal Adjustment Factor to Peak

The variance in volumes over time, and specifically the decrease in volume between 2019 and 2022, represent the impact of the COVID-19 pandemic on work schedules and commuting patterns. Traffic volume trends nation- and region-wide confirm that traffic volumes have generally returned to pre-pandemic levels in 2023; however, current NHDOT guidance requests that 2022 and 2023 traffic volumes should be adjusted upward to assume a return to 2019 pre-pandemic volumes. This likely represents a conservative analysis but cannot be adequately confirmed as such until multiple years of data can confirm current trends in post-pandemic traffic volumes.

Based on a review of the collected traffic volumes and comparison to the 2019 traffic volumes, it was determined the 2022 existing peak hour traffic volumes should be adjusted by a factor of 53% during the weekday morning peak period, and 45% during the weekday afternoon peak period and the 2023 existing peak hour traffic volumes should be adjusted by a factor of 37% during the weekday morning peak period, and 16% during the weekday afternoon peak period. These adjustment factors were determined by reviewing the historical NHDOT traffic volume data during the peak hour time periods and comparing it to the 2022 and 2023 peak hour volumes. Because the 2019, 2022, and

2023 peak hour time periods do not align due to changes in travel patterns, the higher peak hour traffic volume for each year was used as a basis for comparison. NHDOT seasonal adjustment factors were applied to both the historical volumes and existing traffic volumes per NHDOT guidelines.

While the application of these adjustment factors aligns with NHDOT guidance on review and adjustment of post-pandemic traffic volumes, it should be understood that application of adjustment factors based on ATR data from Pease Boulevard across all turning movements within the study area may artificially inflate turning movements and overstate calculated operational delay and resultant capacity analysis results.

The raw TMC and ATR data are provided in Appendix A. The NHDOT historical traffic volumes on Pease Boulevard, seasonal adjustment factors, and historical growth rates are enclosed in Appendix B. The Traffic Volume Adjustment Factor calculation is provided in Appendix C. Adjusted 2023 Existing Peak Hour Traffic Volumes are provided in Figure 2.

2.4 Capacity and Queue Analyses - Existing Conditions

Capacity and queue analyses were performed for the study intersections for the 2023 Existing Conditions during the weekday morning and weekday afternoon peak hours. Analyses were conducted using Trafficware Synchro Studio 11 software, which conducts the analysis based on *Highway Capacity Manual (HCM)* methodology. Consistent with NHDOT guidelines, analyses for signalized intersections were conducted using methods of the 2000 HCM, while analysis for unsignalized intersections utilized the HCM 6th Edition methodology. The analysis results are categorized in terms of Level of Service (LOS), which describes the qualitative intersection operational conditions based on the calculated average delay per vehicle. A summary of the HCM capacity analysis methodology and a detailed definition of LOS is provided in Appendix G. The queue analysis results are summarized based upon the length of vehicle queueing on an intersection approach. For unsignalized intersections, queues are quantified for 95th percentile (design queues). For signalized intersections, queues are quantified by 95th percentile (design) and 50th percentile (average) queues. Tables 4 and 5 in Section 7 summarize the capacity and queue analyses results, respectively. Capacity analysis worksheets with full inputs, settings, and results are provided in Appendix H.

As shown in Table 4, the conservative application of COVID adjustment factors to represent a pre-pandemic condition creates an assumed pre-pandemic Existing condition which predicts notable operational delay throughout the study area. While many intersections and individual intersection approaches operate at LOS D or better during the peak hours, the following predict unfavorable and failing operations:

- **Pease Boulevard at International Drive:**
 - The intersection operates at overall LOS F with failing operations on the northbound right turn movement during the weekday afternoon peak hour.
- **Pease Boulevard at US Route 4 Southbound Ramps:**
 - The intersection operates at overall LOS F during the weekday morning peak hour with failing operations on the southbound right turn movement.
 - The westbound left movement operates at LOS E during the weekday afternoon peak hour.

- **Pease Boulevard at US Route 4 Northbound Ramps:**
 - The intersection operates at overall LOS E, with failing operations on the northbound left turn movement during the weekday morning peak hour.
 - Predicted 95th percentile queues exceed the available storage on the northbound left movement during the weekday morning peak hour.
- **Route 33 (Greenland Road) at Grafton Road:**
 - The intersection operates at overall LOS F during the weekday morning peak and afternoon peak hours.
 - The eastbound left and through movements operate at LOS F during the weekday morning peak hour.
 - The eastbound left, westbound through, and southbound right movements operate at LOS F during the weekday afternoon peak hour.
 - Predicted 95th percentile queues exceed the available storage on the eastbound left movement during the weekday morning peak hour.
- **Corporate Drive at International Drive:**
 - The intersection operates at overall LOS F during the weekday morning peak and afternoon peak hours.
 - The southbound left and through movements operate at LOS F during the weekday morning peak hour.
 - The westbound right and northbound through movements operate at LOS F during the weekday afternoon peak hour.
 - Predicted 95th percentile queues exceed the available storage on the southbound left movement during the weekday morning peak hour and westbound right movement during the weekday afternoon peak hour.
- **New Hampshire Avenue/Corporate Drive at International Drive/Durham Street:**
 - The stop-controlled International Drive approach operates at LOS F during the weekday morning and weekday afternoon peak hours.
- **Corporate Drive at Goose Bay Drive (West):**
 - The northbound movement operates at LOS F during the weekday afternoon peak hour.
- **Corporate Drive at Grafton Road:**
 - The eastbound left movement on Grafton Road operates at LOS F during the weekday morning and weekday afternoon peak hours.
- **Grafton Road at I-95 Southbound Off-ramp:**
 - The ramp approach operates at LOS F during the weekday morning peak hour.

2.5 Collision History

Collision data was collected from police reports from the City of Portsmouth Police Department for the most recent three-year period between January 2020 and December 2022 for the study area intersections. Table 2 on the following page provides a summary of the collisions within the study area. Appendix F includes detailed collision summaries for each of the study intersections.

As shown in Table 2, there were 42 motor vehicle collisions reported in the study area during the three-year period analyzed. Collisions occurred most frequently at the intersections of Corporate Drive at International Drive and Gosling Road at US Route 4 Northbound ramps. Both intersections experienced 11 collisions, accounting for about half of the reported total. The intersection of Pease Boulevard at US Route 4 Southbound ramps experienced the third highest number of collisions with 7, or about 17% of the reported total. The New Hampshire Avenue at International Drive intersection experienced 6 collisions, equating to approximately 14% of the total. The intersection of Route 33 (Greenland Road) at Grafton Road experienced 5 collisions, or 12% of the reported total. Finally, the intersections of Pease Boulevard at International Drive and Corporate Drive at Grafton Road each experienced one collision. The remaining study intersections did not have any reported collisions based on data provided by the City of Portsmouth.

TABLE 2

Study Area Collision History Summary

	2019	2020	2021	Total	Percent
Corporate Drive at International Drive	7	2	2	11	26.2%
Gosling Road at US Route 4 NB Ramps	0	3	8	11	26.2%
Pease Boulevard at US Route 4 SB Ramps	3	3	1	7	16.7%
New Hampshire Avenue at International Drive	3	1	2	6	14.3%
Route 33 (Greenland Road) at Grafton Road	1	2	2	5	11.9%
Pease Boulevard at International Drive	0	0	1	1	2.4%
Corporate Drive at Grafton Road	1	0	0	1	2.4%
TOTAL	15	11	16	42	100%

More detailed collision history summary data is provided in Appendix F. The most frequent types of collision were angle and rear-end, accounting for about 45% and 31% of the total collisions within the study area, respectively. The next most frequent collision type was sideswipe – same direction, which made up about 14% of the total collisions. The remaining collisions were fixed object, overturn/ rollover, or unknown, each of which accounting for less than 3% of the total collisions.

About 76% of collisions occurred on weekdays, spread throughout the day, with the remaining 24% occurring on weekends. Eight out of the 42 reported collisions in the study area occurred when the weather was clear, one occurred in snowy conditions, and the weather was unknown for the remaining 33 collisions. Similarly, eight of the 42 reported collisions occurred when the road surface was dry, one with snow on the roadway, and an unknown road surface condition for the remaining 33 collisions.

The collision data indicates no reported fatalities. One reported serious injury was reported for an angle collision at the intersection of New Hampshire Avenue at International Drive. The remaining 41 collisions resulted in minor injuries or property damage only. There were no pedestrian or cyclist collisions reported in the three-year period.

2.6 Public Transportation

The Cooperative Alliance for Seacoast Transportation (COAST) provides transit service within the study area. Bus Route 42 is the primary bus route in the study area with stops along Corporate Drive, including at the intersection of Corporate Drive at Redhook Way which is the closest existing stop to the site. Bus Route 42 also has stops along Grafton Road to the Portsmouth Transportation Center/Park & Ride and provides service to downtown Portsmouth. The route operates from 6:43AM to 6:34PM Monday through Friday. Bus Route 40 also operates in the study area with a bus stop at the Portsmouth Transportation Center and provides access to downtown Portsmouth. The route operates from 7:24 AM to 7:46 PM Monday through Friday. Bus Route 42 and 40 map and schedule are included in Appendix K.

Section 3

No Build Conditions

The No-Build Condition represents the projection of traffic volumes and operating conditions without the anticipated additional site generated traffic. Consistent with NHDOT guidelines, the study area is analyzed for an Opening Year (2025) and Design Year (2035). This section describes the growth and development considerations included in the 2025 and 2035 No-Build traffic volumes.

3.1 Traffic Growth

To develop the traffic volumes for the 2025 and 2035 No-Build Conditions, the 2023 Existing traffic volumes were grown by one percent per year to represent the general growth of traffic on the study area roadways. This growth rate is consistent with the average growth rate in NHDOT Region E - Southeast, the region in which Portsmouth is located. Background NHDOT growth data is included in Appendix B.

NHDOT and the Pease Development Authority (PDA) were contacted about other planned/approved developments in the area that may add new traffic to the study area prior to 2025. The following developments were identified:

- Pease Surface Transportation Master Plan: Traffic volumes for the full occupancy of existing buildings and projects that are planned or under construction are included in the 2025 and 2035 No-Build Condition.
- 100 New Hampshire Avenue: Traffic volumes for the approximately 209,750 square foot advanced manufacturing facility in the Pease Tradeport area are included in the 2025 and 2035 No-Build Conditions.

Traffic volumes for these projects were obtained from record studies and assigned to the study area intersections in the No-Build Conditions. Data for background development projects are included in Appendix D. It is assumed that other smaller developments or small vacancies in existing developments are captured by the background traffic growth rate.

The 2025 and 2035 No-Build traffic volumes for the weekday morning and weekday evening peak hours are shown in Figures 3 and 4, respectively.

3.2 Planned Roadway Improvements

Information obtained by NHDOT was used to identify roadway improvement projects in the area that may affect future traffic operations. A traffic signal project is proposed at the intersection of International Drive at Corporate Drive/ Manchester Square as identified in the NHDOT Ten-Year Plan (NHDOT Project No. 42612) and was considered when developing the 2035 No-Build Conditions analysis. The project is partially funded with preliminary design scheduled for 2027 and construction currently scheduled for 2030. The improvement was included in the 2035 No-Build and 2035 Build Conditions analyses.

3.3 Capacity and Queue Analyses - No-Build Conditions

Capacity and queue analyses were conducted for the 2025 and 2035 No-Build Conditions traffic volumes for both peak periods using the methodology described in Section 2.4. Tables 4 and 5 in Section 7 summarize the capacity and queue results, respectively. Capacity analysis worksheets with full inputs, settings, and results are provided in Appendix H.

The increase in expected future traffic based on the one percent per year compounded growth rate and the site-specific development added to the future No-Build Conditions result in some degradation of operations when compared to existing conditions. As described in Section 3.2, the proposed traffic signal at the intersection of International Drive at Corporate Drive/ Manchester Square is included in the 2035 No-Build Condition. In the 2025 No-Build Condition, most overall intersections and individual intersection approaches operate a similar LOS to the Existing Condition, which includes adjustment to an assumed pre-pandemic traffic level. The 2035 No-Build Condition includes some additional degradation of LOS based on the addition of ten years of compounded annual growth. The following identifies intersections and approaches which predict a degradation of LOS or increased delay exceeding available storage between the 2022 Existing and 2025 No-Build Condition, and/or between the 2025 and 2035 No-Build Condition:

- **Pease Boulevard at US Route 4 Southbound Ramps:**
 - The intersection continues to operate at overall LOS F during the weekday morning peak hour with failing operations on the southbound right movement. Both 50th and 95th percentile queues also exceed available storage in the 2035 weekday morning peak hour.
 - The westbound left movement degrades to LOS F in the 2035 weekday afternoon peak hour. The southbound left movement degrades to LOS E in the 2035 weekday morning peak hour.
- **Pease Boulevard at US Route 4 Northbound Ramps:**
 - The intersection continues to operate at overall LOS E in the 2025 No-Build Condition but degrades to LOS F in the 2035 No-Build Condition during the weekday morning peak hour.
 - In the 2035 No-build Condition, the eastbound left turn movement degrades to LOS E during the weekday afternoon peak hour.
 - The northbound left movement experiences design queues that exceed available storage in both No-Build years during the weekday morning peak hour.
- **Route 33 (Greenland Road) at Grafton Road:**
 - The intersection continues to operate at LOS F during the weekday morning and weekday afternoon peak hours.
 - The eastbound through movement degrades to LOS E in the 2025 No-Build Condition and to LOS F in the 2035 No-Build Condition during the weekday afternoon peak hour.
 - The southbound left turn movement design queues exceed available storage in 2035 during the weekday afternoon peak hour.

- **Corporate Drive at International Drive:**
 - The intersection continues to operate at overall LOS F in the 2025 No-Build Condition during the weekday morning peak and afternoon peak hours.
 - Overall intersection operations improve to LOS B and LOS C during the weekday morning and weekday afternoon peak hours, respectively, in the 2035 No-Build Condition following the proposed signalization of the intersection.
- **Corporate Drive at Lonza North Driveway:**
 - The Lonza North driveway approach degrades to LOS F in the 2035 No-Build Condition during the weekday afternoon peak hour.
- **New Hampshire Avenue/Corporate Drive at International Drive/Durham Street:**
 - The stop-controlled Durham Street approach degrades to LOS E during the weekday morning peak hour and to LOS F during the weekday afternoon peak hour in the 2035 No-Build Condition.
- **Corporate Drive at Grafton Road:**
 - The eastbound left movement continues to operate at LOS F in the 2025 and 2035 No-Build Condition during both peak periods. 95th percentile queues are estimated to continue to exceed available storage as well in 2025 and 2035.
- **Grafton Road at I-95 Southbound Off-Ramp:**
 - The westbound right turn movement continues to operate at LOS F in both No-Build years during the weekday morning peak hour.

Section 4

Proposed Conditions

The proposed 800,000+/- SF industrial facility will include approximately 700 parking spaces located in one proposed garage. The proposed development is expected to be complete and occupied in 2025. The Site Layout Plan is presented in Appendix I.

4.1 Site Access

Access to the Site will be provided via one full access, unsignalized driveway on Goose Bay Drive. The proposed driveway is located directly opposite the one-way existing Lonza garage entrance. All employees will utilize this driveway on Goose Bay Drive to access the site. A gated driveway is proposed on Corporate Drive, east of Redhook Way. This driveway will only be utilized for occasional deliveries to Building 3 following completion of the full build-out.

Based on the reconfiguration of Goose Bay Drive as shown in the proposed Site Layout Plan, intersection sight distance was not reviewed. There will be no conflicting through traffic with vehicles exiting the proposed driveway due to the roadway reconfiguration.

4.2 Multi-Modal Accommodations

Multi-modal access is provided in the general vicinity of the proposed development. Site improvements include a sidewalk along the eastern side of the Goose Bay Drive and a sidewalk along the southern side of Corporate Drive between the two Goose Bay Drive intersections. Improvements also include a crosswalk across Corporate Drive at the Wentworth Douglass driveway and on Goose Bay Drive at Corporate Drive to provide a continuous sidewalk network on the southern side of Corporate Drive. Additionally, internal sidewalks and crosswalks are proposed on site to accommodate pedestrians. Existing sidewalks adjacent to the site connect to a multi-use path along Grafton Road and Route 33 (Greenland Road). These facilities may encourage cycling and walking to the development.

In addition, the previously mentioned COAST bus stop is located at the intersection of Corporate Drive at Redhook Way with bus connection at the Portsmouth Transportation Center to downtown Portsmouth. The proposed sidewalk infrastructure coupled with the existing infrastructure in place create a robust pedestrian network in the Tradeport Area.

4.3 Trip Generation

Site generated traffic volumes were estimated using site-specific data based on existing facility operating characteristics and the proposed development program. Because the existing facility is currently operating on a hybrid schedule, turning movement counts collected in 2018 were used as a basis for the existing trip generation estimate.

The proposed site generated traffic volumes were calculated based on both the number of proposed full-time employees and the proposed building size. The 2018 turning movement counts serve as the basis for each estimate. The existing 1,139 full-time employees and the proposed 1,020 employees serve as a basis for the estimate based on the number of

employees. The existing building size of 898,000 square feet, and the proposed building size of 800,000 square feet serve as the basis for the estimate based on building size. Trip generation is based on the peak hour of the generator (site). Table 3 summarizes the trip generation estimates.

TABLE 3

Site-Generated Traffic Summary

Existing - 1,139 Employees (Site Peak Hour)			
Peak Hour Period	Enter	Exit	Total
Weekday Morning	154	76	230
Weekday Afternoon	15	160	175
Proposed - Based on Proposed 1,020 FTE Employees			
Peak Hour Period	Enter	Exit	Total
Weekday Morning	138	68	206
Weekday Afternoon	13	144	157
Proposed - Based on Proposed 800,000 SF Building			
Peak Hour Period	Enter	Exit	Total
Weekday Morning	137	68	205
Weekday Afternoon	13	144	157

Based on employees, the project is projected to generate 206 trips during the weekday morning peak hour (138 entering, 68 exiting) and 157 trips during the weekday afternoon peak hour (13 entering, 144 exiting). Based on building size, the project is expected to generate 205 trips during the weekday morning peak hour (137 entering, 68 exiting) and 157 vehicles (13 entering, 144 exiting) during the weekday afternoon peak hour. It was determined to use the higher number of trips based on proposed employees in order to present a conservative estimate of predicted trips.

As noted previously, Lonza is currently working under a hybrid work policy, currently averaging approximately 50% of employees working in the office on a typical day. However, for the purposes of this TIA, no trip reduction credit was taken for future employees working from home. Therefore, the trip generation estimate including all full-time employees is considered conservative and assumes a return to in-person work for all employees. As noted above, trip generation is based on the peak hour of the generator and applied to the peak hour of the study area network, which also results in a conservative approach.

While the nearby COAST bus stop and sidewalk facilities in the area may provide additional options for employees to travel to the proposed development, no credit was taken for mode share trips.

4.4 Arrival and Departure Distribution

The distribution of the proposed site generated traffic entering and exiting the Site was applied to the roadway network based on zip code data for current Lonza employees' place of residence.

Arrival and departure distribution patterns are shown in Figure 5, and are as follows:

- 40% Northwest to/from US Route 4
- 25% South to/from I-95
 - 15% via Route 33
 - 10% via US Route 4
- 10% Northeast to/from I-95 (via Route 33)
- 10% West (Local) to/from Route 33
- 5% East to/from Pease Boulevard/Gosling Road
- 5% East (Local) to/from Route 33
- 5% (Local)to/ from US Route 1 / US Route 1 Bypass (via US Route 4)

Figure 6 shows the proposed site generated traffic distributed to the study area roadways for the weekday morning and afternoon peak hours. Trip distribution based on employee zip code is included in Appendix L.

4.5 Goose Bay Drive Realignment

A portion of Goose Bay Drive is proposed to be reconfigured as part of the project. Approximately 1,700 feet of the roadway beginning at the west end of Goose Bay Drive at the intersection with Corporate Drive will be converted to a private driveway for the Lonza site. Employee-only access gates will be installed along the private roadway. The portion of Goose Bay Drive running north to south to the east of the Lonza development will remain a public road, maintaining access to Corporate Center at Pease. A gate is proposed at the southern extent of Goose Bay Drive, approximately 150 feet south of the Corporate Center driveway to restrict through traffic. A cul-de-sac is proposed at the southern extent of Goose Bay Drive to provide vehicles with a means to turn around if necessary. Existing traffic volumes on Goose Bay Drive were reassigned and incorporated into the 2025 and 2035 Build Conditions traffic volumes and analyses. The reassigned Goose Bay Drive traffic volumes are shown in Appendix E.

Section 5

Build Conditions

The anticipated site generated traffic volumes associated with the proposed development were added to the 2025 and 2035 No-Build Conditions traffic volumes to develop the 2025 and 2035 Build Conditions traffic volumes, which are presented in Figure 7 and 8, respectively, for the weekday morning and afternoon peaks.

5.1 Capacity and Queue Analyses – Build Conditions

Capacity and queue analyses were conducted for the 2025 and 2035 Build Conditions for the peak hours using the methodology described in Section 2.4. Tables 4 and 5 in Section 7 summarize the capacity and queue results, respectively. Capacity analysis worksheets with full inputs, settings, and results are provided in Appendix H.

Many of the study area intersections and individual intersection approaches continue to operate at acceptable LOS D or better during the peak hours in the 2025 and 2035 Build Conditions. Study area intersections that were identified in Section 2.4 and 3.3 to operate at LOS E or LOS F in the No-Build Conditions continue to operate at the same LOS under Build Conditions, except for the following:

- **Pease Boulevard at International Drive:**
 - The intersection continues to operate at overall LOS F with failing operations on the northbound right turn movement during the weekday afternoon peak hour.
 - The westbound left movement degrades to LOS E in the 2035 Build Condition during the weekday morning peak hour.
- **Pease Boulevard at US Route 4 Northbound Ramps:**
 - The eastbound left movement degrades to LOS E in the 2025 Build Condition and to LOS F in the 2035 Build Condition during the weekday afternoon peak hour.
 - 95th percentile queues exceed available storage on the eastbound left and through movements in the 2035 Build Condition during the weekday afternoon peak hour.
- **Corporate Drive at Goose Bay Drive (West):**
 - The Goose Bay Drive northbound approach degrades to LOS F in the 2025 and 2035 Build Condition during the weekday morning peak hour. The northbound approach continues to operate at LOS F in the 2025 and 2035 Build Conditions.
 - 95th percentile queues exceed available storage on the northbound approach in the 2025 and 2035 Build Condition during the weekday afternoon peak hour.

A review of calculated queue lengths in Table 5 reveals that the majority of queues are unchanged between the No-Build and Build Conditions for both 2025 and 2035 or increase by approximately 1-2 car lengths or fewer. However, the following increases in queues were noted:

- The westbound left movement at the intersection of Pease Boulevard at International Drive experiences an increase in predicted 95th percentile queues of two and five car lengths in 2025 and 2035, respectively, during the weekday morning peak hour.
- The northbound right movement at the intersection of Pease Boulevard at International Drive sees an increase in predicted 95th percentile queues of approximately three car lengths in the 2025 and 2035 Build Condition during the afternoon peak hour. This movement does experience failing operations.
- Large increases in queues in 2025 and 2035 are projected on the Goose Bay Drive (West) northbound approach at the intersection with Corporate Drive due to the increase in site traffic exiting the site during the weekday afternoon peak hour.
- Large increases in design queues are estimated on the southbound left movement from International Drive to Corporate Drive during the weekday morning peak period and westbound right movement from Corporate Drive to International Drive in the 2025 Build Condition, however the queueing deficiency is mitigated with the proposed traffic signal in 2035.

Section 6

Conclusions & Recommendations

1. Lonza Biologics proposes to construct a 800,000+/- square foot industrial development within three buildings on portions of the vacant lot between Goose Bay Drive and Corporate Drive in the Pease Tradeport area in Portsmouth, NH. The development will provide approximately 700 parking spaces in one proposed parking garage to accommodate employee parking. The first phase of the proposed development is expected to be complete and occupied by 2025.
2. Employee access to the Site will be provided via one full access, unsignalized driveway opposite the existing Lonza parking garage entrance. Access will be controlled with proposed gates on the existing Goose Bay Drive in advance of the proposed site driveway. A proposed driveway on Corporate Drive will be restricted with a gate and be accessed for infrequent deliveries to Building 3 following completion of later project phases.
3. The proposed land use for the project site is industrial, which will support current biotech and pharmaceutical uses for Lonza. Site-specific data including traffic counts, existing and proposed number of employees, and existing and proposed building area were used as a basis for the estimate. The estimate assumed all employees are working on site. This likely represents a conservative estimate as Lonza is currently operating under a hybrid policy, averaging approximately 50% of employees in the facility each day.
4. Based on the trip generation estimate, the project is expected to generate 206 trips during the weekday morning peak hour (138 entering, 68 exiting) and 157 trips during the weekday afternoon peak hour (13 entering, 144 exiting). Trip generation is estimated based on the peak hour of the generator (site) and applied to the peak hour of the study area network, also representing a conservative approach.
5. The project proposes internal and adjacent roadway sidewalk connections, creating and promoting connections to a robust existing sidewalk network along study area roadways.
6. Vehicle collision history, compiled from local police and historic reports, do not indicate a significant or notable pattern of collisions in the study area.
7. Consistent with NHDOT guidelines, existing traffic volumes have been adjusted based on a comparison between 2022, 2023 and 2019 data to represent a pre-pandemic condition. Application of adjustment factors based on ATR data from Pease Boulevard across all turning movements within the study area may artificially inflate turning movements and overstate calculated operational delay and resultant capacity analysis results. Existing traffic volumes adjusted to an assumed pre-pandemic condition predict notable operational delay throughout the study area.
8. The capacity analyses show that the study area intersections will continue to operate at the same LOS under Build Conditions as in No-Build Conditions for both the 2025 opening year and 2035 design year, with the following exceptions:

- a. The westbound left and northbound right movements at the intersection of Pease Boulevard at International Drive degrade from LOS D to LOS E in the weekday morning peak hour between the 2035 No-Build and Build Condition.
 - b. The eastbound left movement at the intersection of Pease Boulevard at US Route 4 Northbound Ramps degrades from LOS D to LOS E in the 2025 Build Condition and from LOS E to LOS F in the 2035 Build Condition during the weekday afternoon peak hour.
 - c. The Goose Bay Drive northbound approach Corporate Drive at Goose Bay Drive (West) degrades to LOS F in the 2025 and 2035 Build Condition during the weekday morning peak hour.
9. Based on the results of the foregoing analysis, it is the professional opinion of Tighe & Bond that while the adjustment of collected volumes to an assumed pre-pandemic condition and the addition of background growth on a 12-year horizon to the 2035 design year results in undesirable LOS at some area intersections, the addition of site-generated traffic is expected to have a negligible effect on traffic operations within the study area.

Section 7 Additional Tables

TABLE 4 (CONTINUED)

Intersection Operation Summary - Capacity

Lane Use	Weekday Morning Peak Hour										Weekday Afternoon Peak Hour																				
	2023 Existing		2025 No Build		2025 Build		2025 No Build		2025 Build		2023 Existing		2025 No Build		2025 Build		2025 No Build		2025 Build												
	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C	LOS	V/C											
Unsignalized TWSC - Corporate Drive at Goose Bay Drive (East)																															
Corporate Drive	WB	A	7.7	0.01	A	7.7	0.01	A	7.8	0.00	A	8.0	0.01	A	8.1	0.00	A	7.4	0.00	A	7.4	0.01	A	0.0	0.00	A	7.6	0.01	A	0.0	0.00
Goose Bay Drive (East)	NB	B	11.2	0.08	B	11.3	0.09	A	0.0	0.00	B	12.5	0.10	A	0.0	0.00	A	9.9	0.04	B	10.0	0.05	B	11.4	0.03	B	11.2	0.06	B	12.9	0.04
Unsignalized TWSC - Goose Bay Drive at Corporate Center Driveway																															
Corporate Center Driveway	WB	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	8.5	0.02	A	8.5	0.02	A	0.0	0.00	A	8.5	0.02	A	0.0	0.00
Goose Bay Drive (East)	SB	A	7.3	0.01	A	7.3	0.01	A	0.0	0.00	A	7.3	0.01	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00
Unsignalized TWSC - Goose Bay Drive at Lonza South Driveway																															
Lonza South Driveway	EB	A	9.6	0.02	A	9.7	0.02	A	9.3	0.01	A	9.7	0.02	A	9.3	0.02	A	8.7	0.01	A	8.7	0.01	A	8.6	0.01	A	8.7	0.01	A	8.6	0.01
Goose Bay Drive (West)	NB	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00
Unsignalized TWSC - Goose Bay Drive at Lonza Parking Garage Driveway / Proposed Site Driveway																															
Proposed Site Driveway	WB	--	--	--	--	--	--	A	8.8	0.07	--	--	--	A	8.8	0.07	--	--	--	--	--	--	B	13.7	0.27	--	--	--	B	14.6	0.29
Goose Bay Drive	NB	A	8.1	0.01	A	8.1	0.01	A	8.1	0.01	A	8.2	0.01	A	8.2	0.01	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00
	SB	--	--	--	--	--	--	A	7.5	0.10	--	--	--	A	7.5	0.10	--	--	--	--	--	--	A	8.4	0.01	--	--	--	A	8.6	0.01
Unsignalized TWSC - Corporate Drive at Granite State Driveway																															
Granite State Driveway	WB	B	13.4	0.03	B	13.6	0.03	B	13.6	0.03	C	16.0	0.04	C	16.0	0.04	C	15.9	0.03	C	16.1	0.03	C	16.1	0.03	C	19.0	0.05	C	19.0	0.05
International Drive	SB	A	7.7	0.01	A	7.7	0.01	A	7.7	0.01	A	7.9	0.01	A	7.9	0.01	A	9.1	0.01	A	9.2	0.01	A	9.2	0.01	A	9.5	0.01	A	9.5	0.01
Unsignalized TWSC - Corporate Drive at Lonza North Driveway																															
Lonza North Driveway	WB	B	12.7	0.07	B	12.8	0.08	B	12.8	0.08	B	14.8	0.10	B	14.8	0.10	D	26.7	0.63	D	28.6	0.66	D	28.6	0.66	F	50.6	0.84	F	50.6	0.84
International Drive	SB	A	7.6	0.02	A	7.6	0.02	A	7.6	0.02	A	7.8	0.02	A	7.8	0.02	A	8.9	0.02	A	9.0	0.02	A	9.0	0.02	A	9.3	0.02	A	9.3	0.02
Unsignalized TWSC - Corporate Drive at Lonza South Driveway																															
Lonza South Driveway	WB	A	9.3	0.01	A	9.4	0.01	A	9.4	0.01	A	9.8	0.01	A	9.8	0.01	B	11.6	0.03	B	11.7	0.03	B	11.7	0.03	B	12.4	0.04	B	12.4	0.04
International Drive	SB	A	7.6	0.01	A	7.6	0.01	A	7.6	0.01	A	7.8	0.01	A	7.8	0.01	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00
Unsignalized TWSC - New Hampshire Avenue / Corporate Drive at International Drive / Durham Street																															
Durham Street	EB	D	27.1	0.14	D	32.5	0.16	D	32.5	0.16	E	41.2	0.22	E	41.2	0.22	D	28.2	0.38	E	37.3	0.47	E	37.3	0.47	F	54.1	0.61	F	54.1	0.61
International Drive	WB	F	62.5	0.74	F	105.3	0.92	F	105.3	0.92	F	223.7	1.25	F	223.7	1.25	F	323.0	1.59	F	506.9	2.00	F	506.9	2.00	F	820.1	2.68	F	820.1	2.68
Corporate Drive	NB	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	0.0	0.00	A	8.4	0.00	A	8.6	0.00	A	8.6	0.00	A	8.8	0.00	A	8.8	0.00
New Hampshire Avenue	SB	A	9.7	0.04	B	10.1	0.04	B	10.1	0.04	B	10.6	0.05	B	10.6	0.05	A	8.2	0.00	A	8.3	0.00	A	8.3	0.00	A	8.4	0.00	A	8.4	0.00
Unsignalized TWSC - Corporate Drive at Grafton Road																															
Grafton Road	EBL	F	107.9	1.16	F	158.2	1.29	F	216.0	1.42	F	236.0	1.47	F	304.4	1.62	F	150.6	1.19	F	242.2	1.42	F	461.3	1.90	F	473.3	1.94	F	815.9	2.68
	EBR	B	10.7	0.37	B	10.7	0.38	B	11.2	0.42	B	11.2	0.42	B	11.7	0.47	A	8.7	0.08	A	8.7	0.08	A	8.8	0.09	A	8.8	0.09	A	8.8	0.10
Corporate Drive	NBL	A	8.0	0.05	A	8.1	0.06	A	8.2	0.08	A	8.2	0.06	A	8.3	0.09	B	12.2	0.34	B	13.2	0.38	B	14.3	0.46	C	15.1	0.45	C	16.9	0.54
Unsignalized - Grafton Road at I-95 SB Off Ramp																															
I-95 SB Off-ramp	WB	F	592.5	2.13	F	859.4	2.72	F	974.6	2.96	F	1366.0	3.81	F	1552	4.10	B	13.1	0.15	B	13.7	0.18	B	13.8	0.18	B	14.8	0.21	B	14.9	0.21

TABLE 5
Intersection Operation Summary - Queues (In Feet)

		Weekday Morning Peak Hour										Weekday Afternoon Peak Hour										
Lane Use	Available Storage	2023 Existing		2025 No Build		2025 Build		2035 No Build		2035 Build		2023 Existing		2025 No Build		2025 Build		2035 No Build		2035 Build		
		50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	
Traffic Signal - Pease Boulevard at International Drive																						
Pease Boulevard	EBL	290	2	9	2	9	2	9	2	9	2	9	0	0	0	0	0	0	0	0	0	
	EBT	>1000	31	56	37	64	38	64	43	69	43	69	87	135	101	153	102	154	123	188	124	190
	WBL	690	304	391	320	409	397	464	488	549	576	672	53	93	56	98	58	101	96	155	98	158
	WBT	>1000	70	271	80	303	90	303	107	343	107	343	17	31	20	35	20	35	22	36	22	36
International Drive	NBT	840	7	25	7	25	7	25	9	27	9	27	4	18	4	19	4	18	5	22	5	22
	NBR	530	92	143	98	147	118	173	134	192	155	242	404	623	433	664	489	732	578	876	641	955
	SBR	>1000	6	16	6	17	7	17	7	18	7	18	24	46	26	49	26	49	33	62	33	62
Traffic Signal - Pease Boulevard at US Route 4 SB On/Off Ramps																						
Pease Boulevard	EBT	>1000	41	52	45	55	50	61	56	67	61	72	204	225	220	242	236	258	252	274	269	291
	EBR	530	0	29	0	29	0	30	0	31	0	32	63	173	74	190	113	243	154	308	203	420
	WBL	370	63	67	65	67	65	65	75	70	75	67	261	356	267	361	267	352	303	359	303	358
	WBT	370	332	307	341	310	357	314	391	324	407	328	51	94	57	95	58	95	77	94	78	95
US Route 4 SB On/ Off Ramps	SBL	520	242	248	248	253	248	253	282	284	282	284	124	172	126	175	126	175	142	194	142	194
	SBR	520	478	455	529	501	597	560	685	638	744	688	0	27	0	28	0	28	0	29	0	30
Traffic Signal - Pease Boulevard at US Route 4 NB On/Off Ramps																						
Pease Boulevard	EBL	375	28	32	29	34	36	42	33	40	39	47	243	293	258	314	282	351	290	365	326	414
	EBT	375	285	336	294	341	295	341	334	355	334	357	111	127	115	131	112	141	126	190	124	443
	WBT	460	70	106	77	116	79	117	93	135	95	138	294	355	308	371	308	371	358	464	359	464
US Route 4 NB On/ Off Ramps	NBL	360	387	404	401	416	432	444	499	505	530	532	65	99	66	101	67	102	74	111	75	111
	NBR	360	0	18	0	17	5	23	18	36	23	42	0	47	0	47	0	47	0	49	0	49
Traffic Signal - Greenland Road (Route 33) at Grafton Road																						
Greenland Road (State Route 33)	EBL	400	422	632	440	643	454	656	516	705	529	717	205	334	211	341	211	341	239	373	240	374
	EBT	>1000	526	671	552	689	553	689	668	785	670	785	391	497	405	512	405	512	484	591	484	591
	WBT	>1000	123	179	126	183	126	183	144	235	144	235	327	443	337	455	337	455	396	516	396	516
	WBR	275	0	62	0	64	0	65	0	67	0	69	0	40	0	42	0	42	0	44	0	44
Grafton Road	SBL	300	61	83	67	90	68	92	72	99	73	100	138	256	159	296	163	303	180	336	184	342
	SBR	1000	0	24	0	25	1	26	4	29	10	36	397	572	438	614	470	648	517	696	549	730
Traffic Signal - Corporate Drive at International Drive																						
Corporate Drive	EBL	300	--	--	--	--	--	47	97	60	97	--	--	--	--	--	--	59	94	59	94	
	EBTR	>1000	--	--	--	--	--	36	82	47	82	--	--	--	--	--	--	2	13	2	13	
	WBL	175	--	--	--	--	--	9	30	12	30	--	--	--	--	--	--	4	11	4	11	
	WBT	525	--	--	--	--	--	8	28	11	28	--	--	--	--	--	--	10	22	10	22	
	WBR	675	--	--	--	--	--	0	32	0	36	--	--	--	--	--	--	211	251	308	349	
	NBL	175	--	--	--	--	--	5	22	6	22	--	--	--	--	--	--	7	26	8	26	
International Drive	NBTR	>1000	--	--	--	--	--	54	106	70	106	--	--	--	--	--	--	171	275	204	275	
	SBL	850	--	--	--	--	--	265	363	434	538	--	--	--	--	--	--	47	110	64	132	
	SBT	850	--	--	--	--	--	128	186	134	186	--	--	--	--	--	--	49	107	61	107	
	SBR	250	--	--	--	--	--	0	9	0	9	--	--	--	--	--	--	0	31	0	31	
Unsignalized AWSC - Corporate Drive at International Drive																						
Corporate Drive	EBL	300	--	23	--	23	--	--	--	--	--	--	55	--	57	--	57	--	--	--	--	
	EBR	>1000	--	20	--	23	--	23	--	--	--	--	5	--	5	--	5	--	--	--	--	
	WBL	175	--	3	--	3	--	3	--	--	--	--	3	--	3	--	3	--	--	--	--	
	WBT	525	--	3	--	3	--	3	--	--	--	--	5	--	5	--	5	--	--	--	--	
	WBR	675	--	20	--	20	--	40	--	--	--	--	735	--	785	--	1165	--	--	--	--	
	NBL	175	--	3	--	3	--	3	--	--	--	--	3	--	3	--	3	--	--	--	--	
International Drive	NBT	>1000	--	18	--	18	--	18	--	--	--	--	270	--	285	--	280	--	--	--	--	
	NBTR	175	--	25	--	25	--	28	--	--	--	--	65	--	68	--	70	--	--	--	--	
	SBL	850	--	928	--	982	--	1443	--	--	--	--	15	--	15	--	20	--	--	--	--	
	SBT	850	--	400	--	433	--	497	--	--	--	--	23	--	25	--	25	--	--	--	--	
	SBR	250	--	30	--	30	--	33	--	--	--	--	20	--	23	--	20	--	--	--	--	

TABLE 5 (CONTINUED)

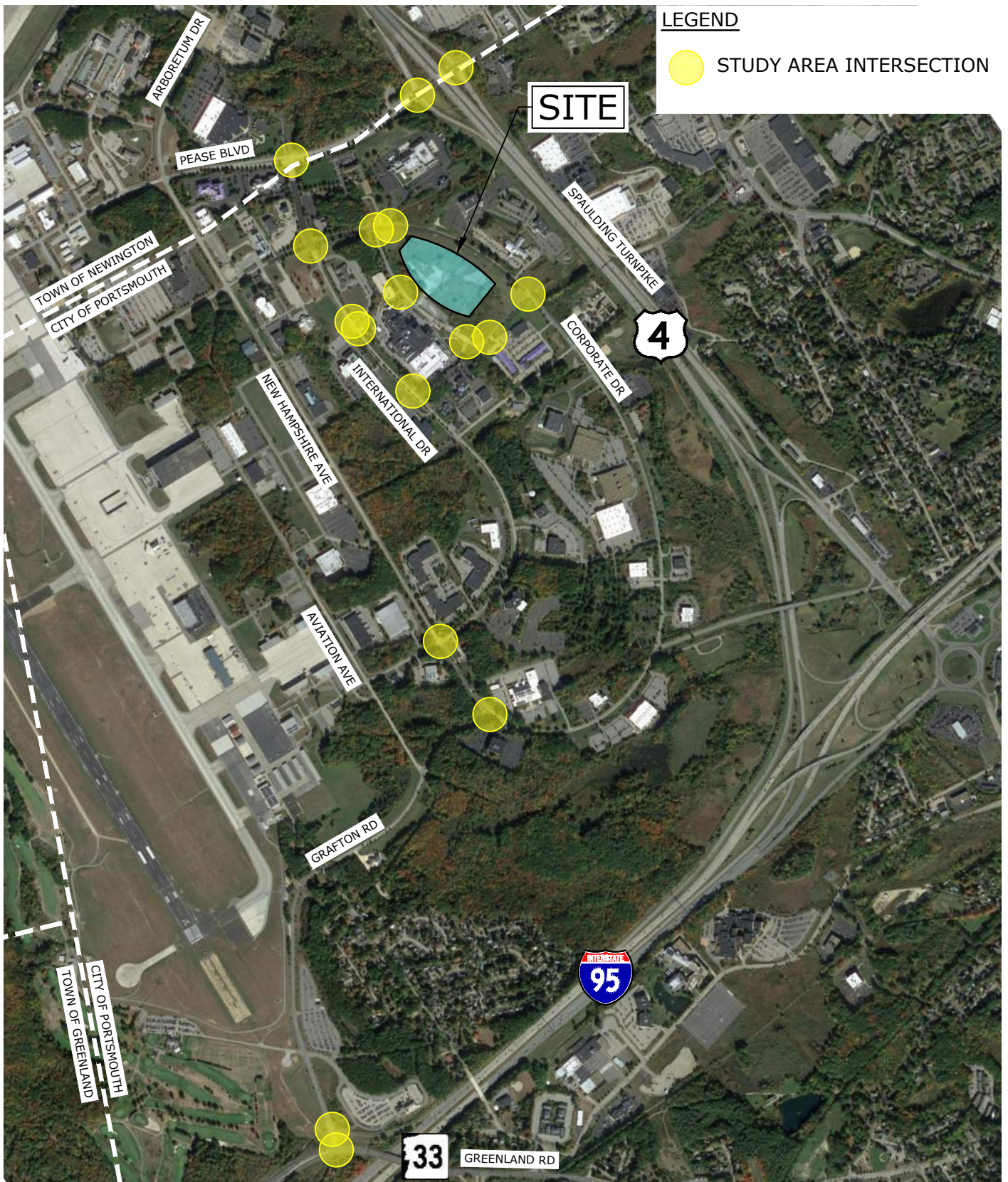
Intersection Operation Summary - Queues (In Feet)

Lane Use	Available Storage	Weekday Morning Peak Hour										Weekday Afternoon Peak Hour									
		2023 Existing		2025 No Build		2025 Build		2023 Existing		2025 No Build		2025 Build		2023 Existing		2025 No Build		2025 Build			
		50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th	50 th	95 th		
Unsignalized TWSC - Corporate Drive at Goose Bay Drive (West)																					
Corportate Drive	WB	120	--	3	--	3	--	13	--	5	--	15	--	0	--	0	--	0	--	0	
Goose Bay Drive (West)	NB	685	--	8	--	10	--	118	--	15	--	195	--	260	--	283	--	1258	--	598	
Unsignalized TWSC - Corporate Drive at Redhook Way																					
Corportate Drive	EB	120	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Redhook Way	SB	320	--	0	--	0	--	0	--	3	--	3	--	5	--	5	--	5	--	8	
Unsignalized TWSC - Corporate Drive at Goose Bay Drive (East)																					
Corportate Drive	WB	360	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Goose Bay Drive (East)	NB	580	--	5	--	8	--	0	--	8	--	0	--	3	--	3	--	3	--	5	
Unsignalized TWSC - Goose Bay Drive at Corporate Center Driveway																					
Corporate Center Driveway	WB	100	--	0	--	0	--	0	--	0	--	0	--	0	--	3	--	0	--	3	
Goose Bay Drive (East)	SB	580	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Unsignalized TWSC - Goose Bay Drive at Lonza South Driveway																					
Lonza South Driveway	EB	200	--	0	--	0	--	0	--	3	--	3	--	0	--	0	--	0	--	0	
Goose Bay Drive (West)	NB	250	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Unsignalized TWSC - Goose Bay Drive at Lonza Parking Garage Driveway/ Proposed Site Driveway																					
Proposed Site Driveway	WB	300	--	--	--	--	--	5	--	--	--	5	--	--	--	--	--	28	--	--	
Goose Bay Drive	NB	200	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
	SB	675	--	0	--	--	--	0	--	0	--	8	--	0	--	0	--	0	--	0	
Unsignalized TWSC - Corporate Drive at Granite State Driveway																					
Granite State Driveway	WB	340	--	3	--	3	--	3	--	3	--	3	--	3	--	3	--	3	--	3	
International Drive	SB	470	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Unsignalized TWSC - Corporate Drive at Lonza North Driveway																					
Lonza North Driveway	WB	200	--	5	--	5	--	5	--	8	--	8	--	105	--	115	--	115	--	193	
Corporate Drive	SB	85	--	3	--	3	--	3	--	3	--	3	--	3	--	3	--	3	--	3	
Unsignalized TWSC - Corporate Drive at Lonza South Driveway																					
Lonza South Driveway	WB	100	--	0	--	0	--	0	--	0	--	0	--	3	--	3	--	3	--	3	
International Drive	SB	400	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
Unsignalized TWSC - New Hampshire Avenue/ Corporate Drive at International Drive/ Durham Street																					
Durham Street	EB	860	--	13	--	15	--	15	--	20	--	20	--	43	--	55	--	55	--	83	
International Drive	WB	>1000	--	123	--	168	--	168	--	255	--	255	--	585	--	718	--	718	--	932	
Corporate Drive	NB	920	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	--	0	
New Hampshire Avenue	SB	>1000	--	3	--	3	--	3	--	3	--	3	--	0	--	0	--	0	--	0	
Unsignalized TWSC - Corporate Drive at Grafton Road																					
Grafton Road	EBL	220	--	668	--	898	--	1070	--	1223	--	1403	--	393	--	538	--	715	--	785	
	EBR	220	--	43	--	45	--	53	--	53	--	63	--	8	--	8	--	8	--	8	
Corporate Drive	NBL	>1000	--	5	--	5	--	8	--	5	--	8	--	38	--	45	--	60	--	60	
Unsignalized TWSC - Grafton Road at I-95 SB Off Ramp																					
I-95 SB Off Ramp	WB	>1000	--	545	--	685	--	710	--	838	--	853	--	13	--	18	--	18	--	20	

Section 8

Figures

May 19, 2023-9:48am Plotted By: MStoutz
Tighe & Bond, Inc. J:\L\0700 Lonza Biologics Expansion was 1576F\026_Project\Albacore\Drawings\AutoCAD\Figures\L0700-026 Site Location Map.dwg



LONZA BIOLOGICS INDUSTRIAL DEVELOPMENT
PORTSMOUTH, NH

SITE LOCATION MAP

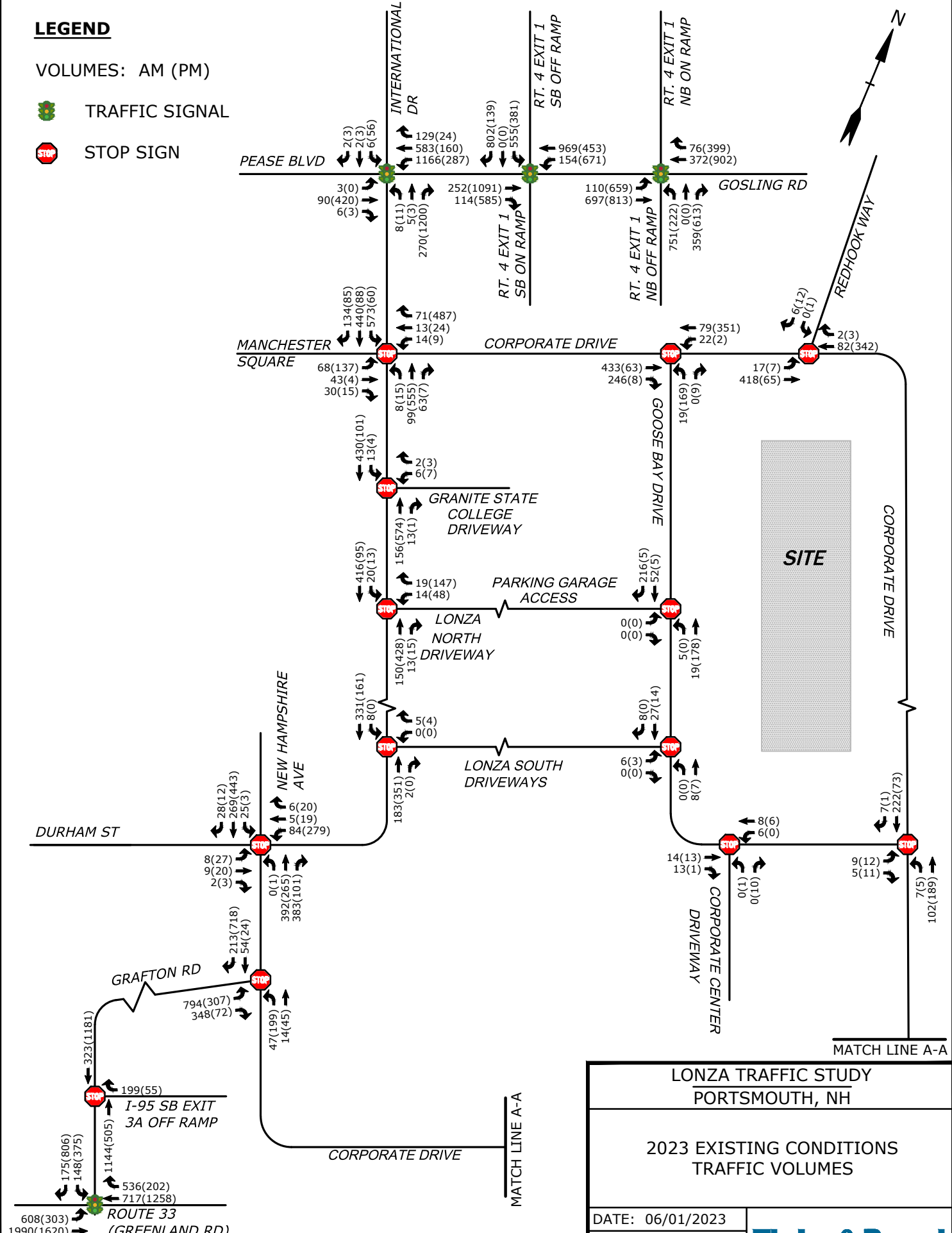
NORTH 
NO SCALE
FIGURE 1

LEGEND

VOLUMES: AM (PM)

TRAFFIC SIGNAL

STOP SIGN



LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
2023 EXISTING CONDITIONS	
TRAFFIC VOLUMES	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 2	

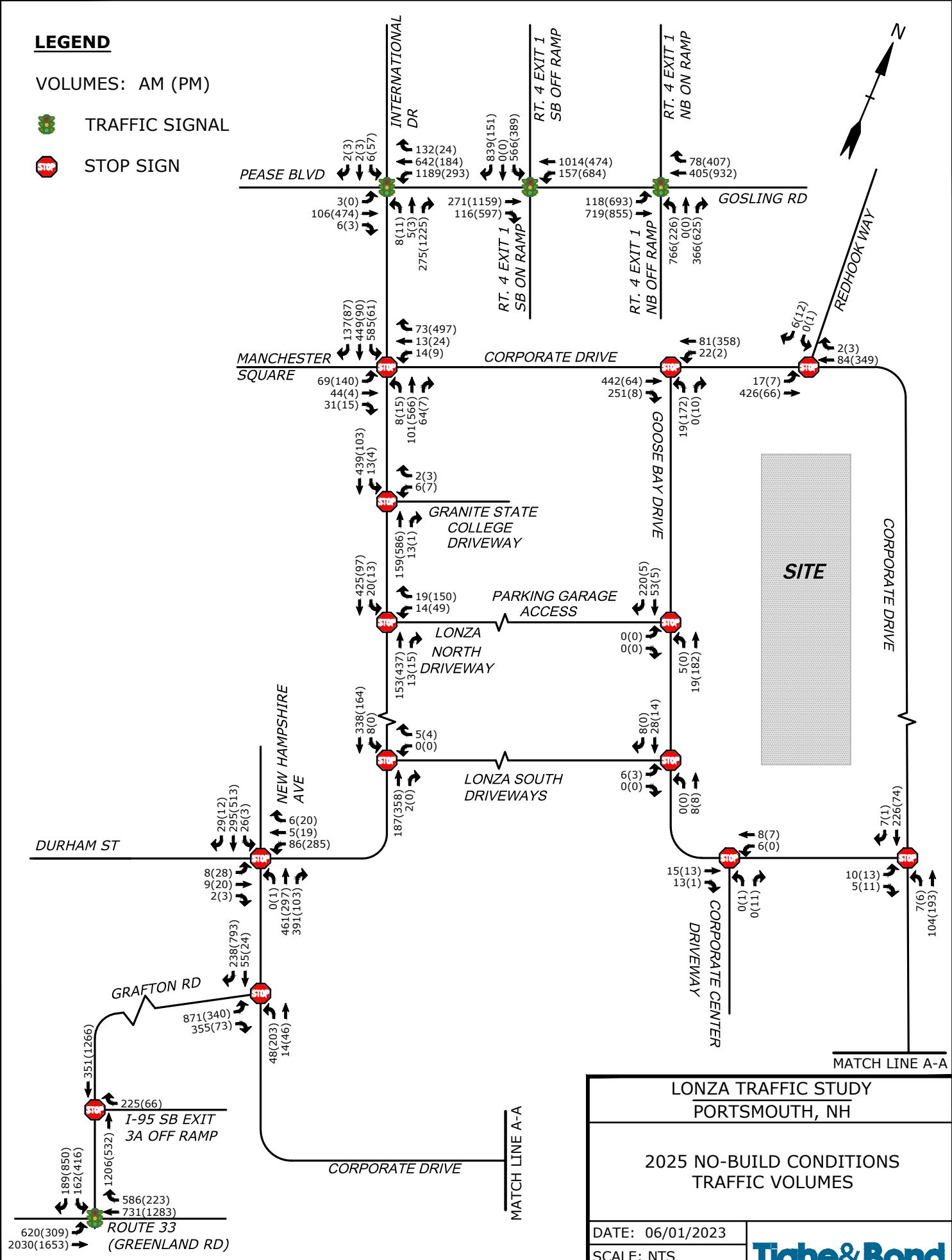
Jun 01, 2023-10:33am Plotted By: RCase Tighe & Bond, Inc. J:\L07000 Lonza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg


LEGEND

VOLUMES: AM (PM)

 TRAFFIC SIGNAL

 STOP SIGN



LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
2025 NO-BUILD CONDITIONS	
TRAFFIC VOLUMES	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 3	

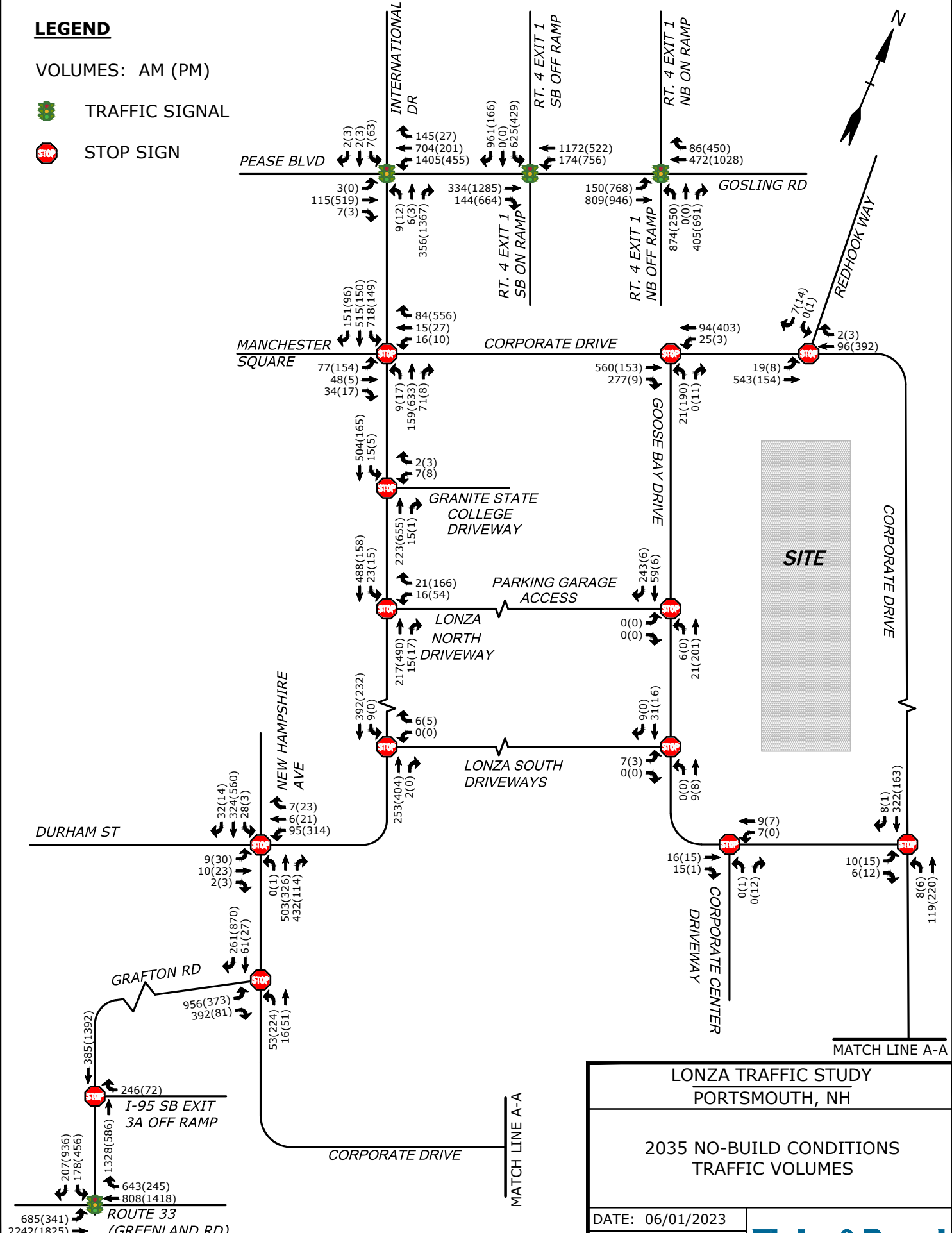
Jun 01, 2023-10:34am Plotted By: RCase Tighe & Bond, Inc. J:\L07000 Lanza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg


LEGEND

VOLUMES: AM (PM)

 TRAFFIC SIGNAL

 STOP SIGN




LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
2035 NO-BUILD CONDITIONS	
TRAFFIC VOLUMES	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 4	

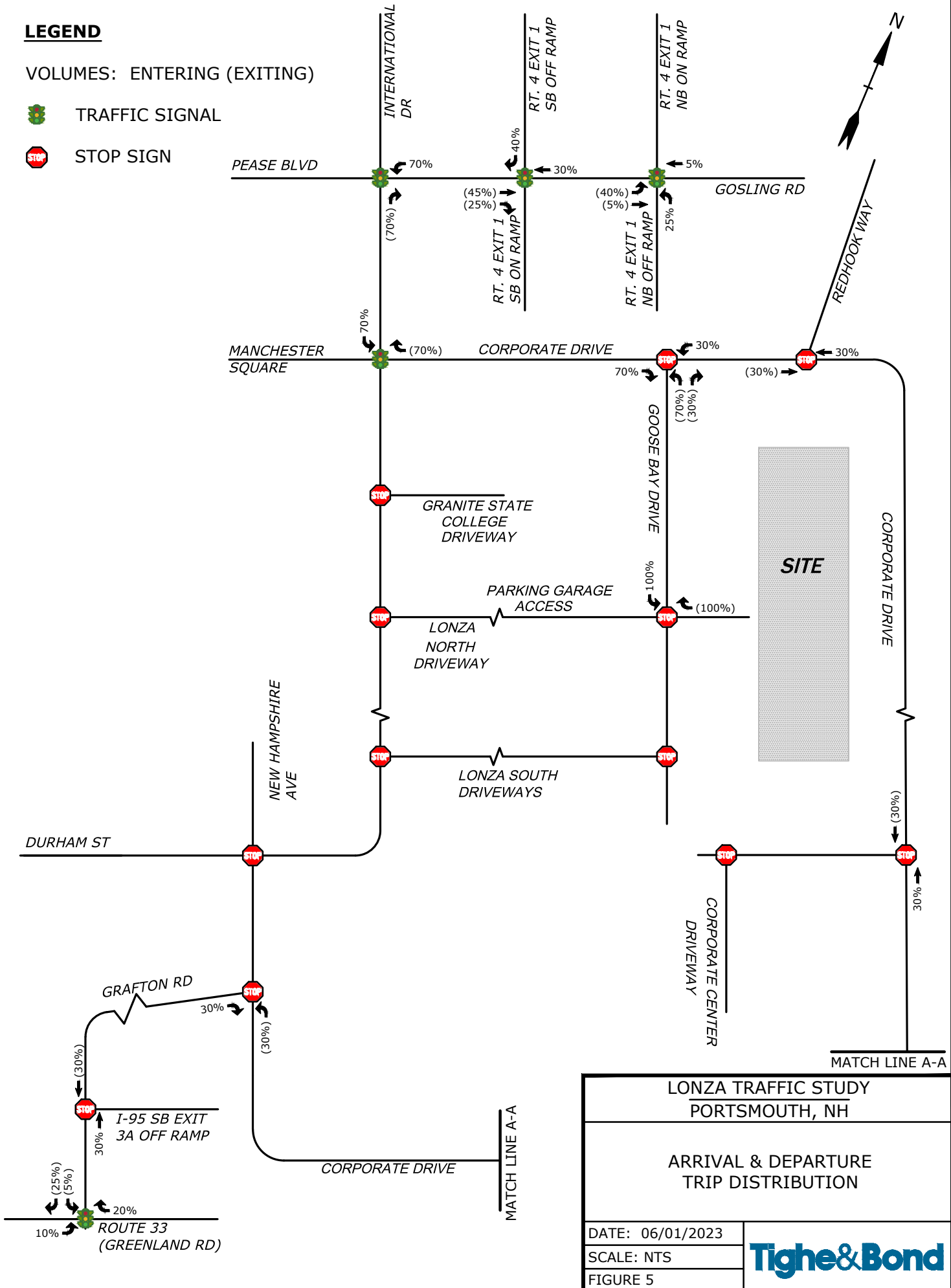
Jun 01, 2023-10:34am Plotted By: RCase Tighe & Bond, Inc. J:\L0700 Lonza Biologics Expansion was 1576F\026_Project Albarcor\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg


LEGEND

VOLUMES: ENTERING (EXITING)

 TRAFFIC SIGNAL

 STOP SIGN




LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
ARRIVAL & DEPARTURE TRIP DISTRIBUTION	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 5	

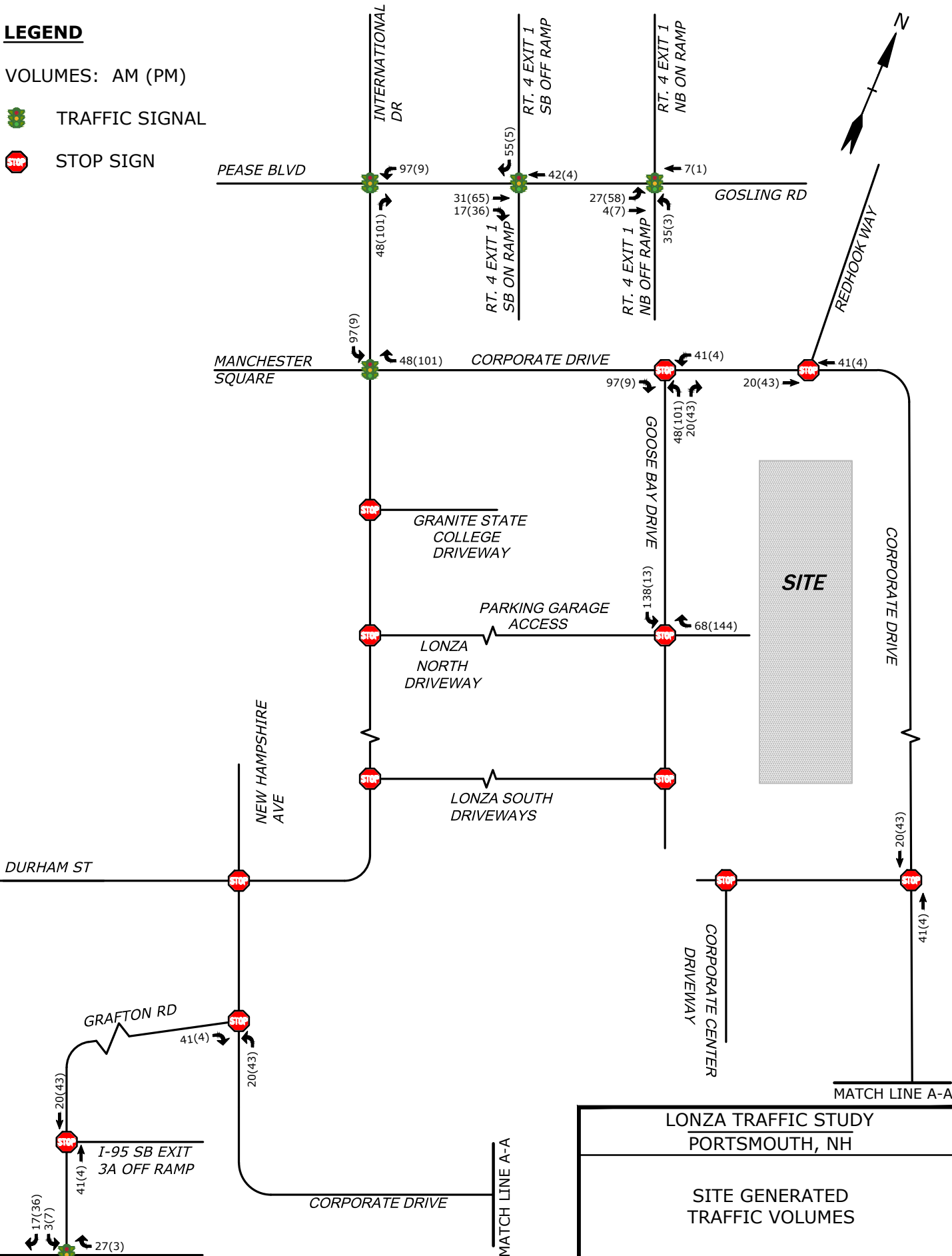
Jun 01, 2023-10:34am Plotted By: RCase Tighe & Bond, Inc.: \\L07000 Lonza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg


LEGEND

VOLUMES: AM (PM)

 TRAFFIC SIGNAL

 STOP SIGN



LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
SITE GENERATED TRAFFIC VOLUMES	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 6	

LEGEND

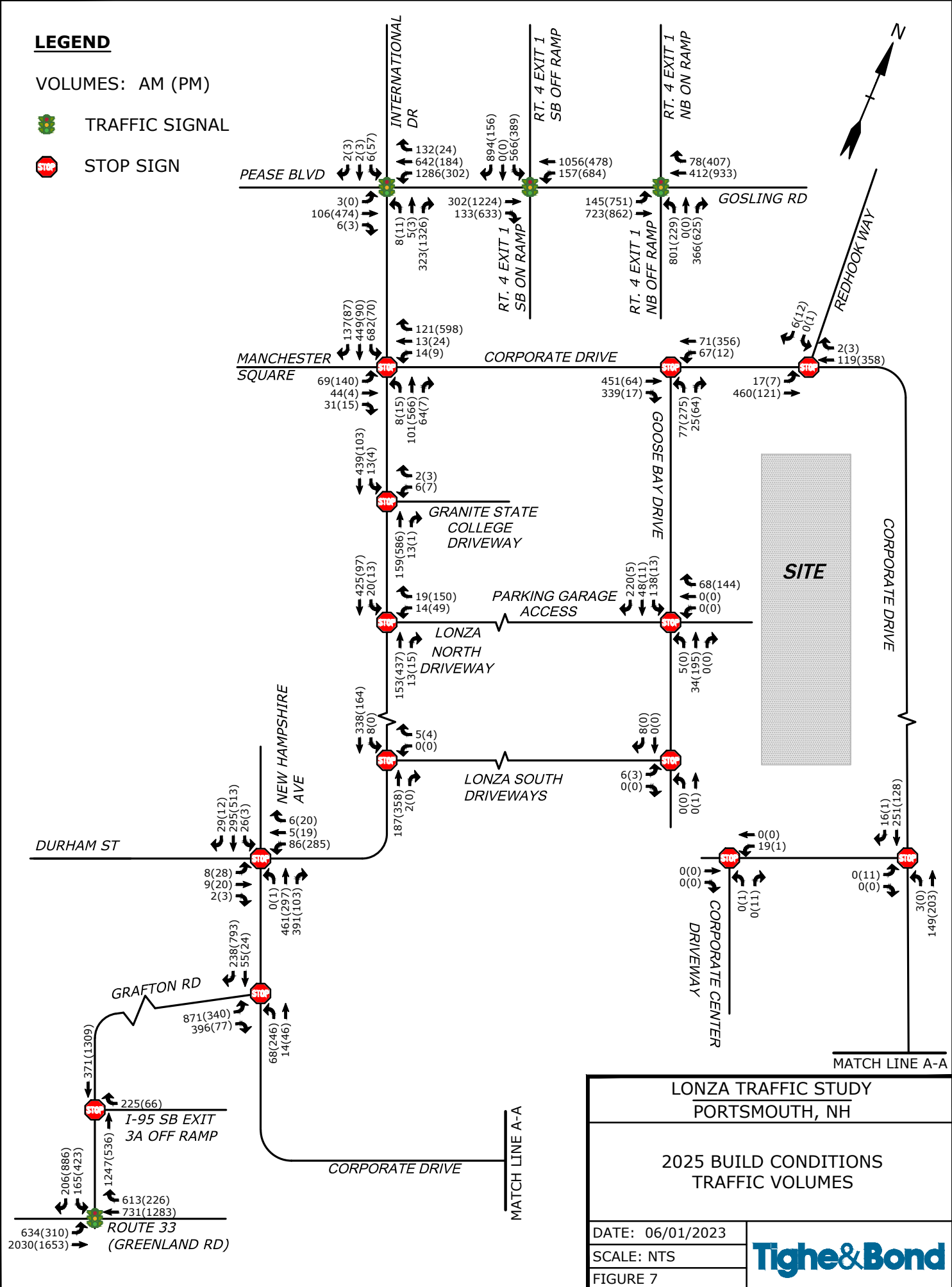
VOLUMES: AM (PM)



TRAFFIC SIGNAL



STOP SIGN



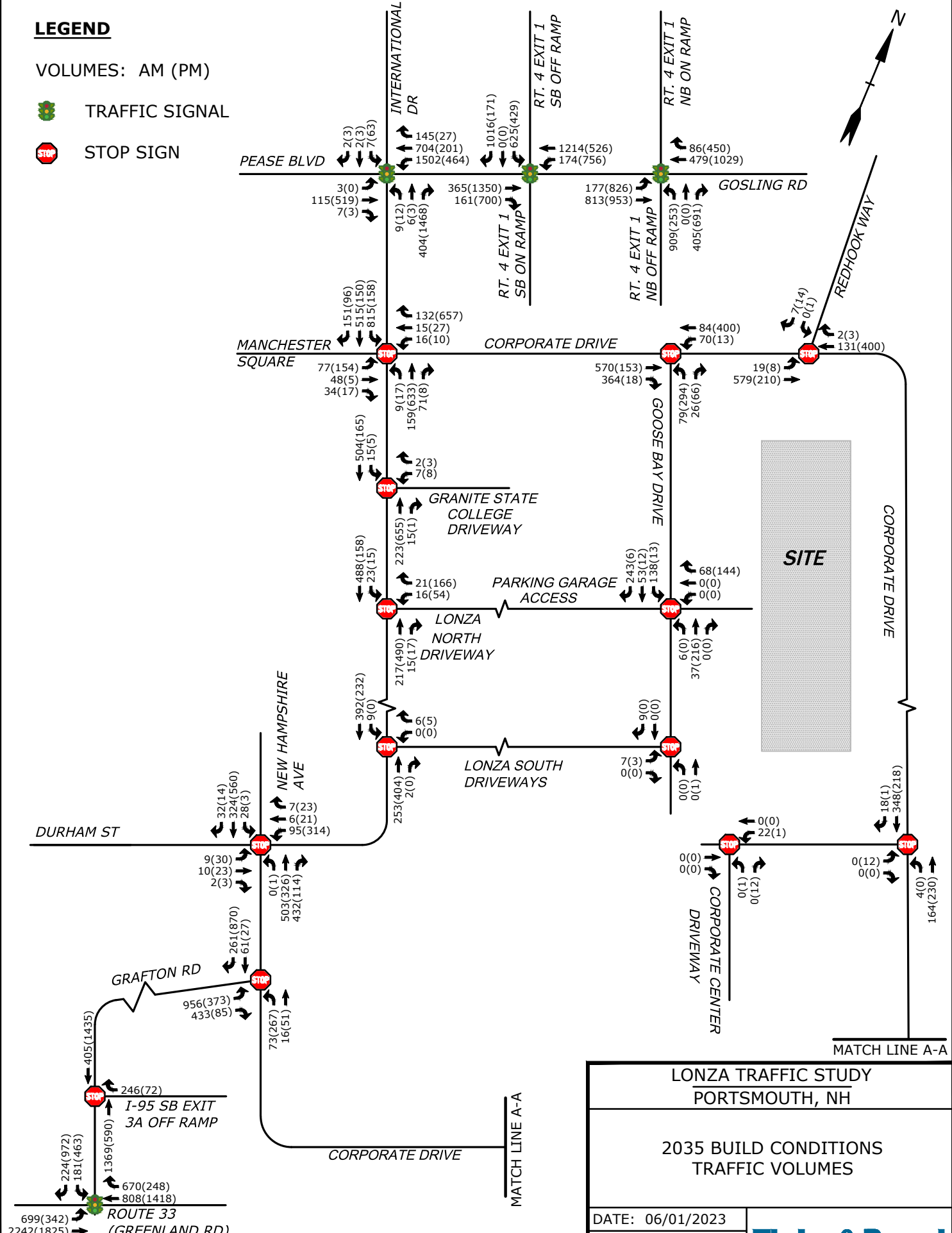
<p align="center">LONZA TRAFFIC STUDY PORTSMOUTH, NH</p>	
<p align="center">2025 BUILD CONDITIONS TRAFFIC VOLUMES</p>	
DATE: 06/01/2023	
SCALE: NTS	
FIGURE 7	

LEGEND

VOLUMES: AM (PM)

TRAFFIC SIGNAL

STOP SIGN



LONZA TRAFFIC STUDY
PORTSMOUTH, NH

2035 BUILD CONDITIONS
TRAFFIC VOLUMES

DATE: 06/01/2023	
SCALE: NTS	
FIGURE 8	

Jun 01, 2023-10:34am Plotted By: RCase Tighe & Bond, Inc. J:\L07000 Lonza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg

APPENDIX A
Traffic Count Data

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 1
 Location: Portsmouth, NH
 Street 1: Pease Blvd
 Street 2: International Drive
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	35	0	0	0	0	0	0	14	0	0	117	54	7
7:15 AM	0	0	1	29	0	1	0	0	0	0	9	1	1	150	76	8
7:30 AM	0	2	0	34	0	1	0	0	0	0	8	1	0	170	80	16
7:45 AM	0	1	0	40	0	0	1	0	0	1	14	0	0	235	110	14
8:00 AM	0	2	1	35	0	1	0	1	0	1	15	1	0	167	90	26
8:15 AM	0	0	2	44	0	1	0	0	0	0	14	2	0	168	90	26
8:30 AM	0	0	1	39	0	0	0	0	0	0	20	1	0	124	73	12
8:45 AM	0	1	0	55	0	3	0	1	0	3	14	0	0	114	83	9

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	4	0	246	0	9	0	0	0	0	90	0	0	49	32	2
4:15 PM	0	0	0	227	0	9	0	0	0	0	76	1	0	56	32	2
4:30 PM	0	2	2	242	0	14	2	1	0	0	82	1	0	56	28	4
4:45 PM	0	2	0	180	0	10	0	1	0	0	65	0	0	54	28	10
5:00 PM	0	1	0	225	0	24	0	2	0	0	107	3	0	40	25	1
5:15 PM	0	1	0	146	0	19	0	1	0	0	83	4	0	24	29	2
5:30 PM	0	0	0	104	0	13	0	2	0	0	45	0	1	28	25	2
5:45 PM	0	0	0	90	0	16	0	0	0	0	31	3	1	25	16	6

AM PEAK HOUR 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	5	3	153	0	3	1	1	0	2	51	4	0	740	370	82
PHF	0.88				0.63				0.84				0.83			
HV %	0.0%	0.0%	0.0%	5.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	2.0%	0.0%	0.0%	0.9%	1.1%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	8	2	895	0	42	2	2	0	0	313	2	0	215	120	18
PHF	0.91				0.68				0.88				0.96			
HV %	0.0%	0.0%	0.0%	0.6%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.6%	0.0%	0.0%	1.9%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 1
 Location: Portsmouth, NH
 Street 1: Pease Blvd
 Street 2: International Drive
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound			Pease Blvd Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
7:15 AM	0	0	0	2	0	0	0	0	0	0	0	0	0	3	1	0
7:30 AM	0	0	0	6	0	0	0	0	0	0	1	0	0	1	3	0
7:45 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	3	0	0
8:00 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	1	0	0
8:15 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	2	1	0
8:30 AM	0	0	0	1	0	0	0	0	0	0	1	0	0	2	1	0
8:45 AM	0	0	0	4	0	0	0	0	0	0	1	0	0	5	1	0

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound			Pease Blvd Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	1	0	0	0	0	0	0	1	0	0	0	0	0
4:15 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	1	0	0	0	0	0	0	1	0	0	3	0	0
4:45 PM	0	0	0	2	0	0	0	0	0	0	0	0	0	1	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0
5:15 PM	0	0	0	1	0	0	0	0	0	0	1	1	0	0	0	0
5:30 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM PHF	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound			Pease Blvd Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	10	0	0	0	0	0	0	1	0	0	8	4	0
	0.42				0.00				0.25			0.75				

PM PEAK HOUR 4:30 PM to 5:30 PM PHF	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound			Pease Blvd Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	4	0	0	0	0	0	0	4	1	0	4	0	0
	0.50				0.00				0.63			0.33				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 1
 Location: Portsmouth, NH
 Street 1: Pease Blvd
 Street 2: International Drive
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PEDESTRIANS & BICYCLES

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	International Drive Northbound				International Drive Southbound				Pease Blvd Eastbound				Pease Blvd Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Southbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	38	0	91	0	0	41	21	0	15	81	0
7:15 AM	0	0	0	0	0	65	0	86	0	0	23	16	0	16	105	0
7:30 AM	0	0	0	0	0	73	0	104	0	0	17	16	1	22	113	0
7:45 AM	0	0	0	0	0	96	0	152	0	0	34	19	1	17	175	0
8:00 AM	0	0	0	0	0	61	0	94	0	0	47	15	1	21	121	0
8:15 AM	0	0	0	0	0	71	0	94	0	0	38	13	0	22	126	0
8:30 AM	0	0	0	0	0	59	0	77	0	0	43	21	0	18	121	0
8:45 AM	0	0	0	0	0	64	0	72	0	0	47	16	0	35	119	0

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	66	0	14	0	0	129	89	2	81	63	0
4:15 PM	0	0	0	0	0	55	0	21	0	0	151	74	0	90	54	0
4:30 PM	0	0	0	0	0	57	0	27	0	0	162	73	0	99	68	0
4:45 PM	0	0	0	0	0	50	1	21	0	0	133	96	3	92	77	0
5:00 PM	0	0	0	0	0	59	0	11	0	0	187	99	0	103	62	0
5:15 PM	0	0	0	0	0	64	0	23	0	0	119	57	0	88	52	0
5:30 PM	0	0	0	0	0	55	0	16	0	0	96	67	1	94	39	0
5:45 PM	0	0	0	0	0	49	0	25	1	0	79	55	0	74	50	0

AM PEAK HOUR 7:30 AM to 8:30 AM	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	301	0	444	0	0	136	63	3	82	535	0
PHF	0.00				0.75				0.80			0.80				
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	1.0%	0.0%	1.4%	0.0%	0.0%	2.2%	9.5%	0.0%	12.2%	1.3%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	221	1	80	0	0	633	342	3	384	261	0
PHF	0.00				0.90				0.85			0.94				
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	1.3%	0.0%	0.0%	0.5%	0.6%	0.0%	0.8%	1.1%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Southbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

HEAVY VEHICLES

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	1	0	0	0	0	1	1	0	2	2	0
7:15 AM	0	0	0	0	0	1	0	0	0	0	1	0	0	1	1	0
7:30 AM	0	0	0	0	0	0	0	3	0	0	0	3	0	6	3	0
7:45 AM	0	0	0	0	0	2	0	3	0	0	2	2	0	1	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	2	4	0
8:15 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	1	0	0
8:30 AM	0	0	0	0	0	2	0	1	0	0	2	0	0	3	2	0
8:45 AM	0	0	0	0	0	0	0	1	0	0	5	2	0	2	3	0

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	3	1	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0
4:30 PM	0	0	0	0	0	0	0	1	0	0	2	0	0	0	1	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	1	1	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	1	1	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	1	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	1	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM PHF	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	3	0	6	0	0	4	6	0	10	8	0
	0.00				0.45				0.63			0.50				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	1	0	0	2	3	0	5	3	0
	0.00				0.25				0.63			0.50				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Southbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
8:15 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	3

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	Route 4 Southbound On-Ramp Northbound				Route 4 Southbound Off-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 7
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Northbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	68	0	38	0	0	0	0	0	24	56	0	0	0	27	10
7:15 AM	0	76	0	47	0	0	0	0	0	17	72	0	0	0	46	9
7:30 AM	0	71	0	47	0	0	0	0	0	4	85	0	0	0	70	12
7:45 AM	0	130	0	66	0	0	0	0	0	18	111	0	0	0	59	14
8:00 AM	0	94	0	53	0	0	0	0	0	16	91	0	0	0	48	9
8:15 AM	0	98	0	39	0	0	0	0	0	12	97	0	0	0	47	10
8:30 AM	0	94	0	41	0	0	0	0	0	15	87	0	0	0	52	9
8:45 AM	0	85	0	55	0	0	0	0	0	16	95	0	0	0	64	13

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	29	0	86	0	0	0	0	0	79	118	0	0	0	111	51
4:15 PM	0	28	1	94	0	0	0	0	0	89	117	0	0	0	122	51
4:30 PM	0	30	0	89	0	0	0	0	0	89	120	0	0	0	140	72
4:45 PM	0	36	0	94	0	0	0	0	0	91	108	0	0	0	130	44
5:00 PM	0	36	0	80	0	0	0	0	0	116	130	0	0	0	135	66
5:15 PM	0	24	0	94	0	0	0	0	0	72	108	0	0	0	117	63
5:30 PM	0	16	0	92	0	0	0	0	0	57	91	0	0	0	114	57
5:45 PM	0	24	0	73	0	0	0	0	0	45	80	0	0	0	100	52

AM PEAK HOUR 7:45 AM to 8:45 AM	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	416	0	199	0	0	0	0	0	61	386	0	0	0	206	42
PHF	0.78				0.00				0.87			0.85				
HV %	0.0%	2.4%	0.0%	3.5%	0.0%	0.0%	0.0%	0.0%	0.0%	4.9%	1.6%	0.0%	0.0%	0.0%	2.4%	4.8%

PM PEAK HOUR 4:15 PM to 5:15 PM	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	130	1	357	0	0	0	0	0	385	475	0	0	0	527	233
PHF	0.94				0.00				0.87			0.90				
HV %	0.0%	1.5%	0.0%	1.1%	0.0%	0.0%	0.0%	0.0%	0.0%	0.3%	0.4%	0.0%	0.0%	0.0%	0.8%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 7
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Northbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



HEAVY VEHICLES

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	2	0	5	0	0	0	0	0	0	1	0	0	0	2	0
7:15 AM	0	1	0	7	0	0	0	0	0	2	1	0	0	0	1	1
7:30 AM	0	3	0	1	0	0	0	0	0	0	0	0	0	0	8	0
7:45 AM	0	2	0	4	0	0	0	0	0	2	2	0	0	0	0	2
8:00 AM	0	5	0	1	0	0	0	0	0	0	1	0	0	0	2	0
8:15 AM	0	0	0	1	0	0	0	0	0	0	1	0	0	0	1	0
8:30 AM	0	3	0	1	0	0	0	0	0	1	2	0	0	0	2	0
8:45 AM	0	3	0	2	0	0	0	0	0	1	5	0	0	0	3	0

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	3	0
4:15 PM	0	0	0	3	0	0	0	0	0	0	0	0	0	0	1	0
4:30 PM	0	0	0	0	0	0	0	0	0	1	1	0	0	0	1	0
4:45 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1	0
5:00 PM	0	1	0	1	0	0	0	0	0	0	1	0	0	0	1	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1
5:30 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	1	0	0	0	0	0	1	0	0	0	0	1	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	8	0	17	0	0	0	0	0	4	4	0	0	0	11	3
	0.78				0.00				0.50			0.44				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound			Newington Street Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	2	0	3	0	0	0	0	0	1	1	0	0	0	6	0
	0.42				0.00				0.25			0.50				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTM #: Location 7
 Location: Portsmouth, NH
 Street 1: Newington Street
 Street 2: Route 4 Northbound On/Off-Ramps
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PEDESTRIANS & BICYCLES

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:45 AM to 8:45 AM	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	Route 4 Northbound Off-Ramp Northbound				Route 4 Northbound On-Ramp Southbound				Newington Street Eastbound				Newington Street Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTM #: Location 12
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: Greenland Road (Route 33)
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	8	0	25	0	52	142	0	0	0	67	26
7:15 AM	0	0	0	0	0	19	0	12	0	53	222	0	0	0	82	39
7:30 AM	0	0	0	0	0	12	0	19	0	68	305	0	0	0	90	70
7:45 AM	0	0	0	0	0	18	0	19	0	128	292	0	0	0	82	99
8:00 AM	0	0	0	0	0	20	0	36	0	74	269	0	0	0	117	59
8:15 AM	0	0	0	0	0	28	0	19	0	67	236	0	0	0	108	69
8:30 AM	0	0	0	0	0	14	0	25	0	80	209	0	0	0	97	57
8:45 AM	0	0	0	0	0	15	0	29	0	73	204	0	0	0	84	64

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	63	0	122	0	32	247	0	0	0	207	43
4:15 PM	0	0	0	0	0	36	0	102	0	37	225	0	0	0	154	37
4:30 PM	0	0	0	0	0	60	0	123	0	45	265	0	0	0	179	33
4:45 PM	0	0	0	0	0	50	0	104	0	46	207	0	0	0	178	22
5:00 PM	0	0	0	0	0	58	0	140	0	34	237	0	0	0	205	18
5:15 PM	0	0	0	0	0	51	0	104	0	23	238	0	0	0	173	26
5:30 PM	0	0	0	0	0	39	0	103	0	31	185	0	0	0	145	23
5:45 PM	0	0	0	0	0	25	0	63	0	29	216	0	0	0	117	27

AM PEAK HOUR 7:30 AM to 8:30 AM	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	78	0	93	0	337	1102	0	0	0	397	297
PHF	0.00				0.76				0.86				0.96			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	5.1%	0.0%	5.4%	0.0%	0.3%	4.1%	0.0%	0.0%	0.0%	8.3%	1.7%

PM PEAK HOUR 4:30 PM to 5:30 PM	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	219	0	471	0	148	947	0	0	0	735	99
PHF	0.00				0.87				0.88				0.93			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	1.4%	0.0%	1.3%	0.0%	0.7%	2.1%	0.0%	0.0%	0.0%	2.4%	2.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 12
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: Greenland Road (Route 33)
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



HEAVY VEHICLES

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	4	0	0	7	0	0	0	6	1
7:15 AM	0	0	0	0	0	2	0	0	0	1	4	0	0	0	6	4
7:30 AM	0	0	0	0	0	1	0	2	0	0	13	0	0	0	4	1
7:45 AM	0	0	0	0	0	1	0	1	0	1	12	0	0	0	10	0
8:00 AM	0	0	0	0	0	0	0	2	0	0	8	0	0	0	8	1
8:15 AM	0	0	0	0	0	2	0	0	0	0	12	0	0	0	11	3
8:30 AM	0	0	0	0	0	0	0	1	0	2	14	0	0	0	5	3
8:45 AM	0	0	0	0	0	0	0	1	0	1	9	0	0	0	9	2

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	1	0	0	6	0	0	0	12	0
4:15 PM	0	0	0	0	0	2	0	0	0	0	6	0	0	0	2	2
4:30 PM	0	0	0	0	0	1	0	3	0	1	5	0	0	0	5	0
4:45 PM	0	0	0	0	0	0	0	1	0	0	3	0	0	0	4	1
5:00 PM	0	0	0	0	0	0	0	2	0	0	7	0	0	0	4	0
5:15 PM	0	0	0	0	0	2	0	0	0	0	5	0	0	0	5	1
5:30 PM	0	0	0	0	0	0	0	0	0	0	4	0	0	0	9	1
5:45 PM	0	0	0	0	0	0	0	2	0	0	5	0	0	0	2	2

AM PEAK HOUR 7:45 AM to 8:45 AM PHF	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	3	0	4	0	3	46	0	0	0	34	7
	0.00				0.88				0.77				0.73			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	3	0	5	0	1	20	0	0	0	23	3
	0.00				0.50				0.88				0.54			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 12
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: Greenland Road (Route 33)
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:30 PM to 5:30 PM	Northbound				Grafton Road Southbound				Greenland Road (Route 33) Eastbound				Greenland Road (Route 33) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 2
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Corporate Drive/Manchester Square
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	1	23	9	0	64	52	9	0	2	1	2	0	2	1	11
7:15 AM	0	2	13	6	0	83	50	11	0	1	2	3	0	4	1	7
7:30 AM	0	1	9	8	0	84	58	17	0	12	12	5	0	3	1	10
7:45 AM	0	0	17	11	0	120	89	25	0	7	7	3	0	3	2	12
8:00 AM	0	0	18	14	0	81	57	22	0	15	3	3	0	1	3	7
8:15 AM	0	4	19	5	0	64	75	21	0	9	4	8	0	2	2	16
8:30 AM	0	2	13	4	0	54	43	15	0	11	7	5	0	1	2	17
8:45 AM	0	3	12	7	0	52	44	11	0	9	3	4	0	2	4	35

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	4	106	0	0	8	13	18	0	23	3	5	0	1	5	107
4:15 PM	0	3	90	2	0	17	14	16	0	22	0	4	0	2	5	119
4:30 PM	0	1	121	0	0	12	17	16	0	35	0	0	0	2	6	88
4:45 PM	0	3	99	3	0	8	22	14	0	23	0	2	0	2	2	50
5:00 PM	0	4	133	1	0	7	13	7	0	29	0	0	0	0	1	62
5:15 PM	0	2	82	0	0	3	9	4	0	13	1	1	0	1	2	49
5:30 PM	0	0	53	3	0	9	9	0	0	5	0	0	0	3	1	41
5:45 PM	0	1	44	0	0	4	15	0	0	12	0	0	0	1	3	24

AM PEAK HOUR 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	5	63	38	0	349	279	85	0	43	26	19	0	9	8	45
PHF	0.83				0.76				0.76				0.78			
HV %	0.0%	0.0%	0.0%	2.6%	0.0%	1.7%	0.0%	0.0%	0.0%	0.0%	3.8%	5.3%	0.0%	0.0%	12.5%	17.8%

PM PEAK HOUR 4:00 PM to 5:00 PM	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	11	416	5	0	45	66	64	0	103	3	11	0	7	18	364
PHF	0.89				0.93				0.84				0.77			
HV %	0.0%	0.0%	0.7%	0.0%	0.0%	4.4%	3.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	5.6%	0.8%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 2
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Corporate Drive/Manchester Square
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	2	0	0	0	0	0	0	0	0	1	1
7:30 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	5
7:45 AM	0	0	0	1	0	3	0	0	0	0	0	0	0	0	0	1
8:00 AM	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0	1
8:15 AM	0	0	0	0	0	1	0	0	0	0	1	1	0	0	1	1
8:30 AM	0	0	0	0	0	3	0	0	0	0	0	1	0	0	1	1
8:45 AM	0	0	1	1	0	4	1	1	0	0	0	0	0	0	0	3

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
4:15 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1	1
4:30 PM	0	0	1	0	0	2	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	1
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1
5:30 PM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 8:00 AM to 9:00 AM PHF	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	1	1	0	9	1	1	0	0	1	2	0	0	2	6
	0.25				0.46				0.38				0.67			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	3	0	0	2	2	0	0	0	0	0	0	0	1	3
	0.38				0.50				0.00				0.50			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 2
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Corporate Drive/Manchester Square
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PEDESTRIANS & BICYCLES

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	1
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	International Drive Northbound				International Drive Southbound				Manchester Square Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 3
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (West)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	4	0	0	0	0	0	0	0	0	43	31	0	2	10	0
7:15 AM	0	3	0	0	0	0	0	0	0	0	63	27	0	4	9	0
7:30 AM	0	4	0	0	0	0	0	0	0	0	67	37	0	2	10	0
7:45 AM	0	2	0	0	0	0	0	0	0	0	82	57	0	5	15	0
8:00 AM	0	2	0	0	0	0	0	0	0	0	63	35	0	3	9	0
8:15 AM	0	3	0	1	0	0	0	0	0	0	49	24	0	3	17	0
8:30 AM	0	1	0	1	0	0	0	0	0	0	47	18	0	2	19	0
8:45 AM	0	15	0	0	0	0	0	0	0	0	43	19	0	0	26	0

Start Time	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	25	0	0	0	0	0	0	0	0	10	1	0	1	89	0
4:15 PM	0	80	0	4	0	0	0	0	0	0	18	1	0	0	46	0
4:30 PM	0	16	0	2	0	0	0	0	0	0	11	1	0	0	80	0
4:45 PM	0	6	0	1	0	0	0	0	0	0	8	3	0	0	48	0
5:00 PM	0	3	0	0	0	0	0	0	0	0	7	1	0	1	58	0
5:15 PM	0	9	0	0	0	0	0	0	0	0	3	0	0	0	45	0
5:30 PM	0	2	0	0	0	0	0	0	0	0	8	5	0	0	43	0
5:45 PM	0	6	0	0	0	0	0	0	0	0	1	3	0	1	22	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	11	0	0	0	0	0	0	0	0	275	156	0	14	43	0
PHF	0.69				0.00				0.78				0.71			
HV %	0.0%	36.4%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.4%	4.5%	0.0%	0.0%	11.6%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	127	0	7	0	0	0	0	0	0	47	6	0	1	263	0
PHF	0.40				0.00				0.70				0.73			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	4.3%	0.0%	0.0%	0.0%	1.5%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 3
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (West)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound			Corporate Drive Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	2	0
7:30 AM	0	2	0	0	0	0	0	0	0	0	0	1	0	0	3	0
7:45 AM	0	1	0	0	0	0	0	0	0	0	0	4	0	0	0	0
8:00 AM	0	1	0	0	0	0	0	0	0	0	0	1	0	0	0	0
8:15 AM	0	1	0	0	0	0	0	0	0	0	1	0	0	0	1	0
8:30 AM	0	1	0	1	0	0	0	0	0	0	0	2	0	0	0	0
8:45 AM	0	3	0	0	0	0	0	0	0	0	2	3	0	0	0	0

Start Time	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound			Corporate Drive Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM PHF	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound			Corporate Drive Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	4	0	0	0	0	0	0	0	0	1	7	0	0	5	0
	0.50				0.00				0.50			0.42				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Goose Bay Drive (West) Northbound				Goose Bay Drive (West) Southbound				Corporate Drive Eastbound			Corporate Drive Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	0	0	2	0	0	0	4	0
	0.00				0.00				0.25			0.50				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 3
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (West)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

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 Office: 978-746-1259
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 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Goose Bay Drive (West) Northbound				Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Goose Bay Drive (West) Northbound				Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Goose Bay Drive (West) Northbound				Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Goose Bay Drive (West) Northbound				Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 4
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Redhook Way
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	2	0	1	42	0	1	0	8	2
7:15 AM	0	0	0	0	0	0	0	0	0	4	59	0	0	0	12	0
7:30 AM	0	0	0	0	0	0	0	2	0	3	66	0	0	0	11	1
7:45 AM	0	0	0	0	0	0	0	2	0	2	79	0	1	0	18	0
8:00 AM	0	0	0	0	0	0	0	0	0	2	61	0	0	0	11	0
8:15 AM	0	0	0	0	0	1	0	1	0	3	48	0	0	0	19	2
8:30 AM	0	0	0	0	0	0	0	0	0	0	49	0	0	0	22	0
8:45 AM	0	0	0	0	0	1	0	1	0	5	38	0	0	0	25	0

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	7	0	2	7	0	0	0	84	0
4:15 PM	0	0	0	0	0	0	0	0	0	1	21	0	0	0	46	1
4:30 PM	0	0	0	0	0	1	0	1	0	2	12	0	0	0	79	1
4:45 PM	0	0	0	0	0	0	0	1	1	0	9	0	0	0	47	0
5:00 PM	0	0	0	0	0	0	0	2	1	0	7	0	0	0	57	0
5:15 PM	0	0	0	0	0	0	0	6	0	1	3	0	0	0	39	0
5:30 PM	0	0	0	0	0	0	0	1	0	0	8	0	0	0	43	0
5:45 PM	0	0	0	0	0	0	0	3	0	0	1	0	0	0	20	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	4	0	11	265	0	1	0	52	1
PHF	0.00				0.50				0.85				0.71			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	25.0%	0.0%	0.0%	0.4%	0.0%	0.0%	0.0%	7.7%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	1	0	9	1	5	49	0	0	0	256	2
PHF	0.00				0.36				0.63				0.77			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	11.1%	0.0%	40.0%	0.0%	0.0%	0.0%	0.0%	1.2%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 4
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Redhook Way
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1
7:15 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	2	0
7:30 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	2	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	1	1	0	0	0	1	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	1	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2	0
4:30 PM	0	0	0	0	0	0	0	0	0	2	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	1	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 8:00 AM to 9:00 AM PHF	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	0	0	1	5	0	0	0	2
	0.00				0.00				0.75				0.50			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	1	0	2	0	0	0	0	3
	0.00				0.25				0.25				0.38			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 4
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Redhook Way
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
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 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	1	0	0	0	1	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Northbound				Redhook Way Southbound				Corporate Drive Eastbound				Corporate Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Matthew Stoutz, PE, PTOE, RSP1

Project #: 1202_5_TB
 BTD #: Location 5
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (East)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	1	12	0	0	0	17	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	13	0	0	0	30	2	0	3	0	2	0	0	0	0
7:30 AM	0	1	18	0	0	0	37	1	0	1	0	1	0	0	0	0
7:45 AM	0	3	18	0	0	0	37	1	0	0	0	0	0	0	0	0
8:00 AM	0	0	16	0	0	0	37	0	0	1	0	0	0	0	0	0
8:15 AM	0	3	16	0	0	0	26	4	0	0	0	1	0	0	0	0
8:30 AM	0	0	22	0	0	0	22	0	0	1	0	0	0	0	0	0
8:45 AM	0	0	16	0	0	0	20	0	0	0	0	2	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	1	44	0	0	0	11	0	0	3	0	2	0	0	0	0
4:15 PM	0	0	29	0	0	0	11	0	0	2	0	4	0	0	0	0
4:30 PM	0	1	41	0	0	0	17	1	0	3	0	2	0	0	0	0
4:45 PM	0	1	28	0	0	0	16	0	0	1	0	0	0	0	0	0
5:00 PM	0	0	30	0	0	0	9	0	0	2	0	2	0	0	0	0
5:15 PM	0	0	21	0	0	0	7	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	24	0	0	0	10	0	0	2	0	0	0	0	0	0
5:45 PM	0	0	13	0	0	0	2	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Corporate Drive Northbound WB				Corporate Drive Southbound EB				Goose Bay Drive (East) Eastbound NB				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	4	65	0	0	0	141	4	0	5	0	3	0	0	0	0
PHF	0.82				0.95				0.40				0.00			
HV %	0.0%	0.0%	4.6%	0.0%	0.0%	0.0%	0.7%	0.0%	0.0%	20.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Corporate Drive Northbound WB				Corporate Drive Southbound EB				Goose Bay Drive (East) Eastbound NB				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	3	142	0	0	0	55	1	0	9	0	8	0	0	0	0
PHF	0.81				0.78				0.71				0.00			
HV %	0.0%	0.0%	1.4%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	11.1%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 5
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (East)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



HEAVY VEHICLES

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	1	0	0	0	0	0	0	1	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	2	0	0	0	0	1	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	1	0	0	0	0	0	0	1	0	0	0	0	0	0
4:15 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	4	0	0	0	1	0	0	1	0	0	0	0	0	0
	0.50				0.25				0.25				0.00			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	2	0	0	0	0	0	0	1	0	0	0	0	0	0
	0.50				0.00				0.25				0.00			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 5
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Goose Bay Drive (East)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F

BOSTON TRAFFIC DATA

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 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	3	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Corporate Drive Northbound				Corporate Drive Southbound				Goose Bay Drive (East) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Corporate Center Driveway
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	5	3	0	2	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	2	2	0	1	1	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	1	3	0
8:00 AM	0	0	0	0	0	0	0	0	1	0	1	2	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	6	1	0
8:30 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0

Start Time	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	1	0	2	0	0	0	0	0	0	3	0	0	0	1	0
4:15 PM	0	0	0	2	0	0	0	0	0	0	4	0	0	0	0	0
4:30 PM	0	0	0	3	0	0	0	0	0	0	2	0	0	0	2	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	1	1	0	0	1	0
5:00 PM	0	0	0	2	0	0	0	0	0	0	2	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Corporate Center Driveway Northbound WB				Southbound				Goose Bay Drive Eastbound NB				Goose Bay Drive Westbound SB			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	1	0	8	8	0	4	4	0
PHF	0.00				0.00				0.53				0.50			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	12.5%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Corporate Center Driveway Northbound WB				Southbound				Goose Bay Drive Eastbound NB				Goose Bay Drive Westbound SB			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	1	0	7	0	0	0	0	0	0	10	1	0	0	4	0
PHF	0.67				0.00				0.69				0.50			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	10.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Corporate Center Driveway
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	Corporate Center Driveway Northbound				Corporate Center Driveway Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Corporate Center Driveway Northbound				Corporate Center Driveway Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	Corporate Center Driveway Northbound				Corporate Center Driveway Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
	0.00				0.00				0.25				0.00			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Corporate Center Driveway Northbound				Corporate Center Driveway Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0
	0.00				0.00				0.25				0.00			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 6
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Corporate Center Driveway
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	8
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	12
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	10
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1

Start Time	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	9
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	3
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	40

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Corporate Center Driveway Northbound				Southbound				Goose Bay Drive Eastbound				Goose Bay Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	19

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 7
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	8	0	0	1	0	0	0	0	0	0
7:30 AM	0	0	1	0	0	0	4	2	0	0	0	0	0	0	0	0
7:45 AM	0	0	3	0	0	0	2	0	0	2	0	0	0	0	0	0
8:00 AM	0	0	1	0	0	0	3	3	0	1	0	0	0	0	0	0
8:15 AM	0	0	0	0	1	0	0	1	0	2	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	1	0	0	1	0	0	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	2	0	0	0	2	0	0	2	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	2	0	0	0	2	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Goose Bay Drive Northbound WB				Goose Bay Drive Southbound EB				Lonza Biologics Driveway (South) Eastbound NB				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	5	0	0	0	17	5	0	4	0	0	0	0	0	0
PHF	0.42				0.69				0.50				0.00			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	5.9%	80.0%	0.0%	75.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Goose Bay Drive Northbound WB				Goose Bay Drive Southbound EB				Lonza Biologics Driveway (South) Eastbound NB				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	5	0	0	0	10	0	0	2	0	0	0	0	0	0
PHF	0.63				0.63				0.25				0.00			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	10.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 7
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



HEAVY VEHICLES

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	1	1	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	3	0	1	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM PHF	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	1	4	0	3	0	0	0	0	0	0
	0.00				0.42				0.75				0.00			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
	0.00				0.25				0.00				0.00			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 7
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F

BOSTON TRAFFIC DATA

PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	2	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	1	0	0	0	2	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	1	0	0	0	3	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	3	0	0	0	4	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	2	0	0	0	3	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	3	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	7	0	0	0	5	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Biologics Driveway (South) Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	3	0	0	0	3	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 8
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Parking Garage Entrance Dr
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	1	5	0	0	0	8	23	0	0	0	0	0	0	0	0
7:15 AM	0	1	3	0	0	0	7	23	0	0	0	0	0	0	0	0
7:30 AM	0	0	2	0	0	0	7	32	0	0	0	0	0	0	0	0
7:45 AM	0	1	3	0	0	0	11	50	0	0	0	0	0	0	0	0
8:00 AM	0	1	3	0	0	0	8	31	0	0	0	0	0	0	0	0
8:15 AM	0	0	4	0	0	0	3	24	0	0	0	0	0	0	0	0
8:30 AM	0	0	2	0	0	0	5	15	0	0	0	0	0	0	0	0
8:45 AM	0	1	14	0	0	0	5	14	0	0	0	0	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	24	0	0	0	1	1	0	0	0	0	0	0	0	0
4:15 PM	0	0	84	0	0	0	2	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	17	0	0	0	0	1	0	0	0	0	0	0	0	0
4:45 PM	0	0	7	0	0	0	1	2	0	0	0	0	0	0	0	0
5:00 PM	0	0	3	0	0	0	2	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	9	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	1	2	0	0	0	2	3	0	0	0	0	0	0	0	0
5:45 PM	0	0	6	0	0	0	0	4	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:15 AM to 8:15 AM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	3	11	0	0	0	33	136	0	0	0	0	0	0	0	0
PHF	0.88				0.69				0.00				0.00			
HV %	0.0%	0.0%	18.2%	0.0%	0.0%	0.0%	15.2%	0.7%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:00 PM to 5:00 PM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	132	0	0	0	4	4	0	0	0	0	0	0	0	0
PHF	0.39				0.67				0.00				0.00			
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTM #: Location 8
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Parking Garage Entrance Dr
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



HEAVY VEHICLES

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	1	0	0	0	2	1	0	0	0	0	0	0	0	0
8:15 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	2	0	0	0	3	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 8:00 AM to 9:00 AM PHF	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	6	0	0	0	6	1	0	0	0	0	0	0	0	0
	0.75				0.58				0.00				0.00			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
	0.00				0.00				0.00				0.00			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 8
 Location: Portsmouth, NH
 Street 1: Goose Bay Drive
 Street 2: Lonza Parking Garage Entrance Dr
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



PEDESTRIANS & BICYCLES

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	1	0	0	0	0

Start Time	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	1	0	0	0	0	0	0	0	1	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:15 AM to 8:15 AM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Goose Bay Drive Northbound				Goose Bay Drive Southbound				Lonza Parking Garage Entrance Driveway Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 9
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Granite State College Drive (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	24	1	0	1	53	0	0	0	0	0	0	0	0	1
7:15 AM	0	0	19	4	0	0	49	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	19	1	0	2	56	0	0	0	0	0	0	2	0	0
7:45 AM	0	0	25	1	0	1	82	0	0	0	0	0	0	1	0	0
8:00 AM	0	0	29	4	0	1	55	0	0	0	0	0	0	0	0	1
8:15 AM	0	0	26	2	0	4	80	0	0	0	0	0	0	1	0	0
8:30 AM	0	0	19	3	0	1	47	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	18	1	1	1	47	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	102	1	0	1	18	0	0	0	0	0	0	3	0	1
4:15 PM	0	0	87	0	0	0	19	0	0	0	0	0	0	1	0	1
4:30 PM	0	0	111	1	0	0	22	0	0	0	0	0	0	2	0	0
4:45 PM	0	0	94	0	0	2	24	0	0	0	0	0	0	1	0	1
5:00 PM	0	0	138	0	0	1	11	0	0	0	0	0	0	1	0	0
5:15 PM	0	0	77	0	0	0	11	0	0	0	0	0	0	2	0	0
5:30 PM	0	0	54	0	0	0	11	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	43	1	0	0	16	0	0	0	0	0	0	1	0	1

AM PEAK HOUR 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	99	8	0	8	273	0	0	0	0	0	0	4	0	1
PHF	0.81				0.84				0.00			0.63				
HV %	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.7%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	430	1	0	3	76	0	0	0	0	0	0	5	0	2
PHF	0.78				0.76				0.00			0.88				
HV %	0.0%	0.0%	0.7%	0.0%	0.0%	0.0%	3.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 9
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Granite State College Drive (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 8:00 AM to 9:00 AM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0
	0.25				0.25				0.00			0.00				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Granite State College Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	3	0	0	0	3	0	0	0	0	0	0	0	0	0
	0.38				0.75				0.00			0.00				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 9
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Granite State College Drive (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PEDESTRIANS & BICYCLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Granite State College Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Granite State College Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound				Granite State College Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound				Granite State College Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 10
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (North)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	10	4	0	4	49	0	0	0	0	0	0	6	0	15
7:15 AM	0	0	18	2	0	3	46	0	0	0	0	0	0	4	0	5
7:30 AM	0	0	17	3	0	3	55	0	0	0	0	0	0	4	0	2
7:45 AM	0	0	23	3	0	5	78	0	0	0	0	0	0	2	0	4
8:00 AM	0	0	29	1	0	2	53	0	0	0	0	0	0	1	0	4
8:15 AM	0	0	26	1	0	3	78	0	0	0	0	0	0	2	0	2
8:30 AM	0	0	19	2	0	1	46	0	0	0	0	0	0	2	0	3
8:45 AM	0	0	18	4	0	1	46	0	0	0	0	0	0	2	0	1

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	76	3	0	2	19	0	0	0	0	0	0	8	0	27
4:15 PM	0	0	61	1	0	1	19	0	0	0	0	0	0	8	0	26
4:30 PM	0	0	78	6	0	4	20	0	0	0	0	0	0	18	0	33
4:45 PM	0	0	62	1	0	4	21	0	0	0	0	0	0	5	0	33
5:00 PM	0	0	120	3	0	1	11	0	0	0	0	0	0	5	0	18
5:15 PM	0	0	61	1	0	0	13	0	0	0	0	0	0	0	0	16
5:30 PM	0	0	42	2	1	1	9	0	0	0	0	0	0	5	0	11
5:45 PM	0	0	34	0	0	3	14	0	0	0	0	0	0	2	0	10

AM PEAK HOUR 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	95	8	0	13	264	0	0	0	0	0	0	9	0	12
PHF	0.86				0.83				0.00			0.88				
HV %	0.0%	0.0%	1.1%	62.5%	0.0%	0.0%	0.4%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	44.4%	0.0%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	321	11	0	10	71	0	0	0	0	0	0	36	0	110
PHF	0.67				0.81				0.00			0.72				
HV %	0.0%	0.0%	0.9%	45.5%	0.0%	0.0%	2.8%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	13.9%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 10
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (North)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	3	0	0	0	0	0	0	0	0	0	3	0	0
7:15 AM	0	0	0	2	0	0	0	0	0	0	0	0	0	2	0	0
7:30 AM	0	0	0	2	0	0	0	0	0	0	0	0	0	2	0	0
7:45 AM	0	0	1	2	0	0	0	0	0	0	0	0	0	1	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	1	0	0	1	0	0	0	0	0	0	1	0	0
8:30 AM	0	0	0	2	0	0	0	0	0	0	0	0	0	2	0	0
8:45 AM	0	0	2	0	0	0	0	0	0	0	0	0	0	1	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	2	0	0	0	0	0	0	0	0	0	2	0	0
4:15 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	2	0	0
4:30 PM	0	0	1	4	0	0	0	0	0	0	0	0	0	3	0	0
4:45 PM	0	0	2	1	0	0	1	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	1	0	0	1	0	0	0	0	0	0	1	0	1
5:45 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	1	9	0	0	0	0	0	0	0	0	0	8	0	0
	0.83				0.00				0.00			0.67				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (North) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	3	7	0	0	2	0	0	0	0	0	0	7	0	0
	0.50				0.50				0.00			0.58				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 10
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (North)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

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PEDESTRIANS & BICYCLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (North) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	13	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	15	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	8	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	5	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (North) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	9	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	15	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	7	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	6	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	10	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	4	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (North) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	46	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (North) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	38	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTM #: Location 11
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	17	0	0	1	38	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	23	0	0	1	42	0	0	0	0	0	0	0	0	1
7:30 AM	0	0	22	0	0	2	48	0	0	0	0	0	0	0	0	1
7:45 AM	0	0	32	1	0	1	65	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	32	0	0	0	41	0	0	0	0	0	0	0	0	1
8:15 AM	0	0	30	0	0	2	56	0	0	0	0	0	0	0	0	1
8:30 AM	0	0	24	0	0	0	38	0	0	0	0	0	0	1	0	0
8:45 AM	0	0	22	0	0	1	25	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	65	0	0	1	26	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	45	0	0	0	26	0	0	0	0	0	0	0	0	3
4:30 PM	0	0	72	0	0	0	41	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	49	0	0	0	33	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	97	0	0	0	21	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	45	0	0	0	19	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	32	0	0	0	17	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	20	0	0	0	17	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	116	1	0	5	210	0	0	0	0	0	0	0	0	3
PHF	0.89				0.81				0.00			0.75				
HV %	0.0%	0.0%	5.2%	100.0%	0.0%	0.0%	1.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	263	0	0	0	121	0	0	0	0	0	0	0	0	3
PHF	0.68				0.74				0.00			0.25				
HV %	0.0%	0.0%	3.0%	0.0%	0.0%	0.0%	6.6%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 11
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	3	0	0	0	3	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	2	0	0	0	3	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	3	1	0	0	1	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	2	0	0	0	4	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	1	0	0	0	3	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	4	0	0	0	3	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	3	0	0	0	2	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	10	1	0	0	8	0	0	0	0	0	0	0	0	0
	0.69				0.67				0.00			0.00				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	International Drive Northbound				International Drive Southbound				Eastbound			Lonza Biologics Driveway (South) Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	10	0	0	0	9	0	0	0	0	0	0	0	0	0
	0.63				0.75				0.00			0.00				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 11
 Location: Portsmouth, NH
 Street 1: International Drive
 Street 2: Lonza Biologics Driveway (South)
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

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PEDESTRIANS & BICYCLES

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:30 AM to 8:30 AM	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	International Drive Northbound				International Drive Southbound				Eastbound				Lonza Biologics Driveway (South) Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 12
 Location: Portsmouth, NH
 Street 1: New Hampshire Ave/Corporate Dr
 Street 2: International Drive/Durham Street
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	33	29	0	3	17	6	0	0	1	0	0	8	0	2
7:15 AM	0	0	43	40	0	5	24	4	0	2	1	0	0	8	2	1
7:30 AM	0	0	55	46	0	7	30	6	0	0	1	0	0	14	0	0
7:45 AM	0	0	55	71	0	7	43	9	0	2	2	0	0	10	1	2
8:00 AM	0	0	67	70	0	2	44	4	0	2	0	0	0	10	0	0
8:15 AM	0	0	63	45	0	2	41	3	0	1	2	0	0	21	1	1
8:30 AM	0	0	64	57	0	5	43	2	0	0	2	1	0	12	1	1
8:45 AM	0	1	50	35	0	4	47	2	0	0	1	0	0	14	0	0

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	63	22	0	1	66	4	0	10	2	0	0	53	4	8
4:15 PM	0	0	49	13	0	1	59	2	0	2	4	2	0	39	5	1
4:30 PM	0	1	38	19	0	1	93	4	0	10	7	0	0	57	2	4
4:45 PM	0	0	55	27	0	0	84	1	0	4	1	0	0	52	2	6
5:00 PM	0	0	57	17	0	0	96	2	0	4	3	0	0	61	5	4
5:15 PM	0	0	27	18	0	0	69	3	0	1	0	1	0	48	2	5
5:30 PM	0	0	32	7	0	1	48	0	0	0	0	1	0	31	0	3
5:45 PM	0	0	28	8	0	0	40	1	0	0	2	0	0	18	1	2

AM PEAK HOUR 7:45 AM to 8:45 AM	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	249	243	0	16	171	18	0	5	6	1	0	53	3	4
PHF	0.90				0.87				0.75				0.65			
HV %	0.0%	0.0%	1.6%	2.5%	0.0%	0.0%	2.9%	0.0%	0.0%	20.0%	0.0%	0.0%	0.0%	3.8%	0.0%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	1	199	76	0	2	332	9	0	20	15	2	0	209	14	15
PHF	0.84				0.88				0.54				0.85			
HV %	0.0%	0.0%	1.5%	1.3%	0.0%	0.0%	0.6%	11.1%	0.0%	0.0%	13.3%	0.0%	0.0%	0.0%	14.3%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 12
 Location: Portsmouth, NH
 Street 1: New Hampshire Ave/Corporate Dr
 Street 2: International Drive/Durham Street
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F



HEAVY VEHICLES

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	2	0	0	1	0	0	1	0	0	0	1	0	0
7:30 AM	0	0	0	1	0	0	1	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	3	0	0	0	1	0	0	1	0	0	0	1	0	0
8:15 AM	0	0	0	1	0	0	1	0	0	0	0	0	0	1	0	0
8:30 AM	0	0	1	3	0	0	3	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	1	0	0	0	0	0	1	0	0	0	0	2	0
4:15 PM	0	0	1	0	0	0	1	0	0	0	1	0	0	0	1	0
4:30 PM	0	0	0	1	0	0	0	0	0	0	1	0	0	0	0	0
4:45 PM	0	0	2	0	0	0	1	0	0	0	0	0	0	0	1	0
5:00 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	1	0	0	1	0	0	0	0	1	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 8:00 AM to 9:00 AM PHF	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	5	4	0	0	7	0	0	1	0	0	0	2	0	0
	0.56				0.58				0.25				0.50			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	3	2	0	0	2	0	0	1	2	0	0	0	4	0
	0.63				0.50				0.75				0.50			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 12
 Location: Portsmouth, NH
 Street 1: New Hampshire Ave/Corporate Dr
 Street 2: International Drive/Durham Street
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Cloudy, 35°F

BOSTON TRAFFIC DATA

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 www.BostonTrafficData.com

PEDESTRIANS & BICYCLES

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1

Start Time	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	2
4:15 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	1	0	0	0	0	0	0	0	1
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:45 AM to 8:45 AM	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	Corporate Drive Northbound				New Hampshire Avenue Southbound				Durham Street Eastbound				International Drive Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	1

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 13
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Grafton Road
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	2	0	0	0	2	21	0	64	0	27	0	0	0	0
7:15 AM	0	5	0	0	0	0	8	19	0	83	0	28	0	0	0	0
7:30 AM	0	6	1	0	0	0	1	40	0	107	0	40	0	0	0	0
7:45 AM	0	4	1	0	0	0	10	29	0	132	0	57	0	0	0	0
8:00 AM	0	12	2	0	0	0	9	36	0	141	0	54	0	0	0	0
8:15 AM	0	7	2	0	0	0	8	39	0	111	0	51	0	0	0	0
8:30 AM	0	7	4	0	0	0	7	31	0	120	0	59	0	0	0	0
8:45 AM	0	14	5	0	0	0	12	29	0	92	0	61	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	34	7	0	0	0	4	111	0	75	0	12	0	0	0	0
4:15 PM	0	34	3	0	0	0	3	102	0	58	0	15	0	0	0	0
4:30 PM	0	44	3	0	0	0	3	147	0	52	0	7	0	0	0	0
4:45 PM	0	29	10	0	0	0	9	125	0	67	0	16	0	0	0	0
5:00 PM	0	42	18	0	0	0	3	164	0	53	0	16	0	0	0	0
5:15 PM	0	21	3	0	0	0	2	114	0	41	0	10	0	0	0	0
5:30 PM	0	20	1	0	0	0	5	71	0	37	0	10	0	0	0	0
5:45 PM	0	10	4	0	0	0	2	50	0	32	0	7	0	0	0	0

AM PEAK HOUR 7:45 AM to 8:45 AM	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	30	9	0	0	0	34	135	0	504	0	221	0	0	0	0
PHF	0.70				0.90				0.93			0.00				
HV %	0.0%	3.3%	11.1%	0.0%	0.0%	0.0%	0.0%	4.4%	0.0%	1.4%	0.0%	1.4%	0.0%	0.0%	0.0%	0.0%

PM PEAK HOUR 4:15 PM to 5:15 PM	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	149	34	0	0	0	18	538	0	230	0	54	0	0	0	0
PHF	0.76				0.83				0.86			0.00				
HV %	0.0%	0.7%	2.9%	0.0%	0.0%	0.0%	0.0%	0.9%	0.0%	2.2%	0.0%	1.9%	0.0%	0.0%	0.0%	0.0%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 13
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Grafton Road
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F



HEAVY VEHICLES

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	1	0	0	0	0	0	0	0	0	2	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	2	0	1	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	1	0	1	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	3	0	1	0	0	0	0
8:00 AM	0	1	0	0	0	0	0	2	0	1	0	1	0	0	0	0
8:15 AM	0	0	1	0	0	0	0	3	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	1	0	3	0	1	0	0	0	0
8:45 AM	0	2	0	0	0	0	0	0	0	1	0	1	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	2	1	0	0	0	0	0	0	0	0	1	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	2	0	1	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	1	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	3	0	2	0	0	0	0	0	0
5:00 PM	0	1	1	0	0	0	0	0	0	1	0	1	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:45 AM to 8:45 AM PHF	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	1	1	0	0	0	0	6	0	7	0	3	0	0	0	0
	0.50				0.50				0.63			0.00				

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound			Westbound				
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	2	1	0	0	0	0	5	0	4	0	1	0	0	0	0
	0.25				0.42				0.63			0.00				

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 1202_5_TB
 BTD #: Location 13
 Location: Portsmouth, NH
 Street 1: Corporate Drive
 Street 2: Grafton Road
 Count Date: 3/7/2023
 Day of Week: Tuesday
 Weather: Clouds & Sun, 40°F

BOSTON TRAFFIC DATA

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PEDESTRIANS & BICYCLES

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	2	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:45 AM to 8:45 AM	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:15 PM to 5:15 PM	Corporate Drive Northbound				Corporate Drive Southbound				Grafton Road Eastbound				Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 11
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: I-95 Southbound Off-Ramp
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PASSENGER CARS & HEAVY VEHICLES COMBINED

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	78	0	0	0	33	0	0	0	0	0	0	0	0	7
7:15 AM	0	0	92	0	0	0	31	0	0	0	0	0	0	0	0	26
7:30 AM	0	0	138	0	0	0	31	0	0	0	0	0	0	0	0	26
7:45 AM	0	0	227	0	0	0	37	0	0	0	0	0	0	0	0	36
8:00 AM	0	0	133	0	0	0	56	0	0	0	0	0	0	0	0	23
8:15 AM	0	0	136	0	0	0	47	0	0	0	0	0	0	0	0	23
8:30 AM	0	0	137	0	0	0	39	0	0	0	0	0	0	0	0	28
8:45 AM	0	0	137	0	0	0	44	0	0	0	0	0	0	0	0	24

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	75	0	0	0	185	0	0	0	0	0	0	0	0	11
4:15 PM	0	0	74	0	0	0	138	0	0	0	0	0	0	0	0	2
4:30 PM	0	0	78	0	0	0	183	0	0	0	0	0	0	0	0	11
4:45 PM	0	0	68	0	0	0	154	0	0	0	0	0	0	0	0	8
5:00 PM	0	0	52	0	0	0	198	0	0	0	0	0	0	0	0	6
5:15 PM	0	0	49	0	0	0	155	0	0	0	0	0	0	0	0	6
5:30 PM	0	0	54	0	0	0	142	0	0	0	0	0	0	0	0	12
5:45 PM	0	0	56	0	0	0	88	0	0	0	0	0	0	0	0	8

AM PEAK HOUR 7:45 AM to 8:45 AM	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	633	0	0	0	179	0	0	0	0	0	0	0	0	110
PHF	0.70				0.80				0.00				0.76			
HV %	0.0%	0.0%	1.6%	0.0%	0.0%	0.0%	3.9%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	2.7%

PM PEAK HOUR 4:00 PM to 5:00 PM	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	295	0	0	0	660	0	0	0	0	0	0	0	0	32
PHF	0.95				0.89				0.00				0.73			
HV %	0.0%	0.0%	1.4%	0.0%	0.0%	0.0%	1.2%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	12.5%

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 11
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: I-95 Southbound Off-Ramp
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



HEAVY VEHICLES

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
7:00 AM	0	0	1	0	0	0	4	0	0	0	0	0	0	0	0	2
7:15 AM	0	0	5	0	0	0	2	0	0	0	0	0	0	0	0	1
7:30 AM	0	0	1	0	0	0	3	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	3
8:15 AM	0	0	3	0	0	0	2	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	5	0	0	0	1	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	3	0	0	0	1	0	0	0	0	0	0	0	0	1

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
4:00 PM	0	0	0	0	0	0	1	0	0	0	0	0	0	0	0	2
4:15 PM	0	0	2	0	0	0	2	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	1	0	0	0	4	0	0	0	0	0	0	0	0	2
4:45 PM	0	0	1	0	0	0	1	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	2	0	0	0	0	0	0	0	0	1
5:15 PM	0	0	1	0	0	0	2	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	1	0	0	0	0	0	0	0	0	0	0	0	0	1
5:45 PM	0	0	2	0	0	0	2	0	0	0	0	0	0	0	0	0

AM PEAK HOUR 7:00 AM to 8:00 AM PHF	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	8	0	0	0	11	0	0	0	0	0	0	0	0	3
	0.40				0.69				0.00				0.38			

PM PEAK HOUR 4:00 PM to 5:00 PM PHF	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right	U-Turn	Left	Thru	Right
	0	0	4	0	0	0	8	0	0	0	0	0	0	0	0	4
	0.50				0.50				0.00				0.50			

Client: Matthew Stoutz, PE, PTOE, RSP1
 Project #: 856_010_TB
 BTD #: Location 11
 Location: Portsmouth, NH
 Street 1: Grafton Road
 Street 2: I-95 Southbound Off-Ramp
 Count Date: 2/17/2022
 Day of Week: Thursday
 Weather: Cloudy, 55°F



PEDESTRIANS & BICYCLES

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
7:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
7:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:00 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:15 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:30 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
8:45 AM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Start Time	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
4:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:15 PM	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
4:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:00 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:15 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:30 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5:45 PM	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

AM PEAK HOUR ¹ 7:45 AM to 8:45 AM	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

PM PEAK HOUR ¹ 4:00 PM to 5:00 PM	Grafton Road Northbound				Grafton Road Southbound				Eastbound				I-95 Southbound Off-Ramp Westbound			
	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED	Left	Thru	Right	PED
	0	1	0	0	0	0	0	0	0	0	0	0	0	0	0	0

¹ NOTE: Peak hour summaries here correspond to peak hours identified for passenger cars and heavy vehicles combined.

Volume Report

Job 1202_5_TB_ATR 1A
Area Portsmouth, NH
Location Pease Blvd (Newington St) EB, 200' west of Rte 4 SB Ramps



Tuesday, March 7, 2023

Time	Total	EB				Time	Total	EB				
0000	57	57		0		1200	221	221		0		
0015	27	27		0		1215	171	171		0		
0030	48	48		0		1230	146	146		0		
0045	10	142	10	142	0	1245	126	664	126	664	0	0
0100	13		13		0	1300	132		132		0	
0115	9		9		0	1315	111		111		0	
0130	5		5		0	1330	130		130		0	
0145	9	36	9	36	0	1345	153	526	153	526	0	0
0200	4		4		0	1400	150		150		0	
0215	2		2		0	1415	142		142		0	
0230	7		7		0	1430	243		243		0	
0245	4	17	4	17	0	1445	193	728	193	728	0	0
0300	1		1		0	1500	223		223		0	
0315	4		4		0	1515	165		165		0	
0330	7		7		0	1530	281		281		0	
0345	5	17	5	17	0	1545	202	871	202	871	0	0
0400	6		6		0	1600	325		325		0	
0415	7		7		0	1615	307		307		0	
0430	6		6		0	1630	325		325		0	
0445	9	28	9	28	0	1645	250	1207	250	1207	0	0
0500	8		8		0	1700	339		339		0	
0515	10		10		0	1715	238		238		0	
0530	13		13		0	1730	165		165		0	
0545	18	49	18	49	0	1745	146	888	146	888	0	0
0600	24		24		0	1800	137		137		0	
0615	16		16		0	1815	92		92		0	
0630	26		26		0	1830	78		78		0	
0645	37	103	37	103	0	1845	58	365	58	365	0	0
0700	48		48		0	1900	85		85		0	
0715	41		41		0	1915	43		43		0	
0730	42		42		0	1930	41		41		0	
0745	52	183	52	183	0	1945	34	203	34	203	0	0
0800	51		51		0	2000	50		50		0	
0815	61		61		0	2015	17		17		0	
0830	60		60		0	2030	28		28		0	
0845	70	242	70	242	0	2045	17	112	17	112	0	0
0900	78		78		0	2100	12		12		0	
0915	87		87		0	2115	17		17		0	
0930	93		93		0	2130	15		15		0	
0945	88	346	88	346	0	2145	18	62	18	62	0	0
1000	98		98		0	2200	21		21		0	
1015	104		104		0	2215	9		9		0	
1030	109		109		0	2230	7		7		0	
1045	111	422	111	422	0	2245	19	56	19	56	0	0
1100	137		137		0	2300	20		20		0	
1115	143		143		0	2315	16		16		0	
1130	150		150		0	2330	60		60		0	
1145	185	615	185	615	0	2345	32	128	32	128	0	0
Total	8010		8010		0				8010		0	

Volume Report

Job 1202_5_TB_ATR 1A
Area Portsmouth, NH
Location Pease Blvd (Newington St) EB, 200' west of Rte 4 SB Ramps



PO BOX 1723, Framingham, MA 01701
 Office: 978-746-1259
 DataRequest@BostonTrafficData.com
 www.BostonTrafficData.com

Wednesday, March 8, 2023

Time	Total	EB				Time	Total	EB			
0000	58	58		0		1200	236	236		0	
0015	24	24		0		1215	182	182		0	
0030	42	42		0		1230	195	195		0	
0045	15	15	139	0	0	1245	152	152	765	0	0
0100	16	16		0		1300	126	126		0	
0115	11	11		0		1315	117	117		0	
0130	9	9		0		1330	128	128		0	
0145	5	5	41	0	0	1345	144	144	515	0	0
0200	5	5		0		1400	153	153		0	
0215	7	7		0		1415	137	137		0	
0230	4	4		0		1430	255	255		0	
0245	3	3	19	0	0	1445	215	215	760	0	0
0300	1	1		0		1500	261	261		0	
0315	1	1		0		1515	157	157		0	
0330	13	13		0		1530	263	263		0	
0345	5	5	20	0	0	1545	221	221	902	0	0
0400	4	4		0		1600	330	330		0	
0415	9	9		0		1615	318	318		0	
0430	5	5		0		1630	352	352		0	
0445	11	11	29	0	0	1645	245	245	1245	0	0
0500	7	7		0		1700	332	332		0	
0515	12	12		0		1715	242	242		0	
0530	14	14		0		1730	193	193		0	
0545	19	19	52	0	0	1745	155	155	922	0	0
0600	29	29		0		1800	144	144		0	
0615	21	21		0		1815	79	79		0	
0630	20	20		0		1830	74	74		0	
0645	45	45	115	0	0	1845	82	82	379	0	0
0700	56	56		0		1900	88	88		0	
0715	39	39		0		1915	49	49		0	
0730	37	37		0		1930	36	36		0	
0745	61	61	193	0	0	1945	39	39	212	0	0
0800	57	57		0		2000	44	44		0	
0815	69	69		0		2015	26	26		0	
0830	79	79		0		2030	21	21		0	
0845	75	75	280	0	0	2045	21	21	112	0	0
0900	81	81		0		2100	17	17		0	
0915	92	92		0		2115	10	10		0	
0930	85	85		0		2130	25	25		0	
0945	99	99	357	0	0	2145	19	19	71	0	0
1000	106	106		0		2200	15	15		0	
1015	116	116		0		2215	11	11		0	
1030	98	98		0		2230	10	10		0	
1045	135	135	455	0	0	2245	11	11	47	0	0
1100	161	161		0		2300	22	22		0	
1115	159	159		0		2315	5	5		0	
1130	183	183		0		2330	45	45		0	
1145	178	178	681	0	0	2345	32	32	104	0	0
Total	8415	8415	0	0	0	Total	8415	8415	0	0	0

Volume Report

Job 1202_5_TB_ATR 1B
Area Portsmouth, NH
Location Pease Blvd (Newington St) WB, 200' west of Rte 4 SB Ramps



Tuesday, March 7, 2023

Time	Total	WB				Time	Total	WB			
0000	6	6			0	1200	142	142			0
0015	6	6			0	1215	157	157			0
0030	3	3			0	1230	150	150			0
0045	5	20	5	20	0	1245	196	645	196	645	0
0100	3		3		0	1300	151		151		0
0115	1		1		0	1315	128		128		0
0130	4		4		0	1330	139		139		0
0145	0	8	0	8	0	1345	121	539	121	539	0
0200	8		8		0	1400	120		120		0
0215	3		3		0	1415	116		116		0
0230	4		4		0	1430	113		113		0
0245	2	17	2	17	0	1445	121	470	121	470	0
0300	4		4		0	1500	89		89		0
0315	3		3		0	1515	113		113		0
0330	7		7		0	1530	98		98		0
0345	6	20	6	20	0	1545	80	380	80	380	0
0400	3		3		0	1600	79		79		0
0415	7		7		0	1615	89		89		0
0430	19		19		0	1630	88		88		0
0445	33	62	33	62	0	1645	84	340	84	340	0
0500	77		77		0	1700	63		63		0
0515	132		132		0	1715	50		50		0
0530	178		178		0	1730	56		56		0
0545	202	589	202	589	0	1745	45	214	45	214	0
0600	130		130		0	1800	54		54		0
0615	150		150		0	1815	61		61		0
0630	163		163		0	1830	35		35		0
0645	245	688	245	688	0	1845	27	177	27	177	0
0700	180		180		0	1900	24		24		0
0715	219		219		0	1915	26		26		0
0730	260		260		0	1930	35		35		0
0745	313	972	313	972	0	1945	28	113	28	113	0
0800	275		275		0	2000	19		19		0
0815	241		241		0	2015	31		31		0
0830	184		184		0	2030	14		14		0
0845	193	893	193	893	0	2045	16	80	16	80	0
0900	146		146		0	2100	14		14		0
0915	126		126		0	2115	11		11		0
0930	90		90		0	2130	8		8		0
0945	114	476	114	476	0	2145	7	40	7	40	0
1000	89		89		0	2200	4		4		0
1015	108		108		0	2215	7		7		0
1030	104		104		0	2230	5		5		0
1045	105	406	105	406	0	2245	7	23	7	23	0
1100	89		89		0	2300	7		7		0
1115	106		106		0	2315	2		2		0
1130	114		114		0	2330	5		5		0
1145	128	437	128	437	0	2345	6	20	6	20	0
Total	7629		7629		0						

Volume Report

Job 1202_5_TB_ATR 1B
Area Portsmouth, NH
Location Pease Blvd (Newington St) WB, 200' west of Rte 4 SB Ramps



Wednesday, March 8, 2023

Time	Total	WB				Time	Total	WB				
0000	4	4		0		1200	145	145		0		
0015	3	3		0		1215	196	196		0		
0030	0	0		0		1230	161	161		0		
0045	0	7	0	7	0	1245	178	680	178	680	0	0
0100	6	6		0		1300	164	164		0		
0115	2	2		0		1315	136	136		0		
0130	5	5		0		1330	158	158		0		
0145	4	17	4	17	0	1345	124	582	124	582	0	0
0200	5	5		0		1400	123	123		0		
0215	3	3		0		1415	106	106		0		
0230	1	1		0		1430	125	125		0		
0245	3	12	3	12	0	1445	130	484	130	484	0	0
0300	0	0		0		1500	99	99		0		
0315	0	0		0		1515	102	102		0		
0330	7	7		0		1530	91	91		0		
0345	7	14	7	14	0	1545	93	385	93	385	0	0
0400	8	8		0		1600	54	54		0		
0415	11	11		0		1615	78	78		0		
0430	21	21		0		1630	87	87		0		
0445	37	77	37	77	0	1645	90	309	90	309	0	0
0500	68	68		0		1700	65	65		0		
0515	127	127		0		1715	67	67		0		
0530	162	162		0		1730	57	57		0		
0545	206	563	206	563	0	1745	57	246	57	246	0	0
0600	137	137		0		1800	41	41		0		
0615	151	151		0		1815	44	44		0		
0630	170	170		0		1830	44	44		0		
0645	259	717	259	717	0	1845	24	153	24	153	0	0
0700	179	179		0		1900	38	38		0		
0715	224	224		0		1915	32	32		0		
0730	264	264		0		1930	28	28		0		
0745	335	1002	335	1002	0	1945	33	131	33	131	0	0
0800	262	262		0		2000	21	21		0		
0815	274	274		0		2015	22	22		0		
0830	221	221		0		2030	12	12		0		
0845	248	1005	248	1005	0	2045	22	77	22	77	0	0
0900	133	133		0		2100	26	26		0		
0915	135	135		0		2115	19	19		0		
0930	114	114		0		2130	14	14		0		
0945	119	501	119	501	0	2145	8	67	8	67	0	0
1000	102	102		0		2200	8	8		0		
1015	122	122		0		2215	0	0		0		
1030	112	112		0		2230	7	7		0		
1045	124	460	124	460	0	2245	4	19	4	19	0	0
1100	97	97		0		2300	5	5		0		
1115	124	124		0		2315	3	3		0		
1130	149	149		0		2330	7	7		0		
1145	133	503	133	503	0	2345	5	20	5	20	0	0
Total	8031	8031	0	0	0							

APPENDIX B
NHDOT Traffic Data

Location Info		Count Data Info	
Location ID	82379024	Start Date	7/18/2018
Type	I-SECTION	End Date	7/19/2018
Functional Class	7	Start Time	12:00 AM
Located On	Pease Blvd	End Time	12:00 AM
		Direction	2-WAY
Direction	2-WAY	Notes	nhdot
Community	PORTSMOUTH	Count Source	8.2379E+11
MPO_ID		File Name	823790243070.prn
HPMS ID		Weather	
Agency	New Hampshire DOT	Study	
		Owner	iwong
		QC Status	Accepted
Interval: 60 mins			
Time	Hourly Count		
00:00 - 01:00	251		
01:00 - 02:00	46		
02:00 - 03:00	123		
03:00 - 04:00	92		
04:00 - 05:00	184		
05:00 - 06:00	416		
06:00 - 07:00	1130		
07:00 - 08:00	1664		
08:00 - 09:00	1817		
09:00 - 10:00	1277		
10:00 - 11:00	1079		
11:00 - 12:00	1570		
12:00 - 13:00	2098		
13:00 - 14:00	1616		
14:00 - 15:00	1424		
15:00 - 16:00	1936		
16:00 - 17:00	2032		
17:00 - 18:00	1831		
18:00 - 19:00	989		
19:00 - 20:00	603		
20:00 - 21:00	417		
21:00 - 22:00	343		
22:00 - 23:00	210		
23:00 - 24:00	166		
TOTAL	23314		

Year 2018 Monthly Data

Group 4 Averages: Urban Highways

Month	ADT	Adjustment to Average	Adjustment to Peak	GROUP	COUNTER	TOWN	LOCATION
January	11,282	1.13	1.24	04	02051003	BOW	NH 3A south of Robinson Rd
February	11,848	1.08	1.18	04	02089001	CHICHESTER	NH 28 (Suncook Valley Rd) north of Bear Hill Rd
March	11,828	1.08	1.18	04	02091001	CLAREMONT	NH 12/103 east of Vermont SL
April	12,491	1.02	1.12	04	62099056	CONCORD	NH 106 (Sheep Davis Rd) at Loudon TL (north of Ashby Rd)
May	13,587	0.94	1.03	04	72099278	CONCORD	US 3 (Fisherville Rd) north of Sewalls Falls Rd
June	13,911	0.92	1.00	04	02125001	DOVER	Dover Point Rd south of Thornwood Ln
July	13,765	0.93	1.01	04	02133021	DURHAM	US 4 east of NH 108
August	13,945	0.92	1.00	04	82197076	HAMPTON	US 1 (Lafayette Rd) south of Ramp to NH 101
September	13,168	0.97	1.06	04	02229022	HUDSON*	<i>Circumferential Hwy east of Nashua TL</i>
October	13,367	0.96	1.04	04	02253025	LEBANON	NH 120 1 mile south of Hanover TL (south of Lahaye Dr)
November	12,215	1.05	1.14	04	02255001	LEE	NH 125 (Calef Hwy) north of Pinkham Rd
December	11,963	1.07	1.17	04	02287001	MARLBOROUGH	NH 12 at Swanzey TL
				04	02297001	MERRIMACK	US 3 (Daniel Webster Hwy) north of Hilton Dr
Average ADT:	12,781			04	02303001	MILFORD*	<i>NH 101A at Amherst TL (west of Overlook Dr)</i>
Peak ADT:	13,945			04	02315051	NASHUA*	<i>NH 111 (Bridge / Ferry St) at Hudson TL</i>
				04	02339001	NEWPORT	NH 10 1 mile south of Croydon TL (north of Corbin Rd)
				04	02345001	NORTH HAMPTON	US 1 (Lafayette Rd) north of North Rd
				04	62387052	RINDGE*	<i>US 202 at Jaffrey TL (north of County Rd)</i>
				04	02445001	TEMPLE	NH 101 at Wilton TL (west of Old County Farm Rd)
				04	02489001	WINDHAM	NH 28 at Derry TL (north of Northland Rd)

** denotes counter that is not included in calculation*

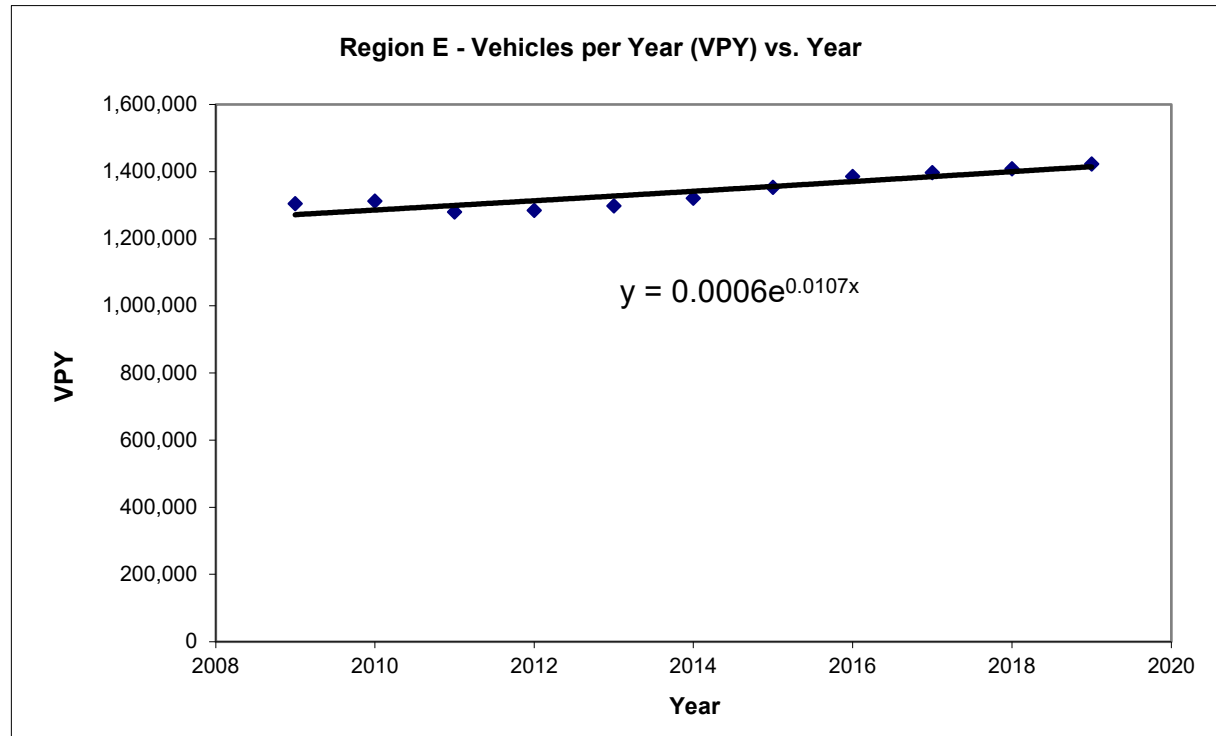
Year 2019 Monthly Data

Group 4 Averages: Urban Highways

Month	ADT	Adjustment to Average	Adjustment to Peak	GROUP	COUNTER	TOWN	LOCATION
January	11,431	1.12	1.23	04	02051003	BOW	NH 3A south of Robinson Rd
February	11,848	1.08	1.18	04	02089001	CHICHESTER	NH 28 (Suncook Valley Rd) north of Bear Hill Rd
March	12,141	1.06	1.15	04	02091001	CLAREMONT	NH 12/103 east of Vermont SL
April	12,860	1.00	1.09	04	62099056	CONCORD	NH 106 (Sheep Davis Rd) at Loudon TL (north of Ashby Rd)
May	13,551	0.95	1.03	04	72099278	CONCORD	US 3 (Fisherville Rd) north of Sewalls Falls Rd
June	13,785	0.93	1.02	04	02125001	DOVER	Dover Point Rd south of Thornwood Ln
July	13,942	0.92	1.01	04	02133021	DURHAM	US 4 east of NH 108
August	14,016	0.92	1.00	04	82197076	HAMPTON	US 1 (Lafayette Rd) south of Ramp to NH 101
September	13,379	0.96	1.05	04	02229022	HUDSON*	<i>Circumferential Hwy east of Nashua TL</i>
October	13,339	0.96	1.05	04	02253025	LEBANON	NH 120 1 mile south of Hanover TL (south of Lahaye Dr)
November	12,265	1.05	1.14	04	02255001	LEE	NH 125 (Calef Hwy) north of Pinkham Rd
December	11,496	1.12	1.22	04	02287001	MARLBOROUGH	NH 12 at Swanzey TL
				04	02297001	MERRIMACK	US 3 (Daniel Webster Hwy) north of Hilton Dr
Average ADT:	12,838			04	02303001	MILFORD*	<i>NH 101A at Amherst TL (west of Overlook Dr)</i>
Peak ADT:	14,016			04	02315051	NASHUA*	<i>NH 111 (Bridge / Ferry St) at Hudson TL</i>
				04	02339001	NEWPORT	NH 10 1 mile south of Croydon TL (north of Corbin Rd)
				04	02345001	NORTH HAMPTON	US 1 (Lafayette Rd) north of North Rd
				04	62387052	RINDGE*	<i>US 202 at Jaffrey TL (north of County Rd)</i>
				04	02445001	TEMPLE	NH 101 at Wilton TL (west of Old County Farm Rd)
				04	02489001	WINDHAM	NH 28 at Derry TL (north of Northland Rd)

** denotes counter that is not included in calculation*

Year	Total
2009	1303948
2010	1312251
2011	1279824
2012	1284314
2013	1298171
2014	1320862
2015	1353486
2016	1385361
2017	1396932
2018	1408237
2019	1422176
CAGR	0.87%
Exp	1.07%
Avg	0.97%



APPENDIX C

Traffic Volume Adjustment Calculation

Traffic Volume Adjustment Factor Calculation

Peak Hour	Feb 2022	2022 Seasonally Adjust to Peak ¹	March 2023	2023 Seasonally Adjust to Peak ²	NHDOT Count Station Data (Loc ID 82379024) - Pease Blvd, West of Route 4 SB Ramps			2022 Adjustment Factor (to 2019)	2023 Adjustment Factor (to 2019)
					July 2018	2018 Seasonally Adjusted ²	Grown to 2019 ³		
AM Peak	1027	1212	1175	1351	1817	1835	1854	53%	37%
PM Peak	1210	1428	1551	1783	2032	2052	2073	45%	16%

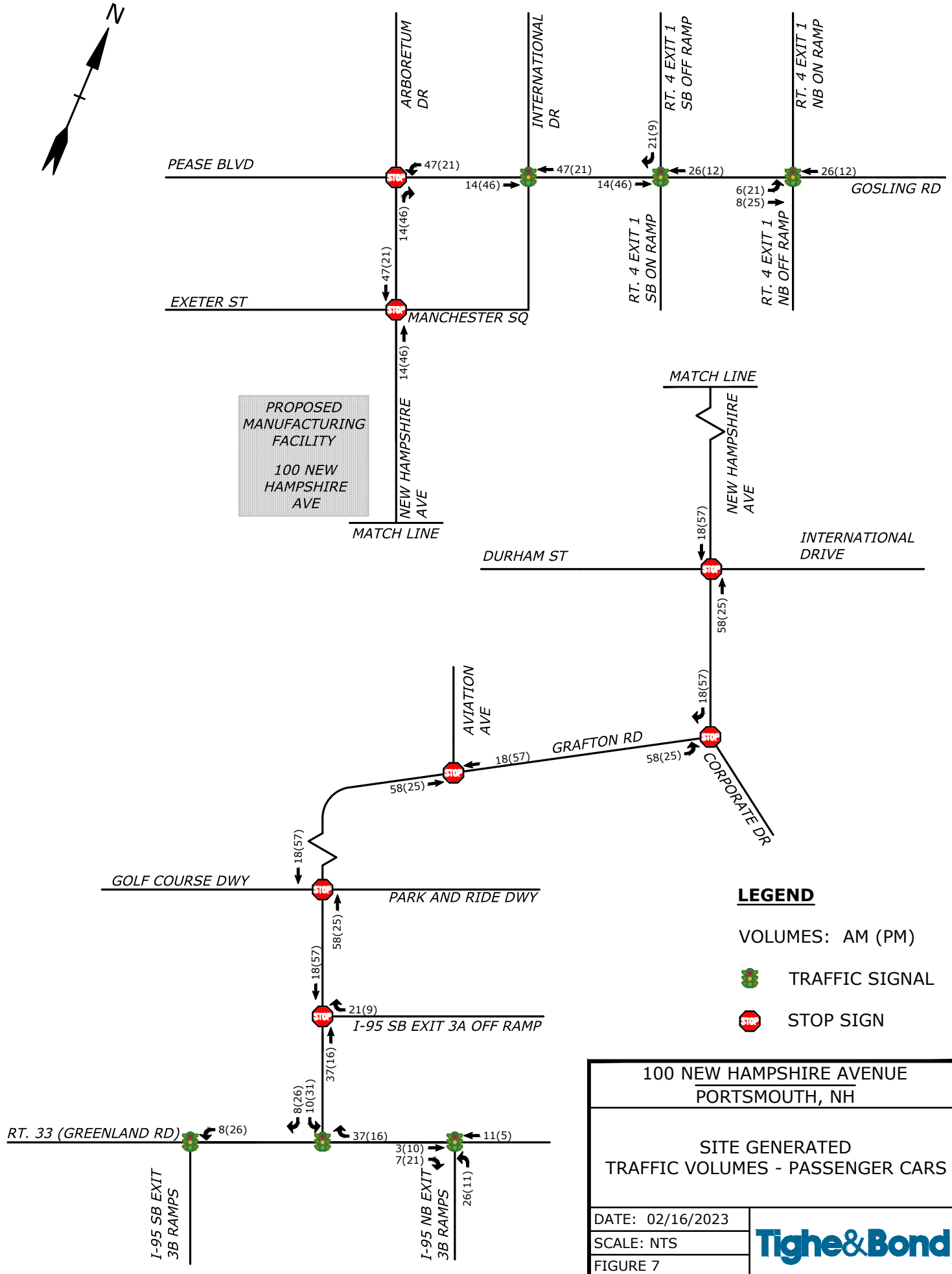
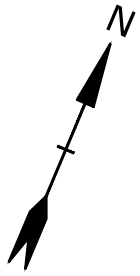
¹ 2019 Seasonal Adjustment Factor to Peak (Feb) 1.18
² 2019 Seasonal Adjustment Factor to Peak (March) 1.15
² 2018 Seasonal Adjustment Factor to Peak 1.01
² 2019 Seasonal Adjustment Factor 1.0
³ 2019 Annual Growth 1.0%

2019 NHDOT Group 4 Adjustment to Peak for February
 2019 NHDOT Group 4 Adjustment to Peak for March
 2018 NHDOT Group 4 Adjustment to Peak for July
 2019 NHDOT Group 4 Adjustment to Peak for August
 Per LOC ID 82379024 growth from 2018 to 2019

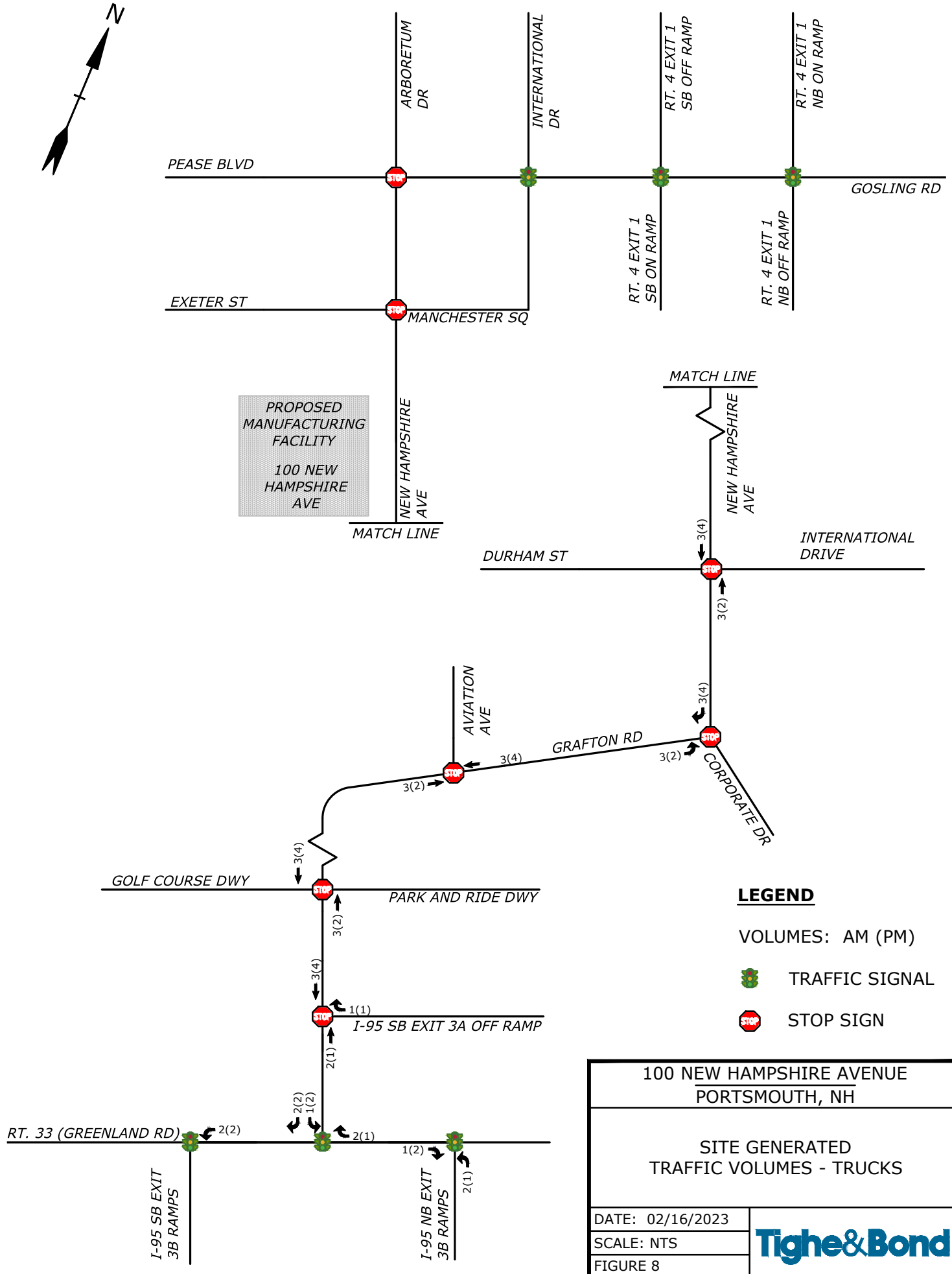
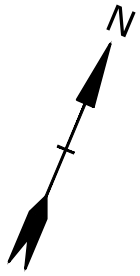
APPENDIX D

Background Development Traffic Volumes

Feb 16, 2023 9:09am Plotted By: RCase Tighe & Bond, Inc. \\tighenond.com\data\Projects\p0595 Pro Con General Proposals\p0595-015 100 NH Avenue\Drawings\Figures\AutoCAD\Figures\Traffic Volume Figures.dwg






Feb 16, 2023 9:10am Plotted By: RCase Tighe & Bond, Inc. \\tighbond.com\data\Projects\p0595\Pro Con General Proposals\p0595-015 100 NH Avenue\Drawings\Figures\AutoCAD\Figures\Traffic Volume Figures.dwg



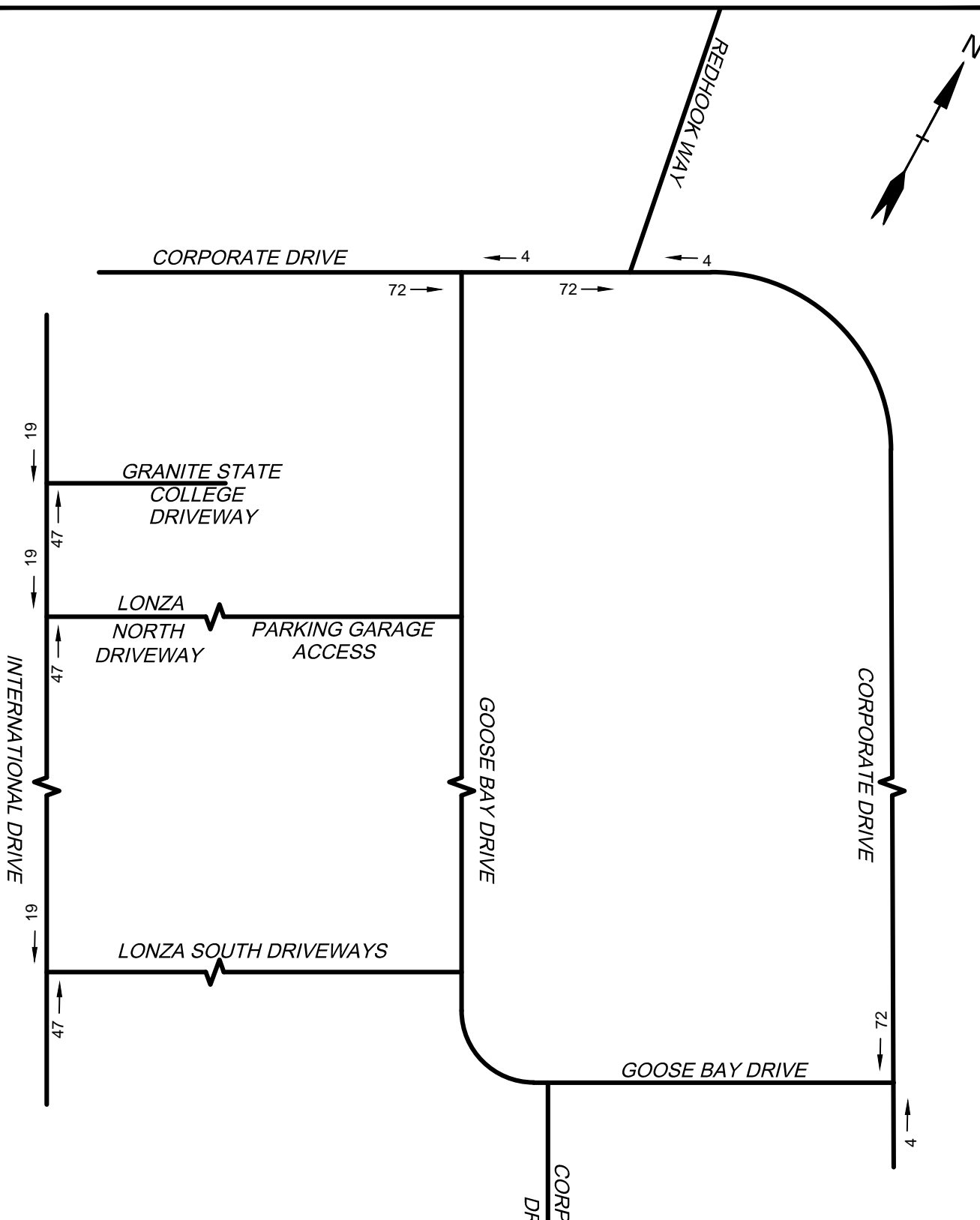
PROPOSED
MANUFACTURING
FACILITY
100 NEW
HAMPSHIRE
AVE

LEGEND

- VOLUMES: AM (PM)
-  TRAFFIC SIGNAL
-  STOP SIGN

100 NEW HAMPSHIRE AVENUE PORTSMOUTH, NH	
SITE GENERATED TRAFFIC VOLUMES - TRUCKS	
DATE: 02/16/2023	
SCALE: NTS	
FIGURE 8	

Feb 27, 2018-4:40pm Plotted By: DWBradshaw
 Tighe & Bond, Inc. \\nas-wfo\data\Projects\LL0700 Lonza Biologics Expansion was 1576\F013 Iron Parcel Redevelopment\Drawings_Figures\AutoCAD\Figures\Traffic Volumes_recover.dwg



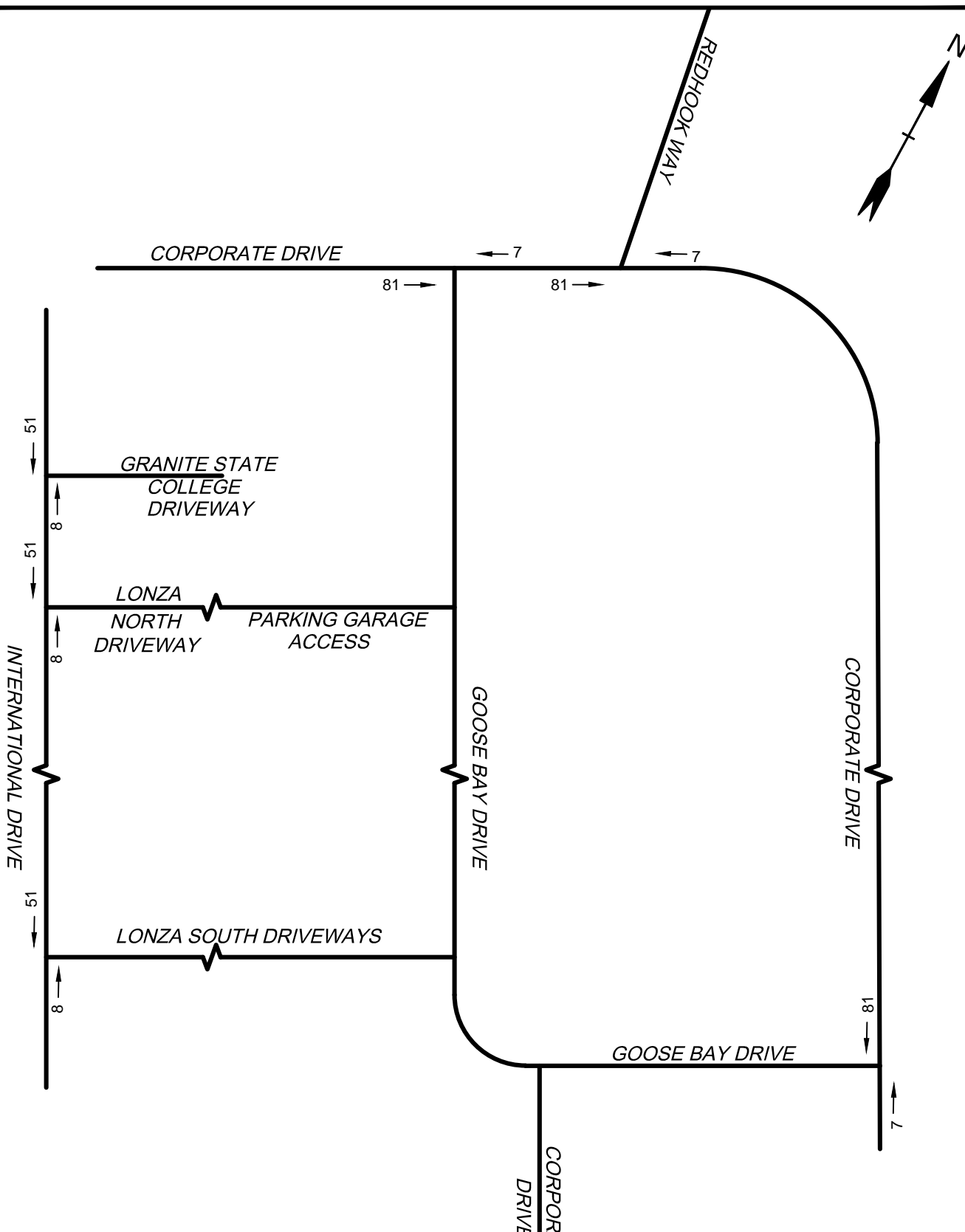
Lonza Biologics Expansion Project
 Portsmouth, NH

AM PEAK HOUR
 BACKGROUND TRIPS
 PEASE MASTER PLAN

DATE:	02/26/18
SCALE:	NO SCALE
FIGURE A1	



Feb 27, 2018-4:40pm Plotted By: DWBradshaw
 Tighe & Bond, Inc. \\nas-wfo\data\Projects\LL0700 Lonza Biologics Expansion was 1576\F013 Iron Parcel Redevelopment\Drawings_Figures\AutoCAD\Figures\Traffic Volumes_recover.dwg



Lonza Biologics Expansion Project
 Portsmouth, NH

PM PEAK HOUR
 BACKGROUND TRIPS
 PEASE MASTER PLAN

DATE:	02/26/18
SCALE:	NO SCALE
FIGURE A2	




APPENDIX E

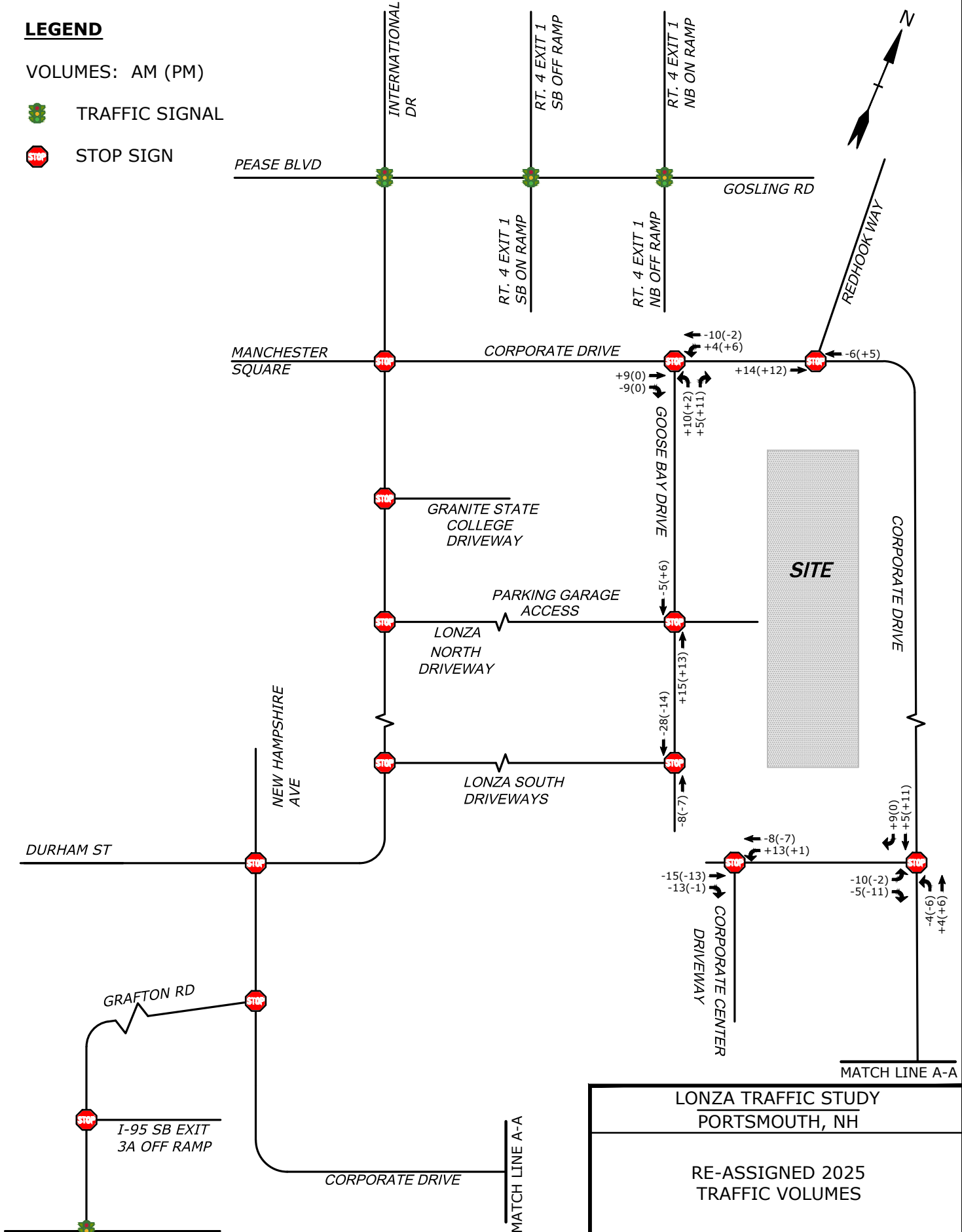
Reassigned Traffic Volumes


LEGEND

VOLUMES: AM (PM)

 TRAFFIC SIGNAL

 STOP SIGN




LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
RE-ASSIGNED 2025 TRAFFIC VOLUMES	
DATE: 05/19/2023	
SCALE: NTS	
FIGURE 1	

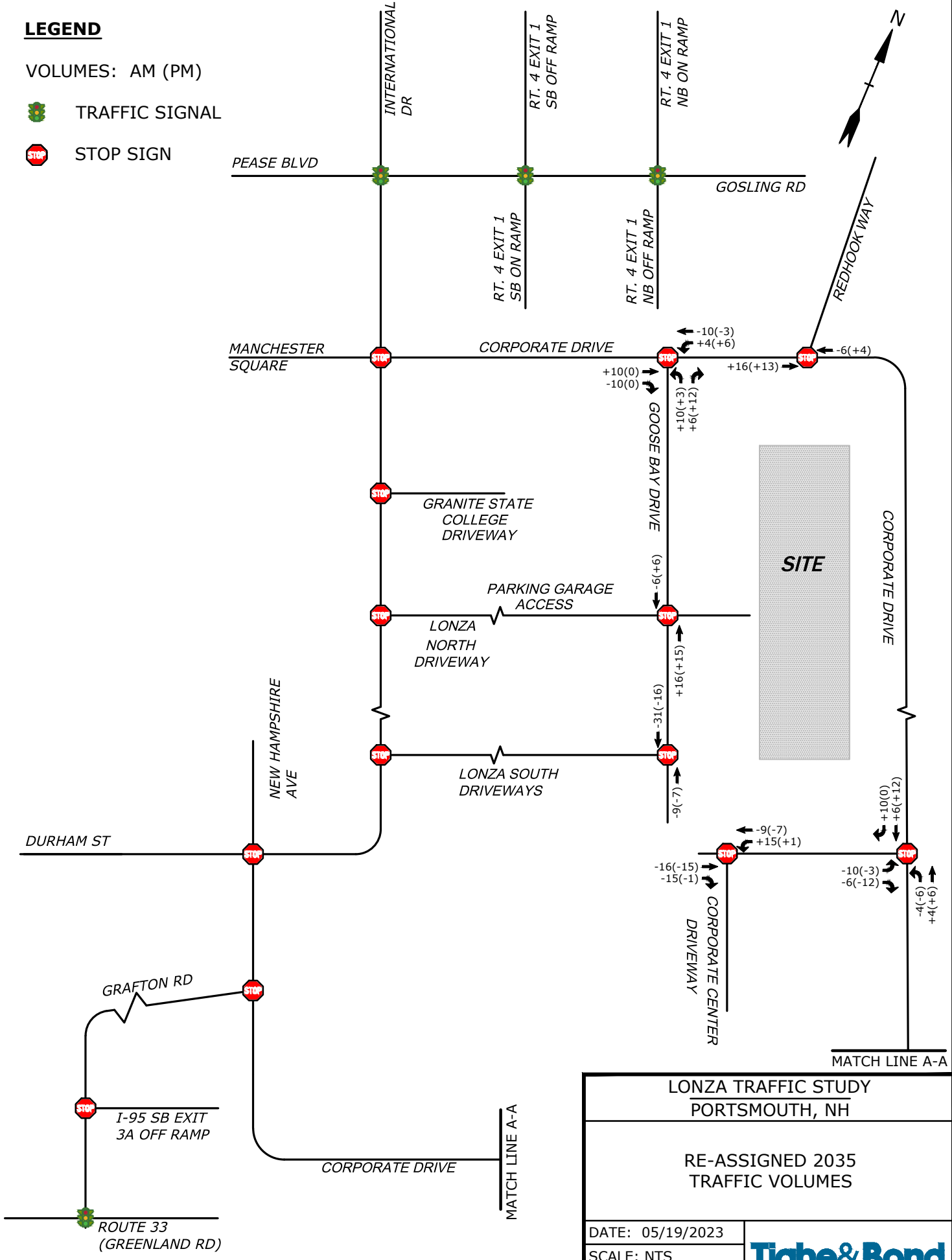
May 19, 2023-10:49am Plotted By: MStoutz Tighe & Bond, Inc. J:\L0700\Lonza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg


LEGEND

VOLUMES: AM (PM)

 TRAFFIC SIGNAL

 STOP SIGN



LONZA TRAFFIC STUDY	
PORTSMOUTH, NH	
RE-ASSIGNED 2035 TRAFFIC VOLUMES	
DATE: 05/19/2023	
SCALE: NTS	
FIGURE 2	

May 19, 2023-10:49am Plotted By: MStoutz Tighe & Bond, Inc. J:\L0700\Lonza Biologics Expansion was 1576F\026_Project Albacore\Drawings\AutoCAD\Figures\L0700-026 Traffic Volume Figures.dwg

APPENDIX F

Collision History Summary

Intersection Collision History Summary

Intersection: Pease Boulevard

at

International Drive

COLLISION TYPE

	2020	2021	2022	Total	Percent
Fixed Object	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday Off-Peak	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

WEATHER

	2020	2021	2022	Total	Percent
Other/Unknown	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Other/Unknown	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	0	1	0	1	100.0%
TOTAL	0	1	0	1	100%

Intersection Collision History SummaryIntersection: **Pease Boulevard**

at

US Route 4 SB Ramps**COLLISION TYPE**

	2020	2021	2022	Total	Percent
Angle	2	2	0	4	57.1%
Rear-End	0	1	0	1	14.3%
Overturn/Rollover	0	0	1	1	14.3%
Sideswipe, Same Direction	1	0	0	1	14.3%
TOTAL	3	3	1	7	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	3	3	1	7	100.0%
TOTAL	3	3	1	7	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	3	3	0	6	100.0%
TOTAL	3	3	0	6	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	3	3	1	7	100.0%
TOTAL	3	3	1	7	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday 6-9 A.M.	1	0	0	1	14.3%
Weekday Off-Peak	2	1	0	3	42.9%
Weekend Off-Peak	0	2	1	3	42.9%
TOTAL	3	3	1	7	100%

WEATHER

	2020	2021	2022	Total	Percent
Clear	2	3	0	5	71.4%
Snow	1	0	0	1	14.3%
Other/Unknown	0	0	1	1	14.3%
TOTAL	3	3	1	7	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Dry	2	3	0	5	71.4%
Snow	1	0	0	1	14.3%
Other/Unknown	0	0	1	1	14.3%
TOTAL	3	3	1	7	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	3	3	1	7	100.0%
TOTAL	3	3	1	7	100%

Intersection Collision History Summary

**Intersection: Gosling Road/Pease Boulevard at
US Route 4 NB Ramps**

COLLISION TYPE

	2020	2021	2022	Total	Percent
Rear-End	0	1	3	4	36.4%
Angle	0	1	2	3	27.3%
Sideswipe, Same Direction	0	1	3	4	36.4%
TOTAL	0	3	8	11	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	0	3	8	11	100.0%
TOTAL	0	3	8	11	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	0	3	8	11	100.0%
TOTAL	0	3	8	11	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	0	3	8	11	100.0%
TOTAL	0	3	8	11	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday 6-9 A.M.	0	0	1	1	9.1%
Weekday 3-6 P.M.	0	0	2	2	18.2%
Weekday Off-Peak	0	3	2	5	45.5%
Saturday 11 A.M. - 2 P.M.	0	0	2	2	18.2%
Weekend Off-Peak	0	0	1	1	9.1%
TOTAL	0	3	8	11	100%

WEATHER

	2020	2021	2022	Total	Percent
Clear	0	3	0	3	27.3%
Other/Unknown	0	0	8	8	72.7%
TOTAL	0	3	8	11	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Dry	0	3	0	3	27.3%
Other/Unknown	0	0	8	8	72.7%
TOTAL	0	3	8	11	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	0	3	8	11	100.0%
TOTAL	0	3	8	11	100%

Intersection Collision History Summary

**Intersection: Route 33 (Greenland Road)
Grafton Road**

at

COLLISION TYPE

	2020	2021	2022	Total	Percent
Rear-End	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday 3-6 P.M.	1	0	1	2	40.0%
Weekday Off-Peak	0	1	0	1	20.0%
Saturday 11 A.M. - 2 P.M.	0	1	0	1	20.0%
Weekend Off-Peak	0	0	1	1	20.0%
TOTAL	1	2	2	5	100%

WEATHER

	2020	2021	2022	Total	Percent
Other/Unknown	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Other/Unknown	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	1	2	2	5	100.0%
TOTAL	1	2	2	5	100%

Intersection Collision History Summary

**Intersection: Corporate Drive
International Drive**

at

COLLISION TYPE

	2020	2021	2022	Total	Percent
Rear-End	2	0	1	3	30.0%
Head-On	1	0	0	1	10.0%
Angle	3	2	1	5	50.0%
Sideswipe, Same Direction	1	0	0	1	10.0%
TOTAL	7	2	2	10	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	6	2	2	10	100.0%
TOTAL	6	2	2	10	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	7	2	2	11	100.0%
TOTAL	7	2	2	11	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	7	2	2	11	100.0%
TOTAL	7	2	2	11	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday 6-9 A.M.	1	1	1	3	27.3%
Weekday 3-6 P.M.	3	0	0	3	27.3%
Weekday Off-Peak	2	1	1	4	36.4%
Weekend Off-Peak	1	0	0	1	9.1%
TOTAL	7	2	2	11	100%

WEATHER

	2020	2021	2022	Total	Percent
Other/Unknown	7	2	2	11	100.0%
TOTAL	7	2	2	11	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Other/Unknown	7	2	2	11	100.0%
TOTAL	7	2	2	11	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	7	2	2	11	100.0%
TOTAL	7	2	2	11	100%

Intersection Collision History Summary

**Intersection: New Hampshire Avenue
International Drive**

at

COLLISION TYPE

	2020	2021	2022	Total	Percent
Other/Unknown	1	0	0	1	16.7%
Angle	2	1	2	5	83.3%
TOTAL	3	1	2	6	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	3	1	2	6	100.0%
TOTAL	3	1	2	6	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	3	1	2	6	100.0%
TOTAL	3	1	2	6	100%

SEVERITY

	2020	2021	2022	Total	Percent
Serious Injury	1	0	0	1	16.7%
Minor Injury / Property Damage Only (PDO)	2	1	2	5	83.3%
TOTAL	3	1	2	6	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday 3-6 P.M.	0	0	1	1	16.7%
Weekday Off-Peak	3	1	0	4	66.7%
Weekend Off-Peak	0	0	1	1	16.7%
TOTAL	3	1	2	6	100%

WEATHER

	2020	2021	2022	Total	Percent
Other/Unknown	3	1	2	6	100.0%
TOTAL	3	1	2	6	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Other/Unknown	3	1	2	6	100.0%
TOTAL	3	1	2	6	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	3	1	2	6	100.0%
TOTAL	3	1	2	6	100%

Intersection Collision History Summary

**Intersection: Grafton Drive
Corporate Drive**

at

COLLISION TYPE

	2020	2021	2022	Total	Percent
Angle	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

CONTRIBUTING FACTOR

	2020	2021	2022	Total	Percent
Other/Unknown	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

COLLISION EVENT

	2020	2021	2022	Total	Percent
Motor Vehicle	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

SEVERITY

	2020	2021	2022	Total	Percent
Minor Injury / Property Damage Only (PDO)	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

DAY & TIME

	2020	2021	2022	Total	Percent
Weekday Off-Peak	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

WEATHER

	2020	2021	2022	Total	Percent
Other/Unknown	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

ROAD SURFACE CONDITION

	2020	2021	2022	Total	Percent
Other/Unknown	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

LIGHT CONDITIONS

	2020	2021	2022	Total	Percent
Other/Unknown	1	0	0	1	100.0%
TOTAL	1	0	0	1	100%

APPENDIX G

Capacity Analysis Methodology

CAPACITY ANALYSIS METHODOLOGY

A primary result of capacity analysis is the assignment of levels of service to traffic facilities under various traffic flow conditions. The capacity analysis methodology is based on the concepts and procedures in the *Highway Capacity Manual* (HCM).¹ The concept of level of service (LOS) is defined as a qualitative measure describing operational conditions within a traffic stream and their perception by motorists and/or passengers. A level-of-service definition provides an index to quality of traffic flow in terms of such factors as speed, travel time, freedom to maneuver, traffic interruptions, comfort, convenience, and safety.

Six levels of service are defined for each type of facility. They are given letter designations from A to F, with LOS A representing the best operating conditions and LOS F the worst. Since the level of service of a traffic facility is a function of the traffic flows placed upon it, such a facility may operate at a wide range of levels of service, depending on the time of day, day of week, or period of year. A description of the operating condition under each level of service is provided below:

- *LOS A* describes conditions with little to no delay to motorists.
- *LOS B* represents a desirable level with relatively low delay to motorists.
- *LOS C* describes conditions with average delays to motorists.
- *LOS D* describes operations where the influence of congestion becomes more noticeable. Delays are still within an acceptable range.
- *LOS E* represents operating conditions with high delay values. This level is considered by many agencies to be the limit of acceptable delay.
- *LOS F* is considered to be unacceptable to most drivers with high delay values that often occur, when arrival flow rates exceed the capacity of the intersection.

Signalized Intersections

Levels of service for signalized intersections are also calculated using the operational analysis methodology of the HCM. The methodology for signalized intersections assesses the effects of signal type, timing, phasing, and progression; vehicle mix; and geometrics on average *control* delay. Control delay is used to establish the operating characteristics for an intersection or an approach to an intersection. Volume-to-capacity (v/c) ratios are also used to help signify the utilization of a lane group's capacity at an intersection. A v/c ratio of ≥ 1.00 represents conditions when the traffic signal cycle capacity is fully utilized and indicates a capacity failure. The level-of-service criteria for signalized intersections are shown in Table A-1.

¹*Highway Capacity Manual, 6TH Edition: A Guide for Multimodal Mobility Analysis*. Washington, D.C.: Transportation Research Board, 2016.

Unsignalized Intersections

Levels of service for unsignalized intersections are calculated using the operational analysis methodology of the HCM. The procedure accounts for lane configuration on both the minor and major street approaches, conflicting traffic stream volumes, and the type of intersection control (STOP, YIELD, or all-way STOP control). The definition of level of service for unsignalized intersections is a function of average *control* delay. Control delay at an unsignalized intersection is defined as the total elapsed time from when a vehicle stops at the end of the queue until the vehicle departs from the stop line. This time includes the time required for the vehicle to travel from the last-in-queue position to the first-in-queue position.

Volume-to-capacity (v/c) ratios are also used to help signify the utilization of a movement's capacity at an intersection. A v/c ratio of ≥ 1.00 represents conditions when the movement is fully utilized and indicates a capacity failure. The capacity of the movements is based on the distribution of gaps in the major street traffic stream, the selection of gaps to complete the desired movement, and the follow-up headways for each driver in the queue. When an unsignalized intersection is located within 0.25 miles of a signalized intersection, traffic flows may not be random and some platoon structure may exist, thereby affecting the minor street operations. The level-of-service criteria for unsignalized intersections are shown in Table A-1.

TABLE A-1
Level-of-Service Criteria for Intersections

Level of Service	Signalized Intersection Criteria	Unsignalized Intersection Criteria	V/C Ratio >1.00 ^a
	Average Control Delay (Seconds per Vehicle)	Average Control Delay (Seconds per Vehicle)	
A	≤ 10	≤ 10	F
B	>10 and ≤ 20	>10 and ≤ 15	F
C	>20 and ≤ 35	>15 and ≤ 25	F
D	>35 and ≤ 55	>25 and ≤ 35	F
E	>55 and ≤ 80	>35 and ≤ 50	F
F	>80	>50	F

Note: ^aFor approach-based and intersection-wide assessments, LOS is defined solely by control delay.




















Source: *Highway Capacity Manual, 6th Edition: A Guide for Multimodal Mobility Analysis*. Washington, D.C.: Transportation Research Board, 2016. Exhibit 19-8, Pg. 19-16.

For signalized intersections, this delay criterion may be applied in assigning level-of-service designations to individual lane groups, to individual intersection approaches, or to the entire intersection. For unsignalized intersections, this delay criterion may be applied in assigning level-of-service designations to individual lane groups on the minor street approaches or to the left turns from the major street approaches.

APPENDIX H













Capacity Analysis Worksheets

101: International Dr & Pease Blvd
 2023 Existing Conditions Weekday AM Peak

													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	3	90	6	1166	583	129	8	5	270	6	2	2	
Future Volume (vph)	3	90	6	1166	583	129	8	5	270	6	2	2	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12	
Total Lost time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Lane Util. Factor	1.00	0.95		0.97	0.95			1.00	0.88		1.00		
Frt	1.00	0.99		1.00	0.97			1.00	0.85		0.97		
Flt Protected	0.95	1.00		0.95	1.00			0.97	1.00		0.97		
Satd. Flow (prot)	1805	3511		3467	3469			1783	2682		2035		
Flt Permitted	0.95	1.00		0.95	1.00			0.87	1.00		0.86		
Satd. Flow (perm)	1805	3511		3467	3469			1597	2682		1810		
Peak-hour factor, PHF	0.84	0.84	0.84	0.83	1.00	0.83	0.88	0.88	0.88	0.63	0.63	0.63	
Adj. Flow (vph)	4	107	7	1405	583	155	9	6	307	10	3	3	
RTOR Reduction (vph)	0	4	0	0	11	0	0	0	0	0	2	0	
Lane Group Flow (vph)	4	110	0	1405	727	0	0	15	307	0	14	0	
Heavy Vehicles (%)	0%	2%	0%	1%	1%	0%	0%	0%	6%	0%	0%	0%	
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA		
Protected Phases	6	2		1	5			8			4		
Permitted Phases							8		8		4		
Actuated Green, G (s)	5.5	12.5		44.0	52.0			15.4	15.4		15.4		
Effective Green, g (s)	5.5	12.5		44.0	52.0			15.4	15.4		15.4		
Actuated g/C Ratio	0.06	0.14		0.49	0.58			0.17	0.17		0.17		
Clearance Time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Vehicle Extension (s)	2.0	3.0		3.0	3.0			3.0	3.0		3.0		
Lane Grp Cap (vph)	110	488		1696	2006			273	459		310		
v/s Ratio Prot	0.00	c0.03		c0.41	c0.21								
v/s Ratio Perm								0.01	c0.11		0.01		
v/c Ratio	0.04	0.22		0.83	0.36			0.05	0.67		0.04		
Uniform Delay, d1	39.7	34.4		19.7	10.1			31.2	34.9		31.1		
Progression Factor	1.00	1.00		1.00	1.00			1.00	1.00		1.00		
Incremental Delay, d2	0.0	0.2		3.5	0.1			0.1	3.7		0.1		
Delay (s)	39.8	34.6		23.2	10.2			31.2	38.5		31.2		
Level of Service	D	C		C	B			C	D		C		
Approach Delay (s)		34.8			18.7			38.2			31.2		
Approach LOS		C			B			D			C		
Intersection Summary													
HCM 2000 Control Delay			21.9		HCM 2000 Level of Service					C			
HCM 2000 Volume to Capacity ratio			0.69										
Actuated Cycle Length (s)			89.9		Sum of lost time (s)					18.0			
Intersection Capacity Utilization			55.6%		ICU Level of Service					B			
Analysis Period (min)			15										
























c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2023 Existing Conditions Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↘↗
Traffic Volume (vph)	0	252	114	154	969	0	0	0	0	555	0	802
Future Volume (vph)	0	252	114	154	969	0	0	0	0	555	0	802
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		5981	1419	2918	3455					3467		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		5981	1419	2918	3455					3467		2814
Peak-hour factor, PHF	0.80	0.80	0.80	0.80	0.80	0.80	0.92	0.92	0.92	0.75	0.75	0.75
Adj. Flow (vph)	0	315	142	192	1211	0	0	0	0	740	0	1069
RTOR Reduction (vph)	0	0	97	0	0	0	0	0	0	0	0	117
Lane Group Flow (vph)	0	315	46	193	1211	0	0	0	0	740	0	952
Heavy Vehicles (%)	0%	2%	10%	12%	1%	0%	2%	2%	2%	1%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		32.7	32.7	25.0	63.7					25.0		25.0
Effective Green, g (s)		32.7	32.7	25.0	63.7					25.0		25.0
Actuated g/C Ratio		0.32	0.32	0.25	0.63					0.25		0.25
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		1942	460	724	2185					860		698
v/s Ratio Prot		0.05	0.03	0.07	c0.35					0.21		c0.34
v/s Ratio Perm												
v/c Ratio		0.16	0.10	0.27	0.55					0.86		1.36
Uniform Delay, d1		24.2	23.7	30.5	10.5					36.2		37.9
Progression Factor		1.00	1.00	0.88	1.62					1.00		1.00
Incremental Delay, d2		0.1	0.2	0.1	0.3					9.5		172.7
Delay (s)		24.3	23.9	26.8	17.2					45.7		210.6
Level of Service		C	C	C	B					D		F
Approach Delay (s)		24.2			18.5			0.0			143.2	
Approach LOS		C			B			A			F	
Intersection Summary												
HCM 2000 Control Delay			80.7			HCM 2000 Level of Service				F		
HCM 2000 Volume to Capacity ratio			0.84									
Actuated Cycle Length (s)			100.7			Sum of lost time (s)				18.0		
Intersection Capacity Utilization			64.8%			ICU Level of Service				C		
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2023 Existing Conditions Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	 	 			  		 		 			
Traffic Volume (vph)	110	697	0	0	372	76	751	0	359	0	0	0
Future Volume (vph)	110	697	0	0	372	76	751	0	359	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Fr _t	1.00	1.00			0.97		1.00		0.85			
Fl _t Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3113	3421			4932		3433		2733			
Fl _t Permitted	0.45	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	1462	3421			4932		3433		2733			
Peak-hour factor, PHF	0.87	0.87	0.87	0.85	0.85	0.85	0.78	0.78	0.78	0.92	0.92	0.92
Adj. Flow (vph)	126	801	0	0	438	89	963	0	460	0	0	0
RTOR Reduction (vph)	0	0	0	0	27	0	0	0	346	0	0	0
Lane Group Flow (vph)	126	801	0	0	500	0	963	0	114	0	0	0
Heavy Vehicles (%)	5%	2%	0%	0%	2%	5%	2%	2%	4%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	49.7	32.7			40.7		25.0		25.0			
Effective Green, g (s)	49.7	32.7			40.7		25.0		25.0			
Actuated g/C Ratio	0.49	0.32			0.40		0.25		0.25			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	1000	1110			1993		852		678			
v/s Ratio Prot	c0.02	c0.23			c0.10		c0.28		0.04			
v/s Ratio Perm	0.04											
v/c Ratio	0.13	0.72			0.25		1.13		0.17			
Uniform Delay, d ₁	13.5	30.0			19.9		37.9		29.7			
Progression Factor	1.16	1.31			1.00		1.00		1.00			
Incremental Delay, d ₂	0.1	2.2			0.1		73.3		0.2			
Delay (s)	15.7	41.5			20.0		111.1		29.9			
Level of Service	B	D			C		F		C			
Approach Delay (s)		38.0			20.0		84.9				0.0	
Approach LOS		D			C		F				A	
Intersection Summary												
HCM 2000 Control Delay			57.9				HCM 2000 Level of Service			E		
HCM 2000 Volume to Capacity ratio			0.67									
Actuated Cycle Length (s)			100.7				Sum of lost time (s)			18.0		
Intersection Capacity Utilization			64.8%				ICU Level of Service			C		
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2023 Existing Conditions Weekday AM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	608	1990	717	536	148	175
Future Volume (vph)	608	1990	717	536	148	175
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3471	3343	1583	1719	1538
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3471	3343	1583	1719	1538
Peak-hour factor, PHF	0.86	0.86	0.96	0.96	0.76	0.76
Adj. Flow (vph)	707	2314	747	558	195	230
RTOR Reduction (vph)	0	0	0	388	0	179
Lane Group Flow (vph)	707	2314	747	170	195	51
Heavy Vehicles (%)	1%	4%	8%	2%	5%	5%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	9.9	33.9	18.0	18.0	13.1	13.1
Effective Green, g (s)	9.9	33.9	18.0	18.0	13.1	13.1
Actuated g/C Ratio	0.17	0.57	0.31	0.31	0.22	0.22
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	299	1994	1019	482	381	341
v/s Ratio Prot	c0.40	c0.67	0.22		c0.11	0.03
v/s Ratio Perm				0.11		
v/c Ratio	2.36	1.16	0.73	0.35	0.51	0.15
Uniform Delay, d1	24.6	12.6	18.3	16.0	20.1	18.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	624.3	78.2	4.7	2.0	1.5	0.3
Delay (s)	648.9	90.8	23.0	18.0	21.7	18.7
Level of Service	F	F	C	B	C	B
Approach Delay (s)		221.4	20.9		20.1	
Approach LOS		F	C		C	
Intersection Summary						
HCM 2000 Control Delay			148.3		HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio			1.31			
Actuated Cycle Length (s)			59.0		Sum of lost time (s)	18.0
Intersection Capacity Utilization			76.9%		ICU Level of Service	D
Analysis Period (min)			15			
c Critical Lane Group						

201: International Drive & Corporate Drive
 2023 Existing Conditions Weekday AM Peak

Intersection	
Intersection Delay, s/veh	115.4
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↶	↷		↶	↷	↶	↶	↷		↶	↷	↶
Traffic Vol, veh/h	68	43	30	14	13	71	8	99	63	573	440	134
Future Vol, veh/h	68	43	30	14	13	71	8	99	63	573	440	134
Peak Hour Factor	0.76	0.76	0.76	0.78	0.78	0.78	0.83	0.83	0.83	0.76	0.76	0.76
Heavy Vehicles, %	0	4	5	0	13	18	0	0	3	2	0	0
Mvmt Flow	89	57	39	18	17	91	10	119	76	754	579	176
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	14.2	13.5	13.7	150.1
HCM LOS	B	B	B	F

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	34%	0%	59%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	66%	0%	41%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	8	66	96	68	73	14	13	71	573	440	134
LT Vol	8	0	0	68	0	14	0	0	573	0	0
Through Vol	0	66	33	0	43	0	13	0	0	440	0
RT Vol	0	0	63	0	30	0	0	71	0	0	134
Lane Flow Rate	10	80	116	89	96	18	17	91	754	579	176
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.024	0.185	0.256	0.225	0.222	0.046	0.042	0.213	1.468	1.04	0.282
Departure Headway (Hd)	9.296	8.789	8.375	9.319	8.6	9.688	9.406	8.786	7.111	6.572	5.865
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	387	411	431	387	420	372	383	411	520	556	617
Service Time	6.996	6.489	6.075	7.019	6.3	7.388	7.106	6.486	4.811	4.272	3.565
HCM Lane V/C Ratio	0.026	0.195	0.269	0.23	0.229	0.048	0.044	0.221	1.45	1.041	0.285
HCM Control Delay	12.2	13.5	13.9	14.7	13.7	12.9	12.5	13.8	240.8	74.5	10.9
HCM Lane LOS	B	B	B	B	B	B	B	B	F	F	B
HCM 95th-tile Q	0.1	0.7	1	0.9	0.8	0.1	0.1	0.8	37.1	16	1.2

202: Goose Bay Drive & Corporate Drive
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	433	246	22	79	19	0
Future Vol, veh/h	433	246	22	79	19	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	71	71	69	69
Heavy Vehicles, %	1	5	0	12	36	0
Mvmt Flow	555	315	31	111	28	0

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	870	0	886 713
Stage 1	-	-	-	-	713 -
Stage 2	-	-	-	-	173 -
Critical Hdwy	-	-	4.1	-	6.76 6.2
Critical Hdwy Stg 1	-	-	-	-	5.76 -
Critical Hdwy Stg 2	-	-	-	-	5.76 -
Follow-up Hdwy	-	-	2.2	-	3.824 3.3
Pot Cap-1 Maneuver	-	-	783	-	275 435
Stage 1	-	-	-	-	429 -
Stage 2	-	-	-	-	781 -
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	783	-	263 435
Mov Cap-2 Maneuver	-	-	-	-	263 -
Stage 1	-	-	-	-	429 -
Stage 2	-	-	-	-	748 -

Approach	EB	WB	NB
HCM Control Delay, s	0	2.1	20.3
HCM LOS			C

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	263	-	-	783	-
HCM Lane V/C Ratio	0.105	-	-	0.04	-
HCM Control Delay (s)	20.3	-	-	9.8	0
HCM Lane LOS	C	-	-	A	A
HCM 95th %tile Q(veh)	0.3	-	-	0.1	-

203: Corporate Drive & Redhook Way
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	17	418	82	2	0	6
Future Vol, veh/h	17	418	82	2	0	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	85	85	71	71	50	50
Heavy Vehicles, %	0	1	8	0	0	25
Mvmt Flow	20	492	115	3	0	12

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	118	0	-	0	649 117
Stage 1	-	-	-	-	117 -
Stage 2	-	-	-	-	532 -
Critical Hdwy	4.1	-	-	-	6.4 6.45
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.2	-	-	-	3.5 3.525
Pot Cap-1 Maneuver	1483	-	-	-	438 876
Stage 1	-	-	-	-	913 -
Stage 2	-	-	-	-	593 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	1483	-	-	-	432 876
Mov Cap-2 Maneuver	-	-	-	-	432 -
Stage 1	-	-	-	-	901 -
Stage 2	-	-	-	-	593 -

Approach	EB	WB	SB
HCM Control Delay, s	0.3	0	9.2
HCM LOS			A

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	1483	-	-	-	876
HCM Lane V/C Ratio	0.013	-	-	-	0.014
HCM Control Delay (s)	7.5	-	-	-	9.2
HCM Lane LOS	A	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	0

204: Goose Bay Drive & Corporate Drive
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	1.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	222	7	7	102	9	5
Future Vol, veh/h	222	7	7	102	9	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	95	95	82	82	25	40
Heavy Vehicles, %	1	0	0	5	20	0
Mvmt Flow	234	7	9	124	36	13

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	241	0	380
Stage 1	-	-	-	-	238
Stage 2	-	-	-	-	142
Critical Hdwy	-	-	4.1	-	6.6
Critical Hdwy Stg 1	-	-	-	-	5.6
Critical Hdwy Stg 2	-	-	-	-	5.6
Follow-up Hdwy	-	-	2.2	-	3.68
Pot Cap-1 Maneuver	-	-	1337	-	588
Stage 1	-	-	-	-	761
Stage 2	-	-	-	-	843
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1337	-	584
Mov Cap-2 Maneuver	-	-	-	-	584
Stage 1	-	-	-	-	761
Stage 2	-	-	-	-	837

Approach	EB	WB	NB
HCM Control Delay, s	0	0.5	11.2
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	629	-	-	1337	-
HCM Lane V/C Ratio	0.077	-	-	0.006	-
HCM Control Delay (s)	11.2	-	-	7.7	0
HCM Lane LOS	B	-	-	A	A
HCM 95th %tile Q(veh)	0.2	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	1.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	14	13	6	8
Future Vol, veh/h	0	0	14	13	6	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	53	53	50	50
Heavy Vehicles, %	0	0	0	13	0	0
Mvmt Flow	0	0	26	25	12	16

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	79	39	0	0	51
Stage 1	39	-	-	-	-
Stage 2	40	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	929	1038	-	-	1568
Stage 1	989	-	-	-	-
Stage 2	988	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	922	1038	-	-	1568
Mov Cap-2 Maneuver	922	-	-	-	-
Stage 1	989	-	-	-	-
Stage 2	980	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	0	0	3.1
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	1568	-
HCM Lane V/C Ratio	-	-	0.008	-
HCM Control Delay (s)	-	-	0	7.3
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

206: Goose Bay Drive & Lonza South Dwy
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	1.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	6	0	0	8	27	8
Future Vol, veh/h	6	0	0	8	27	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	50	50	42	42	69	69
Heavy Vehicles, %	75	0	0	0	6	80
Mvmt Flow	12	0	0	19	39	12

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	64	45	51	0	0
Stage 1	45	-	-	-	-
Stage 2	19	-	-	-	-
Critical Hdwy	7.15	6.2	4.1	-	-
Critical Hdwy Stg 1	6.15	-	-	-	-
Critical Hdwy Stg 2	6.15	-	-	-	-
Follow-up Hdwy	4.175	3.3	2.2	-	-
Pot Cap-1 Maneuver	788	1031	1568	-	-
Stage 1	819	-	-	-	-
Stage 2	844	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	788	1031	1568	-	-
Mov Cap-2 Maneuver	788	-	-	-	-
Stage 1	819	-	-	-	-
Stage 2	844	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	9.6	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1568	-	788	-	-
HCM Lane V/C Ratio	-	-	0.015	-	-
HCM Control Delay (s)	0	-	9.6	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2023 Existing Conditions Weekday AM Peak

Intersection												
Int Delay, s/veh	0.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	5	19	0	0	52	216
Future Vol, veh/h	0	0	0	0	0	0	5	19	0	0	52	216
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	88	88	92	92	69	69
Heavy Vehicles, %	2	2	2	2	2	2	0	18	2	2	15	1
Mvmt Flow	0	0	0	0	0	0	6	22	0	0	75	313

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	266	266	232	266	422	22	388	0	0	22	0	0
Stage 1	232	232	-	34	34	-	-	-	-	-	-	-
Stage 2	34	34	-	232	388	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	687	640	807	687	523	1055	1182	-	-	1593	-	-
Stage 1	771	713	-	982	867	-	-	-	-	-	-	-
Stage 2	982	867	-	771	609	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	684	637	807	684	520	1055	1182	-	-	1593	-	-
Mov Cap-2 Maneuver	684	637	-	684	520	-	-	-	-	-	-	-
Stage 1	767	713	-	977	863	-	-	-	-	-	-	-
Stage 2	977	863	-	771	609	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		0		1.7		0	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1182	-	-	-	-	1593	-	-
HCM Lane V/C Ratio	0.005	-	-	-	-	-	-	-
HCM Control Delay (s)	8.1	0	-	0	0	0	-	-
HCM Lane LOS	A	A	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	6	2	156	13	13	430
Future Vol, veh/h	6	2	156	13	13	430
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	63	63	81	81	84	84
Heavy Vehicles, %	0	0	0	0	0	1
Mvmt Flow	10	3	193	16	15	512

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	743	201	0	0	209
Stage 1	201	-	-	-	-
Stage 2	542	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	386	845	-	-	1374
Stage 1	838	-	-	-	-
Stage 2	587	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	380	845	-	-	1374
Mov Cap-2 Maneuver	380	-	-	-	-
Stage 1	838	-	-	-	-
Stage 2	578	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.4	0	0.2
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	441	1374
HCM Lane V/C Ratio	-	-	0.029	0.011
HCM Control Delay (s)	-	-	13.4	7.7
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	14	19	150	13	20	416
Future Vol, veh/h	14	19	150	13	20	416
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	86	86	83	83
Heavy Vehicles, %	44	0	1	63	0	1
Mvmt Flow	16	22	174	15	24	501

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	731	182	0	0	189	0
Stage 1	182	-	-	-	-	-
Stage 2	549	-	-	-	-	-
Critical Hdwy	6.84	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.896	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	333	866	-	-	1397	-
Stage 1	758	-	-	-	-	-
Stage 2	503	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	325	866	-	-	1397	-
Mov Cap-2 Maneuver	325	-	-	-	-	-
Stage 1	758	-	-	-	-	-
Stage 2	491	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	12.7	0	0.3
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	508	1397
HCM Lane V/C Ratio	-	-	0.074	0.017
HCM Control Delay (s)	-	-	12.7	7.6
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.2	0.1

210: International Drive & Lonza South Driveway
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	5	183	2	8	331
Future Vol, veh/h	0	5	183	2	8	331
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	75	75	89	89	81	81
Heavy Vehicles, %	0	0	5	100	0	2
Mvmt Flow	0	7	206	2	10	409

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	636	207	0	0	208
Stage 1	207	-	-	-	-
Stage 2	429	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	445	839	-	-	1375
Stage 1	832	-	-	-	-
Stage 2	661	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	441	839	-	-	1375
Mov Cap-2 Maneuver	441	-	-	-	-
Stage 1	832	-	-	-	-
Stage 2	655	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	9.3	0	0.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	839	1375
HCM Lane V/C Ratio	-	-	0.008	0.007
HCM Control Delay (s)	-	-	9.3	7.6
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2023 Existing Conditions Weekday AM Peak

Intersection												
Int Delay, s/veh	7.2											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔			↔			↔	
Traffic Vol, veh/h	8	9	2	84	5	6	0	392	383	25	269	28
Future Vol, veh/h	8	9	2	84	5	6	0	392	383	25	269	28
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	75	75	75	65	65	65	90	90	90	87	87	87
Heavy Vehicles, %	20	0	0	4	0	0	0	2	3	0	3	0
Mvmt Flow	11	12	3	129	8	9	0	436	426	29	309	32

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1041	1245	325	1040	1048	649	341	0	0	862	0	0
Stage 1	383	383	-	649	649	-	-	-	-	-	-	-
Stage 2	658	862	-	391	399	-	-	-	-	-	-	-
Critical Hdwy	7.3	6.5	6.2	7.14	6.5	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.68	4	3.3	3.536	4	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	193	176	721	207	230	473	1229	-	-	789	-	-
Stage 1	605	616	-	455	469	-	-	-	-	-	-	-
Stage 2	425	375	-	629	606	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	178	168	721	188	219	473	1229	-	-	789	-	-
Mov Cap-2 Maneuver	178	168	-	188	219	-	-	-	-	-	-	-
Stage 1	605	588	-	455	469	-	-	-	-	-	-	-
Stage 2	410	375	-	586	578	-	-	-	-	-	-	-

Approach	EB		WB		NB			SB		
HCM Control Delay, s	27.1		62.5		0			0.8		
HCM LOS	D		F							

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1229	-	-	188	197	789	-	-
HCM Lane V/C Ratio	-	-	-	0.135	0.742	0.036	-	-
HCM Control Delay (s)	0	-	-	27.1	62.5	9.7	0	-
HCM Lane LOS	A	-	-	D	F	A	A	-
HCM 95th %tile Q(veh)	0	-	-	0.5	4.9	0.1	-	-

212: Corporate Dr & Grafton Rd
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	60					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	794	348	47	14	54	213
Future Vol, veh/h	794	348	47	14	54	213
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	93	93	70	70	90	90
Heavy Vehicles, %	1	1	3	11	0	4
Mvmt Flow	854	374	67	20	60	237

Major/Minor	Minor2	Major1	Major2		
Conflicting Flow All	214	60	297	0	-
Stage 1	60	-	-	-	-
Stage 2	154	-	-	-	-
Critical Hdwy	6.41	6.21	4.13	-	-
Critical Hdwy Stg 1	5.41	-	-	-	-
Critical Hdwy Stg 2	5.41	-	-	-	-
Follow-up Hdwy	3.509	3.309	2.227	-	-
Pot Cap-1 Maneuver	~ 777	1008	1259	-	-
Stage 1	965	-	-	-	-
Stage 2	877	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	~ 736	1008	1259	-	-
Mov Cap-2 Maneuver	~ 736	-	-	-	-
Stage 1	914	-	-	-	-
Stage 2	877	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	78.3	6.2	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1259	-	736	1008	-	-
HCM Lane V/C Ratio	0.053	-	1.16	0.371	-	-
HCM Control Delay (s)	8	-	107.9	10.7	-	-
HCM Lane LOS	A	-	F	B	-	-
HCM 95th %tile Q(veh)	0.2	-	26.7	1.7	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2023 Existing Conditions Weekday AM Peak

Intersection						
Int Delay, s/veh	67.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↖↗
Traffic Vol, veh/h	0	199	1144	0	0	323
Future Vol, veh/h	0	199	1144	0	0	323
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	76	76	70	70	80	80
Heavy Vehicles, %	2	3	2	2	2	4
Mvmt Flow	0	262	1634	0	0	404




















Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	- 1634	0	- - -
Stage 1	-	-	- - -
Stage 2	-	-	- - -
Critical Hdwy	- 6.245	-	- - -
Critical Hdwy Stg 1	-	-	- - -
Critical Hdwy Stg 2	-	-	- - -
Follow-up Hdwy	-3.3285	-	- - -
Pot Cap-1 Maneuver	0 ~ 123	-	0 0 -
Stage 1	0	-	0 0 -
Stage 2	0	-	0 0 -
Platoon blocked, %		-	-
Mov Cap-1 Maneuver	- ~ 123	-	- - -
Mov Cap-2 Maneuver	-	-	- - -
Stage 1	-	-	- - -
Stage 2	-	-	- - -

Approach	WB	NB	SB
HCM Control Delay, s	\$ 592.5	0	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 123	-
HCM Lane V/C Ratio	- 2.129	-
HCM Control Delay (s)	-\$ 592.5	-
HCM Lane LOS	- F	-
HCM 95th %tile Q(veh)	- 21.8	-













Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

101: International Dr & Pease Blvd
 2023 Existing Conditions Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	0	420	3	287	160	24	11	3	1200	56	3	3
Future Volume (vph)	0	420	3	287	160	24	11	3	1200	56	3	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor		0.95		0.97	0.95			1.00	0.88		1.00	
Frt		1.00		1.00	0.98			1.00	0.85		0.99	
Flt Protected		1.00		0.95	1.00			0.96	1.00		0.96	
Satd. Flow (prot)		3571		3433	3539			1766	2814		2047	
Flt Permitted		1.00		0.95	1.00			0.83	1.00		0.74	
Satd. Flow (perm)		3571		3433	3539			1529	2814		1594	
Peak-hour factor, PHF	0.88	0.88	0.88	0.96	0.96	0.96	0.91	0.91	0.91	0.68	0.68	0.68
Adj. Flow (vph)	0	477	3	299	167	25	12	3	1319	82	4	4
RTOR Reduction (vph)	0	0	0	0	7	0	0	0	0	0	1	0
Lane Group Flow (vph)	0	480	0	299	185	0	0	15	1319	0	89	0
Heavy Vehicles (%)	0%	1%	0%	2%	0%	0%	0%	0%	1%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8		4		4
Permitted Phases							8		8		4	
Actuated Green, G (s)		13.9		11.6	31.5			20.1	20.1		20.1	
Effective Green, g (s)		13.9		11.6	31.5			20.1	20.1		20.1	
Actuated g/C Ratio		0.22		0.18	0.50			0.32	0.32		0.32	
Clearance Time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)		3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)		780		626	1752			483	889		503	
v/s Ratio Prot		c0.13		c0.09	0.05							
v/s Ratio Perm								0.01	c0.47		0.06	
v/c Ratio		0.62		0.48	0.11			0.03	1.48		0.18	
Uniform Delay, d1		22.4		23.3	8.5			15.0	21.8		15.8	
Progression Factor		1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d2		1.5		0.6	0.0			0.0	223.7		0.2	
Delay (s)		23.9		23.9	8.6			15.0	245.5		15.9	
Level of Service		C		C	A			B	F		B	
Approach Delay (s)		23.9			17.9			242.9			15.9	
Approach LOS		C			B			F			B	
Intersection Summary												
HCM 2000 Control Delay			144.3			HCM 2000 Level of Service			F			
HCM 2000 Volume to Capacity ratio			0.96									
Actuated Cycle Length (s)			63.6			Sum of lost time (s)			18.0			
Intersection Capacity Utilization			73.7%			ICU Level of Service			D			
Analysis Period (min)			15									
























c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2023 Existing Conditions Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↘↗
Traffic Volume (vph)	0	1091	585	671	453	0	0	0	0	381	0	139
Future Volume (vph)	0	1091	585	671	453	0	0	0	0	381	0	139
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		6040	1546	3236	3455					3502		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		6040	1546	3236	3455					3502		2814
Peak-hour factor, PHF	0.85	0.85	0.85	0.94	0.94	0.94	0.92	0.92	0.92	0.90	0.90	0.90
Adj. Flow (vph)	0	1284	688	714	482	0	0	0	0	423	0	154
RTOR Reduction (vph)	0	0	364	0	0	0	0	0	0	0	0	118
Lane Group Flow (vph)	0	1284	324	714	482	0	0	0	0	423	0	36
Heavy Vehicles (%)	0%	1%	1%	1%	1%	0%	0%	0%	0%	0%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		35.0	35.0	25.0	61.4					23.8		23.8
Effective Green, g (s)		35.0	35.0	25.0	61.4					23.8		23.8
Actuated g/C Ratio		0.34	0.34	0.25	0.60					0.23		0.23
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2076	531	794	2083					818		657
v/s Ratio Prot		c0.21	0.21	c0.22	0.14					c0.12		0.01
v/s Ratio Perm												
v/c Ratio		0.62	0.61	0.90	0.23					0.52		0.05
Uniform Delay, d1		27.8	27.7	37.2	9.3					34.0		30.3
Progression Factor		1.00	1.00	1.37	1.08					1.00		1.00
Incremental Delay, d2		0.8	2.9	10.0	0.1					1.1		0.1
Delay (s)		28.6	30.6	61.0	10.2					35.1		30.3
Level of Service		C	C	E	B					D		C
Approach Delay (s)		29.3			40.5			0.0			33.8	
Approach LOS		C			D			A			C	
Intersection Summary												
HCM 2000 Control Delay			33.6			HCM 2000 Level of Service					C	
HCM 2000 Volume to Capacity ratio			0.67									
Actuated Cycle Length (s)			101.8			Sum of lost time (s)					18.0	
Intersection Capacity Utilization			81.2%			ICU Level of Service					D	
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2023 Existing Conditions Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	 	 			  		 		 			
Traffic Volume (vph)	659	813	0	0	902	399	222	0	613	0	0	0
Future Volume (vph)	659	813	0	0	902	399	222	0	613	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.95		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3236	3455			4914		3433		2814			
Flt Permitted	0.11	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	389	3455			4914		3433		2814			
Peak-hour factor, PHF	0.87	0.87	0.92	0.90	0.90	0.90	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	757	934	0	0	1002	443	236	0	652	0	0	0
RTOR Reduction (vph)	0	0	0	0	75	0	0	0	500	0	0	0
Lane Group Flow (vph)	757	934	0	0	1370	0	236	0	152	0	0	0
Heavy Vehicles (%)	1%	1%	0%	0%	1%	0%	2%	0%	1%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	58.6	35.0			36.4		23.8		23.8			
Effective Green, g (s)	58.6	35.0			36.4		23.8		23.8			
Actuated g/C Ratio	0.58	0.34			0.36		0.23		0.23			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	883	1187			1757		802		657			
v/s Ratio Prot	c0.20	0.27			0.28		c0.07		0.05			
v/s Ratio Perm	c0.29											
v/c Ratio	0.86	0.79			0.78		0.29		0.23			
Uniform Delay, d1	26.5	30.0			29.1		32.1		31.6			
Progression Factor	1.68	0.56			1.00		1.00		1.00			
Incremental Delay, d2	7.1	3.3			2.6		0.4		0.4			
Delay (s)	51.5	20.1			31.8		32.5		32.0			
Level of Service	D	C			C		C		C			
Approach Delay (s)		34.1			31.8			32.1			0.0	
Approach LOS		C			C			C			A	
Intersection Summary												
HCM 2000 Control Delay			32.8		HCM 2000 Level of Service				C			
HCM 2000 Volume to Capacity ratio			0.68									
Actuated Cycle Length (s)			101.8		Sum of lost time (s)				18.0			
Intersection Capacity Utilization			81.2%		ICU Level of Service				D			
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2023 Existing Conditions Weekday PM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	303	1620	1258	202	375	806
Future Volume (vph)	303	1620	1258	202	375	806
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3539	3539	1583	1787	1599
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3539	3539	1583	1787	1599
Peak-hour factor, PHF	0.88	0.88	0.93	0.93	0.87	0.87
Adj. Flow (vph)	344	1841	1353	217	431	926
RTOR Reduction (vph)	0	0	0	151	0	166
Lane Group Flow (vph)	344	1841	1353	66	431	760
Heavy Vehicles (%)	1%	2%	2%	2%	1%	1%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	5.0	29.0	18.0	18.0	18.0	18.0
Effective Green, g (s)	5.0	29.0	18.0	18.0	18.0	18.0
Actuated g/C Ratio	0.08	0.49	0.31	0.31	0.31	0.31
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	151	1739	1079	482	545	487
v/s Ratio Prot	c0.19	0.52	c0.38		0.24	c0.48
v/s Ratio Perm				0.04		
v/c Ratio	2.28	1.06	1.25	0.14	0.79	1.56
Uniform Delay, d1	27.0	15.0	20.5	14.9	18.8	20.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	595.7	39.0	122.0	0.6	8.1	262.1
Delay (s)	622.7	54.0	142.5	15.5	26.9	282.6
Level of Service	F	D	F	B	C	F
Approach Delay (s)		143.6	124.9		201.4	
Approach LOS		F	F		F	
Intersection Summary						
HCM 2000 Control Delay			153.2		HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio			1.51			
Actuated Cycle Length (s)			59.0		Sum of lost time (s)	18.0
Intersection Capacity Utilization			94.7%		ICU Level of Service	F
Analysis Period (min)			15			
c Critical Lane Group						

201: International Drive & Corporate Drive
 2023 Existing Conditions Weekday PM Peak

Intersection	
Intersection Delay, s/veh	95.7
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↶	↷		↶	↷	↶	↶	↷		↶	↷	↶
Traffic Vol, veh/h	137	4	15	9	24	487	15	555	7	60	88	85
Future Vol, veh/h	137	4	15	9	24	487	15	555	7	60	88	85
Peak Hour Factor	0.84	0.84	0.84	0.77	0.77	0.77	0.89	0.89	0.89	0.93	0.93	0.93
Heavy Vehicles, %	0	0	0	0	6	1	0	1	0	4	3	0
Mvmt Flow	163	5	18	12	31	632	17	624	8	65	95	91
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	19.9	191.8	48.3	15.6
HCM LOS	C	F	E	C

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	96%	0%	21%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	4%	0%	79%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	15	370	192	137	19	9	24	487	60	88	85
LT Vol	15	0	0	137	0	9	0	0	60	0	0
Through Vol	0	370	185	0	4	0	24	0	0	88	0
RT Vol	0	0	7	0	15	0	0	487	0	0	85
Lane Flow Rate	17	416	216	163	23	12	31	632	65	95	91
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.041	0.953	0.492	0.442	0.055	0.029	0.075	1.374	0.176	0.245	0.218
Departure Headway (Hd)	9.567	9.069	9.026	10.281	9.228	9.02	8.617	7.822	10.805	10.267	9.486
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	377	403	401	352	390	397	416	468	334	352	381
Service Time	7.267	6.769	6.726	7.981	6.928	6.765	6.362	5.567	8.505	7.967	7.186
HCM Lane V/C Ratio	0.045	1.032	0.539	0.463	0.059	0.03	0.075	1.35	0.195	0.27	0.239
HCM Control Delay	12.7	64.4	20.2	20.9	12.5	12	12.1	204	15.8	16.3	14.8
HCM Lane LOS	B	F	C	C	B	B	B	F	C	C	B
HCM 95th-tile Q	0.1	10.8	2.6	2.2	0.2	0.1	0.2	29.4	0.6	0.9	0.8

202: Goose Bay Drive & Corporate Drive
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	21.7					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	63	8	2	351	169	9
Future Vol, veh/h	63	8	2	351	169	9
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	70	70	73	73	40	40
Heavy Vehicles, %	4	0	0	2	0	0
Mvmt Flow	90	11	3	481	423	23

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	101	0	583
Stage 1	-	-	-	-	96
Stage 2	-	-	-	-	487
Critical Hdwy	-	-	4.1	-	6.4
Critical Hdwy Stg 1	-	-	-	-	5.4
Critical Hdwy Stg 2	-	-	-	-	5.4
Follow-up Hdwy	-	-	2.2	-	3.5
Pot Cap-1 Maneuver	-	-	1504	-	478
Stage 1	-	-	-	-	933
Stage 2	-	-	-	-	622
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1504	-	477
Mov Cap-2 Maneuver	-	-	-	-	477
Stage 1	-	-	-	-	933
Stage 2	-	-	-	-	620

Approach	EB	WB	NB
HCM Control Delay, s	0	0	50.2
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	490	-	-	1504	-
HCM Lane V/C Ratio	0.908	-	-	0.002	-
HCM Control Delay (s)	50.2	-	-	7.4	0
HCM Lane LOS	F	-	-	A	A
HCM 95th %tile Q(veh)	10.4	-	-	0	-

203: Corporate Drive & Redhook Way
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	0.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	7	65	342	3	1	12
Future Vol, veh/h	7	65	342	3	1	12
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	63	63	77	77	36	36
Heavy Vehicles, %	40	0	0	1	0	11
Mvmt Flow	11	103	444	4	3	33

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	448	0	0	571	446
Stage 1	-	-	-	446	-
Stage 2	-	-	-	125	-
Critical Hdwy	4.5	-	-	6.4	6.31
Critical Hdwy Stg 1	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	5.4	-
Follow-up Hdwy	2.56	-	-	3.5	3.399
Pot Cap-1 Maneuver	938	-	-	486	594
Stage 1	-	-	-	649	-
Stage 2	-	-	-	906	-
Platoon blocked, %		-	-		
Mov Cap-1 Maneuver	938	-	-	480	594
Mov Cap-2 Maneuver	-	-	-	480	-
Stage 1	-	-	-	641	-
Stage 2	-	-	-	906	-

Approach	EB	WB	SB
HCM Control Delay, s	0.9	0	11.6
HCM LOS			B

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	938	-	-	-	583
HCM Lane V/C Ratio	0.012	-	-	-	0.062
HCM Control Delay (s)	8.9	-	-	-	11.6
HCM Lane LOS	A	-	-	-	B
HCM 95th %tile Q(veh)	0	-	-	-	0.2

204: Goose Bay Drive & Corporate Drive
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	73	1	5	189	12	11
Future Vol, veh/h	73	1	5	189	12	11
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	81	81	71	71
Heavy Vehicles, %	0	0	0	1	11	0
Mvmt Flow	94	1	6	233	17	15

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	95	0	340
Stage 1	-	-	-	-	95
Stage 2	-	-	-	-	245
Critical Hdwy	-	-	4.1	-	6.51
Critical Hdwy Stg 1	-	-	-	-	5.51
Critical Hdwy Stg 2	-	-	-	-	5.51
Follow-up Hdwy	-	-	2.2	-	3.599
Pot Cap-1 Maneuver	-	-	1512	-	638
Stage 1	-	-	-	-	907
Stage 2	-	-	-	-	775
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1512	-	635
Mov Cap-2 Maneuver	-	-	-	-	635
Stage 1	-	-	-	-	907
Stage 2	-	-	-	-	771

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	9.9
HCM LOS			A

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	760	-	-	1512	-
HCM Lane V/C Ratio	0.043	-	-	0.004	-
HCM Control Delay (s)	9.9	-	-	7.4	0
HCM Lane LOS	A	-	-	A	A
HCM 95th %tile Q(veh)	0.1	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	2.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	1	10	13	1	0	6
Future Vol, veh/h	1	10	13	1	0	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	67	67	69	69	50	50
Heavy Vehicles, %	0	0	10	0	0	0
Mvmt Flow	1	15	19	1	0	12

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	32	20	0	0	20
Stage 1	20	-	-	-	-
Stage 2	12	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	987	1064	-	-	1609
Stage 1	1008	-	-	-	-
Stage 2	1016	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	987	1064	-	-	1609
Mov Cap-2 Maneuver	987	-	-	-	-
Stage 1	1008	-	-	-	-
Stage 2	1016	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	8.5	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	1057	1609
HCM Lane V/C Ratio	-	-	0.016	-
HCM Control Delay (s)	-	-	8.5	0
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

206: Goose Bay Drive & Lonza South Dwy
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	2.3					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	3	0	0	7	14	0
Future Vol, veh/h	3	0	0	7	14	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	25	25	63	63	63	63
Heavy Vehicles, %	0	0	0	0	10	0
Mvmt Flow	12	0	0	11	22	0

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	33	22	22	0	0
Stage 1	22	-	-	-	-
Stage 2	11	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-
Pot Cap-1 Maneuver	986	1061	1607	-	-
Stage 1	1006	-	-	-	-
Stage 2	1017	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	986	1061	1607	-	-
Mov Cap-2 Maneuver	986	-	-	-	-
Stage 1	1006	-	-	-	-
Stage 2	1017	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	8.7	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1607	-	986	-	-
HCM Lane V/C Ratio	-	-	0.012	-	-
HCM Control Delay (s)	0	-	8.7	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2023 Existing Conditions Weekday PM Peak

Intersection												
Int Delay, s/veh	0											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	0	178	0	0	5	5
Future Vol, veh/h	0	0	0	0	0	0	0	178	0	0	5	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	39	39	92	92	67	67
Heavy Vehicles, %	2	2	2	2	2	2	0	0	2	2	0	0
Mvmt Flow	0	0	0	0	0	0	0	456	0	0	7	7

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	467	467	11	467	470	456	14	0	0	456	0	0
Stage 1	11	11	-	456	456	-	-	-	-	-	-	-
Stage 2	456	456	-	11	14	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	506	493	1070	506	492	604	1617	-	-	1105	-	-
Stage 1	1010	886	-	584	568	-	-	-	-	-	-	-
Stage 2	584	568	-	1010	884	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	506	493	1070	506	492	604	1617	-	-	1105	-	-
Mov Cap-2 Maneuver	506	493	-	506	492	-	-	-	-	-	-	-
Stage 1	1010	886	-	584	568	-	-	-	-	-	-	-
Stage 2	584	568	-	1010	884	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		0		0		0	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1617	-	-	-	-	1105	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	0	0	0	-	-
HCM Lane LOS	A	-	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	7	3	574	1	4	101
Future Vol, veh/h	7	3	574	1	4	101
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	78	78	76	76
Heavy Vehicles, %	0	0	1	0	0	4
Mvmt Flow	8	3	736	1	5	133

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	880	737	0	0	737	0
Stage 1	737	-	-	-	-	-
Stage 2	143	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	320	422	-	-	878	-
Stage 1	477	-	-	-	-	-
Stage 2	889	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	318	422	-	-	878	-
Mov Cap-2 Maneuver	318	-	-	-	-	-
Stage 1	477	-	-	-	-	-
Stage 2	884	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	15.9	0	0.3
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	343	878
HCM Lane V/C Ratio	-	-	0.033	0.006
HCM Control Delay (s)	-	-	15.9	9.1
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	6.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	W	T	T	T	T
Traffic Vol, veh/h	48	147	428	15	13	95
Future Vol, veh/h	48	147	428	15	13	95
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	72	72	67	67	81	81
Heavy Vehicles, %	14	0	1	46	0	3
Mvmt Flow	67	204	639	22	16	117

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	799	650	0	0	661	0
Stage 1	650	-	-	-	-	-
Stage 2	149	-	-	-	-	-
Critical Hdwy	6.54	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.54	-	-	-	-	-
Critical Hdwy Stg 2	5.54	-	-	-	-	-
Follow-up Hdwy	3.626	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	339	473	-	-	937	-
Stage 1	498	-	-	-	-	-
Stage 2	850	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	333	473	-	-	937	-
Mov Cap-2 Maneuver	333	-	-	-	-	-
Stage 1	498	-	-	-	-	-
Stage 2	835	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	26.7	0	1.1
HCM LOS	D		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	429	937
HCM Lane V/C Ratio	-	-	0.631	0.017
HCM Control Delay (s)	-	-	26.7	8.9
HCM Lane LOS	-	-	D	A
HCM 95th %tile Q(veh)	-	-	4.2	0.1

210: International Drive & Lonza South Driveway
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	4	351	0	0	161
Future Vol, veh/h	0	4	351	0	0	161
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	68	68	74	74
Heavy Vehicles, %	0	0	3	0	0	7
Mvmt Flow	0	16	516	0	0	218

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	734	516	0	0	516	0
Stage 1	516	-	-	-	-	-
Stage 2	218	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	390	563	-	-	1060	-
Stage 1	603	-	-	-	-	-
Stage 2	823	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	390	563	-	-	1060	-
Mov Cap-2 Maneuver	390	-	-	-	-	-
Stage 1	603	-	-	-	-	-
Stage 2	823	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	11.6	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	563	1060
HCM Lane V/C Ratio	-	-	0.028	-
HCM Control Delay (s)	-	-	11.6	0
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2023 Existing Conditions Weekday PM Peak

Intersection												
Int Delay, s/veh	86.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	27	20	3	279	19	20	1	265	101	3	443	12
Future Vol, veh/h	27	20	3	279	19	20	1	265	101	3	443	12
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	54	54	54	85	85	85	84	84	84	88	88	88
Heavy Vehicles, %	0	13	0	0	14	0	0	2	1	0	1	11
Mvmt Flow	50	37	6	328	22	24	1	315	120	3	503	14

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	916	953	510	915	900	375	517	0	0	435	0	0
Stage 1	516	516	-	377	377	-	-	-	-	-	-	-
Stage 2	400	437	-	538	523	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.63	6.2	7.1	6.64	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4.117	3.3	3.5	4.126	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	255	248	567	~256	266	676	1059	-	-	1135	-	-
Stage 1	546	517	-	649	595	-	-	-	-	-	-	-
Stage 2	630	561	-	531	511	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	230	247	567	~223	265	676	1059	-	-	1135	-	-
Mov Cap-2 Maneuver	230	247	-	~223	265	-	-	-	-	-	-	-
Stage 1	545	515	-	648	594	-	-	-	-	-	-	-
Stage 2	585	560	-	486	509	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	28.2		\$ 323		0		0.1	
HCM LOS	D		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1059	-	-	246	235	1135	-	-
HCM Lane V/C Ratio	0.001	-	-	0.376	1.592	0.003	-	-
HCM Control Delay (s)	8.4	0	-	28.2	\$ 323	8.2	0	-
HCM Lane LOS	A	A	-	D	F	A	A	-
HCM 95th %tile Q(veh)	0	-	-	1.7	23.4	0	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2023 Existing Conditions Weekday PM Peak

Intersection						
Int Delay, s/veh	34.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	307	72	199	45	24	718
Future Vol, veh/h	307	72	199	45	24	718
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	86	86	76	76	83	83
Heavy Vehicles, %	2	2	1	3	0	1
Mvmt Flow	357	84	262	59	29	865

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	612	29	894	0	0
Stage 1	29	-	-	-	-
Stage 2	583	-	-	-	-
Critical Hdwy	6.42	6.22	4.11	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.209	-	-
Pot Cap-1 Maneuver	456	1046	763	-	-
Stage 1	994	-	-	-	-
Stage 2	558	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	~ 300	1046	763	-	-
Mov Cap-2 Maneuver	~ 300	-	-	-	-
Stage 1	653	-	-	-	-
Stage 2	558	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	123.6	9.9	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	763	-	300	1046	-	-
HCM Lane V/C Ratio	0.343	-	1.19	0.08	-	-
HCM Control Delay (s)	12.2	-	150.6	8.7	-	-
HCM Lane LOS	B	-	F	A	-	-
HCM 95th %tile Q(veh)	1.5	-	15.7	0.3	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2023 Existing Conditions Weekday PM Peak





















Intersection						
Int Delay, s/veh	0.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↖↗
Traffic Vol, veh/h	0	55	505	0	0	1181
Future Vol, veh/h	0	55	505	0	0	1181
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	73	73	95	95	89	89
Heavy Vehicles, %	0	13	0	1	0	1
Mvmt Flow	0	75	532	0	0	1327

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	-	532	0	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Critical Hdwy	-	6.395	-	-	-	-
Critical Hdwy Stg 1	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-
Follow-up Hdwy	-	3.4235	-	-	-	-
Pot Cap-1 Maneuver	0	521	-	0	0	-
Stage 1	0	-	-	0	0	-
Stage 2	0	-	-	0	0	-
Platoon blocked, %			-			-
Mov Cap-1 Maneuver	-	521	-	-	-	-
Mov Cap-2 Maneuver	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.1	0	0
HCM LOS	B		













Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 521	-
HCM Lane V/C Ratio	- 0.145	-
HCM Control Delay (s)	- 13.1	-
HCM Lane LOS	- B	-
HCM 95th %tile Q(veh)	- 0.5	-

101: International Dr & Pease Blvd
 2025 No Build Condition Weekday AM Peak

													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	3	106	6	1189	642	132	8	5	275	6	2	2	
Future Volume (vph)	3	106	6	1189	642	132	8	5	275	6	2	2	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12	
Total Lost time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Lane Util. Factor	1.00	0.95		0.97	0.95			1.00	0.88		1.00		
Fr _t	1.00	0.99		1.00	0.97			1.00	0.85		0.97		
Fl _t Protected	0.95	1.00		0.95	1.00			0.97	1.00		0.97		
Satd. Flow (prot)	1805	3515		3467	3475			1783	2682		2035		
Fl _t Permitted	0.95	1.00		0.95	1.00			0.87	1.00		0.86		
Satd. Flow (perm)	1805	3515		3467	3475			1598	2682		1811		
Peak-hour factor, PHF	0.84	0.84	0.84	0.83	1.00	0.83	0.88	0.88	0.88	0.63	0.63	0.63	
Adj. Flow (vph)	4	126	7	1433	642	159	9	6	312	10	3	3	
RTOR Reduction (vph)	0	4	0	0	10	0	0	0	0	0	2	0	
Lane Group Flow (vph)	4	129	0	1433	791	0	0	15	313	0	14	0	
Heavy Vehicles (%)	0%	2%	0%	1%	1%	0%	0%	0%	6%	0%	0%	0%	
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA		
Protected Phases	6	2		1	5			8		4		4	
Permitted Phases							8		8		4		
Actuated Green, G (s)	5.8	13.0		46.0	54.2			15.7	15.7		15.7		
Effective Green, g (s)	5.8	13.0		46.0	54.2			15.7	15.7		15.7		
Actuated g/C Ratio	0.06	0.14		0.50	0.58			0.17	0.17		0.17		
Clearance Time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Vehicle Extension (s)	2.0	3.0		3.0	3.0			3.0	3.0		3.0		
Lane Grp Cap (vph)	112	492		1720	2031			270	454		306		
v/s Ratio Prot	0.00	c0.04		c0.41	c0.23								
v/s Ratio Perm								0.01	c0.12		0.01		
v/c Ratio	0.04	0.26		0.83	0.39			0.06	0.69		0.04		
Uniform Delay, d ₁	40.8	35.6		20.1	10.4			32.3	36.2		32.2		
Progression Factor	1.00	1.00		1.00	1.00			1.00	1.00		1.00		
Incremental Delay, d ₂	0.0	0.3		3.6	0.1			0.1	4.3		0.1		
Delay (s)	40.9	35.9		23.7	10.5			32.4	40.5		32.3		
Level of Service	D	D		C	B			C	D		C		
Approach Delay (s)		36.0			18.9			40.2			32.3		
Approach LOS		D			B			D			C		
Intersection Summary													
HCM 2000 Control Delay			22.4									HCM 2000 Level of Service	C
HCM 2000 Volume to Capacity ratio			0.71										
Actuated Cycle Length (s)			92.7									Sum of lost time (s)	18.0
Intersection Capacity Utilization			56.3%									ICU Level of Service	B
Analysis Period (min)			15										

c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2025 No Build Condition Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↘↗
Traffic Volume (vph)	0	271	116	157	1014	0	0	0	0	566	0	839
Future Volume (vph)	0	271	116	157	1014	0	0	0	0	566	0	839
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		5981	1419	2918	3455					3467		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		5981	1419	2918	3455					3467		2814
Peak-hour factor, PHF	0.80	0.80	0.80	0.80	0.80	0.80	0.92	0.92	0.92	0.75	0.75	0.75
Adj. Flow (vph)	0	339	145	196	1268	0	0	0	0	755	0	1119
RTOR Reduction (vph)	0	0	97	0	0	0	0	0	0	0	0	104
Lane Group Flow (vph)	0	339	48	196	1268	0	0	0	0	755	0	1015
Heavy Vehicles (%)	0%	2%	10%	12%	1%	0%	2%	2%	2%	1%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		33.3	33.3	25.0	64.3					25.0		25.0
Effective Green, g (s)		33.3	33.3	25.0	64.3					25.0		25.0
Actuated g/C Ratio		0.33	0.33	0.25	0.63					0.25		0.25
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		1966	466	720	2193					855		694
v/s Ratio Prot		0.06	0.03	0.07	c0.37					0.22		c0.36
v/s Ratio Perm												
v/c Ratio		0.17	0.10	0.27	0.58					0.88		1.46
Uniform Delay, d1		24.2	23.6	30.8	10.7					36.7		38.1
Progression Factor		1.00	1.00	0.90	1.58					1.00		1.00
Incremental Delay, d2		0.1	0.2	0.1	0.3					11.4		216.1
Delay (s)		24.3	23.8	27.7	17.2					48.2		254.2
Level of Service		C	C	C	B					D		F
Approach Delay (s)		24.1			18.6			0.0			171.2	
Approach LOS		C			B			A			F	
Intersection Summary												
HCM 2000 Control Delay			94.1			HCM 2000 Level of Service				F		
HCM 2000 Volume to Capacity ratio			0.88									
Actuated Cycle Length (s)			101.3			Sum of lost time (s)				18.0		
Intersection Capacity Utilization			67.4%			ICU Level of Service				C		
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2025 No Build Condition Weekday AM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	118	719	0	0	405	78	766	0	366	0	0	0	
Future Volume (vph)	118	719	0	0	405	78	766	0	366	0	0	0	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12	
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0				
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88				
Frt	1.00	1.00			0.98		1.00		0.85				
Flt Protected	0.95	1.00			1.00		0.95		1.00				
Satd. Flow (prot)	3113	3421			4938		3433		2733				
Flt Permitted	0.43	1.00			1.00		0.95		1.00				
Satd. Flow (perm)	1402	3421			4938		3433		2733				
Peak-hour factor, PHF	0.87	0.87	0.87	0.85	0.85	0.85	0.78	0.78	0.78	0.92	0.92	0.92	
Adj. Flow (vph)	136	826	0	0	476	92	982	0	469	0	0	0	
RTOR Reduction (vph)	0	0	0	0	25	0	0	0	353	0	0	0	
Lane Group Flow (vph)	136	826	0	0	543	0	982	0	116	0	0	0	
Heavy Vehicles (%)	5%	2%	0%	0%	2%	5%	2%	2%	4%	0%	0%	0%	
Turn Type	pm+pt	NA			NA		Prot		Prot				
Protected Phases	1	6			2		3		3				
Permitted Phases	6												
Actuated Green, G (s)	50.3	33.3			41.3		25.0		25.0				
Effective Green, g (s)	50.3	33.3			41.3		25.0		25.0				
Actuated g/C Ratio	0.50	0.33			0.41		0.25		0.25				
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0				
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0				
Lane Grp Cap (vph)	983	1124			2013		847		674				
v/s Ratio Prot	c0.02	c0.24			c0.11		c0.29		0.04				
v/s Ratio Perm	0.05												
v/c Ratio	0.14	0.73			0.27		1.16		0.17				
Uniform Delay, d1	13.4	30.1			20.0		38.1		30.0				
Progression Factor	1.14	1.29			1.00		1.00		1.00				
Incremental Delay, d2	0.1	2.3			0.2		84.8		0.3				
Delay (s)	15.4	41.2			20.1		122.9		30.3				
Level of Service	B	D			C		F		C				
Approach Delay (s)		37.6			20.1			93.0			0.0		
Approach LOS		D			C			F			A		
Intersection Summary													
HCM 2000 Control Delay			61.2		HCM 2000 Level of Service				E				
HCM 2000 Volume to Capacity ratio			0.69										
Actuated Cycle Length (s)			101.3		Sum of lost time (s)				18.0				
Intersection Capacity Utilization			67.4%		ICU Level of Service				C				
Analysis Period (min)			15										

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2025 No Build Condition Weekday AM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	620	2030	731	586	162	189
Future Volume (vph)	620	2030	731	586	162	189
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3471	3343	1583	1719	1538
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3471	3343	1583	1719	1538
Peak-hour factor, PHF	0.86	0.86	0.96	0.96	0.76	0.76
Adj. Flow (vph)	721	2360	761	610	213	249
RTOR Reduction (vph)	0	0	0	424	0	192
Lane Group Flow (vph)	721	2360	761	186	213	57
Heavy Vehicles (%)	1%	4%	8%	2%	5%	5%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	9.5	33.5	18.0	18.0	13.5	13.5
Effective Green, g (s)	9.5	33.5	18.0	18.0	13.5	13.5
Actuated g/C Ratio	0.16	0.57	0.31	0.31	0.23	0.23
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	287	1970	1019	482	393	351
v/s Ratio Prot	c0.40	c0.68	0.23		c0.12	0.04
v/s Ratio Perm				0.12		
v/c Ratio	2.51	1.20	0.75	0.39	0.54	0.16
Uniform Delay, d1	24.8	12.8	18.4	16.1	20.0	18.2
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	690.8	94.3	5.0	2.3	1.9	0.3
Delay (s)	715.5	107.1	23.4	18.5	21.9	18.5
Level of Service	F	F	C	B	C	B
Approach Delay (s)		249.4	21.2		20.1	
Approach LOS		F	C		C	

Intersection Summary

HCM 2000 Control Delay	164.2	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.36		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	80.6%	ICU Level of Service	D
Analysis Period (min)	15		
c Critical Lane Group			

201: International Drive & Corporate Drive
 2025 No Build Condition Weekday AM Peak

Intersection	
Intersection Delay, s/veh	124.5
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↶	↷		↶	↷	↶	↶	↷		↶	↷	↶
Traffic Vol, veh/h	69	44	31	14	13	73	8	101	64	585	449	137
Future Vol, veh/h	69	44	31	14	13	73	8	101	64	585	449	137
Peak Hour Factor	0.76	0.76	0.76	0.78	0.78	0.78	0.83	0.83	0.83	0.76	0.76	0.76
Heavy Vehicles, %	0	4	5	0	13	18	0	0	3	2	0	0
Mvmt Flow	91	58	41	18	17	94	10	122	77	770	591	180
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	14.3	13.7	13.8	162.3
HCM LOS	B	B	B	F

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	34%	0%	59%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	66%	0%	41%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	8	67	98	69	75	14	13	73	585	449	137
LT Vol	8	0	0	69	0	14	0	0	585	0	0
Through Vol	0	67	34	0	44	0	13	0	0	449	0
RT Vol	0	0	64	0	31	0	0	73	0	0	137
Lane Flow Rate	10	81	118	91	99	18	17	94	770	591	180
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.024	0.188	0.26	0.227	0.228	0.046	0.042	0.218	1.509	1.069	0.291
Departure Headway (Hd)	9.374	8.867	8.453	9.385	8.663	9.761	9.48	8.859	7.056	6.517	5.81
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	384	407	427	385	417	369	380	408	516	555	613
Service Time	7.074	6.567	6.153	7.085	6.363	7.461	7.18	6.559	4.843	4.304	3.597
HCM Lane V/C Ratio	0.026	0.199	0.276	0.236	0.237	0.049	0.045	0.23	1.492	1.065	0.294
HCM Control Delay	12.3	13.6	14.1	14.8	13.9	12.9	12.6	14	258.4	83.3	11
HCM Lane LOS	B	B	B	B	B	B	B	B	F	F	B
HCM 95th-tile Q	0.1	0.7	1	0.9	0.9	0.1	0.1	0.8	39.3	17.3	1.2

202: Goose Bay Drive & Corporate Drive
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	442	251	22	81	19	0
Future Vol, veh/h	442	251	22	81	19	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	71	71	69	69
Heavy Vehicles, %	1	5	0	12	36	0
Mvmt Flow	567	322	31	114	28	0

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	889	0	904 728
Stage 1	-	-	-	-	728 -
Stage 2	-	-	-	-	176 -
Critical Hdwy	-	-	4.1	-	6.76 6.2
Critical Hdwy Stg 1	-	-	-	-	5.76 -
Critical Hdwy Stg 2	-	-	-	-	5.76 -
Follow-up Hdwy	-	-	2.2	-	3.824 3.3
Pot Cap-1 Maneuver	-	-	771	-	268 427
Stage 1	-	-	-	-	422 -
Stage 2	-	-	-	-	779 -
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	771	-	256 427
Mov Cap-2 Maneuver	-	-	-	-	256 -
Stage 1	-	-	-	-	422 -
Stage 2	-	-	-	-	746 -

Approach	EB	WB	NB
HCM Control Delay, s	0	2.1	20.8
HCM LOS			C

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	256	-	-	771	-
HCM Lane V/C Ratio	0.108	-	-	0.04	-
HCM Control Delay (s)	20.8	-	-	9.9	0
HCM Lane LOS	C	-	-	A	A
HCM 95th %tile Q(veh)	0.4	-	-	0.1	-

203: Corporate Drive & Redhook Way
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	17	426	84	2	0	6
Future Vol, veh/h	17	426	84	2	0	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	85	85	71	71	50	50
Heavy Vehicles, %	0	1	8	0	0	25
Mvmt Flow	20	501	118	3	0	12

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	121	0	-	0	661 120
Stage 1	-	-	-	-	120 -
Stage 2	-	-	-	-	541 -
Critical Hdwy	4.1	-	-	-	6.4 6.45
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.2	-	-	-	3.5 3.525
Pot Cap-1 Maneuver	1479	-	-	-	431 873
Stage 1	-	-	-	-	910 -
Stage 2	-	-	-	-	588 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	1479	-	-	-	425 873
Mov Cap-2 Maneuver	-	-	-	-	425 -
Stage 1	-	-	-	-	897 -
Stage 2	-	-	-	-	588 -

Approach	EB	WB	SB
HCM Control Delay, s	0.3	0	9.2
HCM LOS			A

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	1479	-	-	-	873
HCM Lane V/C Ratio	0.014	-	-	-	0.014
HCM Control Delay (s)	7.5	-	-	-	9.2
HCM Lane LOS	A	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	0

204: Goose Bay Drive & Corporate Drive
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1.5					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	226	7	7	104	10	5
Future Vol, veh/h	226	7	7	104	10	5
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	95	95	82	82	25	40
Heavy Vehicles, %	1	0	0	5	20	0
Mvmt Flow	238	7	9	127	40	13

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	245	0	387
Stage 1	-	-	-	-	242
Stage 2	-	-	-	-	145
Critical Hdwy	-	-	4.1	-	6.6
Critical Hdwy Stg 1	-	-	-	-	5.6
Critical Hdwy Stg 2	-	-	-	-	5.6
Follow-up Hdwy	-	-	2.2	-	3.68
Pot Cap-1 Maneuver	-	-	1333	-	583
Stage 1	-	-	-	-	758
Stage 2	-	-	-	-	840
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1333	-	579
Mov Cap-2 Maneuver	-	-	-	-	579
Stage 1	-	-	-	-	758
Stage 2	-	-	-	-	834

Approach	EB	WB	NB
HCM Control Delay, s	0	0.5	11.3
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	620	-	-	1333	-
HCM Lane V/C Ratio	0.085	-	-	0.006	-
HCM Control Delay (s)	11.3	-	-	7.7	0
HCM Lane LOS	B	-	-	A	A
HCM 95th %tile Q(veh)	0.3	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2025 No Build Condition Weekday AM Peak

Intersection

Int Delay, s/veh 1.1

Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	15	13	6	8
Future Vol, veh/h	0	0	15	13	6	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	53	53	50	50
Heavy Vehicles, %	0	0	0	13	0	0
Mvmt Flow	0	0	28	25	12	16

Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	81	41	0
Stage 1	41	-	-
Stage 2	40	-	-
Critical Hdwy	6.4	6.2	-
Critical Hdwy Stg 1	5.4	-	-
Critical Hdwy Stg 2	5.4	-	-
Follow-up Hdwy	3.5	3.3	-
Pot Cap-1 Maneuver	926	1036	-
Stage 1	987	-	-
Stage 2	988	-	-
Platoon blocked, %			
Mov Cap-1 Maneuver	919	1036	-
Mov Cap-2 Maneuver	919	-	-
Stage 1	987	-	-
Stage 2	980	-	-

Approach	WB	NB	SB
HCM Control Delay, s	0	0	3.1
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	1566	-
HCM Lane V/C Ratio	-	-	0.008	-
HCM Control Delay (s)	-	-	0	7.3
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	-	0

206: Goose Bay Drive & Lonza South Dwy
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	6	0	0	8	28	8
Future Vol, veh/h	6	0	0	8	28	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	50	50	42	42	69	69
Heavy Vehicles, %	75	0	0	0	6	80
Mvmt Flow	12	0	0	19	41	12

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	66	47	53	0	0
Stage 1	47	-	-	-	-
Stage 2	19	-	-	-	-
Critical Hdwy	7.15	6.2	4.1	-	-
Critical Hdwy Stg 1	6.15	-	-	-	-
Critical Hdwy Stg 2	6.15	-	-	-	-
Follow-up Hdwy	4.175	3.3	2.2	-	-
Pot Cap-1 Maneuver	786	1028	1566	-	-
Stage 1	818	-	-	-	-
Stage 2	844	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	786	1028	1566	-	-
Mov Cap-2 Maneuver	786	-	-	-	-
Stage 1	818	-	-	-	-
Stage 2	844	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	9.7	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1566	-	786	-	-
HCM Lane V/C Ratio	-	-	0.015	-	-
HCM Control Delay (s)	0	-	9.7	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2025 No Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	0.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	5	19	0	0	53	220
Future Vol, veh/h	0	0	0	0	0	0	5	19	0	0	53	220
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	88	88	92	92	69	69
Heavy Vehicles, %	2	2	2	2	2	2	0	18	2	2	15	1
Mvmt Flow	0	0	0	0	0	0	6	22	0	0	77	319

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	271	271	237	271	430	22	396	0	0	22	0	0
Stage 1	237	237	-	34	34	-	-	-	-	-	-	-
Stage 2	34	34	-	237	396	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	682	636	802	682	518	1055	1174	-	-	1593	-	-
Stage 1	766	709	-	982	867	-	-	-	-	-	-	-
Stage 2	982	867	-	766	604	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	679	633	802	679	515	1055	1174	-	-	1593	-	-
Mov Cap-2 Maneuver	679	633	-	679	515	-	-	-	-	-	-	-
Stage 1	762	709	-	977	863	-	-	-	-	-	-	-
Stage 2	977	863	-	766	604	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		0		1.7		0	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1174	-	-	-	-	1593	-	-
HCM Lane V/C Ratio	0.005	-	-	-	-	-	-	-
HCM Control Delay (s)	8.1	0	-	0	0	0	-	-
HCM Lane LOS	A	A	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	6	2	159	13	13	439
Future Vol, veh/h	6	2	159	13	13	439
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	63	63	81	81	84	84
Heavy Vehicles, %	0	0	0	0	0	1
Mvmt Flow	10	3	196	16	15	523

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	757	204	0	0	212
Stage 1	204	-	-	-	-
Stage 2	553	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	378	842	-	-	1370
Stage 1	835	-	-	-	-
Stage 2	580	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	372	842	-	-	1370
Mov Cap-2 Maneuver	372	-	-	-	-
Stage 1	835	-	-	-	-
Stage 2	571	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.6	0	0.2
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	432	1370
HCM Lane V/C Ratio	-	-	0.029	0.011
HCM Control Delay (s)	-	-	13.6	7.7
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	R	T	R	L	T
Traffic Vol, veh/h	14	19	153	13	20	425
Future Vol, veh/h	14	19	153	13	20	425
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	86	86	83	83
Heavy Vehicles, %	44	0	1	63	0	1
Mvmt Flow	16	22	178	15	24	512

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	746	186	0	0	193
Stage 1	186	-	-	-	-
Stage 2	560	-	-	-	-
Critical Hdwy	6.84	6.2	-	-	4.1
Critical Hdwy Stg 1	5.84	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-
Follow-up Hdwy	3.896	3.3	-	-	2.2
Pot Cap-1 Maneuver	326	861	-	-	1392
Stage 1	754	-	-	-	-
Stage 2	497	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	318	861	-	-	1392
Mov Cap-2 Maneuver	318	-	-	-	-
Stage 1	754	-	-	-	-
Stage 2	485	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	12.8	0	0.3
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	499	1392
HCM Lane V/C Ratio	-	-	0.075	0.017
HCM Control Delay (s)	-	-	12.8	7.6
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.2	0.1

210: International Drive & Lonza South Driveway
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	0	5	187	2	8	338
Future Vol, veh/h	0	5	187	2	8	338
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	75	75	89	89	81	81
Heavy Vehicles, %	0	0	5	100	0	2
Mvmt Flow	0	7	210	2	10	417

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	648	211	0	0	212
Stage 1	211	-	-	-	-
Stage 2	437	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	438	834	-	-	1370
Stage 1	829	-	-	-	-
Stage 2	655	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	434	834	-	-	1370
Mov Cap-2 Maneuver	434	-	-	-	-
Stage 1	829	-	-	-	-
Stage 2	648	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	9.4	0	0.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	834	1370
HCM Lane V/C Ratio	-	-	0.008	0.007
HCM Control Delay (s)	-	-	9.4	7.6
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2025 No Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	11.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	8	9	2	86	5	6	0	461	391	26	295	29
Future Vol, veh/h	8	9	2	86	5	6	0	461	391	26	295	29
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	75	75	75	65	65	65	90	90	90	87	87	87
Heavy Vehicles, %	20	0	0	4	0	0	0	2	3	0	3	0
Mvmt Flow	11	12	3	132	8	9	0	512	434	30	339	33

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1154	1362	356	1152	1161	729	372	0	0	946	0	0
Stage 1	416	416	-	729	729	-	-	-	-	-	-	-
Stage 2	738	946	-	423	432	-	-	-	-	-	-	-
Critical Hdwy	7.3	6.5	6.2	7.14	6.5	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.68	4	3.3	3.536	4	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	160	149	693	173	197	426	1198	-	-	734	-	-
Stage 1	580	595	-	411	431	-	-	-	-	-	-	-
Stage 2	383	343	-	605	586	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	146	141	693	155	187	426	1198	-	-	734	-	-
Mov Cap-2 Maneuver	146	141	-	155	187	-	-	-	-	-	-	-
Stage 1	580	564	-	411	431	-	-	-	-	-	-	-
Stage 2	368	343	-	559	556	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	32.5		105.3		0		0.8	
HCM LOS	D		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1198	-	-	156	163	734	-	-
HCM Lane V/C Ratio	-	-	-	0.162	0.916	0.041	-	-
HCM Control Delay (s)	0	-	-	32.5	105.3	10.1	0	-
HCM Lane LOS	A	-	-	D	F	B	A	-
HCM 95th %tile Q(veh)	0	-	-	0.6	6.7	0.1	-	-

212: Corporate Dr & Grafton Rd
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	88.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	871	355	48	14	55	238
Future Vol, veh/h	871	355	48	14	55	238
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	93	93	70	70	90	90
Heavy Vehicles, %	1	1	3	11	0	4
Mvmt Flow	937	382	69	20	61	264

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	219	61	325	0	-	0
Stage 1	61	-	-	-	-	-
Stage 2	158	-	-	-	-	-
Critical Hdwy	6.41	6.21	4.13	-	-	-
Critical Hdwy Stg 1	5.41	-	-	-	-	-
Critical Hdwy Stg 2	5.41	-	-	-	-	-
Follow-up Hdwy	3.509	3.309	2.227	-	-	-
Pot Cap-1 Maneuver	~ 771	1007	1229	-	-	-
Stage 1	964	-	-	-	-	-
Stage 2	~ 873	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	~ 728	1007	1229	-	-	-
Mov Cap-2 Maneuver	~ 728	-	-	-	-	-
Stage 1	~ 910	-	-	-	-	-
Stage 2	~ 873	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	115.5	6.3	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1229	-	728	1007	-	-
HCM Lane V/C Ratio	0.056	-	1.286	0.379	-	-
HCM Control Delay (s)	8.1	-	158.2	10.7	-	-
HCM Lane LOS	A	-	F	B	-	-
HCM 95th %tile Q(veh)	0.2	-	35.9	1.8	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2025 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	103.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↕
Traffic Vol, veh/h	0	225	1206	0	0	351
Future Vol, veh/h	0	225	1206	0	0	351
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	76	76	70	70	80	80
Heavy Vehicles, %	2	3	2	2	2	4
Mvmt Flow	0	296	1723	0	0	439

Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	-	1723	0
Stage 1	-	-	-
Stage 2	-	-	-
Critical Hdwy	-	6.245	-
Critical Hdwy Stg 1	-	-	-
Critical Hdwy Stg 2	-	-	-
Follow-up Hdwy	-	3.3285	-
Pot Cap-1 Maneuver	0 ~ 109	-	0
Stage 1	0	-	0
Stage 2	0	-	0
Platoon blocked, %	-	-	-
Mov Cap-1 Maneuver	-	~ 109	-
Mov Cap-2 Maneuver	-	-	-
Stage 1	-	-	-
Stage 2	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	\$ 859.4	0	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 109	-
HCM Lane V/C Ratio	- 2.716	-
HCM Control Delay (s)	-\$ 859.4	-
HCM Lane LOS	- F	-
HCM 95th %tile Q(veh)	- 27.4	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon













101: International Dr & Pease Blvd
 2025 No Build Condition Weekday PM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	0	474	3	293	184	24	11	3	1225	57	3	3
Future Volume (vph)	0	474	3	293	184	24	11	3	1225	57	3	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor		0.95		0.97	0.95			1.00	0.88		1.00	
Fr _t		1.00		1.00	0.98			1.00	0.85		0.99	
Fl _t Protected		1.00		0.95	1.00			0.96	1.00		0.96	
Satd. Flow (prot)		3571		3433	3548			1766	2814		2047	
Fl _t Permitted		1.00		0.95	1.00			0.83	1.00		0.74	
Satd. Flow (perm)		3571		3433	3548			1526	2814		1587	
Peak-hour factor, PHF	0.88	0.88	0.88	0.96	0.96	0.96	0.91	0.91	0.91	0.68	0.68	0.68
Adj. Flow (vph)	0	539	3	305	192	25	12	3	1346	84	4	4
RTOR Reduction (vph)	0	0	0	0	5	0	0	0	0	0	1	0
Lane Group Flow (vph)	0	542	0	305	212	0	0	15	1346	0	91	0
Heavy Vehicles (%)	0%	1%	0%	2%	0%	0%	0%	0%	1%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8		4		4
Permitted Phases							8		8		4	
Actuated Green, G (s)		15.2		11.9	33.1			20.1	20.1		20.1	
Effective Green, g (s)		15.2		11.9	33.1			20.1	20.1		20.1	
Actuated g/C Ratio		0.23		0.18	0.51			0.31	0.31		0.31	
Clearance Time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)		3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)		832		626	1801			470	867		489	
v/s Ratio Prot		c0.15		c0.09	0.06							
v/s Ratio Perm								0.01	c0.48		0.06	
v/c Ratio		0.65		0.49	0.12			0.03	1.55		0.19	
Uniform Delay, d ₁		22.6		23.9	8.4			15.8	22.6		16.5	
Progression Factor		1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d ₂		1.8		0.6	0.0			0.0	254.3		0.2	
Delay (s)		24.4		24.5	8.4			15.8	276.9		16.7	
Level of Service		C		C	A			B	F		B	
Approach Delay (s)		24.4			17.8			274.0			16.7	
Approach LOS		C			B			F			B	
Intersection Summary												
HCM 2000 Control Delay			157.7			HCM 2000 Level of Service			F			
HCM 2000 Volume to Capacity ratio			0.99									
Actuated Cycle Length (s)			65.2			Sum of lost time (s)			18.0			
Intersection Capacity Utilization			76.1%			ICU Level of Service			D			
Analysis Period (min)			15									

c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2025 No Build Condition Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↘↗
Traffic Volume (vph)	0	1159	597	684	474	0	0	0	0	389	0	151
Future Volume (vph)	0	1159	597	684	474	0	0	0	0	389	0	151
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		6040	1546	3236	3455					3502		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		6040	1546	3236	3455					3502		2814
Peak-hour factor, PHF	0.85	0.85	0.85	0.94	0.94	0.94	0.92	0.92	0.92	0.90	0.90	0.90
Adj. Flow (vph)	0	1364	702	728	504	0	0	0	0	432	0	168
RTOR Reduction (vph)	0	0	365	0	0	0	0	0	0	0	0	128
Lane Group Flow (vph)	0	1364	337	728	504	0	0	0	0	432	0	40
Heavy Vehicles (%)	0%	1%	1%	1%	1%	0%	0%	0%	0%	0%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		35.0	35.0	25.0	60.9					24.0		24.0
Effective Green, g (s)		35.0	35.0	25.0	60.9					24.0		24.0
Actuated g/C Ratio		0.34	0.34	0.25	0.60					0.24		0.24
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2072	530	793	2062					824		662
v/s Ratio Prot		c0.23	0.22	c0.22	0.15					c0.12		0.01
v/s Ratio Perm												
v/c Ratio		0.66	0.64	0.92	0.24					0.52		0.06
Uniform Delay, d1		28.4	28.2	37.5	9.7					34.0		30.2
Progression Factor		1.00	1.00	1.37	1.12					1.00		1.00
Incremental Delay, d2		1.0	3.5	11.4	0.1					1.1		0.1
Delay (s)		29.5	31.6	62.6	10.9					35.2		30.3
Level of Service		C	C	E	B					D		C
Approach Delay (s)		30.2			41.5			0.0			33.8	
Approach LOS		C			D			A			C	
Intersection Summary												
HCM 2000 Control Delay			34.3			HCM 2000 Level of Service				C		
HCM 2000 Volume to Capacity ratio			0.70									
Actuated Cycle Length (s)			102.0			Sum of lost time (s)				18.0		
Intersection Capacity Utilization			82.6%			ICU Level of Service				E		
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2025 No Build Condition Weekday PM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	693	855	0	0	932	407	226	0	625	0	0	0
Future Volume (vph)	693	855	0	0	932	407	226	0	625	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.95		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3236	3455			4916		3433		2814			
Flt Permitted	0.11	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	389	3455			4916		3433		2814			
Peak-hour factor, PHF	0.87	0.87	0.92	0.90	0.90	0.90	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	797	983	0	0	1036	452	240	0	665	0	0	0
RTOR Reduction (vph)	0	0	0	0	75	0	0	0	509	0	0	0
Lane Group Flow (vph)	797	983	0	0	1413	0	240	0	156	0	0	0
Heavy Vehicles (%)	1%	1%	0%	0%	1%	0%	2%	0%	1%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	59.1	35.0			35.9		24.0		24.0			
Effective Green, g (s)	59.1	35.0			35.9		24.0		24.0			
Actuated g/C Ratio	0.58	0.34			0.35		0.24		0.24			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	898	1185			1730		807		662			
v/s Ratio Prot	c0.21	0.28			0.29		c0.07		0.06			
v/s Ratio Perm	c0.30											
v/c Ratio	0.89	0.83			0.82		0.30		0.24			
Uniform Delay, d1	27.4	30.8			30.1		32.1		31.6			
Progression Factor	1.67	0.54			1.00		1.00		1.00			
Incremental Delay, d2	8.8	4.4			3.5		0.4		0.4			
Delay (s)	54.6	20.9			33.6		32.5		32.0			
Level of Service	D	C			C		C		C			
Approach Delay (s)		36.0			33.6			32.1			0.0	
Approach LOS		D			C			C			A	
Intersection Summary												
HCM 2000 Control Delay			34.3		HCM 2000 Level of Service				C			
HCM 2000 Volume to Capacity ratio			0.71									
Actuated Cycle Length (s)			102.0		Sum of lost time (s)				18.0			
Intersection Capacity Utilization			82.6%		ICU Level of Service				E			
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2025 No Build Condition Weekday PM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	309	1653	1283	223	416	850
Future Volume (vph)	309	1653	1283	223	416	850
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3539	3539	1583	1787	1599
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3539	3539	1583	1787	1599
Peak-hour factor, PHF	0.88	0.88	0.93	0.93	0.87	0.87
Adj. Flow (vph)	351	1878	1380	240	478	977
RTOR Reduction (vph)	0	0	0	167	0	166
Lane Group Flow (vph)	351	1878	1380	73	478	811
Heavy Vehicles (%)	1%	2%	2%	2%	1%	1%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	5.0	29.0	18.0	18.0	18.0	18.0
Effective Green, g (s)	5.0	29.0	18.0	18.0	18.0	18.0
Actuated g/C Ratio	0.08	0.49	0.31	0.31	0.31	0.31
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	151	1739	1079	482	545	487
v/s Ratio Prot	c0.20	0.53	c0.39		0.27	c0.51
v/s Ratio Perm				0.05		
v/c Ratio	2.32	1.08	1.28	0.15	0.88	1.67
Uniform Delay, d1	27.0	15.0	20.5	14.9	19.5	20.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	616.3	46.7	132.8	0.7	15.1	308.3
Delay (s)	643.3	61.7	153.3	15.6	34.6	328.8
Level of Service	F	E	F	B	C	F
Approach Delay (s)		153.3	132.9		232.1	
Approach LOS		F	F		F	

Intersection Summary

HCM 2000 Control Delay	168.7	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.57		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	98.1%	ICU Level of Service	F
Analysis Period (min)	15		
c Critical Lane Group			

201: International Drive & Corporate Drive
 2025 No Build Condition Weekday PM Peak

Intersection	
Intersection Delay, s/veh	104.3
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↶	↷		↶	↷	↶	↶	↷		↶	↷	↶
Traffic Vol, veh/h	140	4	15	9	24	497	15	566	7	61	90	87
Future Vol, veh/h	140	4	15	9	24	497	15	566	7	61	90	87
Peak Hour Factor	0.84	0.84	0.84	0.77	0.77	0.77	0.89	0.89	0.89	0.93	0.93	0.93
Heavy Vehicles, %	0	0	0	0	6	1	0	1	0	4	3	0
Mvmt Flow	167	5	18	12	31	645	17	636	8	66	97	94
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	20.4	210	52.5	15.9
HCM LOS	C	F	F	C

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	96%	0%	21%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	4%	0%	79%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	15	377	196	140	19	9	24	497	61	90	87
LT Vol	15	0	0	140	0	9	0	0	61	0	0
Through Vol	0	377	189	0	4	0	24	0	0	90	0
RT Vol	0	0	7	0	15	0	0	497	0	0	87
Lane Flow Rate	17	424	220	167	23	12	31	645	66	97	94
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.041	0.977	0.504	0.455	0.055	0.03	0.075	1.419	0.18	0.252	0.225
Departure Headway (Hd)	9.697	9.199	9.155	10.415	9.363	9.112	8.708	7.913	10.964	10.426	9.643
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	371	399	396	348	385	393	412	465	329	346	375
Service Time	7.397	6.899	6.855	8.115	7.063	6.854	6.451	5.655	8.664	8.126	7.343
HCM Lane V/C Ratio	0.046	1.063	0.556	0.48	0.06	0.031	0.075	1.387	0.201	0.28	0.251
HCM Control Delay	12.8	70.5	20.8	21.5	12.6	12.1	12.2	223.1	16.1	16.6	15.1
HCM Lane LOS	B	F	C	C	B	B	B	F	C	C	C
HCM 95th-tile Q	0.1	11.4	2.7	2.3	0.2	0.1	0.2	31.4	0.6	1	0.9

202: Goose Bay Drive & Corporate Drive
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	24.3					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	64	8	2	358	172	10
Future Vol, veh/h	64	8	2	358	172	10
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	70	70	73	73	40	40
Heavy Vehicles, %	4	0	0	2	0	0
Mvmt Flow	91	11	3	490	430	25

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	102	0	593
Stage 1	-	-	-	-	97
Stage 2	-	-	-	-	496
Critical Hdwy	-	-	4.1	-	6.4
Critical Hdwy Stg 1	-	-	-	-	5.4
Critical Hdwy Stg 2	-	-	-	-	5.4
Follow-up Hdwy	-	-	2.2	-	3.5
Pot Cap-1 Maneuver	-	-	1503	-	472
Stage 1	-	-	-	-	932
Stage 2	-	-	-	-	616
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1503	-	471
Mov Cap-2 Maneuver	-	-	-	-	471
Stage 1	-	-	-	-	932
Stage 2	-	-	-	-	614

Approach	EB	WB	NB
HCM Control Delay, s	0	0	56.2
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	485	-	-	1503	-
HCM Lane V/C Ratio	0.938	-	-	0.002	-
HCM Control Delay (s)	56.2	-	-	7.4	0
HCM Lane LOS	F	-	-	A	A
HCM 95th %tile Q(veh)	11.3	-	-	0	-

203: Corporate Drive & Redhook Way
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.9					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	7	66	349	3	1	12
Future Vol, veh/h	7	66	349	3	1	12
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	63	63	77	77	36	36
Heavy Vehicles, %	40	0	0	1	0	11
Mvmt Flow	11	105	453	4	3	33

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	457	0	0	582	455
Stage 1	-	-	-	455	-
Stage 2	-	-	-	127	-
Critical Hdwy	4.5	-	-	6.4	6.31
Critical Hdwy Stg 1	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	5.4	-
Follow-up Hdwy	2.56	-	-	3.5	3.399
Pot Cap-1 Maneuver	930	-	-	479	587
Stage 1	-	-	-	643	-
Stage 2	-	-	-	904	-
Platoon blocked, %		-	-		
Mov Cap-1 Maneuver	930	-	-	473	587
Mov Cap-2 Maneuver	-	-	-	473	-
Stage 1	-	-	-	635	-
Stage 2	-	-	-	904	-

Approach	EB	WB	SB
HCM Control Delay, s	0.9	0	11.7
HCM LOS			B

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	930	-	-	-	576
HCM Lane V/C Ratio	0.012	-	-	-	0.063
HCM Control Delay (s)	8.9	-	-	-	11.7
HCM Lane LOS	A	-	-	-	B
HCM 95th %tile Q(veh)	0	-	-	-	0.2

204: Goose Bay Drive & Corporate Drive
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	74	1	6	193	13	11
Future Vol, veh/h	74	1	6	193	13	11
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	81	81	71	71
Heavy Vehicles, %	0	0	0	1	11	0
Mvmt Flow	95	1	7	238	18	15

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	96	0	348
Stage 1	-	-	-	-	96
Stage 2	-	-	-	-	252
Critical Hdwy	-	-	4.1	-	6.51
Critical Hdwy Stg 1	-	-	-	-	5.51
Critical Hdwy Stg 2	-	-	-	-	5.51
Follow-up Hdwy	-	-	2.2	-	3.599
Pot Cap-1 Maneuver	-	-	1510	-	631
Stage 1	-	-	-	-	906
Stage 2	-	-	-	-	769
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1510	-	628
Mov Cap-2 Maneuver	-	-	-	-	628
Stage 1	-	-	-	-	906
Stage 2	-	-	-	-	765

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	10
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	748	-	-	1510	-
HCM Lane V/C Ratio	0.045	-	-	0.005	-
HCM Control Delay (s)	10	-	-	7.4	0
HCM Lane LOS	B	-	-	A	A
HCM 95th %tile Q(veh)	0.1	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	2.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	1	11	13	1	0	7
Future Vol, veh/h	1	11	13	1	0	7
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	67	67	69	69	50	50
Heavy Vehicles, %	0	0	10	0	0	0
Mvmt Flow	1	16	19	1	0	14

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	34	20	0	0	20
Stage 1	20	-	-	-	-
Stage 2	14	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	984	1064	-	-	1609
Stage 1	1008	-	-	-	-
Stage 2	1014	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	984	1064	-	-	1609
Mov Cap-2 Maneuver	984	-	-	-	-
Stage 1	1008	-	-	-	-
Stage 2	1014	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	8.5	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	1057	1609
HCM Lane V/C Ratio	-	-	0.017	-
HCM Control Delay (s)	-	-	8.5	0
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0.1	0

206: Goose Bay Drive & Lonza South Dwy
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	2.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	3	0	0	8	14	0
Future Vol, veh/h	3	0	0	8	14	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	25	25	63	63	63	63
Heavy Vehicles, %	0	0	0	0	10	0
Mvmt Flow	12	0	0	13	22	0

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	35	22	22	0	0
Stage 1	22	-	-	-	-
Stage 2	13	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-
Pot Cap-1 Maneuver	983	1061	1607	-	-
Stage 1	1006	-	-	-	-
Stage 2	1015	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	983	1061	1607	-	-
Mov Cap-2 Maneuver	983	-	-	-	-
Stage 1	1006	-	-	-	-
Stage 2	1015	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	8.7	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1607	-	983	-	-
HCM Lane V/C Ratio	-	-	0.012	-	-
HCM Control Delay (s)	0	-	8.7	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2025 No Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	0											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	0	182	0	0	5	5
Future Vol, veh/h	0	0	0	0	0	0	0	182	0	0	5	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	39	39	92	92	67	67
Heavy Vehicles, %	2	2	2	2	2	2	0	0	2	2	0	0
Mvmt Flow	0	0	0	0	0	0	0	467	0	0	7	7

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	478	478	11	478	481	467	14	0	0	467	0	0
Stage 1	11	11	-	467	467	-	-	-	-	-	-	-
Stage 2	467	467	-	11	14	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	498	486	1070	498	485	596	1617	-	-	1094	-	-
Stage 1	1010	886	-	576	562	-	-	-	-	-	-	-
Stage 2	576	562	-	1010	884	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	498	486	1070	498	485	596	1617	-	-	1094	-	-
Mov Cap-2 Maneuver	498	486	-	498	485	-	-	-	-	-	-	-
Stage 1	1010	886	-	576	562	-	-	-	-	-	-	-
Stage 2	576	562	-	1010	884	-	-	-	-	-	-	-

Approach	EB		WB		NB			SB		
HCM Control Delay, s	0		0		0			0		
HCM LOS	A		A							

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1617	-	-	-	-	1094	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	0	0	0	-	-
HCM Lane LOS	A	-	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		B			A
Traffic Vol, veh/h	7	3	586	1	4	103
Future Vol, veh/h	7	3	586	1	4	103
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	78	78	76	76
Heavy Vehicles, %	0	0	1	0	0	4
Mvmt Flow	8	3	751	1	5	136

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	898	752	0	0	752	0
Stage 1	752	-	-	-	-	-
Stage 2	146	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	312	413	-	-	867	-
Stage 1	469	-	-	-	-	-
Stage 2	886	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	310	413	-	-	867	-
Mov Cap-2 Maneuver	310	-	-	-	-	-
Stage 1	469	-	-	-	-	-
Stage 2	881	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	16.1	0	0.3
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	335	867
HCM Lane V/C Ratio	-	-	0.034	0.006
HCM Control Delay (s)	-	-	16.1	9.2
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	7.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	49	150	437	15	13	97
Future Vol, veh/h	49	150	437	15	13	97
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	72	72	67	67	81	81
Heavy Vehicles, %	14	0	1	46	0	3
Mvmt Flow	68	208	652	22	16	120

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	815	663	0	0	674	0
Stage 1	663	-	-	-	-	-
Stage 2	152	-	-	-	-	-
Critical Hdwy	6.54	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.54	-	-	-	-	-
Critical Hdwy Stg 2	5.54	-	-	-	-	-
Follow-up Hdwy	3.626	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	331	465	-	-	927	-
Stage 1	491	-	-	-	-	-
Stage 2	847	-	-	-	-	-
Platoon blocked, %			-	-	-	-
Mov Cap-1 Maneuver	325	465	-	-	927	-
Mov Cap-2 Maneuver	325	-	-	-	-	-
Stage 1	491	-	-	-	-	-
Stage 2	832	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	28.6	0	1.1
HCM LOS	D		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	420	927
HCM Lane V/C Ratio	-	-	0.658	0.017
HCM Control Delay (s)	-	-	28.6	9
HCM Lane LOS	-	-	D	A
HCM 95th %tile Q(veh)	-	-	4.6	0.1

210: International Drive & Lonza South Driveway
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	0	4	358	0	0	164
Future Vol, veh/h	0	4	358	0	0	164
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	68	68	74	74
Heavy Vehicles, %	0	0	3	0	0	7
Mvmt Flow	0	16	526	0	0	222

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	748	526	0	0	526	0
Stage 1	526	-	-	-	-	-
Stage 2	222	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	383	556	-	-	1051	-
Stage 1	597	-	-	-	-	-
Stage 2	820	-	-	-	-	-
Platoon blocked, %			-	-	-	-
Mov Cap-1 Maneuver	383	556	-	-	1051	-
Mov Cap-2 Maneuver	383	-	-	-	-	-
Stage 1	597	-	-	-	-	-
Stage 2	820	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	11.7	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	556	1051
HCM Lane V/C Ratio	-	-	0.029	-
HCM Control Delay (s)	-	-	11.7	0
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2025 No Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	126.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	28	20	3	285	19	20	1	297	103	3	513	12
Future Vol, veh/h	28	20	3	285	19	20	1	297	103	3	513	12
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	54	54	54	85	85	85	84	84	84	88	88	88
Heavy Vehicles, %	0	13	0	0	14	0	0	2	1	0	1	11
Mvmt Flow	52	37	6	335	22	24	1	354	123	3	583	14

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1037	1075	590	1036	1021	416	597	0	0	477	0	0
Stage 1	596	596	-	418	418	-	-	-	-	-	-	-
Stage 2	441	479	-	618	603	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.63	6.2	7.1	6.64	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4.117	3.3	3.5	4.126	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	211	210	511	~212	225	641	989	-	-	1096	-	-
Stage 1	494	475	-	616	570	-	-	-	-	-	-	-
Stage 2	599	537	-	480	470	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	187	209	511	~180	224	641	989	-	-	1096	-	-
Mov Cap-2 Maneuver	187	209	-	~180	224	-	-	-	-	-	-	-
Stage 1	494	473	-	615	569	-	-	-	-	-	-	-
Stage 2	554	536	-	436	468	-	-	-	-	-	-	-

Approach	EB	WB	NB	SB
HCM Control Delay, s	37.3	\$ 506.9	0	0
HCM LOS	E	F		

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	989	-	-	203	191	1096	-	-
HCM Lane V/C Ratio	0.001	-	-	0.465	1.996	0.003	-	-
HCM Control Delay (s)	8.6	0	-	37.3	\$ 506.9	8.3	0	-
HCM Lane LOS	A	A	-	E	F	A	A	-
HCM 95th %tile Q(veh)	0	-	-	2.2	28.7	0	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2025 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	55.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	340	73	203	46	24	793
Future Vol, veh/h	340	73	203	46	24	793
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	86	86	76	76	83	83
Heavy Vehicles, %	2	2	1	3	0	1
Mvmt Flow	395	85	267	61	29	955

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	624	29	984	0	0
Stage 1	29	-	-	-	-
Stage 2	595	-	-	-	-
Critical Hdwy	6.42	6.22	4.11	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.209	-	-
Pot Cap-1 Maneuver	449	1046	706	-	-
Stage 1	994	-	-	-	-
Stage 2	551	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	~ 279	1046	706	-	-
Mov Cap-2 Maneuver	~ 279	-	-	-	-
Stage 1	618	-	-	-	-
Stage 2	551	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	200.9	10.7	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	706	-	279	1046	-	-
HCM Lane V/C Ratio	0.378	-	1.417	0.081	-	-
HCM Control Delay (s)	13.2	-	242.2	8.7	-	-
HCM Lane LOS	B	-	F	A	-	-
HCM 95th %tile Q(veh)	1.8	-	21.5	0.3	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2025 No Build Condition Weekday PM Peak

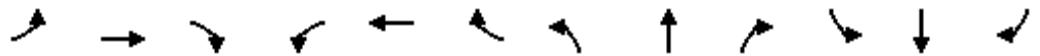
Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↖↗
Traffic Vol, veh/h	0	66	532	0	0	1266
Future Vol, veh/h	0	66	532	0	0	1266
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	73	73	95	95	89	89
Heavy Vehicles, %	0	13	0	1	0	1
Mvmt Flow	0	90	560	0	0	1422

Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	-	560	0
Stage 1	-	-	-
Stage 2	-	-	-
Critical Hdwy	-	6.395	-
Critical Hdwy Stg 1	-	-	-
Critical Hdwy Stg 2	-	-	-
Follow-up Hdwy	-	3.4235	-
Pot Cap-1 Maneuver	0	502	-
Stage 1	0	-	-
Stage 2	0	-	-
Platoon blocked, %	-	-	-
Mov Cap-1 Maneuver	-	502	-
Mov Cap-2 Maneuver	-	-	-
Stage 1	-	-	-
Stage 2	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.7	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	-	502
HCM Lane V/C Ratio	-	0.18
HCM Control Delay (s)	-	13.7
HCM Lane LOS	-	B
HCM 95th %tile Q(veh)	-	0.7

101: International Dr & Pease Blvd
 2025 Build Condition Weekday AM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↖	↗		↖	↗			↖	↗		↗	↖
Traffic Volume (vph)	3	106	6	1286	642	132	8	5	323	6	2	2
Future Volume (vph)	3	106	6	1286	642	132	8	5	323	6	2	2
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor	1.00	0.95		0.97	0.95			1.00	0.88		1.00	
Frt	1.00	0.99		1.00	0.97			1.00	0.85		0.97	
Flt Protected	0.95	1.00		0.95	1.00			0.97	1.00		0.97	
Satd. Flow (prot)	1805	3515		3467	3475			1783	2682		2035	
Flt Permitted	0.95	1.00		0.95	1.00			0.88	1.00		0.87	
Satd. Flow (perm)	1805	3515		3467	3475			1609	2682		1824	
Peak-hour factor, PHF	0.84	0.84	0.84	0.83	1.00	0.83	0.88	0.88	0.88	0.63	0.63	0.63
Adj. Flow (vph)	4	126	7	1549	642	159	9	6	367	10	3	3
RTOR Reduction (vph)	0	4	0	0	10	0	0	0	0	0	2	0
Lane Group Flow (vph)	4	129	0	1549	791	0	0	15	367	0	14	0
Heavy Vehicles (%)	0%	2%	0%	1%	1%	0%	0%	0%	6%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8			4	
Permitted Phases							8		8	4		
Actuated Green, G (s)	6.1	12.8		50.1	57.8			17.6	17.6		17.6	
Effective Green, g (s)	6.1	12.8		50.1	57.8			17.6	17.6		17.6	
Actuated g/C Ratio	0.06	0.13		0.51	0.59			0.18	0.18		0.18	
Clearance Time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)	2.0	3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)	111	456		1763	2039			287	479		325	
v/s Ratio Prot	0.00	c0.04		c0.45	c0.23							
v/s Ratio Perm								0.01	c0.14		0.01	
v/c Ratio	0.04	0.28		0.88	0.39			0.05	0.77		0.04	
Uniform Delay, d1	43.4	38.7		21.5	10.9			33.5	38.5		33.5	
Progression Factor	1.00	1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d2	0.0	0.3		5.3	0.1			0.1	7.2		0.1	
Delay (s)	43.5	39.0		26.8	11.0			33.6	45.7		33.5	
Level of Service	D	D		C	B			C	D		C	
Approach Delay (s)		39.2			21.4			45.2			33.5	
Approach LOS		D			C			D			C	

Intersection Summary

HCM 2000 Control Delay	25.5	HCM 2000 Level of Service	C
HCM 2000 Volume to Capacity ratio	0.76		
Actuated Cycle Length (s)	98.5	Sum of lost time (s)	18.0
Intersection Capacity Utilization	59.1%	ICU Level of Service	B
Analysis Period (min)	15		

c Critical Lane Group
























102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2025 Build Condition Weekday AM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations		↑↑↑	↗	↘	↑↑					↖		↗		
Traffic Volume (vph)	0	302	133	157	1056	0	0	0	0	566	0	894		
Future Volume (vph)	0	302	133	157	1056	0	0	0	0	566	0	894		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900		
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12		
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0		
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88		
Fr _t		1.00	0.85	1.00	1.00					1.00		0.85		
Fl _t Protected		1.00	1.00	0.95	1.00					0.95		1.00		
Satd. Flow (prot)		5981	1419	2918	3455					3467		2814		
Fl _t Permitted		1.00	1.00	0.95	1.00					0.95		1.00		
Satd. Flow (perm)		5981	1419	2918	3455					3467		2814		
Peak-hour factor, PHF	0.80	0.80	0.80	0.80	0.80	0.80	0.92	0.92	0.92	0.75	0.75	0.75		
Adj. Flow (vph)	0	378	166	196	1320	0	0	0	0	755	0	1192		
RTOR Reduction (vph)	0	0	111	0	0	0	0	0	0	0	0	93		
Lane Group Flow (vph)	0	378	55	196	1320	0	0	0	0	755	0	1099		
Heavy Vehicles (%)	0%	2%	10%	12%	1%	0%	2%	2%	2%	1%	0%	1%		
Turn Type		NA	Prot	Prot	NA					Prot		Prot		
Protected Phases		6	6	5	2 5					3		3		
Permitted Phases														
Actuated Green, G (s)		33.5	33.5	25.0	64.5					25.0		25.0		
Effective Green, g (s)		33.5	33.5	25.0	64.5					25.0		25.0		
Actuated g/C Ratio		0.33	0.33	0.25	0.64					0.25		0.25		
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0		
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0		
Lane Grp Cap (vph)		1974	468	718	2195					853		693		
v/s Ratio Prot		0.06	0.04	0.07	c0.38					0.22		c0.39		
v/s Ratio Perm														
v/c Ratio		0.19	0.12	0.27	0.60					0.89		1.59		
Uniform Delay, d ₁		24.3	23.7	30.9	10.9					36.9		38.2		
Progression Factor		1.00	1.00	0.89	1.59					1.00		1.00		
Incremental Delay, d ₂		0.1	0.2	0.1	0.3					11.6		270.7		
Delay (s)		24.4	23.9	27.5	17.7					48.5		308.9		
Level of Service		C	C	C	B					D		F		
Approach Delay (s)		24.3			18.9			0.0			207.9			
Approach LOS		C			B			A			F			
Intersection Summary														
HCM 2000 Control Delay			111.5									HCM 2000 Level of Service	F	
HCM 2000 Volume to Capacity ratio			0.94											
Actuated Cycle Length (s)			101.5							18.0			Sum of lost time (s)	
Intersection Capacity Utilization			76.2%										ICU Level of Service	D
Analysis Period (min)			15											

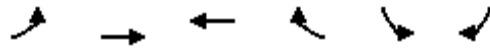
c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2025 Build Condition Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	 	 			  		 		 			
Traffic Volume (vph)	145	723	0	0	412	78	801	0	366	0	0	0
Future Volume (vph)	145	723	0	0	412	78	801	0	366	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.98		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3113	3421			4941		3433		2733			
Flt Permitted	0.42	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	1390	3421			4941		3433		2733			
Peak-hour factor, PHF	0.87	0.87	0.87	0.85	0.85	0.85	0.78	0.78	0.78	0.92	0.92	0.92
Adj. Flow (vph)	167	831	0	0	485	92	1027	0	469	0	0	0
RTOR Reduction (vph)	0	0	0	0	24	0	0	0	339	0	0	0
Lane Group Flow (vph)	167	831	0	0	553	0	1027	0	130	0	0	0
Heavy Vehicles (%)	5%	2%	0%	0%	2%	5%	2%	2%	4%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	50.5	33.5			41.5		25.0		25.0			
Effective Green, g (s)	50.5	33.5			41.5		25.0		25.0			
Actuated g/C Ratio	0.50	0.33			0.41		0.25		0.25			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	980	1129			2020		845		673			
v/s Ratio Prot	c0.03	c0.24			c0.11		c0.30		0.05			
v/s Ratio Perm	0.06											
v/c Ratio	0.17	0.74			0.27		1.22		0.19			
Uniform Delay, d1	13.5	30.1			20.0		38.2		30.3			
Progression Factor	1.13	1.26			1.00		1.00		1.00			
Incremental Delay, d2	0.1	2.3			0.2		107.7		0.3			
Delay (s)	15.4	40.1			20.1		146.0		30.6			
Level of Service	B	D			C		F		C			
Approach Delay (s)		36.0			20.1			109.8			0.0	
Approach LOS		D			C			F			A	
Intersection Summary												
HCM 2000 Control Delay			69.0				HCM 2000 Level of Service				E	
HCM 2000 Volume to Capacity ratio			0.71									
Actuated Cycle Length (s)			101.5				Sum of lost time (s)				18.0	
Intersection Capacity Utilization			76.2%				ICU Level of Service				D	
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2025 Build Condition Weekday AM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	634	2030	731	613	165	206
Future Volume (vph)	634	2030	731	613	165	206
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3471	3343	1583	1719	1538
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3471	3343	1583	1719	1538
Peak-hour factor, PHF	0.86	0.86	0.96	0.96	0.76	0.76
Adj. Flow (vph)	737	2360	761	639	217	271
RTOR Reduction (vph)	0	0	0	444	0	205
Lane Group Flow (vph)	737	2360	761	195	217	66
Heavy Vehicles (%)	1%	4%	8%	2%	5%	5%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	9.4	33.4	18.0	18.0	13.6	13.6
Effective Green, g (s)	9.4	33.4	18.0	18.0	13.6	13.6
Actuated g/C Ratio	0.16	0.57	0.31	0.31	0.23	0.23
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	284	1964	1019	482	396	354
v/s Ratio Prot	c0.41	c0.68	0.23		c0.13	0.04
v/s Ratio Perm				0.12		
v/c Ratio	2.60	1.20	0.75	0.40	0.55	0.19
Uniform Delay, d1	24.8	12.8	18.4	16.3	20.0	18.2
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	727.9	95.9	5.0	2.5	1.9	0.3
Delay (s)	752.7	108.7	23.4	18.8	21.9	18.6
Level of Service	F	F	C	B	C	B
Approach Delay (s)		262.0	21.3		20.1	
Approach LOS		F	C		C	

Intersection Summary			
HCM 2000 Control Delay	170.7	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.38		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	83.1%	ICU Level of Service	E
Analysis Period (min)	15		
c Critical Lane Group			

201: International Drive & Corporate Drive
 2025 Build Condition Weekday AM Peak

Intersection	
Intersection Delay, s/veh	197.2
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↵	↶		↵	↑	↶	↵	↶↷		↵	↑	↶
Traffic Vol, veh/h	69	44	31	14	13	121	8	101	64	682	449	137
Future Vol, veh/h	69	44	31	14	13	121	8	101	64	682	449	137
Peak Hour Factor	0.76	0.76	0.76	0.78	0.78	0.78	0.83	0.83	0.83	0.76	0.76	0.76
Heavy Vehicles, %	0	4	5	0	13	18	0	0	3	2	0	0
Mvmt Flow	91	58	41	18	17	155	10	122	77	897	591	180
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	15.1	16.4	14.8	261.2
HCM LOS	C	C	B	F

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	34%	0%	59%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	66%	0%	41%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	8	67	98	69	75	14	13	121	682	449	137
LT Vol	8	0	0	69	0	14	0	0	682	0	0
Through Vol	0	67	34	0	44	0	13	0	0	449	0
RT Vol	0	0	64	0	31	0	0	121	0	0	137
Lane Flow Rate	10	81	118	91	99	18	17	155	897	591	180
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.025	0.195	0.27	0.234	0.235	0.047	0.042	0.364	1.86	1.136	0.311
Departure Headway (Hd)	9.996	9.488	9.073	9.913	9.192	10.089	9.808	9.187	7.461	6.921	6.212
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	360	380	399	365	393	357	367	394	494	532	582
Service Time	7.696	7.188	6.773	7.613	6.892	7.789	7.508	6.887	5.161	4.621	3.912
HCM Lane V/C Ratio	0.028	0.213	0.296	0.249	0.252	0.05	0.046	0.393	1.816	1.111	0.309
HCM Control Delay	13	14.5	15.1	15.6	14.7	13.3	12.9	17.1	412.7	107.1	11.7
HCM Lane LOS	B	B	C	C	B	B	B	C	F	F	B
HCM 95th-tile Q	0.1	0.7	1.1	0.9	0.9	0.1	0.1	1.6	57.7	19.9	1.3

202: Goose Bay Drive & Corporate Drive
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	7.2					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	451	339	67	71	77	25
Future Vol, veh/h	451	339	67	71	77	25
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	71	71	69	69
Heavy Vehicles, %	1	5	0	12	36	0
Mvmt Flow	578	435	94	100	112	36

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	1013	0	1084
Stage 1	-	-	-	-	796
Stage 2	-	-	-	-	288
Critical Hdwy	-	-	4.1	-	6.76
Critical Hdwy Stg 1	-	-	-	-	5.76
Critical Hdwy Stg 2	-	-	-	-	5.76
Follow-up Hdwy	-	-	2.2	-	3.824
Pot Cap-1 Maneuver	-	-	692	-	207
Stage 1	-	-	-	-	390
Stage 2	-	-	-	-	689
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	692	-	177
Mov Cap-2 Maneuver	-	-	-	-	177
Stage 1	-	-	-	-	390
Stage 2	-	-	-	-	590

Approach	EB	WB	NB
HCM Control Delay, s	0	5.4	58.6
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	204	-	-	692	-
HCM Lane V/C Ratio	0.725	-	-	0.136	-
HCM Control Delay (s)	58.6	-	-	11	0
HCM Lane LOS	F	-	-	B	A
HCM 95th %tile Q(veh)	4.7	-	-	0.5	-

203: Corporate Drive & Redhook Way
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	↙	↑	↘		↙	
Traffic Vol, veh/h	17	460	119	2	0	6
Future Vol, veh/h	17	460	119	2	0	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	85	85	71	71	50	50
Heavy Vehicles, %	0	1	8	0	0	25
Mvmt Flow	20	541	168	3	0	12

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	171	0	-	0	751 170
Stage 1	-	-	-	-	170 -
Stage 2	-	-	-	-	581 -
Critical Hdwy	4.1	-	-	-	6.4 6.45
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.2	-	-	-	3.5 3.525
Pot Cap-1 Maneuver	1418	-	-	-	381 818
Stage 1	-	-	-	-	865 -
Stage 2	-	-	-	-	563 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	1418	-	-	-	376 818
Mov Cap-2 Maneuver	-	-	-	-	376 -
Stage 1	-	-	-	-	853 -
Stage 2	-	-	-	-	563 -

Approach	EB	WB	SB
HCM Control Delay, s	0.3	0	9.5
HCM LOS			A

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	1418	-	-	-	818
HCM Lane V/C Ratio	0.014	-	-	-	0.015
HCM Control Delay (s)	7.6	-	-	-	9.5
HCM Lane LOS	A	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	0

204: Goose Bay Drive & Corporate Drive
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	251	16	3	149	0	0
Future Vol, veh/h	251	16	3	149	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	95	95	82	82	25	40
Heavy Vehicles, %	1	0	0	5	20	0
Mvmt Flow	264	17	4	182	0	0

Major/Minor	Major1	Major2	Minor1			
Conflicting Flow All	0	0	281	0	463	273
Stage 1	-	-	-	-	273	-
Stage 2	-	-	-	-	190	-
Critical Hdwy	-	-	4.1	-	6.6	6.2
Critical Hdwy Stg 1	-	-	-	-	5.6	-
Critical Hdwy Stg 2	-	-	-	-	5.6	-
Follow-up Hdwy	-	-	2.2	-	3.68	3.3
Pot Cap-1 Maneuver	-	-	1293	-	525	771
Stage 1	-	-	-	-	733	-
Stage 2	-	-	-	-	801	-
Platoon blocked, %	-	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1293	-	523	771
Mov Cap-2 Maneuver	-	-	-	-	523	-
Stage 1	-	-	-	-	733	-
Stage 2	-	-	-	-	799	-

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	0
HCM LOS			A

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	-	-	-	1293	-
HCM Lane V/C Ratio	-	-	-	0.003	-
HCM Control Delay (s)	0	-	-	7.8	0
HCM Lane LOS	A	-	-	A	A
HCM 95th %tile Q(veh)	-	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	0	0	19	0
Future Vol, veh/h	0	0	0	0	19	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	53	53	50	50
Heavy Vehicles, %	0	0	0	13	0	0
Mvmt Flow	0	0	0	0	38	0

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	76	0	0	0	0	0
Stage 1	0	-	-	-	-	-
Stage 2	76	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	932	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	952	-	-	-	-	-
Platoon blocked, %						
Mov Cap-1 Maneuver	932	-	-	-	-	-
Mov Cap-2 Maneuver	932	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	952	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	0	0	
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-
HCM Control Delay (s)	-	-	0	-
HCM Lane LOS	-	-	A	-
HCM 95th %tile Q(veh)	-	-	-	-

206: Goose Bay Drive & Lonza South Dwy
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	4.7					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	6	0	0	0	0	8
Future Vol, veh/h	6	0	0	0	0	8
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	50	50	42	42	69	69
Heavy Vehicles, %	75	0	0	0	6	80
Mvmt Flow	12	0	0	0	0	12

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	6	6	12	0	-	0
Stage 1	6	-	-	-	-	-
Stage 2	0	-	-	-	-	-
Critical Hdwy	7.15	6.2	4.1	-	-	-
Critical Hdwy Stg 1	6.15	-	-	-	-	-
Critical Hdwy Stg 2	6.15	-	-	-	-	-
Follow-up Hdwy	4.175	3.3	2.2	-	-	-
Pot Cap-1 Maneuver	855	1083	1620	-	-	-
Stage 1	856	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	855	1083	1620	-	-	-
Mov Cap-2 Maneuver	855	-	-	-	-	-
Stage 1	856	-	-	-	-	-
Stage 2	-	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	9.3	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1620	-	855	-	-
HCM Lane V/C Ratio	-	-	0.014	-	-
HCM Control Delay (s)	0	-	9.3	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2025 Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	2.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	68	5	34	0	138	48	220
Future Vol, veh/h	0	0	0	0	0	68	5	34	0	138	48	220
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	88	88	92	92	69	69
Heavy Vehicles, %	2	2	2	2	2	2	0	18	2	2	15	1
Mvmt Flow	0	0	0	0	0	74	6	39	0	150	70	319

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	618	581	230	581	740	39	389	0	0	39	0	0
Stage 1	530	530	-	51	51	-	-	-	-	-	-	-
Stage 2	88	51	-	530	689	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	402	425	809	425	345	1033	1181	-	-	1571	-	-
Stage 1	533	527	-	962	852	-	-	-	-	-	-	-
Stage 2	920	852	-	533	446	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	335	369	809	382	299	1033	1181	-	-	1571	-	-
Mov Cap-2 Maneuver	335	369	-	382	299	-	-	-	-	-	-	-
Stage 1	530	460	-	957	848	-	-	-	-	-	-	-
Stage 2	850	848	-	465	389	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		8.8		1		2.1	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1181	-	-	-	1033	1571	-	-
HCM Lane V/C Ratio	0.005	-	-	-	0.072	0.095	-	-
HCM Control Delay (s)	8.1	0	-	0	8.8	7.5	0	-
HCM Lane LOS	A	A	-	A	A	A	A	-
HCM 95th %tile Q(veh)	0	-	-	-	0.2	0.3	-	-

208: Granite State Driveway & International Drive
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	6	2	159	13	13	439
Future Vol, veh/h	6	2	159	13	13	439
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	63	63	81	81	84	84
Heavy Vehicles, %	0	0	0	0	0	1
Mvmt Flow	10	3	196	16	15	523

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	757	204	0	0	212	0
Stage 1	204	-	-	-	-	-
Stage 2	553	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	378	842	-	-	1370	-
Stage 1	835	-	-	-	-	-
Stage 2	580	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	372	842	-	-	1370	-
Mov Cap-2 Maneuver	372	-	-	-	-	-
Stage 1	835	-	-	-	-	-
Stage 2	571	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.6	0	0.2
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	432	1370
HCM Lane V/C Ratio	-	-	0.029	0.011
HCM Control Delay (s)	-	-	13.6	7.7
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	W	T	T	T	T
Traffic Vol, veh/h	14	19	153	13	20	425
Future Vol, veh/h	14	19	153	13	20	425
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	86	86	83	83
Heavy Vehicles, %	44	0	1	63	0	1
Mvmt Flow	16	22	178	15	24	512

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	746	186	0	0	193
Stage 1	186	-	-	-	-
Stage 2	560	-	-	-	-
Critical Hdwy	6.84	6.2	-	-	4.1
Critical Hdwy Stg 1	5.84	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-
Follow-up Hdwy	3.896	3.3	-	-	2.2
Pot Cap-1 Maneuver	326	861	-	-	1392
Stage 1	754	-	-	-	-
Stage 2	497	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	318	861	-	-	1392
Mov Cap-2 Maneuver	318	-	-	-	-
Stage 1	754	-	-	-	-
Stage 2	485	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	12.8	0	0.3
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	499	1392
HCM Lane V/C Ratio	-	-	0.075	0.017
HCM Control Delay (s)	-	-	12.8	7.6
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.2	0.1

210: International Drive & Lonza South Driveway
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	5	187	2	8	338
Future Vol, veh/h	0	5	187	2	8	338
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	75	75	89	89	81	81
Heavy Vehicles, %	0	0	5	100	0	2
Mvmt Flow	0	7	210	2	10	417

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	648	211	0	0	212	0
Stage 1	211	-	-	-	-	-
Stage 2	437	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	438	834	-	-	1370	-
Stage 1	829	-	-	-	-	-
Stage 2	655	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	434	834	-	-	1370	-
Mov Cap-2 Maneuver	434	-	-	-	-	-
Stage 1	829	-	-	-	-	-
Stage 2	648	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	9.4	0	0.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	834	1370
HCM Lane V/C Ratio	-	-	0.008	0.007
HCM Control Delay (s)	-	-	9.4	7.6
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2025 Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	11.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	8	9	2	86	5	6	0	461	391	26	295	29
Future Vol, veh/h	8	9	2	86	5	6	0	461	391	26	295	29
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	75	75	75	65	65	65	90	90	90	87	87	87
Heavy Vehicles, %	20	0	0	4	0	0	0	2	3	0	3	0
Mvmt Flow	11	12	3	132	8	9	0	512	434	30	339	33

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1154	1362	356	1152	1161	729	372	0	0	946	0	0
Stage 1	416	416	-	729	729	-	-	-	-	-	-	-
Stage 2	738	946	-	423	432	-	-	-	-	-	-	-
Critical Hdwy	7.3	6.5	6.2	7.14	6.5	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.68	4	3.3	3.536	4	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	160	149	693	173	197	426	1198	-	-	734	-	-
Stage 1	580	595	-	411	431	-	-	-	-	-	-	-
Stage 2	383	343	-	605	586	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	146	141	693	155	187	426	1198	-	-	734	-	-
Mov Cap-2 Maneuver	146	141	-	155	187	-	-	-	-	-	-	-
Stage 1	580	564	-	411	431	-	-	-	-	-	-	-
Stage 2	368	343	-	559	556	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	32.5		105.3		0		0.8	
HCM LOS	D		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1198	-	-	156	163	734	-	-
HCM Lane V/C Ratio	-	-	-	0.162	0.916	0.041	-	-
HCM Control Delay (s)	0	-	-	32.5	105.3	10.1	0	-
HCM Lane LOS	A	-	-	D	F	B	A	-
HCM 95th %tile Q(veh)	0	-	-	0.6	6.7	0.1	-	-

212: Corporate Dr & Grafton Rd
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	115.2					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↖	↗	↖	↗	↗	↖
Traffic Vol, veh/h	871	396	68	14	55	238
Future Vol, veh/h	871	396	68	14	55	238
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	93	93	70	70	90	90
Heavy Vehicles, %	1	1	3	11	0	4
Mvmt Flow	937	426	97	20	61	264

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	275	61	325	0	-	0
Stage 1	61	-	-	-	-	-
Stage 2	214	-	-	-	-	-
Critical Hdwy	6.41	6.21	4.13	-	-	-
Critical Hdwy Stg 1	5.41	-	-	-	-	-
Critical Hdwy Stg 2	5.41	-	-	-	-	-
Follow-up Hdwy	3.509	3.309	2.227	-	-	-
Pot Cap-1 Maneuver	~ 717	1007	1229	-	-	-
Stage 1	964	-	-	-	-	-
Stage 2	~ 824	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	~ 660	1007	1229	-	-	-
Mov Cap-2 Maneuver	~ 660	-	-	-	-	-
Stage 1	~ 888	-	-	-	-	-
Stage 2	~ 824	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	152	6.8	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1229	-	660	1007	-	-
HCM Lane V/C Ratio	0.079	-	1.419	0.423	-	-
HCM Control Delay (s)	8.2	-	216	11.2	-	-
HCM Lane LOS	A	-	F	B	-	-
HCM 95th %tile Q(veh)	0.3	-	42.8	2.1	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2025 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	113.5					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↕↕
Traffic Vol, veh/h	0	225	1247	0	0	371
Future Vol, veh/h	0	225	1247	0	0	371
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	76	76	70	70	80	80
Heavy Vehicles, %	2	3	2	2	2	4
Mvmt Flow	0	296	1781	0	0	464

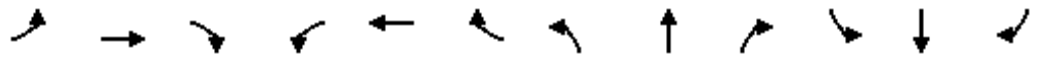
Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	- 1781	0	- - -
Stage 1	-	-	- - -
Stage 2	-	-	- - -
Critical Hdwy	- 6.245	-	- - -
Critical Hdwy Stg 1	-	-	- - -
Critical Hdwy Stg 2	-	-	- - -
Follow-up Hdwy	- 3.3285	-	- - -
Pot Cap-1 Maneuver	0 ~ 100	-	0 0 -
Stage 1	0	-	0 0 -
Stage 2	0	-	0 0 -
Platoon blocked, %		-	-
Mov Cap-1 Maneuver	- ~ 100	-	- - -
Mov Cap-2 Maneuver	-	-	- - -
Stage 1	-	-	- - -
Stage 2	-	-	- - -

Approach	WB	NB	SB
HCM Control Delay, s\$	974.6	0	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 100	-
HCM Lane V/C Ratio	- 2.961	-
HCM Control Delay (s)	-\$ 974.6	-
HCM Lane LOS	- F	-
HCM 95th %tile Q(veh)	- 28.4	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon













101: International Dr & Pease Blvd
 2025 Build Condition Weekday PM Peak


























Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↖	↗		↖	↗			↖	↗		↖	↗
Traffic Volume (vph)	0	474	3	302	184	24	11	3	1326	57	3	3
Future Volume (vph)	0	474	3	302	184	24	11	3	1326	57	3	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor		0.95		0.97	0.95			1.00	0.88		1.00	
Fr _t		1.00		1.00	0.98			1.00	0.85		0.99	
Fl _t Protected		1.00		0.95	1.00			0.96	1.00		0.96	
Satd. Flow (prot)		3571		3433	3548			1766	2814		2047	
Fl _t Permitted		1.00		0.95	1.00			0.83	1.00		0.74	
Satd. Flow (perm)		3571		3433	3548			1525	2814		1586	
Peak-hour factor, PHF	0.88	0.88	0.88	0.96	0.96	0.96	0.91	0.91	0.91	0.68	0.68	0.68
Adj. Flow (vph)	0	539	3	315	192	25	12	3	1457	84	4	4
RTOR Reduction (vph)	0	0	0	0	5	0	0	0	0	0	1	0
Lane Group Flow (vph)	0	542	0	315	212	0	0	15	1457	0	91	0
Heavy Vehicles (%)	0%	1%	0%	2%	0%	0%	0%	0%	1%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8			4	
Permitted Phases							8		8		4	
Actuated Green, G (s)		15.3		12.1	33.4			20.1	20.1		20.1	
Effective Green, g (s)		15.3		12.1	33.4			20.1	20.1		20.1	
Actuated g/C Ratio		0.23		0.18	0.51			0.31	0.31		0.31	
Clearance Time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)		3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)		834		634	1809			467	863		486	
v/s Ratio Prot		c0.15		c0.09	0.06							
v/s Ratio Perm								0.01	c0.52		0.06	
v/c Ratio		0.65		0.50	0.12			0.03	1.69		0.19	
Uniform Delay, d ₁		22.7		24.0	8.4			15.9	22.7		16.7	
Progression Factor		1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d ₂		1.8		0.6	0.0			0.0	314.8		0.2	
Delay (s)		24.4		24.6	8.4			15.9	337.5		16.9	
Level of Service		C		C	A			B	F		B	
Approach Delay (s)		24.4			18.0			334.2			16.9	
Approach LOS		C			B			F			B	
Intersection Summary												
HCM 2000 Control Delay			195.7									F
HCM 2000 Volume to Capacity ratio			1.05									
Actuated Cycle Length (s)			65.5								18.0	
Intersection Capacity Utilization			79.6%									D
ICU Level of Service												
Analysis Period (min)			15									

c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2025 Build Condition Weekday PM Peak

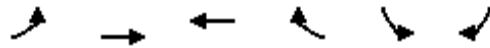
												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↗↘
Traffic Volume (vph)	0	1224	633	684	478	0	0	0	0	389	0	156
Future Volume (vph)	0	1224	633	684	478	0	0	0	0	389	0	156
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		6040	1546	3236	3455					3502		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		6040	1546	3236	3455					3502		2814
Peak-hour factor, PHF	0.85	0.85	0.85	0.94	0.94	0.94	0.92	0.92	0.92	0.90	0.90	0.90
Adj. Flow (vph)	0	1440	745	728	509	0	0	0	0	432	0	173
RTOR Reduction (vph)	0	0	365	0	0	0	0	0	0	0	0	132
Lane Group Flow (vph)	0	1440	380	728	509	0	0	0	0	432	0	41
Heavy Vehicles (%)	0%	1%	1%	1%	1%	0%	0%	0%	0%	0%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		35.0	35.0	25.0	60.2					24.0		24.0
Effective Green, g (s)		35.0	35.0	25.0	60.2					24.0		24.0
Actuated g/C Ratio		0.34	0.34	0.25	0.59					0.24		0.24
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2072	530	793	2039					824		662
v/s Ratio Prot		0.24	c0.25	c0.22	0.15					c0.12		0.01
v/s Ratio Perm												
v/c Ratio		0.69	0.72	0.92	0.25					0.52		0.06
Uniform Delay, d1		28.9	29.2	37.5	10.0					34.0		30.3
Progression Factor		1.00	1.00	1.35	1.12					1.00		1.00
Incremental Delay, d2		1.3	5.7	11.2	0.1					1.1		0.1
Delay (s)		30.2	34.9	62.0	11.4					35.2		30.3
Level of Service		C	C	E	B					D		C
Approach Delay (s)		31.8			41.2			0.0			33.8	
Approach LOS		C			D			A			C	
Intersection Summary												
HCM 2000 Control Delay			35.0			HCM 2000 Level of Service					C	
HCM 2000 Volume to Capacity ratio			0.72									
Actuated Cycle Length (s)			102.0			Sum of lost time (s)					18.0	
Intersection Capacity Utilization			84.8%			ICU Level of Service					E	
Analysis Period (min)			15									
c Critical Lane Group												

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2025 Build Condition Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	 	 			  		 		 			
Traffic Volume (vph)	751	862	0	0	933	407	229	0	625	0	0	0
Future Volume (vph)	751	862	0	0	933	407	229	0	625	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.95		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3236	3455			4917		3433		2814			
Flt Permitted	0.11	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	389	3455			4917		3433		2814			
Peak-hour factor, PHF	0.87	0.87	0.92	0.90	0.90	0.90	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	863	991	0	0	1037	452	244	0	665	0	0	0
RTOR Reduction (vph)	0	0	0	0	76	0	0	0	509	0	0	0
Lane Group Flow (vph)	863	991	0	0	1413	0	244	0	156	0	0	0
Heavy Vehicles (%)	1%	1%	0%	0%	1%	0%	2%	0%	1%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	59.8	35.0			35.2		24.0		24.0			
Effective Green, g (s)	59.8	35.0			35.2		24.0		24.0			
Actuated g/C Ratio	0.59	0.34			0.35		0.24		0.24			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	920	1185			1696		807		662			
v/s Ratio Prot	c0.23	0.29			0.29		c0.07		0.06			
v/s Ratio Perm	c0.32											
v/c Ratio	0.94	0.84			0.83		0.30		0.24			
Uniform Delay, d1	28.5	30.9			30.7		32.1		31.6			
Progression Factor	1.67	0.54			1.00		1.00		1.00			
Incremental Delay, d2	13.6	4.5			4.1		0.4		0.4			
Delay (s)	61.2	21.2			34.8		32.6		32.0			
Level of Service	E	C			C		C		C			
Approach Delay (s)		39.8			34.8			32.1			0.0	
Approach LOS		D			C			C			A	
Intersection Summary												
HCM 2000 Control Delay			36.4				HCM 2000 Level of Service				D	
HCM 2000 Volume to Capacity ratio			0.75									
Actuated Cycle Length (s)			102.0				Sum of lost time (s)				18.0	
Intersection Capacity Utilization			84.8%				ICU Level of Service				E	
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2025 Build Condition Weekday PM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	310	1653	1283	226	423	886
Future Volume (vph)	310	1653	1283	226	423	886
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3539	3539	1583	1787	1599
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3539	3539	1583	1787	1599
Peak-hour factor, PHF	0.88	0.88	0.93	0.93	0.87	0.87
Adj. Flow (vph)	352	1878	1380	243	486	1018
RTOR Reduction (vph)	0	0	0	169	0	166
Lane Group Flow (vph)	352	1878	1380	74	486	852
Heavy Vehicles (%)	1%	2%	2%	2%	1%	1%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	5.0	29.0	18.0	18.0	18.0	18.0
Effective Green, g (s)	5.0	29.0	18.0	18.0	18.0	18.0
Actuated g/C Ratio	0.08	0.49	0.31	0.31	0.31	0.31
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	151	1739	1079	482	545	487
v/s Ratio Prot	c0.20	0.53	c0.39		0.27	c0.53
v/s Ratio Perm				0.05		
v/c Ratio	2.33	1.08	1.28	0.15	0.89	1.75
Uniform Delay, d1	27.0	15.0	20.5	14.9	19.6	20.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	619.2	46.7	132.8	0.7	17.0	345.6
Delay (s)	646.2	61.7	153.3	15.6	36.6	366.1
Level of Service	F	E	F	B	D	F
Approach Delay (s)		154.0	132.7		259.6	
Approach LOS		F	F		F	

Intersection Summary

HCM 2000 Control Delay	177.2	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.61		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	100.3%	ICU Level of Service	G
Analysis Period (min)	15		
c Critical Lane Group			

201: International Drive & Corporate Drive
 2025 Build Condition Weekday PM Peak

Intersection	
Intersection Delay, s/veh	164.8
Intersection LOS	F

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↵	↵		↵	↶	↵	↵	↶↵		↵	↶	↵
Traffic Vol, veh/h	140	4	15	9	24	598	15	566	7	70	90	87
Future Vol, veh/h	140	4	15	9	24	598	15	566	7	70	90	87
Peak Hour Factor	0.84	0.84	0.84	0.77	0.77	0.77	0.89	0.89	0.89	0.93	0.93	0.93
Heavy Vehicles, %	0	0	0	0	6	1	0	1	0	4	3	0
Mvmt Flow	167	5	18	12	31	777	17	636	8	75	97	94
Number of Lanes	1	1	0	1	1	1	1	2	0	1	1	1

Approach	EB	WB	NB	SB
Opposing Approach	WB	EB	SB	NB
Opposing Lanes	3	2	3	3
Conflicting Approach Left	SB	NB	EB	WB
Conflicting Lanes Left	3	3	2	3
Conflicting Approach Right	NB	SB	WB	EB
Conflicting Lanes Right	3	3	3	2
HCM Control Delay	21.3	334.1	55.3	16.8
HCM LOS	C	F	F	C

Lane	NBLn1	NBLn2	NBLn3	EBLn1	EBLn2	WBLn1	WBLn2	WBLn3	SBLn1	SBLn2	SBLn3
Vol Left, %	100%	0%	0%	100%	0%	100%	0%	0%	100%	0%	0%
Vol Thru, %	0%	100%	96%	0%	21%	0%	100%	0%	0%	100%	0%
Vol Right, %	0%	0%	4%	0%	79%	0%	0%	100%	0%	0%	100%
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop	Stop
Traffic Vol by Lane	15	377	196	140	19	9	24	598	70	90	87
LT Vol	15	0	0	140	0	9	0	0	70	0	0
Through Vol	0	377	189	0	4	0	24	0	0	90	0
RT Vol	0	0	7	0	15	0	0	598	0	0	87
Lane Flow Rate	17	424	220	167	23	12	31	777	75	97	94
Geometry Grp	8	8	8	8	8	8	8	8	8	8	8
Degree of Util (X)	0.041	0.982	0.507	0.456	0.055	0.03	0.076	1.718	0.207	0.253	0.225
Departure Headway (Hd)	10.284	9.784	9.74	10.904	9.851	9.161	8.757	7.962	11.565	11.023	10.236
Convergence, Y/N	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes	Yes
Cap	350	373	374	333	366	391	410	458	312	328	353
Service Time	7.984	7.484	7.44	8.604	7.551	6.905	6.501	5.705	9.265	8.723	7.936
HCM Lane V/C Ratio	0.049	1.137	0.588	0.502	0.063	0.031	0.076	1.697	0.24	0.296	0.266
HCM Control Delay	13.4	74.3	22	22.4	13.1	12.2	12.2	351.9	17.3	17.4	15.9
HCM Lane LOS	B	F	C	C	B	B	B	F	C	C	C
HCM 95th-tile Q	0.1	11.2	2.8	2.3	0.2	0.1	0.2	46.6	0.8	1	0.8

202: Goose Bay Drive & Corporate Drive
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	201					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↔			↔	↔	
Traffic Vol, veh/h	64	17	12	356	275	64
Future Vol, veh/h	64	17	12	356	275	64
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	70	70	73	73	40	40
Heavy Vehicles, %	4	0	0	2	0	0
Mvmt Flow	91	24	16	488	688	160

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	115	0	623
Stage 1	-	-	-	-	103
Stage 2	-	-	-	-	520
Critical Hdwy	-	-	4.1	-	6.4
Critical Hdwy Stg 1	-	-	-	-	5.4
Critical Hdwy Stg 2	-	-	-	-	5.4
Follow-up Hdwy	-	-	2.2	-	3.5
Pot Cap-1 Maneuver	-	-	1487	- ~	453
Stage 1	-	-	-	-	926
Stage 2	-	-	-	- ~	601
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1487	- ~	446
Mov Cap-2 Maneuver	-	-	-	- ~	446
Stage 1	-	-	-	-	926
Stage 2	-	-	-	- ~	592

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	\$ 347.8
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	496	-	-	1487	-
HCM Lane V/C Ratio	1.709	-	-	0.011	-
HCM Control Delay (s)	\$ 347.8	-	-	7.4	0
HCM Lane LOS	F	-	-	A	A
HCM 95th %tile Q(veh)	50.3	-	-	0	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

203: Corporate Drive & Redhook Way
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	7	121	358	3	1	12
Future Vol, veh/h	7	121	358	3	1	12
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	63	63	77	77	36	36
Heavy Vehicles, %	40	0	0	1	0	11
Mvmt Flow	11	192	465	4	3	33

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	469	0	-	0	681 467
Stage 1	-	-	-	-	467 -
Stage 2	-	-	-	-	214 -
Critical Hdwy	4.5	-	-	-	6.4 6.31
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.56	-	-	-	3.5 3.399
Pot Cap-1 Maneuver	920	-	-	-	419 578
Stage 1	-	-	-	-	635 -
Stage 2	-	-	-	-	826 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	920	-	-	-	414 578
Mov Cap-2 Maneuver	-	-	-	-	414 -
Stage 1	-	-	-	-	627 -
Stage 2	-	-	-	-	826 -

Approach	EB	WB	SB
HCM Control Delay, s	0.5	0	11.9
HCM LOS			B

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	920	-	-	-	561
HCM Lane V/C Ratio	0.012	-	-	-	0.064
HCM Control Delay (s)	9	-	-	-	11.9
HCM Lane LOS	A	-	-	-	B
HCM 95th %tile Q(veh)	0	-	-	-	0.2

204: Goose Bay Drive & Corporate Drive
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	128	1	0	203	11	0
Future Vol, veh/h	128	1	0	203	11	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	81	81	71	71
Heavy Vehicles, %	0	0	0	1	11	0
Mvmt Flow	164	1	0	251	15	0

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	165	0	416
Stage 1	-	-	-	-	165
Stage 2	-	-	-	-	251
Critical Hdwy	-	-	4.1	-	6.51
Critical Hdwy Stg 1	-	-	-	-	5.51
Critical Hdwy Stg 2	-	-	-	-	5.51
Follow-up Hdwy	-	-	2.2	-	3.599
Pot Cap-1 Maneuver	-	-	1426	-	576
Stage 1	-	-	-	-	843
Stage 2	-	-	-	-	770
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1426	-	576
Mov Cap-2 Maneuver	-	-	-	-	576
Stage 1	-	-	-	-	843
Stage 2	-	-	-	-	770

Approach	EB	WB	NB
HCM Control Delay, s	0	0	11.4
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	576	-	-	1426	-
HCM Lane V/C Ratio	0.027	-	-	-	-
HCM Control Delay (s)	11.4	-	-	0	-
HCM Lane LOS	B	-	-	A	-
HCM 95th %tile Q(veh)	0.1	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	1	11	0	0	1	0
Future Vol, veh/h	1	11	0	0	1	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	67	67	69	69	50	50
Heavy Vehicles, %	0	0	10	0	0	0
Mvmt Flow	1	16	0	0	2	0

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	4	0	0	0	0	0
Stage 1	0	-	-	-	-	-
Stage 2	4	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	1023	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	1024	-	-	-	-	-
Platoon blocked, %						
Mov Cap-1 Maneuver	1023	-	-	-	-	-
Mov Cap-2 Maneuver	1023	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	1024	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s		0	
HCM LOS	-		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-
HCM Control Delay (s)	-	-	-	-
HCM Lane LOS	-	-	-	-
HCM 95th %tile Q(veh)	-	-	-	-

206: Goose Bay Drive & Lonza South Dwy
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	6.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	3	0	0	1	0	0
Future Vol, veh/h	3	0	0	1	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	25	25	63	63	63	63
Heavy Vehicles, %	0	0	0	0	10	0
Mvmt Flow	12	0	0	2	0	0

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	4	2	2	0	-	0
Stage 1	2	-	-	-	-	-
Stage 2	2	-	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-	-
Pot Cap-1 Maneuver	1023	1088	1634	-	-	-
Stage 1	1026	-	-	-	-	-
Stage 2	1026	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	1023	1088	1634	-	-	-
Mov Cap-2 Maneuver	1023	-	-	-	-	-
Stage 1	1026	-	-	-	-	-
Stage 2	1026	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	8.6	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1634	-	1023	-	-
HCM Lane V/C Ratio	-	-	0.012	-	-
HCM Control Delay (s)	0	-	8.6	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Lonza Parking Garage & Goose Bay Drive
 2025 Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	3.3											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	144	0	195	0	13	11	5
Future Vol, veh/h	0	0	0	0	0	144	0	195	0	13	11	5
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	39	39	92	92	67	67
Heavy Vehicles, %	2	2	2	2	2	2	0	0	2	2	0	0
Mvmt Flow	0	0	0	0	0	157	0	500	0	14	16	7

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	627	548	20	548	551	500	23	0	0	500	0	0
Stage 1	48	48	-	500	500	-	-	-	-	-	-	-
Stage 2	579	500	-	48	51	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	396	444	1058	447	442	571	1605	-	-	1064	-	-
Stage 1	965	855	-	553	543	-	-	-	-	-	-	-
Stage 2	501	543	-	965	852	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	285	438	1058	443	436	571	1605	-	-	1064	-	-
Mov Cap-2 Maneuver	285	438	-	443	436	-	-	-	-	-	-	-
Stage 1	965	844	-	553	543	-	-	-	-	-	-	-
Stage 2	364	543	-	952	841	-	-	-	-	-	-	-

Approach	EB	WB	NB	SB
HCM Control Delay, s	0	13.7	0	3.1
HCM LOS	A	B		

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1605	-	-	-	571	1064	-
HCM Lane V/C Ratio	-	-	-	-	0.274	0.013	-
HCM Control Delay (s)	0	-	-	0	13.7	8.4	0
HCM Lane LOS	A	-	-	A	B	A	A
HCM 95th %tile Q(veh)	0	-	-	-	1.1	0	-

208: Granite State Driveway & International Drive
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	FF		FB			FB
Traffic Vol, veh/h	7	3	586	1	4	103
Future Vol, veh/h	7	3	586	1	4	103
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	78	78	76	76
Heavy Vehicles, %	0	0	1	0	0	4
Mvmt Flow	8	3	751	1	5	136

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	898	752	0	0	752	0
Stage 1	752	-	-	-	-	-
Stage 2	146	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	312	413	-	-	867	-
Stage 1	469	-	-	-	-	-
Stage 2	886	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	310	413	-	-	867	-
Mov Cap-2 Maneuver	310	-	-	-	-	-
Stage 1	469	-	-	-	-	-
Stage 2	881	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	16.1	0	0.3
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	335	867
HCM Lane V/C Ratio	-	-	0.034	0.006
HCM Control Delay (s)	-	-	16.1	9.2
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	7.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	W	T	T	T	T
Traffic Vol, veh/h	49	150	437	15	13	97
Future Vol, veh/h	49	150	437	15	13	97
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	72	72	67	67	81	81
Heavy Vehicles, %	14	0	1	46	0	3
Mvmt Flow	68	208	652	22	16	120

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	815	663	0	0	674	0
Stage 1	663	-	-	-	-	-
Stage 2	152	-	-	-	-	-
Critical Hdwy	6.54	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.54	-	-	-	-	-
Critical Hdwy Stg 2	5.54	-	-	-	-	-
Follow-up Hdwy	3.626	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	331	465	-	-	927	-
Stage 1	491	-	-	-	-	-
Stage 2	847	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	325	465	-	-	927	-
Mov Cap-2 Maneuver	325	-	-	-	-	-
Stage 1	491	-	-	-	-	-
Stage 2	832	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	28.6	0	1.1
HCM LOS	D		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	420	927
HCM Lane V/C Ratio	-	-	0.658	0.017
HCM Control Delay (s)	-	-	28.6	9
HCM Lane LOS	-	-	D	A
HCM 95th %tile Q(veh)	-	-	4.6	0.1

210: International Drive & Lonza South Driveway
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	4	358	0	0	164
Future Vol, veh/h	0	4	358	0	0	164
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	68	68	74	74
Heavy Vehicles, %	0	0	3	0	0	7
Mvmt Flow	0	16	526	0	0	222

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	748	526	0	0	526	0
Stage 1	526	-	-	-	-	-
Stage 2	222	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	383	556	-	-	1051	-
Stage 1	597	-	-	-	-	-
Stage 2	820	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	383	556	-	-	1051	-
Mov Cap-2 Maneuver	383	-	-	-	-	-
Stage 1	597	-	-	-	-	-
Stage 2	820	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	11.7	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	556	1051
HCM Lane V/C Ratio	-	-	0.029	-
HCM Control Delay (s)	-	-	11.7	0
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2025 Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	126.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	28	20	3	285	19	20	1	297	103	3	513	12
Future Vol, veh/h	28	20	3	285	19	20	1	297	103	3	513	12
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	54	54	54	85	85	85	84	84	84	88	88	88
Heavy Vehicles, %	0	13	0	0	14	0	0	2	1	0	1	11
Mvmt Flow	52	37	6	335	22	24	1	354	123	3	583	14

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1037	1075	590	1036	1021	416	597	0	0	477	0	0
Stage 1	596	596	-	418	418	-	-	-	-	-	-	-
Stage 2	441	479	-	618	603	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.63	6.2	7.1	6.64	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4.117	3.3	3.5	4.126	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	211	210	511	~ 212	225	641	989	-	-	1096	-	-
Stage 1	494	475	-	616	570	-	-	-	-	-	-	-
Stage 2	599	537	-	480	470	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	187	209	511	~ 180	224	641	989	-	-	1096	-	-
Mov Cap-2 Maneuver	187	209	-	~ 180	224	-	-	-	-	-	-	-
Stage 1	494	473	-	615	569	-	-	-	-	-	-	-
Stage 2	554	536	-	436	468	-	-	-	-	-	-	-

Approach	EB		WB		NB			SB		
HCM Control Delay, s	37.3		\$ 506.9		0			0		
HCM LOS	E		F							

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	989	-	-	203	191	1096	-	-
HCM Lane V/C Ratio	0.001	-	-	0.465	1.996	0.003	-	-
HCM Control Delay (s)	8.6	0	-	37.3	\$ 506.9	8.3	0	-
HCM Lane LOS	A	A	-	E	F	A	A	-
HCM 95th %tile Q(veh)	0	-	-	2.2	28.7	0	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2025 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	101.3					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↘	↗	↘	↗	↗	↘
Traffic Vol, veh/h	340	77	246	46	24	793
Future Vol, veh/h	340	77	246	46	24	793
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	86	86	76	76	83	83
Heavy Vehicles, %	2	2	1	3	0	1
Mvmt Flow	395	90	324	61	29	955

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	738	29	984	0	0
Stage 1	29	-	-	-	-
Stage 2	709	-	-	-	-
Critical Hdwy	6.42	6.22	4.11	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.209	-	-
Pot Cap-1 Maneuver	~ 385	1046	706	-	-
Stage 1	994	-	-	-	-
Stage 2	488	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	~ 208	1046	706	-	-
Mov Cap-2 Maneuver	~ 208	-	-	-	-
Stage 1	538	-	-	-	-
Stage 2	488	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	377.7	12.1	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	706	-	208	1046	-	-
HCM Lane V/C Ratio	0.458	-	1.901	0.086	-	-
HCM Control Delay (s)	14.3	-	461.3	8.8	-	-
HCM Lane LOS	B	-	F	A	-	-
HCM 95th %tile Q(veh)	2.4	-	28.6	0.3	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2025 Build Condition Weekday PM Peak





















Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↑			↑↑
Traffic Vol, veh/h	0	66	536	0	0	1309
Future Vol, veh/h	0	66	536	0	0	1309
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	73	73	95	95	89	89
Heavy Vehicles, %	0	13	0	1	0	1
Mvmt Flow	0	90	564	0	0	1471

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	-	564	0	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Critical Hdwy	-	6.395	-	-	-	-
Critical Hdwy Stg 1	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-
Follow-up Hdwy	-	3.4235	-	-	-	-
Pot Cap-1 Maneuver	0	499	-	0	0	-
Stage 1	0	-	-	0	0	-
Stage 2	0	-	-	0	0	-
Platoon blocked, %			-			-
Mov Cap-1 Maneuver	-	499	-	-	-	-
Mov Cap-2 Maneuver	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	13.8	0	0
HCM LOS	B		













Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 499	-
HCM Lane V/C Ratio	- 0.181	-
HCM Control Delay (s)	- 13.8	-
HCM Lane LOS	- B	-
HCM 95th %tile Q(veh)	- 0.7	-

101: International Dr & Pease Blvd
 2035 No Build Condition Weekday AM Peak

													
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	3	115	7	1405	704	145	9	6	356	7	2	2	
Future Volume (vph)	3	115	7	1405	704	145	9	6	356	7	2	2	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12	
Total Lost time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Lane Util. Factor	1.00	0.95		0.97	0.95			1.00	0.88		1.00		
Frt	1.00	0.99		1.00	0.97			1.00	0.85		0.98		
Flt Protected	0.95	1.00		0.95	1.00			0.97	1.00		0.97		
Satd. Flow (prot)	1805	3514		3467	3474			1784	2682		2036		
Flt Permitted	0.95	1.00		0.95	1.00			0.88	1.00		0.87		
Satd. Flow (perm)	1805	3514		3467	3474			1613	2682		1819		
Peak-hour factor, PHF	0.84	0.84	0.84	0.83	1.00	0.83	0.88	0.88	0.88	0.63	0.63	0.63	
Adj. Flow (vph)	4	137	8	1693	704	175	10	7	405	11	3	3	
RTOR Reduction (vph)	0	4	0	0	11	0	0	0	0	0	2	0	
Lane Group Flow (vph)	4	141	0	1693	868	0	0	17	405	0	15	0	
Heavy Vehicles (%)	0%	2%	0%	1%	1%	0%	0%	0%	6%	0%	0%	0%	
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA		
Protected Phases	6	2		1	5			8			4		
Permitted Phases							8		8		4		
Actuated Green, G (s)	6.3	13.2		50.1	58.0			18.8	18.8		18.8		
Effective Green, g (s)	6.3	13.2		50.1	58.0			18.8	18.8		18.8		
Actuated g/C Ratio	0.06	0.13		0.50	0.58			0.19	0.19		0.19		
Clearance Time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0		
Vehicle Extension (s)	2.0	3.0		3.0	3.0			3.0	3.0		3.0		
Lane Grp Cap (vph)	113	463		1735	2012			302	503		341		
v/s Ratio Prot	0.00	c0.04		c0.49	c0.25								
v/s Ratio Perm								0.01	c0.15		0.01		
v/c Ratio	0.04	0.30		0.98	0.43			0.06	0.81		0.04		
Uniform Delay, d1	44.0	39.3		24.4	11.8			33.4	38.9		33.3		
Progression Factor	1.00	1.00		1.00	1.00			1.00	1.00		1.00		
Incremental Delay, d2	0.0	0.4		16.1	0.1			0.1	9.1		0.1		
Delay (s)	44.1	39.7		40.5	12.0			33.4	48.0		33.3		
Level of Service	D	D		D	B			C	D		C		
Approach Delay (s)		39.8			30.7			47.4			33.3		
Approach LOS		D			C			D			C		
Intersection Summary													
HCM 2000 Control Delay			33.4		HCM 2000 Level of Service					C			
HCM 2000 Volume to Capacity ratio			0.83										
Actuated Cycle Length (s)			100.1		Sum of lost time (s)					18.0			
Intersection Capacity Utilization			66.7%		ICU Level of Service					C			
Analysis Period (min)			15										

c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2035 No Build Condition Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↘↗
Traffic Volume (vph)	0	334	144	174	1172	0	0	0	0	625	0	961
Future Volume (vph)	0	334	144	174	1172	0	0	0	0	625	0	961
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		5981	1419	2918	3455					3467		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		5981	1419	2918	3455					3467		2814
Peak-hour factor, PHF	0.80	0.80	0.80	0.80	0.80	0.80	0.92	0.92	0.92	0.75	0.75	0.75
Adj. Flow (vph)	0	418	180	218	1465	0	0	0	0	833	0	1281
RTOR Reduction (vph)	0	0	119	0	0	0	0	0	0	0	0	72
Lane Group Flow (vph)	0	418	61	218	1465	0	0	0	0	833	0	1209
Heavy Vehicles (%)	0%	2%	10%	12%	1%	0%	2%	2%	2%	1%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		34.5	34.5	25.0	65.5					25.0		25.0
Effective Green, g (s)		34.5	34.5	25.0	65.5					25.0		25.0
Actuated g/C Ratio		0.34	0.34	0.24	0.64					0.24		0.24
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2013	477	711	2207					845		686
v/s Ratio Prot		0.07	0.04	0.07	c0.42					0.24		c0.43
v/s Ratio Perm												
v/c Ratio		0.21	0.13	0.31	0.66					0.99		1.76
Uniform Delay, d1		24.3	23.6	31.7	11.6					38.6		38.8
Progression Factor		1.00	1.00	0.90	1.55					1.00		1.00
Incremental Delay, d2		0.1	0.3	0.1	0.2					27.4		349.1
Delay (s)		24.4	23.8	28.6	18.2					66.0		387.9
Level of Service		C	C	C	B					E		F
Approach Delay (s)		24.2			19.6			0.0			261.0	
Approach LOS		C			B			A			F	
Intersection Summary												
HCM 2000 Control Delay			136.4			HCM 2000 Level of Service				F		
HCM 2000 Volume to Capacity ratio			1.04									
Actuated Cycle Length (s)			102.5			Sum of lost time (s)				18.0		
Intersection Capacity Utilization			82.7%			ICU Level of Service				E		
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2035 No Build Condition Weekday AM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	150	809	0	0	472	86	874	0	405	0	0	0	
Future Volume (vph)	150	809	0	0	472	86	874	0	405	0	0	0	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12	
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0				
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88				
Frt	1.00	1.00			0.98		1.00		0.85				
Flt Protected	0.95	1.00			1.00		0.95		1.00				
Satd. Flow (prot)	3113	3421			4945		3433		2733				
Flt Permitted	0.39	1.00			1.00		0.95		1.00				
Satd. Flow (perm)	1282	3421			4945		3433		2733				
Peak-hour factor, PHF	0.87	0.87	0.87	0.85	0.85	0.85	0.78	0.78	0.78	0.92	0.92	0.92	
Adj. Flow (vph)	172	930	0	0	555	101	1121	0	519	0	0	0	
RTOR Reduction (vph)	0	0	0	0	22	0	0	0	345	0	0	0	
Lane Group Flow (vph)	172	930	0	0	634	0	1121	0	174	0	0	0	
Heavy Vehicles (%)	5%	2%	0%	0%	2%	5%	2%	2%	4%	0%	0%	0%	
Turn Type	pm+pt	NA			NA		Prot		Prot				
Protected Phases	1	6			2		3		3				
Permitted Phases	6												
Actuated Green, G (s)	51.5	34.5			42.5		25.0		25.0				
Effective Green, g (s)	51.5	34.5			42.5		25.0		25.0				
Actuated g/C Ratio	0.50	0.34			0.41		0.24		0.24				
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0				
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0				
Lane Grp Cap (vph)	947	1151			2050		837		666				
v/s Ratio Prot	c0.03	c0.27			c0.13		c0.33		0.06				
v/s Ratio Perm	0.06												
v/c Ratio	0.18	0.81			0.31		1.34		0.26				
Uniform Delay, d1	13.4	31.0			20.1		38.8		31.3				
Progression Factor	1.10	1.25			1.00		1.00		1.00				
Incremental Delay, d2	0.1	3.3			0.2		160.8		0.4				
Delay (s)	14.8	41.9			20.3		199.5		31.7				
Level of Service	B	D			C		F		C				
Approach Delay (s)		37.7			20.3		146.4				0.0		
Approach LOS		D			C		F				A		
Intersection Summary													
HCM 2000 Control Delay			86.8		HCM 2000 Level of Service				F				
HCM 2000 Volume to Capacity ratio			0.78										
Actuated Cycle Length (s)			102.5		Sum of lost time (s)				18.0				
Intersection Capacity Utilization			82.7%		ICU Level of Service				E				
Analysis Period (min)			15										

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2035 No Build Condition Weekday AM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	685	2242	808	643	178	207
Future Volume (vph)	685	2242	808	643	178	207
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3471	3343	1583	1719	1538
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3471	3343	1583	1719	1538
Peak-hour factor, PHF	0.86	0.86	0.96	0.96	0.76	0.76
Adj. Flow (vph)	797	2607	842	670	234	272
RTOR Reduction (vph)	0	0	0	466	0	195
Lane Group Flow (vph)	797	2607	842	204	234	77
Heavy Vehicles (%)	1%	4%	8%	2%	5%	5%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	8.8	32.8	18.0	18.0	14.2	14.2
Effective Green, g (s)	8.8	32.8	18.0	18.0	14.2	14.2
Actuated g/C Ratio	0.15	0.56	0.31	0.31	0.24	0.24
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	266	1929	1019	482	413	370
v/s Ratio Prot	c0.45	c0.75	0.25		c0.14	0.05
v/s Ratio Perm				0.13		
v/c Ratio	3.00	1.35	0.83	0.42	0.57	0.21
Uniform Delay, d1	25.1	13.1	19.0	16.4	19.7	17.9
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	908.4	161.7	7.7	2.7	2.2	0.4
Delay (s)	933.5	174.8	26.7	19.1	21.9	18.3
Level of Service	F	F	C	B	C	B
Approach Delay (s)		352.4	23.3		19.9	
Approach LOS		F	C		B	
Intersection Summary						
HCM 2000 Control Delay			229.6		HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio			1.51			
Actuated Cycle Length (s)			59.0		Sum of lost time (s)	18.0
Intersection Capacity Utilization			87.8%		ICU Level of Service	E
Analysis Period (min)			15			
c Critical Lane Group						

105: International Drive & Corporate Drive
 2035 No Build Condition Weekday AM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR	
Lane Configurations													
Traffic Volume (vph)	77	48	34	16	15	84	9	159	71	718	515	151	
Future Volume (vph)	77	48	34	16	15	84	9	159	71	718	515	151	
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	
Total Lost time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0	
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	0.95		1.00	1.00	1.00	
Frt	1.00	0.94		1.00	1.00	0.85	1.00	0.95		1.00	1.00	0.85	
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00	
Satd. Flow (prot)	1805	1706		1805	1681	1369	1805	3411		1770	1900	1615	
Flt Permitted	0.75	1.00		0.69	1.00	1.00	0.41	1.00		0.42	1.00	1.00	
Satd. Flow (perm)	1416	1706		1306	1681	1369	774	3411		791	1900	1615	
Peak-hour factor, PHF	0.76	0.76	0.76	0.78	0.78	0.78	0.83	0.83	0.83	0.76	0.76	0.76	
Adj. Flow (vph)	101	63	45	21	19	108	11	192	86	945	678	199	
RTOR Reduction (vph)	0	24	0	0	0	91	0	47	0	0	0	61	
Lane Group Flow (vph)	101	84	0	21	19	17	11	231	0	945	678	138	
Heavy Vehicles (%)	0%	4%	5%	0%	13%	18%	0%	0%	3%	2%	0%	0%	
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm	
Protected Phases		4			8			2		1	6		
Permitted Phases	4			8		8	2			6		6	
Actuated Green, G (s)	13.3	13.3		13.3	13.3	13.3	13.0	13.0		57.8	57.8	57.8	
Effective Green, g (s)	13.3	13.3		13.3	13.3	13.3	13.0	13.0		57.8	57.8	57.8	
Actuated g/C Ratio	0.16	0.16		0.16	0.16	0.16	0.16	0.16		0.70	0.70	0.70	
Clearance Time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0	
Vehicle Extension (s)	3.0	3.0		3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0	
Lane Grp Cap (vph)	226	273		209	269	219	121	533		1024	1321	1123	
v/s Ratio Prot		0.05			0.01			0.07		c0.45	0.36		
v/s Ratio Perm	c0.07			0.02		0.01	0.01			c0.19		0.09	
v/c Ratio	0.45	0.31		0.10	0.07	0.08	0.09	0.43		0.92	0.51	0.12	
Uniform Delay, d1	31.6	30.8		29.8	29.6	29.7	30.0	31.7		10.9	6.0	4.2	
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00	
Incremental Delay, d2	1.4	0.6		0.2	0.1	0.2	0.3	0.6		13.3	0.3	0.0	
Delay (s)	33.0	31.5		30.0	29.8	29.8	30.3	32.3		24.2	6.3	4.3	
Level of Service	C	C		C	C	C	C	C		C	A	A	
Approach Delay (s)		32.2			29.9			32.2			15.4		
Approach LOS		C			C			C			B		
Intersection Summary													
HCM 2000 Control Delay			19.6		HCM 2000 Level of Service						B		
HCM 2000 Volume to Capacity ratio			0.87										
Actuated Cycle Length (s)			83.1		Sum of lost time (s)					16.5			
Intersection Capacity Utilization			73.6%		ICU Level of Service					D			
Analysis Period (min)			15										
c Critical Lane Group													

202: Goose Bay Drive & Corporate Drive
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	560	277	25	94	21	0
Future Vol, veh/h	560	277	25	94	21	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	71	71	69	69
Heavy Vehicles, %	1	5	0	12	36	0
Mvmt Flow	718	355	35	132	30	0

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	1073	0	1098
Stage 1	-	-	-	-	896
Stage 2	-	-	-	-	202
Critical Hdwy	-	-	4.1	-	6.76
Critical Hdwy Stg 1	-	-	-	-	5.76
Critical Hdwy Stg 2	-	-	-	-	5.76
Follow-up Hdwy	-	-	2.2	-	3.824
Pot Cap-1 Maneuver	-	-	657	-	203
Stage 1	-	-	-	-	348
Stage 2	-	-	-	-	757
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	657	-	191
Mov Cap-2 Maneuver	-	-	-	-	191
Stage 1	-	-	-	-	348
Stage 2	-	-	-	-	713

Approach	EB	WB	NB
HCM Control Delay, s	0	2.3	27.4
HCM LOS			D

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	191	-	-	657	-
HCM Lane V/C Ratio	0.159	-	-	0.054	-
HCM Control Delay (s)	27.4	-	-	10.8	0
HCM Lane LOS	D	-	-	B	A
HCM 95th %tile Q(veh)	0.6	-	-	0.2	-

203: Corporate Drive & Redhook Way
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	19	543	96	2	0	7
Future Vol, veh/h	19	543	96	2	0	7
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	85	85	71	71	50	50
Heavy Vehicles, %	0	1	8	0	0	25
Mvmt Flow	22	639	135	3	0	14

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	138	0	-	0	820 137
Stage 1	-	-	-	-	137 -
Stage 2	-	-	-	-	683 -
Critical Hdwy	4.1	-	-	-	6.4 6.45
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.2	-	-	-	3.5 3.525
Pot Cap-1 Maneuver	1458	-	-	-	347 854
Stage 1	-	-	-	-	895 -
Stage 2	-	-	-	-	505 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	1458	-	-	-	342 854
Mov Cap-2 Maneuver	-	-	-	-	342 -
Stage 1	-	-	-	-	882 -
Stage 2	-	-	-	-	505 -

Approach	EB	WB	SB
HCM Control Delay, s	0.3	0	9.3
HCM LOS			A

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	1458	-	-	-	854
HCM Lane V/C Ratio	0.015	-	-	-	0.016
HCM Control Delay (s)	7.5	-	-	-	9.3
HCM Lane LOS	A	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	0.1

204: Goose Bay Drive & Corporate Drive
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	322	8	8	119	10	6
Future Vol, veh/h	322	8	8	119	10	6
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	95	95	82	82	25	40
Heavy Vehicles, %	1	0	0	5	20	0
Mvmt Flow	339	8	10	145	40	15

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	347	0	508
Stage 1	-	-	-	-	343
Stage 2	-	-	-	-	165
Critical Hdwy	-	-	4.1	-	6.6
Critical Hdwy Stg 1	-	-	-	-	5.6
Critical Hdwy Stg 2	-	-	-	-	5.6
Follow-up Hdwy	-	-	2.2	-	3.68
Pot Cap-1 Maneuver	-	-	1223	-	494
Stage 1	-	-	-	-	680
Stage 2	-	-	-	-	822
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1223	-	490
Mov Cap-2 Maneuver	-	-	-	-	490
Stage 1	-	-	-	-	680
Stage 2	-	-	-	-	815

Approach	EB	WB	NB
HCM Control Delay, s	0	0.5	12.5
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	534	-	-	1223	-
HCM Lane V/C Ratio	0.103	-	-	0.008	-
HCM Control Delay (s)	12.5	-	-	8	0
HCM Lane LOS	B	-	-	A	A
HCM 95th %tile Q(veh)	0.3	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1.1					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	0	16	15	7	9
Future Vol, veh/h	0	0	16	15	7	9
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	53	53	50	50
Heavy Vehicles, %	0	0	0	13	0	0
Mvmt Flow	0	0	30	28	14	18

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	90	44	0	0	58
Stage 1	44	-	-	-	-
Stage 2	46	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	915	1032	-	-	1559
Stage 1	984	-	-	-	-
Stage 2	982	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	907	1032	-	-	1559
Mov Cap-2 Maneuver	907	-	-	-	-
Stage 1	984	-	-	-	-
Stage 2	973	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	0	0	3.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	-	1559
HCM Lane V/C Ratio	-	-	-	0.009
HCM Control Delay (s)	-	-	0	7.3
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	-	0

206: Goose Bay Drive & Lonza South Dwy
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	1.5					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	7	0	0	9	31	9
Future Vol, veh/h	7	0	0	9	31	9
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	50	50	42	42	69	69
Heavy Vehicles, %	75	0	0	0	6	80
Mvmt Flow	14	0	0	21	45	13

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	73	52	58	0	0
Stage 1	52	-	-	-	-
Stage 2	21	-	-	-	-
Critical Hdwy	7.15	6.2	4.1	-	-
Critical Hdwy Stg 1	6.15	-	-	-	-
Critical Hdwy Stg 2	6.15	-	-	-	-
Follow-up Hdwy	4.175	3.3	2.2	-	-
Pot Cap-1 Maneuver	778	1021	1559	-	-
Stage 1	813	-	-	-	-
Stage 2	842	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	778	1021	1559	-	-
Mov Cap-2 Maneuver	778	-	-	-	-
Stage 1	813	-	-	-	-
Stage 2	842	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	9.7	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1559	-	778	-	-
HCM Lane V/C Ratio	-	-	0.018	-	-
HCM Control Delay (s)	0	-	9.7	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0.1	-	-

207: Goose Bay Drive & Lonza Parking Garage/Proposed Dwy
 2035 No Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	0.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	6	21	0	0	59	243
Future Vol, veh/h	0	0	0	0	0	0	6	21	0	0	59	243
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	88	88	92	92	69	69
Heavy Vehicles, %	2	2	2	2	2	2	0	18	2	2	15	1
Mvmt Flow	0	0	0	0	0	0	7	24	0	0	86	352

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	300	300	262	300	476	24	438	0	0	24	0	0
Stage 1	262	262	-	38	38	-	-	-	-	-	-	-
Stage 2	38	38	-	262	438	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	652	612	777	652	488	1052	1133	-	-	1591	-	-
Stage 1	743	691	-	977	863	-	-	-	-	-	-	-
Stage 2	977	863	-	743	579	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	649	608	777	649	485	1052	1133	-	-	1591	-	-
Mov Cap-2 Maneuver	649	608	-	649	485	-	-	-	-	-	-	-
Stage 1	739	691	-	971	858	-	-	-	-	-	-	-
Stage 2	971	858	-	743	579	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		0		1.8		0	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1133	-	-	-	-	1591	-	-
HCM Lane V/C Ratio	0.006	-	-	-	-	-	-	-
HCM Control Delay (s)	8.2	0	-	0	0	0	-	-
HCM Lane LOS	A	A	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		B			4
Traffic Vol, veh/h	7	2	223	15	15	504
Future Vol, veh/h	7	2	223	15	15	504
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	63	63	81	81	84	84
Heavy Vehicles, %	0	0	0	0	0	1
Mvmt Flow	11	3	275	19	18	600

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	921	285	0	0	294
Stage 1	285	-	-	-	-
Stage 2	636	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	303	759	-	-	1279
Stage 1	768	-	-	-	-
Stage 2	531	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	297	759	-	-	1279
Mov Cap-2 Maneuver	297	-	-	-	-
Stage 1	768	-	-	-	-
Stage 2	520	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	16	0	0.2
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	343	1279
HCM Lane V/C Ratio	-	-	0.042	0.014
HCM Control Delay (s)	-	-	16	7.9
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	16	21	217	15	23	488
Future Vol, veh/h	16	21	217	15	23	488
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	86	86	83	83
Heavy Vehicles, %	44	0	1	63	0	1
Mvmt Flow	18	24	252	17	28	588

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	905	261	0	0	269	0
Stage 1	261	-	-	-	-	-
Stage 2	644	-	-	-	-	-
Critical Hdwy	6.84	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.896	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	260	783	-	-	1306	-
Stage 1	695	-	-	-	-	-
Stage 2	451	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	252	783	-	-	1306	-
Mov Cap-2 Maneuver	252	-	-	-	-	-
Stage 1	695	-	-	-	-	-
Stage 2	437	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	14.8	0	0.4
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	410	1306
HCM Lane V/C Ratio	-	-	0.103	0.021
HCM Control Delay (s)	-	-	14.8	7.8
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.3	0.1

210: International Drive & Lonza South Driveway
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	6	253	2	9	392
Future Vol, veh/h	0	6	253	2	9	392
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	75	75	89	89	81	81
Heavy Vehicles, %	0	0	5	100	0	2
Mvmt Flow	0	8	284	2	11	484

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	791	285	0	0	286
Stage 1	285	-	-	-	-
Stage 2	506	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	361	759	-	-	1288
Stage 1	768	-	-	-	-
Stage 2	610	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	357	759	-	-	1288
Mov Cap-2 Maneuver	357	-	-	-	-
Stage 1	768	-	-	-	-
Stage 2	603	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	9.8	0	0.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	759	1288
HCM Lane V/C Ratio	-	-	0.011	0.009
HCM Control Delay (s)	-	-	9.8	7.8
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2035 No Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	23.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↔			↔			↔			↔	
Traffic Vol, veh/h	9	10	2	95	6	7	0	503	432	28	324	32
Future Vol, veh/h	9	10	2	95	6	7	0	503	432	28	324	32
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	75	75	75	65	65	65	90	90	90	87	87	87
Heavy Vehicles, %	20	0	0	4	0	0	0	2	3	0	3	0
Mvmt Flow	12	13	3	146	9	11	0	559	480	32	372	37

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1264	1494	391	1262	1272	799	409	0	0	1039	0	0
Stage 1	455	455	-	799	799	-	-	-	-	-	-	-
Stage 2	809	1039	-	463	473	-	-	-	-	-	-	-
Critical Hdwy	7.3	6.5	6.2	7.14	6.5	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.68	4	3.3	3.536	4	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	134	124	662	~ 145	169	389	1161	-	-	677	-	-
Stage 1	552	572	-	376	401	-	-	-	-	-	-	-
Stage 2	349	310	-	575	562	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	119	116	662	~ 126	159	389	1161	-	-	677	-	-
Mov Cap-2 Maneuver	119	116	-	~ 126	159	-	-	-	-	-	-	-
Stage 1	552	537	-	376	401	-	-	-	-	-	-	-
Stage 2	332	310	-	524	528	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	41.2		223.7		0		0.8	
HCM LOS	E		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1161	-	-	127	133	677	-	-
HCM Lane V/C Ratio	-	-	-	0.22	1.249	0.048	-	-
HCM Control Delay (s)	0	-	-	41.2	223.7	10.6	0	-
HCM Lane LOS	A	-	-	E	F	B	A	-
HCM 95th %tile Q(veh)	0	-	-	0.8	10.2	0.1	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	130.1					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	956	392	53	16	61	261
Future Vol, veh/h	956	392	53	16	61	261
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	93	93	70	70	90	90
Heavy Vehicles, %	1	1	3	11	0	4
Mvmt Flow	1028	422	76	23	68	290

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	243	68	358	0	0
Stage 1	68	-	-	-	-
Stage 2	175	-	-	-	-
Critical Hdwy	6.41	6.21	4.13	-	-
Critical Hdwy Stg 1	5.41	-	-	-	-
Critical Hdwy Stg 2	5.41	-	-	-	-
Follow-up Hdwy	3.509	3.309	2.227	-	-
Pot Cap-1 Maneuver	~ 748	998	1195	-	-
Stage 1	~ 957	-	-	-	-
Stage 2	~ 858	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	~ 700	998	1195	-	-
Mov Cap-2 Maneuver	~ 700	-	-	-	-
Stage 1	~ 896	-	-	-	-
Stage 2	~ 858	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	170.6	6.3	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1195	-	700	998	-	-
HCM Lane V/C Ratio	0.063	-	1.469	0.422	-	-
HCM Control Delay (s)	8.2	-	236	11.2	-	-
HCM Lane LOS	A	-	F	B	-	-
HCM 95th %tile Q(veh)	0.2	-	48.9	2.1	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2035 No Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	163.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↕
Traffic Vol, veh/h	0	246	1328	0	0	385
Future Vol, veh/h	0	246	1328	0	0	385
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	76	76	70	70	80	80
Heavy Vehicles, %	2	3	2	2	2	4
Mvmt Flow	0	324	1897	0	0	481
Major/Minor	Minor1	Major1		Major2		
Conflicting Flow All	-	1897	0	-	-	
Stage 1	-	-	-	-	-	
Stage 2	-	-	-	-	-	
Critical Hdwy	-	6.245	-	-	-	
Critical Hdwy Stg 1	-	-	-	-	-	
Critical Hdwy Stg 2	-	-	-	-	-	
Follow-up Hdwy	-	3.3285	-	-	-	
Pot Cap-1 Maneuver	0	~ 85	-	0	0	
Stage 1	0	-	-	0	0	
Stage 2	0	-	-	0	0	
Platoon blocked, %			-		-	
Mov Cap-1 Maneuver	-	~ 85	-	-	-	
Mov Cap-2 Maneuver	-	-	-	-	-	
Stage 1	-	-	-	-	-	
Stage 2	-	-	-	-	-	
Approach	WB	NB	SB			
HCM Control Delay, s \$	1366	0	0			
HCM LOS	F					
Minor Lane/Major Mvmt	NBTWBLn1	SBT				
Capacity (veh/h)	-	85	-			
HCM Lane V/C Ratio	-	3.808	-			
HCM Control Delay (s)	-	\$ 1366	-			
HCM Lane LOS	-	F	-			
HCM 95th %tile Q(veh)	-	33.5	-			
Notes						
~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon						













101: International Dr & Pease Blvd
 2035 No Build Condition Weekday PM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↙	↑↗		↙↗	↑↗			↑	↗↘		↖	
Traffic Volume (vph)	0	519	3	455	201	27	12	3	1367	63	3	3
Future Volume (vph)	0	519	3	455	201	27	12	3	1367	63	3	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor		0.95		0.97	0.95			1.00	0.88		1.00	
Fr _t		1.00		1.00	0.98			1.00	0.85		0.99	
Fl _t Protected		1.00		0.95	1.00			0.96	1.00		0.96	
Satd. Flow (prot)		3572		3433	3546			1765	2814		2048	
Fl _t Permitted		1.00		0.95	1.00			0.82	1.00		0.73	
Satd. Flow (perm)		3572		3433	3546			1502	2814		1566	
Peak-hour factor, PHF	0.88	0.88	0.88	0.96	0.96	0.96	0.91	0.91	0.91	0.68	0.68	0.68
Adj. Flow (vph)	0	590	3	474	209	28	13	3	1502	93	4	4
RTOR Reduction (vph)	0	0	0	0	5	0	0	0	0	0	1	0
Lane Group Flow (vph)	0	593	0	474	232	0	0	16	1502	0	100	0
Heavy Vehicles (%)	0%	1%	0%	2%	0%	0%	0%	0%	1%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8			4	
Permitted Phases							8		8		4	
Actuated Green, G (s)		17.4		16.0	39.4			20.2	20.2		20.2	
Effective Green, g (s)		17.4		16.0	39.4			20.2	20.2		20.2	
Actuated g/C Ratio		0.24		0.22	0.55			0.28	0.28		0.28	
Clearance Time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)		3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)		868		767	1951			423	793		441	
v/s Ratio Prot		c0.17		c0.14	0.07							
v/s Ratio Perm								0.01	c0.53		0.06	
v/c Ratio		0.68		0.62	0.12			0.04	1.89		0.23	
Uniform Delay, d ₁		24.6		25.0	7.7			18.6	25.7		19.7	
Progression Factor		1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d ₂		2.2		1.5	0.0			0.0	407.1		0.3	
Delay (s)		26.8		26.5	7.8			18.7	432.8		20.0	
Level of Service		C		C	A			B	F		B	
Approach Delay (s)		26.8			20.3			428.4			20.0	
Approach LOS		C			C			F			B	
Intersection Summary												
HCM 2000 Control Delay			233.6			HCM 2000 Level of Service			F			
HCM 2000 Volume to Capacity ratio			1.12									
Actuated Cycle Length (s)			71.6			Sum of lost time (s)			18.0			
Intersection Capacity Utilization			82.3%			ICU Level of Service			E			
Analysis Period (min)			15									

c Critical Lane Group

102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2035 No Build Condition Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↘↗		↗↘
Traffic Volume (vph)	0	1285	664	756	522	0	0	0	0	429	0	166
Future Volume (vph)	0	1285	664	756	522	0	0	0	0	429	0	166
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		6040	1546	3236	3455					3502		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		6040	1546	3236	3455					3502		2814
Peak-hour factor, PHF	0.85	0.85	0.85	0.94	0.94	0.94	0.92	0.92	0.92	0.90	0.90	0.90
Adj. Flow (vph)	0	1512	781	804	555	0	0	0	0	477	0	184
RTOR Reduction (vph)	0	0	363	0	0	0	0	0	0	0	0	140
Lane Group Flow (vph)	0	1512	418	804	555	0	0	0	0	477	0	44
Heavy Vehicles (%)	0%	1%	1%	1%	1%	0%	0%	0%	0%	0%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		35.0	35.0	25.0	66.0					24.5		24.5
Effective Green, g (s)		35.0	35.0	25.0	66.0					24.5		24.5
Actuated g/C Ratio		0.34	0.34	0.24	0.64					0.24		0.24
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2062	527	789	2224					837		672
v/s Ratio Prot		0.25	c0.27	c0.25	0.16					c0.14		0.02
v/s Ratio Perm												
v/c Ratio		0.73	0.79	1.02	0.25					0.57		0.07
Uniform Delay, d1		29.6	30.5	38.8	7.7					34.4		30.1
Progression Factor		1.00	1.00	1.33	1.26					1.00		1.00
Incremental Delay, d2		1.7	9.2	28.5	0.1					1.5		0.1
Delay (s)		31.3	39.7	80.3	9.8					35.8		30.2
Level of Service		C	D	F	A					D		C
Approach Delay (s)		34.2			51.5			0.0			34.3	
Approach LOS		C			D			A			C	
Intersection Summary												
HCM 2000 Control Delay			39.6			HCM 2000 Level of Service					D	
HCM 2000 Volume to Capacity ratio			0.79									
Actuated Cycle Length (s)			102.5			Sum of lost time (s)					18.0	
Intersection Capacity Utilization			89.9%			ICU Level of Service					E	
Analysis Period (min)			15									

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2035 No Build Condition Weekday PM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	768	946	0	0	1028	450	250	0	691	0	0	0
Future Volume (vph)	768	946	0	0	1028	450	250	0	691	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.95		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3236	3455			4916		3433		2814			
Flt Permitted	0.11	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	389	3455			4916		3433		2814			
Peak-hour factor, PHF	0.87	0.87	0.92	0.90	0.90	0.90	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	883	1087	0	0	1142	500	266	0	735	0	0	0
RTOR Reduction (vph)	0	0	0	0	76	0	0	0	559	0	0	0
Lane Group Flow (vph)	883	1087	0	0	1566	0	266	0	176	0	0	0
Heavy Vehicles (%)	1%	1%	0%	0%	1%	0%	2%	0%	1%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	60.0	35.0			35.0		24.5		24.5			
Effective Green, g (s)	60.0	35.0			35.0		24.5		24.5			
Actuated g/C Ratio	0.59	0.34			0.34		0.24		0.24			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	922	1179			1678		820		672			
v/s Ratio Prot	c0.23	0.31			0.32		c0.08		0.06			
v/s Ratio Perm	c0.33											
v/c Ratio	0.96	0.92			0.93		0.32		0.26			
Uniform Delay, d1	29.4	32.4			32.6		32.2		31.7			
Progression Factor	1.65	0.56			1.00		1.00		1.00			
Incremental Delay, d2	15.9	9.3			10.3		0.5		0.4			
Delay (s)	64.5	27.5			43.0		32.7		32.1			
Level of Service	E	C			D		C		C			
Approach Delay (s)		44.0			43.0			32.2			0.0	
Approach LOS		D			D			C			A	
Intersection Summary												
HCM 2000 Control Delay			41.1				HCM 2000 Level of Service				D	
HCM 2000 Volume to Capacity ratio			0.77									
Actuated Cycle Length (s)			102.5				Sum of lost time (s)				18.0	
Intersection Capacity Utilization			89.9%				ICU Level of Service				E	
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2035 No Build Condition Weekday PM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	341	1825	1418	245	456	936
Future Volume (vph)	341	1825	1418	245	456	936
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3539	3539	1583	1787	1599
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3539	3539	1583	1787	1599
Peak-hour factor, PHF	0.88	0.88	0.93	0.93	0.87	0.87
Adj. Flow (vph)	388	2074	1525	263	524	1076
RTOR Reduction (vph)	0	0	0	183	0	165
Lane Group Flow (vph)	388	2074	1525	80	524	911
Heavy Vehicles (%)	1%	2%	2%	2%	1%	1%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	5.0	29.0	18.0	18.0	18.0	18.0
Effective Green, g (s)	5.0	29.0	18.0	18.0	18.0	18.0
Actuated g/C Ratio	0.08	0.49	0.31	0.31	0.31	0.31
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	151	1739	1079	482	545	487
v/s Ratio Prot	c0.22	0.59	c0.43		0.29	c0.57
v/s Ratio Perm				0.05		
v/c Ratio	2.57	1.19	1.41	0.17	0.96	1.87
Uniform Delay, d1	27.0	15.0	20.5	15.0	20.2	20.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	725.3	92.7	191.5	0.7	29.1	399.2
Delay (s)	752.3	107.7	212.0	15.8	49.2	419.7
Level of Service	F	F	F	B	D	F
Approach Delay (s)		209.3	183.2		298.4	
Approach LOS		F	F		F	
Intersection Summary						
HCM 2000 Control Delay			225.7		HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio			1.75			
Actuated Cycle Length (s)			59.0		Sum of lost time (s)	18.0
Intersection Capacity Utilization			107.2%		ICU Level of Service	G
Analysis Period (min)			15			
c Critical Lane Group						

105: International Drive & Corporate Drive
 2035 No Build Condition Weekday PM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	154	5	17	10	27	556	17	633	8	149	150	96
Future Volume (vph)	154	5	17	10	27	556	17	633	8	149	150	96
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	0.95		1.00	1.00	1.00
Frt	1.00	0.88		1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1805	1681		1805	1792	1599	1805	3568		1736	1845	1615
Flt Permitted	0.73	1.00		0.74	1.00	1.00	0.66	1.00		0.17	1.00	1.00
Satd. Flow (perm)	1395	1681		1407	1792	1599	1245	3568		310	1845	1615
Peak-hour factor, PHF	0.84	0.84	0.84	0.77	0.77	0.77	0.89	0.89	0.89	0.93	0.93	0.93
Adj. Flow (vph)	183	6	20	13	35	722	19	711	9	160	161	103
RTOR Reduction (vph)	0	12	0	0	0	153	0	1	0	0	0	60
Lane Group Flow (vph)	183	14	0	13	35	569	19	719	0	160	161	43
Heavy Vehicles (%)	0%	0%	0%	0%	6%	1%	0%	1%	0%	4%	3%	0%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Actuated Green, G (s)	32.5	32.5		32.5	32.5	32.5	20.1	20.1		32.1	32.1	32.1
Effective Green, g (s)	32.5	32.5		32.5	32.5	32.5	20.1	20.1		32.1	32.1	32.1
Actuated g/C Ratio	0.42	0.42		0.42	0.42	0.42	0.26	0.26		0.42	0.42	0.42
Clearance Time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Vehicle Extension (s)	3.0	3.0		3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0
Lane Grp Cap (vph)	591	713		596	760	678	326	936		269	773	676
v/s Ratio Prot		0.01			0.02			c0.20		c0.06	0.09	
v/s Ratio Perm	0.13			0.01		c0.36	0.02			0.19		0.03
v/c Ratio	0.31	0.02		0.02	0.05	0.84	0.06	0.77		0.59	0.21	0.06
Uniform Delay, d1	14.6	12.8		12.8	12.9	19.7	21.2	26.1		15.8	14.2	13.3
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	0.3	0.0		0.0	0.0	9.0	0.1	3.8		3.5	0.1	0.0
Delay (s)	14.9	12.8		12.8	13.0	28.7	21.2	29.9		19.3	14.3	13.3
Level of Service	B	B		B	B	C	C	C		B	B	B
Approach Delay (s)		14.7			27.7			29.7			16.0	
Approach LOS		B			C			C			B	
Intersection Summary												
HCM 2000 Control Delay			24.8									HCM 2000 Level of Service C
HCM 2000 Volume to Capacity ratio			0.79									
Actuated Cycle Length (s)			76.6								16.5	
Intersection Capacity Utilization			76.3%									ICU Level of Service D
Analysis Period (min)			15									
c Critical Lane Group												

202: Goose Bay Drive & Corporate Drive
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	78.1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	153	9	3	403	190	11
Future Vol, veh/h	153	9	3	403	190	11
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	70	70	73	73	40	40
Heavy Vehicles, %	4	0	0	2	0	0
Mvmt Flow	219	13	4	552	475	28

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	232	0	786
Stage 1	-	-	-	-	226
Stage 2	-	-	-	-	560
Critical Hdwy	-	-	4.1	-	6.4
Critical Hdwy Stg 1	-	-	-	-	5.4
Critical Hdwy Stg 2	-	-	-	-	5.4
Follow-up Hdwy	-	-	2.2	-	3.5
Pot Cap-1 Maneuver	-	-	1348	- ~	364
Stage 1	-	-	-	-	816
Stage 2	-	-	-	-	576
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1348	- ~	363
Mov Cap-2 Maneuver	-	-	-	- ~	363
Stage 1	-	-	-	-	816
Stage 2	-	-	-	-	574

Approach	EB	WB	NB
HCM Control Delay, s	0	0.1	200.5
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	374	-	-	1348	-
HCM Lane V/C Ratio	1.344	-	-	0.003	-
HCM Control Delay (s)	200.5	-	-	7.7	0
HCM Lane LOS	F	-	-	A	A
HCM 95th %tile Q(veh)	23.9	-	-	0	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

203: Corporate Drive & Redhook Way
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.8					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Vol, veh/h	8	154	392	3	1	14
Future Vol, veh/h	8	154	392	3	1	14
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	63	63	77	77	36	36
Heavy Vehicles, %	40	0	0	1	0	11
Mvmt Flow	13	244	509	4	3	39

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	513	0	0	781	511
Stage 1	-	-	-	511	-
Stage 2	-	-	-	270	-
Critical Hdwy	4.5	-	-	6.4	6.31
Critical Hdwy Stg 1	-	-	-	5.4	-
Critical Hdwy Stg 2	-	-	-	5.4	-
Follow-up Hdwy	2.56	-	-	3.5	3.399
Pot Cap-1 Maneuver	884	-	-	366	545
Stage 1	-	-	-	606	-
Stage 2	-	-	-	780	-
Platoon blocked, %		-	-		
Mov Cap-1 Maneuver	884	-	-	361	545
Mov Cap-2 Maneuver	-	-	-	361	-
Stage 1	-	-	-	597	-
Stage 2	-	-	-	780	-

Approach	EB	WB	SB
HCM Control Delay, s	0.5	0	12.4
HCM LOS			B

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	884	-	-	-	527
HCM Lane V/C Ratio	0.014	-	-	-	0.079
HCM Control Delay (s)	9.1	-	-	-	12.4
HCM Lane LOS	A	-	-	-	B
HCM 95th %tile Q(veh)	0	-	-	-	0.3

204: Goose Bay Drive & Corporate Drive
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.9					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	163	1	6	220	15	12
Future Vol, veh/h	163	1	6	220	15	12
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	81	81	71	71
Heavy Vehicles, %	0	0	0	1	11	0
Mvmt Flow	209	1	7	272	21	17

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	210	0	496
Stage 1	-	-	-	-	210
Stage 2	-	-	-	-	286
Critical Hdwy	-	-	4.1	-	6.51
Critical Hdwy Stg 1	-	-	-	-	5.51
Critical Hdwy Stg 2	-	-	-	-	5.51
Follow-up Hdwy	-	-	2.2	-	3.599
Pot Cap-1 Maneuver	-	-	1373	-	517
Stage 1	-	-	-	-	804
Stage 2	-	-	-	-	742
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1373	-	514
Mov Cap-2 Maneuver	-	-	-	-	514
Stage 1	-	-	-	-	804
Stage 2	-	-	-	-	738

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	11.2
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	620	-	-	1373	-
HCM Lane V/C Ratio	0.061	-	-	0.005	-
HCM Control Delay (s)	11.2	-	-	7.6	0
HCM Lane LOS	B	-	-	A	A
HCM 95th %tile Q(veh)	0.2	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	2.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	1	12	15	1	0	7
Future Vol, veh/h	1	12	15	1	0	7
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	67	67	69	69	50	50
Heavy Vehicles, %	0	0	10	0	0	0
Mvmt Flow	1	18	22	1	0	14

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	37	23	0	0	23
Stage 1	23	-	-	-	-
Stage 2	14	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	981	1060	-	-	1605
Stage 1	1005	-	-	-	-
Stage 2	1014	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	981	1060	-	-	1605
Mov Cap-2 Maneuver	981	-	-	-	-
Stage 1	1005	-	-	-	-
Stage 2	1014	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	8.5	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	1053	1605
HCM Lane V/C Ratio	-	-	0.018	-
HCM Control Delay (s)	-	-	8.5	0
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0.1	0

206: Goose Bay Drive & Lonza South Dwy
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	2.1					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	3	0	0	8	16	0
Future Vol, veh/h	3	0	0	8	16	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	25	25	63	63	63	63
Heavy Vehicles, %	0	0	0	0	10	0
Mvmt Flow	12	0	0	13	25	0

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	38	25	25	0	0
Stage 1	25	-	-	-	-
Stage 2	13	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-
Pot Cap-1 Maneuver	979	1057	1603	-	-
Stage 1	1003	-	-	-	-
Stage 2	1015	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	979	1057	1603	-	-
Mov Cap-2 Maneuver	979	-	-	-	-
Stage 1	1003	-	-	-	-
Stage 2	1015	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	8.7	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1603	-	979	-	-
HCM Lane V/C Ratio	-	-	0.012	-	-
HCM Control Delay (s)	0	-	8.7	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Goose Bay Drive & Lonza Parking Garage/Proposed Dwy
 2035 No Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	0											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	0	0	201	0	0	6	6
Future Vol, veh/h	0	0	0	0	0	0	0	201	0	0	6	6
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	39	39	92	92	67	67
Heavy Vehicles, %	2	2	2	2	2	2	0	0	2	2	0	0
Mvmt Flow	0	0	0	0	0	0	0	515	0	0	9	9

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	529	529	14	529	533	515	18	0	0	515	0	0
Stage 1	14	14	-	515	515	-	-	-	-	-	-	-
Stage 2	515	515	-	14	18	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	460	455	1066	460	453	560	1612	-	-	1051	-	-
Stage 1	1006	884	-	543	535	-	-	-	-	-	-	-
Stage 2	543	535	-	1006	880	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	460	455	1066	460	453	560	1612	-	-	1051	-	-
Mov Cap-2 Maneuver	460	455	-	460	453	-	-	-	-	-	-	-
Stage 1	1006	884	-	543	535	-	-	-	-	-	-	-
Stage 2	543	535	-	1006	880	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		0		0		0	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1612	-	-	-	-	1051	-	-
HCM Lane V/C Ratio	-	-	-	-	-	-	-	-
HCM Control Delay (s)	0	-	-	0	0	0	-	-
HCM Lane LOS	A	-	-	A	A	A	-	-
HCM 95th %tile Q(veh)	0	-	-	-	-	0	-	-

208: Granite State Driveway & International Drive
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	R	T	R	L	T
Traffic Vol, veh/h	8	3	655	1	5	165
Future Vol, veh/h	8	3	655	1	5	165
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	78	78	76	76
Heavy Vehicles, %	0	0	1	0	0	4
Mvmt Flow	9	3	840	1	7	217

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	1072	841	0	0	841	0
Stage 1	841	-	-	-	-	-
Stage 2	231	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	246	368	-	-	803	-
Stage 1	426	-	-	-	-	-
Stage 2	812	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	244	368	-	-	803	-
Mov Cap-2 Maneuver	244	-	-	-	-	-
Stage 1	426	-	-	-	-	-
Stage 2	804	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	19	0	0.3
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	269	803
HCM Lane V/C Ratio	-	-	0.046	0.008
HCM Control Delay (s)	-	-	19	9.5
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	12.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	Y		B			A
Traffic Vol, veh/h	54	166	490	17	15	158
Future Vol, veh/h	54	166	490	17	15	158
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	72	72	67	67	81	81
Heavy Vehicles, %	14	0	1	46	0	3
Mvmt Flow	75	231	731	25	19	195

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	977	744	0	0	756	0
Stage 1	744	-	-	-	-	-
Stage 2	233	-	-	-	-	-
Critical Hdwy	6.54	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.54	-	-	-	-	-
Critical Hdwy Stg 2	5.54	-	-	-	-	-
Follow-up Hdwy	3.626	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	264	418	-	-	864	-
Stage 1	449	-	-	-	-	-
Stage 2	778	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	257	418	-	-	864	-
Mov Cap-2 Maneuver	257	-	-	-	-	-
Stage 1	449	-	-	-	-	-
Stage 2	759	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	50.6	0	0.8
HCM LOS	F		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	362	864
HCM Lane V/C Ratio	-	-	0.844	0.021
HCM Control Delay (s)	-	-	50.6	9.3
HCM Lane LOS	-	-	F	A
HCM 95th %tile Q(veh)	-	-	7.7	0.1

210: International Drive & Lonza South Driveway
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	0	5	404	0	0	232
Future Vol, veh/h	0	5	404	0	0	232
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	68	68	74	74
Heavy Vehicles, %	0	0	3	0	0	7
Mvmt Flow	0	20	594	0	0	314

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	908	594	0	0	594	0
Stage 1	594	-	-	-	-	-
Stage 2	314	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	308	509	-	-	992	-
Stage 1	555	-	-	-	-	-
Stage 2	745	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	308	509	-	-	992	-
Mov Cap-2 Maneuver	308	-	-	-	-	-
Stage 1	555	-	-	-	-	-
Stage 2	745	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	12.4	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	509	992
HCM Lane V/C Ratio	-	-	0.039	-
HCM Control Delay (s)	-	-	12.4	0
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2035 No Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	205.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Vol, veh/h	30	23	3	314	21	23	1	326	114	3	560	14
Future Vol, veh/h	30	23	3	314	21	23	1	326	114	3	560	14
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	54	54	54	85	85	85	84	84	84	88	88	88
Heavy Vehicles, %	0	13	0	0	14	0	0	2	1	0	1	11
Mvmt Flow	56	43	6	369	25	27	1	388	136	3	636	16

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1134	1176	644	1133	1116	456	652	0	0	524	0	0
Stage 1	650	650	-	458	458	-	-	-	-	-	-	-
Stage 2	484	526	-	675	658	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.63	6.2	7.1	6.64	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4.117	3.3	3.5	4.126	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	181	182	476	~ 182	197	609	944	-	-	1053	-	-
Stage 1	461	448	-	587	547	-	-	-	-	-	-	-
Stage 2	568	511	-	447	443	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	155	181	476	~ 147	196	609	944	-	-	1053	-	-
Mov Cap-2 Maneuver	155	181	-	~ 147	196	-	-	-	-	-	-	-
Stage 1	460	446	-	586	546	-	-	-	-	-	-	-
Stage 2	517	510	-	398	441	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	54.1		\$ 820.1		0		0	
HCM LOS	F		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	944	-	-	171	157	1053	-	-
HCM Lane V/C Ratio	0.001	-	-	0.606	2.683	0.003	-	-
HCM Control Delay (s)	8.8	0	-	54.1	\$ 820.1	8.4	0	-
HCM Lane LOS	A	A	-	F	F	A	A	-
HCM 95th %tile Q(veh)	0	-	-	3.3	37.3	0	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2035 No Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	106.9					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	373	81	224	51	27	870
Future Vol, veh/h	373	81	224	51	27	870
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	86	86	76	76	83	83
Heavy Vehicles, %	2	2	1	3	0	1
Mvmt Flow	434	94	295	67	33	1048

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	690	33	1081	0	-	0
Stage 1	33	-	-	-	-	-
Stage 2	657	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.11	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.209	-	-	-
Pot Cap-1 Maneuver	~ 411	1041	649	-	-	-
Stage 1	989	-	-	-	-	-
Stage 2	516	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	~ 224	1041	649	-	-	-
Mov Cap-2 Maneuver	~ 224	-	-	-	-	-
Stage 1	539	-	-	-	-	-
Stage 2	516	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	390.4	12.3	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	649	-	224	1041	-	-
HCM Lane V/C Ratio	0.454	-	1.936	0.09	-	-
HCM Control Delay (s)	15.1	-	473.3	8.8	-	-
HCM Lane LOS	C	-	F	A	-	-
HCM 95th %tile Q(veh)	2.4	-	31.4	0.3	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2035 No Build Condition Weekday PM Peak

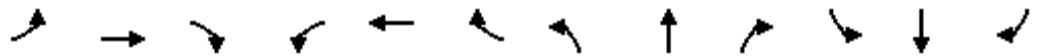
Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↖↗
Traffic Vol, veh/h	0	72	586	0	0	1392
Future Vol, veh/h	0	72	586	0	0	1392
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	73	73	95	95	89	89
Heavy Vehicles, %	0	13	0	1	0	1
Mvmt Flow	0	99	617	0	0	1564

Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	-	617	0
Stage 1	-	-	-
Stage 2	-	-	-
Critical Hdwy	-	6.395	-
Critical Hdwy Stg 1	-	-	-
Critical Hdwy Stg 2	-	-	-
Follow-up Hdwy	-	3.4235	-
Pot Cap-1 Maneuver	0	465	-
Stage 1	0	-	-
Stage 2	0	-	-
Platoon blocked, %	-	-	-
Mov Cap-1 Maneuver	-	465	-
Mov Cap-2 Maneuver	-	-	-
Stage 1	-	-	-
Stage 2	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	14.8	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 465	-
HCM Lane V/C Ratio	- 0.212	-
HCM Control Delay (s)	- 14.8	-
HCM Lane LOS	- B	-
HCM 95th %tile Q(veh)	- 0.8	-

101: International Dr & Pease Blvd
 2035 Build Condition Weekday AM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	3	115	7	1502	704	145	9	6	404	7	2	2
Future Volume (vph)	3	115	7	1502	704	145	9	6	404	7	2	2
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor	1.00	0.95		0.97	0.95			1.00	0.88		1.00	
Fr _t	1.00	0.99		1.00	0.97			1.00	0.85		0.98	
Fl _t Protected	0.95	1.00		0.95	1.00			0.97	1.00		0.97	
Satd. Flow (prot)	1805	3514		3467	3474			1784	2682		2036	
Fl _t Permitted	0.95	1.00		0.95	1.00			0.88	1.00		0.87	
Satd. Flow (perm)	1805	3514		3467	3474			1619	2682		1826	
Peak-hour factor, PHF	0.84	0.84	0.84	0.83	1.00	0.83	0.88	0.88	0.88	0.63	0.63	0.63
Adj. Flow (vph)	4	137	8	1810	704	175	10	7	459	11	3	3
RTOR Reduction (vph)	0	4	0	0	11	0	0	0	0	0	2	0
Lane Group Flow (vph)	4	141	0	1810	868	0	0	17	459	0	15	0
Heavy Vehicles (%)	0%	2%	0%	1%	1%	0%	0%	0%	6%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8			4	
Permitted Phases							8		8	4		
Actuated Green, G (s)	6.4	13.3		50.0	57.9			20.0	20.0		20.0	
Effective Green, g (s)	6.4	13.3		50.0	57.9			20.0	20.0		20.0	
Actuated g/C Ratio	0.06	0.13		0.49	0.57			0.20	0.20		0.20	
Clearance Time (s)	5.0	6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)	2.0	3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)	114	461		1711	1985			319	529		360	
v/s Ratio Prot	0.00	c0.04		c0.52	c0.25							
v/s Ratio Perm								0.01	c0.17		0.01	
v/c Ratio	0.04	0.31		1.06	0.44			0.05	0.87		0.04	
Uniform Delay, d ₁	44.6	39.8		25.6	12.4			33.0	39.4		32.9	
Progression Factor	1.00	1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d ₂	0.0	0.4		38.9	0.2			0.1	14.0		0.0	
Delay (s)	44.6	40.2		64.6	12.6			33.0	53.4		32.9	
Level of Service	D	D		E	B			C	D		C	
Approach Delay (s)		40.3			47.6			52.7			32.9	
Approach LOS		D			D			D			C	
Intersection Summary												
HCM 2000 Control Delay			47.9	HCM 2000 Level of Service				D				
HCM 2000 Volume to Capacity ratio			0.90									
Actuated Cycle Length (s)			101.3	Sum of lost time (s)				18.0				
Intersection Capacity Utilization			69.4%	ICU Level of Service				C				
Analysis Period (min)			15									

c Critical Lane Group


















102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2035 Build Condition Weekday AM Peak



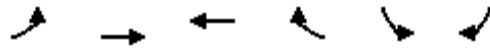
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR		
Lane Configurations		↑↑↑	↗	↘↗	↑↑					↖↗		↖↗		
Traffic Volume (vph)	0	365	161	174	1214	0	0	0	0	625	0	1016		
Future Volume (vph)	0	365	161	174	1214	0	0	0	0	625	0	1016		
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900		
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12		
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0		
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88		
Fr _t		1.00	0.85	1.00	1.00					1.00		0.85		
Fl _t Protected		1.00	1.00	0.95	1.00					0.95		1.00		
Satd. Flow (prot)		5981	1419	2918	3455					3467		2814		
Fl _t Permitted		1.00	1.00	0.95	1.00					0.95		1.00		
Satd. Flow (perm)		5981	1419	2918	3455					3467		2814		
Peak-hour factor, PHF	0.80	0.80	0.80	0.80	0.80	0.80	0.92	0.92	0.92	0.75	0.75	0.75		
Adj. Flow (vph)	0	456	201	218	1518	0	0	0	0	833	0	1355		
RTOR Reduction (vph)	0	0	133	0	0	0	0	0	0	0	0	72		
Lane Group Flow (vph)	0	456	68	218	1518	0	0	0	0	833	0	1283		
Heavy Vehicles (%)	0%	2%	10%	12%	1%	0%	2%	2%	2%	1%	0%	1%		
Turn Type		NA	Prot	Prot	NA					Prot		Prot		
Protected Phases		6	6	5	2 5					3		3		
Permitted Phases														
Actuated Green, G (s)		34.7	34.7	25.0	65.7					25.0		25.0		
Effective Green, g (s)		34.7	34.7	25.0	65.7					25.0		25.0		
Actuated g/C Ratio		0.34	0.34	0.24	0.64					0.24		0.24		
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0		
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0		
Lane Grp Cap (vph)		2020	479	710	2210					843		685		
v/s Ratio Prot		0.08	0.05	0.07	c0.44					0.24		c0.46		
v/s Ratio Perm														
v/c Ratio		0.23	0.14	0.31	0.69					0.99		1.87		
Uniform Delay, d ₁		24.4	23.6	31.8	11.9					38.7		38.9		
Progression Factor		1.00	1.00	0.89	1.57					1.00		1.00		
Incremental Delay, d ₂		0.1	0.3	0.0	0.1					28.0		398.5		
Delay (s)		24.5	23.9	28.4	18.8					66.7		437.3		
Level of Service		C	C	C	B					E		F		
Approach Delay (s)		24.3			20.0			0.0			296.2			
Approach LOS		C			B			A			F			
Intersection Summary														
HCM 2000 Control Delay			152.5									HCM 2000 Level of Service	F	
HCM 2000 Volume to Capacity ratio			1.09											
Actuated Cycle Length (s)			102.7							18.0			Sum of lost time (s)	
Intersection Capacity Utilization			86.8%										ICU Level of Service	E
Analysis Period (min)			15											

c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2035 Build Condition Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	177	813	0	0	479	86	909	0	405	0	0	0
Future Volume (vph)	177	813	0	0	479	86	909	0	405	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.98		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3113	3421			4947		3433		2733			
Flt Permitted	0.39	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	1270	3421			4947		3433		2733			
Peak-hour factor, PHF	0.87	0.87	0.87	0.85	0.85	0.85	0.78	0.78	0.78	0.92	0.92	0.92
Adj. Flow (vph)	203	934	0	0	564	101	1165	0	519	0	0	0
RTOR Reduction (vph)	0	0	0	0	22	0	0	0	331	0	0	0
Lane Group Flow (vph)	203	934	0	0	643	0	1165	0	188	0	0	0
Heavy Vehicles (%)	5%	2%	0%	0%	2%	5%	2%	2%	4%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	51.7	34.7			42.7		25.0		25.0			
Effective Green, g (s)	51.7	34.7			42.7		25.0		25.0			
Actuated g/C Ratio	0.50	0.34			0.42		0.24		0.24			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	944	1155			2056		835		665			
v/s Ratio Prot	c0.04	c0.27			c0.13		c0.34		0.07			
v/s Ratio Perm	0.07											
v/c Ratio	0.22	0.81			0.31		1.40		0.28			
Uniform Delay, d1	13.5	31.0			20.1		38.9		31.6			
Progression Factor	1.09	1.22			1.00		1.00		1.00			
Incremental Delay, d2	0.1	3.4			0.2		185.2		0.5			
Delay (s)	14.8	41.0			20.3		224.0		32.0			
Level of Service	B	D			C		F		C			
Approach Delay (s)		36.4			20.3			164.8			0.0	
Approach LOS		D			C			F			A	
Intersection Summary												
HCM 2000 Control Delay			95.4				HCM 2000 Level of Service		F			
HCM 2000 Volume to Capacity ratio			0.81									
Actuated Cycle Length (s)			102.7				Sum of lost time (s)		18.0			
Intersection Capacity Utilization			86.8%				ICU Level of Service		E			
Analysis Period (min)			15									
c	Critical Lane Group											

104: Route 33 (Greenland Rd) & Grafton Rd
 2035 Build Condition Weekday AM Peak


























Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	699	2242	808	670	181	224
Future Volume (vph)	699	2242	808	670	181	224
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3471	3343	1583	1719	1538
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3471	3343	1583	1719	1538
Peak-hour factor, PHF	0.86	0.86	0.96	0.96	0.76	0.76
Adj. Flow (vph)	813	2607	842	698	238	295
RTOR Reduction (vph)	0	0	0	485	0	195
Lane Group Flow (vph)	813	2607	842	213	238	100
Heavy Vehicles (%)	1%	4%	8%	2%	5%	5%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	8.7	32.7	18.0	18.0	14.3	14.3
Effective Green, g (s)	8.7	32.7	18.0	18.0	14.3	14.3
Actuated g/C Ratio	0.15	0.55	0.31	0.31	0.24	0.24
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	263	1923	1019	482	416	372
v/s Ratio Prot	c0.45	c0.75	0.25		c0.14	0.07
v/s Ratio Perm				0.13		
v/c Ratio	3.09	1.36	0.83	0.44	0.57	0.27
Uniform Delay, d1	25.1	13.1	19.0	16.5	19.7	18.1
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	951.1	163.6	7.7	2.9	2.3	0.5
Delay (s)	976.2	176.7	26.7	19.4	21.9	18.7
Level of Service	F	F	C	B	C	B
Approach Delay (s)		366.8	23.4		20.1	
Approach LOS		F	C		C	

Intersection Summary

HCM 2000 Control Delay	236.9	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.53		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	90.2%	ICU Level of Service	E
Analysis Period (min)	15		
c Critical Lane Group			

105: International Drive & Corporate Drive
 2035 Build Condition Weekday AM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	77	48	34	16	15	132	9	159	71	815	515	151
Future Volume (vph)	77	48	34	16	15	132	9	159	71	815	515	151
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	0.95		1.00	1.00	1.00
Frt	1.00	0.94		1.00	1.00	0.85	1.00	0.95		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1805	1706		1805	1681	1369	1805	3411		1770	1900	1615
Flt Permitted	0.75	1.00		0.69	1.00	1.00	0.41	1.00		0.38	1.00	1.00
Satd. Flow (perm)	1416	1706		1306	1681	1369	774	3411		703	1900	1615
Peak-hour factor, PHF	0.76	0.76	0.76	0.78	0.78	0.78	0.83	0.83	0.83	0.76	0.76	0.76
Adj. Flow (vph)	101	63	45	21	19	169	11	192	86	1072	678	199
RTOR Reduction (vph)	0	24	0	0	0	146	0	49	0	0	0	51
Lane Group Flow (vph)	101	84	0	21	19	23	11	229	0	1072	678	148
Heavy Vehicles (%)	0%	4%	5%	0%	13%	18%	0%	0%	3%	2%	0%	0%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Prot
Protected Phases		4			8			2		1	6	6
Permitted Phases	4			8		8	2			6		
Actuated Green, G (s)	13.3	13.3		13.3	13.3	13.3	12.7	12.7		72.5	72.5	72.5
Effective Green, g (s)	13.3	13.3		13.3	13.3	13.3	12.7	12.7		72.5	72.5	72.5
Actuated g/C Ratio	0.14	0.14		0.14	0.14	0.14	0.13	0.13		0.74	0.74	0.74
Clearance Time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Vehicle Extension (s)	3.0	3.0		3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0
Lane Grp Cap (vph)	192	232		177	228	186	100	442		1124	1408	1197
v/s Ratio Prot		0.05			0.01			0.07		c0.54	0.36	0.09
v/s Ratio Perm	c0.07			0.02		0.02	0.01			c0.17		
v/c Ratio	0.53	0.36		0.12	0.08	0.12	0.11	0.52		0.95	0.48	0.12
Uniform Delay, d1	39.3	38.4		37.1	36.9	37.1	37.6	39.7		13.3	5.1	3.6
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	2.6	1.0		0.3	0.2	0.3	0.5	1.0		16.8	0.3	0.0
Delay (s)	41.9	39.4		37.4	37.1	37.4	38.0	40.7		30.1	5.3	3.6
Level of Service	D	D		D	D	D	D	D		C	A	A
Approach Delay (s)		40.6			37.4			40.6			18.8	
Approach LOS		D			D			D			B	
Intersection Summary												
HCM 2000 Control Delay			24.4									HCM 2000 Level of Service C
HCM 2000 Volume to Capacity ratio			0.92									
Actuated Cycle Length (s)			97.8								16.5	
Intersection Capacity Utilization			79.0%									ICU Level of Service D
Analysis Period (min)			15									
c Critical Lane Group												

202: Goose Bay Drive & Corporate Drive
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	14.3					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	570	364	70	84	79	26
Future Vol, veh/h	570	364	70	84	79	26
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	71	71	69	69
Heavy Vehicles, %	1	5	0	12	36	0
Mvmt Flow	731	467	99	118	114	38

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	1198	0	1281
Stage 1	-	-	-	-	965
Stage 2	-	-	-	-	316
Critical Hdwy	-	-	4.1	-	6.76
Critical Hdwy Stg 1	-	-	-	-	5.76
Critical Hdwy Stg 2	-	-	-	-	5.76
Follow-up Hdwy	-	-	2.2	-	3.824
Pot Cap-1 Maneuver	-	-	590	-	155
Stage 1	-	-	-	-	321
Stage 2	-	-	-	-	668
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	590	-	127
Mov Cap-2 Maneuver	-	-	-	-	127
Stage 1	-	-	-	-	321
Stage 2	-	-	-	-	548

Approach	EB	WB	NB
HCM Control Delay, s	0	5.6	139.4
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	149	-	-	590	-
HCM Lane V/C Ratio	1.021	-	-	0.167	-
HCM Control Delay (s)	139.4	-	-	12.3	0
HCM Lane LOS	F	-	-	B	A
HCM 95th %tile Q(veh)	7.8	-	-	0.6	-

203: Corporate Drive & Redhook Way
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	↖	↑	↗		↖	
Traffic Vol, veh/h	19	579	131	2	0	7
Future Vol, veh/h	19	579	131	2	0	7
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	85	85	71	71	50	50
Heavy Vehicles, %	0	1	8	0	0	25
Mvmt Flow	22	681	185	3	0	14

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	188	0	-	0	912 187
Stage 1	-	-	-	-	187 -
Stage 2	-	-	-	-	725 -
Critical Hdwy	4.1	-	-	-	6.4 6.45
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.2	-	-	-	3.5 3.525
Pot Cap-1 Maneuver	1398	-	-	-	307 799
Stage 1	-	-	-	-	850 -
Stage 2	-	-	-	-	483 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	1398	-	-	-	302 799
Mov Cap-2 Maneuver	-	-	-	-	302 -
Stage 1	-	-	-	-	836 -
Stage 2	-	-	-	-	483 -

Approach	EB	WB	SB
HCM Control Delay, s	0.2	0	9.6
HCM LOS			A

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	1398	-	-	-	799
HCM Lane V/C Ratio	0.016	-	-	-	0.018
HCM Control Delay (s)	7.6	-	-	-	9.6
HCM Lane LOS	A	-	-	-	A
HCM 95th %tile Q(veh)	0	-	-	-	0.1

204: Goose Bay Drive & Corporate Drive
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.1					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	348	18	4	164	0	0
Future Vol, veh/h	348	18	4	164	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	95	95	82	82	25	40
Heavy Vehicles, %	1	0	0	5	20	0
Mvmt Flow	366	19	5	200	0	0

Major/Minor	Major1	Major2	Minor1	Minor2	Minor3
Conflicting Flow All	0	0	385	0	586
Stage 1	-	-	-	-	376
Stage 2	-	-	-	-	210
Critical Hdwy	-	-	4.1	-	6.6
Critical Hdwy Stg 1	-	-	-	-	5.6
Critical Hdwy Stg 2	-	-	-	-	5.6
Follow-up Hdwy	-	-	2.2	-	3.68
Pot Cap-1 Maneuver	-	-	1185	-	444
Stage 1	-	-	-	-	656
Stage 2	-	-	-	-	784
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1185	-	442
Mov Cap-2 Maneuver	-	-	-	-	442
Stage 1	-	-	-	-	656
Stage 2	-	-	-	-	780

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	0
HCM LOS			A

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	-	-	-	1185	-
HCM Lane V/C Ratio	-	-	-	0.004	-
HCM Control Delay (s)	0	-	-	8.1	0
HCM Lane LOS	A	-	-	A	A
HCM 95th %tile Q(veh)	-	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	TT		TT			TT
Traffic Vol, veh/h	0	0	0	0	22	0
Future Vol, veh/h	0	0	0	0	22	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	53	53	50	50
Heavy Vehicles, %	0	0	0	13	0	0
Mvmt Flow	0	0	0	0	44	0

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	88	0	0	0	0	0
Stage 1	0	-	-	-	-	-
Stage 2	88	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	918	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	940	-	-	-	-	-
Platoon blocked, %						
Mov Cap-1 Maneuver	918	-	-	-	-	-
Mov Cap-2 Maneuver	918	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	940	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	0	0	
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-
HCM Control Delay (s)	-	-	0	-
HCM Lane LOS	-	-	A	-
HCM 95th %tile Q(veh)	-	-	-	-

206: Goose Bay Drive & Lonza South Dwy
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	4.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	7	0	0	0	0	9
Future Vol, veh/h	7	0	0	0	0	9
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	50	50	42	42	69	69
Heavy Vehicles, %	75	0	0	0	6	80
Mvmt Flow	14	0	0	0	0	13

Major/Minor	Minor2	Major1		Major2	
Conflicting Flow All	7	7	13	0	0
Stage 1	7	-	-	-	-
Stage 2	0	-	-	-	-
Critical Hdwy	7.15	6.2	4.1	-	-
Critical Hdwy Stg 1	6.15	-	-	-	-
Critical Hdwy Stg 2	6.15	-	-	-	-
Follow-up Hdwy	4.175	3.3	2.2	-	-
Pot Cap-1 Maneuver	854	1081	1619	-	-
Stage 1	855	-	-	-	-
Stage 2	-	-	-	-	-
Platoon blocked, %				-	-
Mov Cap-1 Maneuver	854	1081	1619	-	-
Mov Cap-2 Maneuver	854	-	-	-	-
Stage 1	855	-	-	-	-
Stage 2	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	9.3	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1619	-	854	-	-
HCM Lane V/C Ratio	-	-	0.016	-	-
HCM Control Delay (s)	0	-	9.3	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0.1	-	-

207: Goose Bay Drive & Lonza Parking Garage/Proposed Dwy
2035 Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	2.7											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	68	6	37	0	138	53	243
Future Vol, veh/h	0	0	0	0	0	68	6	37	0	138	53	243
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	88	88	92	92	69	69
Heavy Vehicles, %	2	2	2	2	2	2	0	18	2	2	15	1
Mvmt Flow	0	0	0	0	0	74	7	42	0	150	77	352

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	646	609	253	609	785	42	429	0	0	42	0	0
Stage 1	553	553	-	56	56	-	-	-	-	-	-	-
Stage 2	93	56	-	553	729	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	385	410	786	407	325	1029	1141	-	-	1567	-	-
Stage 1	517	514	-	956	848	-	-	-	-	-	-	-
Stage 2	914	848	-	517	428	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	320	354	786	364	280	1029	1141	-	-	1567	-	-
Mov Cap-2 Maneuver	320	354	-	364	280	-	-	-	-	-	-	-
Stage 1	514	446	-	950	843	-	-	-	-	-	-	-
Stage 2	843	843	-	449	372	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	0		8.8		1.1		2	
HCM LOS	A		A					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1141	-	-	-	1029	1567	-
HCM Lane V/C Ratio	0.006	-	-	-	0.072	0.096	-
HCM Control Delay (s)	8.2	0	-	0	8.8	7.5	0
HCM Lane LOS	A	A	-	A	A	A	A
HCM 95th %tile Q(veh)	0	-	-	-	0.2	0.3	-

208: Granite State Driveway & International Drive
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	7	2	223	15	15	504
Future Vol, veh/h	7	2	223	15	15	504
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	63	63	81	81	84	84
Heavy Vehicles, %	0	0	0	0	0	1
Mvmt Flow	11	3	275	19	18	600

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	921	285	0	0	294
Stage 1	285	-	-	-	-
Stage 2	636	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	303	759	-	-	1279
Stage 1	768	-	-	-	-
Stage 2	531	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	297	759	-	-	1279
Mov Cap-2 Maneuver	297	-	-	-	-
Stage 1	768	-	-	-	-
Stage 2	520	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	16	0	0.2
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	343	1279
HCM Lane V/C Ratio	-	-	0.042	0.014
HCM Control Delay (s)	-	-	16	7.9
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.9					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	16	21	217	15	23	488
Future Vol, veh/h	16	21	217	15	23	488
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	86	86	83	83
Heavy Vehicles, %	44	0	1	63	0	1
Mvmt Flow	18	24	252	17	28	588

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	905	261	0	0	269	0
Stage 1	261	-	-	-	-	-
Stage 2	644	-	-	-	-	-
Critical Hdwy	6.84	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.84	-	-	-	-	-
Critical Hdwy Stg 2	5.84	-	-	-	-	-
Follow-up Hdwy	3.896	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	260	783	-	-	1306	-
Stage 1	695	-	-	-	-	-
Stage 2	451	-	-	-	-	-
Platoon blocked, %			-	-		-
Mov Cap-1 Maneuver	252	783	-	-	1306	-
Mov Cap-2 Maneuver	252	-	-	-	-	-
Stage 1	695	-	-	-	-	-
Stage 2	437	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	14.8	0	0.4
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	410	1306
HCM Lane V/C Ratio	-	-	0.103	0.021
HCM Control Delay (s)	-	-	14.8	7.8
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.3	0.1

210: International Drive & Lonza South Driveway
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	0.2					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	TT		TT			TT
Traffic Vol, veh/h	0	6	253	2	9	392
Future Vol, veh/h	0	6	253	2	9	392
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	75	75	89	89	81	81
Heavy Vehicles, %	0	0	5	100	0	2
Mvmt Flow	0	8	284	2	11	484

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	791	285	0	0	286
Stage 1	285	-	-	-	-
Stage 2	506	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1
Critical Hdwy Stg 1	5.4	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2
Pot Cap-1 Maneuver	361	759	-	-	1288
Stage 1	768	-	-	-	-
Stage 2	610	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	357	759	-	-	1288
Mov Cap-2 Maneuver	357	-	-	-	-
Stage 1	768	-	-	-	-
Stage 2	603	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	9.8	0	0.2
HCM LOS	A		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	759	1288
HCM Lane V/C Ratio	-	-	0.011	0.009
HCM Control Delay (s)	-	-	9.8	7.8
HCM Lane LOS	-	-	A	A
HCM 95th %tile Q(veh)	-	-	0	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2035 Build Condition Weekday AM Peak

Intersection												
Int Delay, s/veh	23.1											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	9	10	2	95	6	7	0	503	432	28	324	32
Future Vol, veh/h	9	10	2	95	6	7	0	503	432	28	324	32
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	75	75	75	65	65	65	90	90	90	87	87	87
Heavy Vehicles, %	20	0	0	4	0	0	0	2	3	0	3	0
Mvmt Flow	12	13	3	146	9	11	0	559	480	32	372	37

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	1264	1494	391	1262	1272	799	409	0	0	1039	0	0
Stage 1	455	455	-	799	799	-	-	-	-	-	-	-
Stage 2	809	1039	-	463	473	-	-	-	-	-	-	-
Critical Hdwy	7.3	6.5	6.2	7.14	6.5	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.3	5.5	-	6.14	5.5	-	-	-	-	-	-	-
Follow-up Hdwy	3.68	4	3.3	3.536	4	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	134	124	662	~ 145	169	389	1161	-	-	677	-	-
Stage 1	552	572	-	376	401	-	-	-	-	-	-	-
Stage 2	349	310	-	575	562	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	119	116	662	~ 126	159	389	1161	-	-	677	-	-
Mov Cap-2 Maneuver	119	116	-	~ 126	159	-	-	-	-	-	-	-
Stage 1	552	537	-	376	401	-	-	-	-	-	-	-
Stage 2	332	310	-	524	528	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB	
HCM Control Delay, s	41.2		223.7		0		0.8	
HCM LOS	E		F					

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1161	-	-	127	133	677	-	-
HCM Lane V/C Ratio	-	-	-	0.22	1.249	0.048	-	-
HCM Control Delay (s)	0	-	-	41.2	223.7	10.6	0	-
HCM Lane LOS	A	-	-	E	F	B	A	-
HCM 95th %tile Q(veh)	0	-	-	0.8	10.2	0.1	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	161.4					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↖	↗	↖	↗	↗	↖
Traffic Vol, veh/h	956	433	73	16	61	261
Future Vol, veh/h	956	433	73	16	61	261
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	93	93	70	70	90	90
Heavy Vehicles, %	1	1	3	11	0	4
Mvmt Flow	1028	466	104	23	68	290

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	299	68	358	0	-	0
Stage 1	68	-	-	-	-	-
Stage 2	231	-	-	-	-	-
Critical Hdwy	6.41	6.21	4.13	-	-	-
Critical Hdwy Stg 1	5.41	-	-	-	-	-
Critical Hdwy Stg 2	5.41	-	-	-	-	-
Follow-up Hdwy	3.509	3.309	2.227	-	-	-
Pot Cap-1 Maneuver	~ 694	998	1195	-	-	-
Stage 1	~ 957	-	-	-	-	-
Stage 2	~ 810	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	~ 634	998	1195	-	-	-
Mov Cap-2 Maneuver	~ 634	-	-	-	-	-
Stage 1	~ 874	-	-	-	-	-
Stage 2	~ 810	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	213.2	6.8	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	1195	-	634	998	-	-
HCM Lane V/C Ratio	0.087	-	1.621	0.467	-	-
HCM Control Delay (s)	8.3	-	\$ 304.4	11.7	-	-
HCM Lane LOS	A	-	F	B	-	-
HCM 95th %tile Q(veh)	0.3	-	56.1	2.5	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2035 Build Condition Weekday AM Peak

Intersection						
Int Delay, s/veh	174.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↕
Traffic Vol, veh/h	0	246	1369	0	0	405
Future Vol, veh/h	0	246	1369	0	0	405
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	76	76	70	70	80	80
Heavy Vehicles, %	2	3	2	2	2	4
Mvmt Flow	0	324	1956	0	0	506

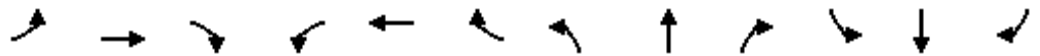
Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	-	1956	0	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-
Critical Hdwy	-	6.245	-	-	-	-
Critical Hdwy Stg 1	-	-	-	-	-	-
Critical Hdwy Stg 2	-	-	-	-	-	-
Follow-up Hdwy	-	3.3285	-	-	-	-
Pot Cap-1 Maneuver	0	~ 79	-	0	0	-
Stage 1	0	-	-	0	0	-
Stage 2	0	-	-	0	0	-
Platoon blocked, %			-			-
Mov Cap-1 Maneuver	-	~ 79	-	-	-	-
Mov Cap-2 Maneuver	-	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	-	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, \$	1502.2	0	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 79	-
HCM Lane V/C Ratio	- 4.097	-
HCM Control Delay (s)	\$ 1502.2	-
HCM Lane LOS	- F	-
HCM 95th %tile Q(veh)	- 34.1	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

101: International Dr & Pease Blvd
 2035 Build Condition Weekday PM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	↖	↕		↗	↕			↕	↗		↕	↖
Traffic Volume (vph)	0	519	3	464	201	27	12	3	1468	63	3	3
Future Volume (vph)	0	519	3	464	201	27	12	3	1468	63	3	3
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	12	12	12	12	12	12	11	12	12	16	12
Total Lost time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Lane Util. Factor		0.95		0.97	0.95			1.00	0.88		1.00	
Fr _t		1.00		1.00	0.98			1.00	0.85		0.99	
Fl _t Protected		1.00		0.95	1.00			0.96	1.00		0.96	
Satd. Flow (prot)		3572		3433	3546			1765	2814		2048	
Fl _t Permitted		1.00		0.95	1.00			0.82	1.00		0.73	
Satd. Flow (perm)		3572		3433	3546			1501	2814		1566	
Peak-hour factor, PHF	0.88	0.88	0.88	0.96	0.96	0.96	0.91	0.91	0.91	0.68	0.68	0.68
Adj. Flow (vph)	0	590	3	483	209	28	13	3	1613	93	4	4
RTOR Reduction (vph)	0	0	0	0	5	0	0	0	0	0	1	0
Lane Group Flow (vph)	0	593	0	483	232	0	0	16	1613	0	100	0
Heavy Vehicles (%)	0%	1%	0%	2%	0%	0%	0%	0%	1%	0%	0%	0%
Turn Type	Prot	NA		Prot	NA		Perm	NA	Perm	Perm	NA	
Protected Phases	6	2		1	5			8			4	
Permitted Phases							8		8		4	
Actuated Green, G (s)		17.5		16.3	39.8			20.2	20.2		20.2	
Effective Green, g (s)		17.5		16.3	39.8			20.2	20.2		20.2	
Actuated g/C Ratio		0.24		0.23	0.55			0.28	0.28		0.28	
Clearance Time (s)		6.0		6.0	6.0			6.0	6.0		6.0	
Vehicle Extension (s)		3.0		3.0	3.0			3.0	3.0		3.0	
Lane Grp Cap (vph)		868		777	1960			421	789		439	
v/s Ratio Prot		c0.17		c0.14	0.07							
v/s Ratio Perm								0.01	c0.57		0.06	
v/c Ratio		0.68		0.62	0.12			0.04	2.04		0.23	
Uniform Delay, d ₁		24.7		25.1	7.7			18.8	25.9		19.9	
Progression Factor		1.00		1.00	1.00			1.00	1.00		1.00	
Incremental Delay, d ₂		2.2		1.6	0.0			0.0	474.4		0.3	
Delay (s)		27.0		26.6	7.7			18.9	500.3		20.2	
Level of Service		C		C	A			B	F		C	
Approach Delay (s)		27.0			20.4			495.6			20.2	
Approach LOS		C			C			F			C	

Intersection Summary

HCM 2000 Control Delay	276.0	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.17		
Actuated Cycle Length (s)	72.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	85.8%	ICU Level of Service	E
Analysis Period (min)	15		

c Critical Lane Group
























102: US Route 4 SB On-Ramp/US Route 4 SB Off-Ramp & Pease Blvd
 2035 Build Condition Weekday PM Peak



Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↑↑↑	↗	↘	↑↑					↖		↗
Traffic Volume (vph)	0	1350	700	756	526	0	0	0	0	429	0	171
Future Volume (vph)	0	1350	700	756	526	0	0	0	0	429	0	171
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	12	10	11	10	11	12	12	12	12	12	12	12
Total Lost time (s)		6.0	6.0	6.0	6.0					6.0		6.0
Lane Util. Factor		0.86	1.00	0.97	0.95					0.97		0.88
Frt		1.00	0.85	1.00	1.00					1.00		0.85
Flt Protected		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (prot)		6040	1546	3236	3455					3502		2814
Flt Permitted		1.00	1.00	0.95	1.00					0.95		1.00
Satd. Flow (perm)		6040	1546	3236	3455					3502		2814
Peak-hour factor, PHF	0.85	0.85	0.85	0.94	0.94	0.94	0.92	0.92	0.92	0.90	0.90	0.90
Adj. Flow (vph)	0	1588	824	804	560	0	0	0	0	477	0	190
RTOR Reduction (vph)	0	0	363	0	0	0	0	0	0	0	0	144
Lane Group Flow (vph)	0	1588	461	804	560	0	0	0	0	477	0	46
Heavy Vehicles (%)	0%	1%	1%	1%	1%	0%	0%	0%	0%	0%	0%	1%
Turn Type		NA	Prot	Prot	NA					Prot		Prot
Protected Phases		6	6	5	2 5					3		3
Permitted Phases												
Actuated Green, G (s)		35.0	35.0	25.0	66.0					24.7		24.7
Effective Green, g (s)		35.0	35.0	25.0	66.0					24.7		24.7
Actuated g/C Ratio		0.34	0.34	0.24	0.64					0.24		0.24
Clearance Time (s)		6.0	6.0	6.0						6.0		6.0
Vehicle Extension (s)		5.0	5.0	4.0						5.0		5.0
Lane Grp Cap (vph)		2058	526	787	2220					842		676
v/s Ratio Prot		0.26	c0.30	c0.25	0.16					c0.14		0.02
v/s Ratio Perm												
v/c Ratio		0.77	0.88	1.02	0.25					0.57		0.07
Uniform Delay, d1		30.3	31.8	38.9	7.8					34.3		30.1
Progression Factor		1.00	1.00	1.33	1.25					1.00		1.00
Incremental Delay, d2		2.2	16.2	29.2	0.1					1.4		0.1
Delay (s)		32.4	48.0	81.1	9.9					35.7		30.2
Level of Service		C	D	F	A					D		C
Approach Delay (s)		37.8			51.8			0.0			34.2	
Approach LOS		D			D			A			C	
Intersection Summary												
HCM 2000 Control Delay			41.5			HCM 2000 Level of Service					D	
HCM 2000 Volume to Capacity ratio			0.83									
Actuated Cycle Length (s)			102.7			Sum of lost time (s)					18.0	
Intersection Capacity Utilization			92.1%			ICU Level of Service					F	
Analysis Period (min)			15									

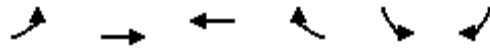
c Critical Lane Group

103: US Route 4 NB Off-ramp/US Route 4 NB On-Ramp & Pease Blvd
 2035 Build Condition Weekday PM Peak

												
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	 	 			  		 		 			
Traffic Volume (vph)	826	953	0	0	1029	450	253	0	691	0	0	0
Future Volume (vph)	826	953	0	0	1029	450	253	0	691	0	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Width	10	11	12	12	12	12	12	12	12	12	12	12
Total Lost time (s)	6.0	6.0			6.0		6.0		6.0			
Lane Util. Factor	0.97	0.95			0.91		0.97		0.88			
Frt	1.00	1.00			0.95		1.00		0.85			
Flt Protected	0.95	1.00			1.00		0.95		1.00			
Satd. Flow (prot)	3236	3455			4916		3433		2814			
Flt Permitted	0.11	1.00			1.00		0.95		1.00			
Satd. Flow (perm)	389	3455			4916		3433		2814			
Peak-hour factor, PHF	0.87	0.87	0.92	0.90	0.90	0.90	0.94	0.94	0.94	0.92	0.92	0.92
Adj. Flow (vph)	949	1095	0	0	1143	500	269	0	735	0	0	0
RTOR Reduction (vph)	0	0	0	0	76	0	0	0	558	0	0	0
Lane Group Flow (vph)	949	1095	0	0	1567	0	269	0	177	0	0	0
Heavy Vehicles (%)	1%	1%	0%	0%	1%	0%	2%	0%	1%	0%	0%	0%
Turn Type	pm+pt	NA			NA		Prot		Prot			
Protected Phases	1	6			2		3		3			
Permitted Phases	6											
Actuated Green, G (s)	60.0	35.0			35.0		24.7		24.7			
Effective Green, g (s)	60.0	35.0			35.0		24.7		24.7			
Actuated g/C Ratio	0.58	0.34			0.34		0.24		0.24			
Clearance Time (s)	6.0	6.0			6.0		6.0		6.0			
Vehicle Extension (s)	4.0	5.0			5.0		5.0		5.0			
Lane Grp Cap (vph)	920	1177			1675		825		676			
v/s Ratio Prot	c0.25	0.32			0.32		c0.08		0.06			
v/s Ratio Perm	c0.35											
v/c Ratio	1.03	0.93			0.94		0.33		0.26			
Uniform Delay, d1	30.4	32.7			32.8		32.1		31.6			
Progression Factor	1.63	0.57			1.00		1.00		1.00			
Incremental Delay, d2	32.9	9.8			10.6		0.5		0.4			
Delay (s)	82.5	28.5			43.3		32.6		32.0			
Level of Service	F	C			D		C		C			
Approach Delay (s)		53.6			43.3			32.2			0.0	
Approach LOS		D			D			C			A	
Intersection Summary												
HCM 2000 Control Delay			45.4				HCM 2000 Level of Service				D	
HCM 2000 Volume to Capacity ratio			0.83									
Actuated Cycle Length (s)			102.7				Sum of lost time (s)				18.0	
Intersection Capacity Utilization			92.1%				ICU Level of Service				F	
Analysis Period (min)			15									

c Critical Lane Group

104: Route 33 (Greenland Rd) & Grafton Rd
 2035 Build Condition Weekday PM Peak



Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations						
Traffic Volume (vph)	342	1825	1418	248	463	972
Future Volume (vph)	342	1825	1418	248	463	972
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Lane Util. Factor	1.00	0.95	0.95	1.00	1.00	1.00
Frt	1.00	1.00	1.00	0.85	1.00	0.85
Flt Protected	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (prot)	1787	3539	3539	1583	1787	1599
Flt Permitted	0.95	1.00	1.00	1.00	0.95	1.00
Satd. Flow (perm)	1787	3539	3539	1583	1787	1599
Peak-hour factor, PHF	0.88	0.88	0.93	0.93	0.87	0.87
Adj. Flow (vph)	389	2074	1525	267	532	1117
RTOR Reduction (vph)	0	0	0	186	0	165
Lane Group Flow (vph)	389	2074	1525	81	532	952
Heavy Vehicles (%)	1%	2%	2%	2%	1%	1%
Turn Type	Prot	NA	NA	Perm	Prot	Prot
Protected Phases	1	6	2		3	3
Permitted Phases				2		
Actuated Green, G (s)	5.0	29.0	18.0	18.0	18.0	18.0
Effective Green, g (s)	5.0	29.0	18.0	18.0	18.0	18.0
Actuated g/C Ratio	0.08	0.49	0.31	0.31	0.31	0.31
Clearance Time (s)	6.0	6.0	6.0	6.0	6.0	6.0
Vehicle Extension (s)	4.0	4.0	4.0	4.0	4.0	4.0
Lane Grp Cap (vph)	151	1739	1079	482	545	487
v/s Ratio Prot	c0.22	0.59	c0.43		0.30	c0.60
v/s Ratio Perm				0.05		
v/c Ratio	2.58	1.19	1.41	0.17	0.98	1.95
Uniform Delay, d1	27.0	15.0	20.5	15.0	20.3	20.5
Progression Factor	1.00	1.00	1.00	1.00	1.00	1.00
Incremental Delay, d2	728.2	92.7	191.5	0.8	32.3	436.8
Delay (s)	755.2	107.7	212.0	15.8	52.6	457.3
Level of Service	F	F	F	B	D	F
Approach Delay (s)		210.0	182.8		326.7	
Approach LOS		F	F		F	

Intersection Summary

HCM 2000 Control Delay	234.3	HCM 2000 Level of Service	F
HCM 2000 Volume to Capacity ratio	1.79		
Actuated Cycle Length (s)	59.0	Sum of lost time (s)	18.0
Intersection Capacity Utilization	109.4%	ICU Level of Service	H
Analysis Period (min)	15		
c Critical Lane Group			

105: International Drive & Corporate Drive
 2035 Build Condition Weekday PM Peak

Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	154	5	17	10	27	657	17	633	8	158	150	96
Future Volume (vph)	154	5	17	10	27	657	17	633	8	158	150	96
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Total Lost time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Lane Util. Factor	1.00	1.00		1.00	1.00	1.00	1.00	0.95		1.00	1.00	1.00
Frt	1.00	0.88		1.00	1.00	0.85	1.00	1.00		1.00	1.00	0.85
Flt Protected	0.95	1.00		0.95	1.00	1.00	0.95	1.00		0.95	1.00	1.00
Satd. Flow (prot)	1805	1681		1805	1792	1599	1805	3568		1736	1845	1615
Flt Permitted	0.73	1.00		0.74	1.00	1.00	0.66	1.00		0.16	1.00	1.00
Satd. Flow (perm)	1395	1681		1407	1792	1599	1245	3568		289	1845	1615
Peak-hour factor, PHF	0.84	0.84	0.84	0.77	0.77	0.77	0.89	0.89	0.89	0.93	0.93	0.93
Adj. Flow (vph)	183	6	20	13	35	853	19	711	9	170	161	103
RTOR Reduction (vph)	0	11	0	0	0	156	0	1	0	0	0	63
Lane Group Flow (vph)	183	15	0	13	35	697	19	719	0	170	161	40
Heavy Vehicles (%)	0%	0%	0%	0%	6%	1%	0%	1%	0%	4%	3%	0%
Turn Type	Perm	NA		Perm	NA	Perm	Perm	NA		pm+pt	NA	Perm
Protected Phases		4			8			2		1	6	
Permitted Phases	4			8		8	2			6		6
Actuated Green, G (s)	39.5	39.5		39.5	39.5	39.5	20.8	20.8		32.9	32.9	32.9
Effective Green, g (s)	39.5	39.5		39.5	39.5	39.5	20.8	20.8		32.9	32.9	32.9
Actuated g/C Ratio	0.47	0.47		0.47	0.47	0.47	0.25	0.25		0.39	0.39	0.39
Clearance Time (s)	6.0	6.0		6.0	6.0	6.0	6.0	6.0		4.5	6.0	6.0
Vehicle Extension (s)	3.0	3.0		3.0	3.0	3.0	3.0	3.0		3.0	3.0	3.0
Lane Grp Cap (vph)	652	786		658	838	748	306	879		242	719	629
v/s Ratio Prot		0.01			0.02			c0.20		c0.06	0.09	
v/s Ratio Perm	0.13			0.01		c0.44	0.02			0.21		0.02
v/c Ratio	0.28	0.02		0.02	0.04	0.93	0.06	0.82		0.70	0.22	0.06
Uniform Delay, d1	13.7	12.1		12.1	12.2	21.2	24.3	30.0		19.3	17.2	16.1
Progression Factor	1.00	1.00		1.00	1.00	1.00	1.00	1.00		1.00	1.00	1.00
Incremental Delay, d2	0.2	0.0		0.0	0.0	18.3	0.1	6.0		8.9	0.2	0.0
Delay (s)	14.0	12.1		12.1	12.2	39.5	24.4	36.0		28.1	17.4	16.2
Level of Service	B	B		B	B	D	C	D		C	B	B
Approach Delay (s)		13.7			38.0			35.7			21.3	
Approach LOS		B			D			D			C	
Intersection Summary												
HCM 2000 Control Delay			31.9									C
HCM 2000 Volume to Capacity ratio			0.87									
Actuated Cycle Length (s)			84.4							16.5		
Intersection Capacity Utilization			82.6%									E
Analysis Period (min)			15									
c Critical Lane Group												

202: Goose Bay Drive & Corporate Drive
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	335.7					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Vol, veh/h	153	18	13	400	294	66
Future Vol, veh/h	153	18	13	400	294	66
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	70	70	73	73	40	40
Heavy Vehicles, %	4	0	0	2	0	0
Mvmt Flow	219	26	18	548	735	165

Major/Minor	Major1	Major2	Minor1		
Conflicting Flow All	0	0	245	0	816 232
Stage 1	-	-	-	-	232 -
Stage 2	-	-	-	-	584 -
Critical Hdwy	-	-	4.1	-	6.4 6.2
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	-	-	2.2	-	3.5 3.3
Pot Cap-1 Maneuver	-	-	1333	- ~	349 812
Stage 1	-	-	-	-	811 -
Stage 2	-	-	-	- ~	561 -
Platoon blocked, %	-	-	-	-	-
Mov Cap-1 Maneuver	-	-	1333	- ~	342 812
Mov Cap-2 Maneuver	-	-	-	- ~	342 -
Stage 1	-	-	-	-	811 -
Stage 2	-	-	-	- ~	550 -

Approach	EB	WB	NB
HCM Control Delay, s	0	0.2	\$ 637.8
HCM LOS			F

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	383	-	-	1333	-
HCM Lane V/C Ratio	2.35	-	-	0.013	-
HCM Control Delay (s)	\$ 637.8	-	-	7.7	0
HCM Lane LOS	F	-	-	A	A
HCM 95th %tile Q(veh)	69.5	-	-	0	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

203: Corporate Drive & Redhook Way
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.7					
Movement	EBL	EBT	WBT	WBR	SBL	SBR
Lane Configurations	↙	↑	↘		↘	
Traffic Vol, veh/h	8	210	400	3	1	14
Future Vol, veh/h	8	210	400	3	1	14
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	0	-
Veh in Median Storage, #	-	0	0	-	0	-
Grade, %	-	0	0	-	0	-
Peak Hour Factor	63	63	77	77	36	36
Heavy Vehicles, %	40	0	0	1	0	11
Mvmt Flow	13	333	519	4	3	39

Major/Minor	Major1	Major2	Minor2		
Conflicting Flow All	523	0	-	0	880 521
Stage 1	-	-	-	-	521 -
Stage 2	-	-	-	-	359 -
Critical Hdwy	4.5	-	-	-	6.4 6.31
Critical Hdwy Stg 1	-	-	-	-	5.4 -
Critical Hdwy Stg 2	-	-	-	-	5.4 -
Follow-up Hdwy	2.56	-	-	-	3.5 3.399
Pot Cap-1 Maneuver	876	-	-	-	320 538
Stage 1	-	-	-	-	600 -
Stage 2	-	-	-	-	711 -
Platoon blocked, %		-	-	-	
Mov Cap-1 Maneuver	876	-	-	-	315 538
Mov Cap-2 Maneuver	-	-	-	-	315 -
Stage 1	-	-	-	-	591 -
Stage 2	-	-	-	-	711 -

Approach	EB	WB	SB
HCM Control Delay, s	0.3	0	12.6
HCM LOS			B

Minor Lane/Major Mvmt	EBL	EBT	WBT	WBR	SBLn1
Capacity (veh/h)	876	-	-	-	514
HCM Lane V/C Ratio	0.014	-	-	-	0.081
HCM Control Delay (s)	9.2	-	-	-	12.6
HCM Lane LOS	A	-	-	-	B
HCM 95th %tile Q(veh)	0	-	-	-	0.3

204: Goose Bay Drive & Corporate Drive
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.4					
Movement	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↔			↔		↔
Traffic Vol, veh/h	218	1	0	230	12	0
Future Vol, veh/h	218	1	0	230	12	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Free	Free	Free	Free	Stop	Stop
RT Channelized	-	None	-	None	-	None
Storage Length	-	-	-	-	0	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	78	78	81	81	71	71
Heavy Vehicles, %	0	0	0	1	11	0
Mvmt Flow	279	1	0	284	17	0

Major/Minor	Major1	Major2	Minor1	Minor2
Conflicting Flow All	0	0	280	564
Stage 1	-	-	-	280
Stage 2	-	-	-	284
Critical Hdwy	-	-	4.1	6.51
Critical Hdwy Stg 1	-	-	-	5.51
Critical Hdwy Stg 2	-	-	-	5.51
Follow-up Hdwy	-	-	2.2	3.599
Pot Cap-1 Maneuver	-	-	1294	472
Stage 1	-	-	-	747
Stage 2	-	-	-	744
Platoon blocked, %	-	-	-	-
Mov Cap-1 Maneuver	-	-	1294	472
Mov Cap-2 Maneuver	-	-	-	472
Stage 1	-	-	-	747
Stage 2	-	-	-	744

Approach	EB	WB	NB
HCM Control Delay, s	0	0	12.9
HCM LOS			B

Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT
Capacity (veh/h)	472	-	-	1294	-
HCM Lane V/C Ratio	0.036	-	-	-	-
HCM Control Delay (s)	12.9	-	-	0	-
HCM Lane LOS	B	-	-	A	-
HCM 95th %tile Q(veh)	0.1	-	-	0	-

205: Goose Bay Drive & Corporate Center Dwy
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Vol, veh/h	1	12	0	0	1	0
Future Vol, veh/h	1	12	0	0	1	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	67	67	69	69	50	50
Heavy Vehicles, %	0	0	10	0	0	0
Mvmt Flow	1	18	0	0	2	0

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	4	0	0	0	0	0
Stage 1	0	-	-	-	-	-
Stage 2	4	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	1023	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	1024	-	-	-	-	-
Platoon blocked, %						
Mov Cap-1 Maneuver	1023	-	-	-	-	-
Mov Cap-2 Maneuver	1023	-	-	-	-	-
Stage 1	-	-	-	-	-	-
Stage 2	1024	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s		0	
HCM LOS	-		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	-	-
HCM Lane V/C Ratio	-	-	-	-
HCM Control Delay (s)	-	-	-	-
HCM Lane LOS	-	-	-	-
HCM 95th %tile Q(veh)	-	-	-	-

206: Goose Bay Drive & Lonza South Dwy
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	6.8					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations						
Traffic Vol, veh/h	3	0	0	1	0	0
Future Vol, veh/h	3	0	0	1	0	0
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	25	25	63	63	63	63
Heavy Vehicles, %	0	0	0	0	10	0
Mvmt Flow	12	0	0	2	0	0

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	4	2	2	0	-	0
Stage 1	2	-	-	-	-	-
Stage 2	2	-	-	-	-	-
Critical Hdwy	6.4	6.2	4.1	-	-	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	2.2	-	-	-
Pot Cap-1 Maneuver	1023	1088	1634	-	-	-
Stage 1	1026	-	-	-	-	-
Stage 2	1026	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	1023	1088	1634	-	-	-
Mov Cap-2 Maneuver	1023	-	-	-	-	-
Stage 1	1026	-	-	-	-	-
Stage 2	1026	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	8.6	0	0
HCM LOS	A		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	SBT	SBR
Capacity (veh/h)	1634	-	1023	-	-
HCM Lane V/C Ratio	-	-	0.012	-	-
HCM Control Delay (s)	0	-	8.6	-	-
HCM Lane LOS	A	-	A	-	-
HCM 95th %tile Q(veh)	0	-	0	-	-

207: Goose Bay Drive & Lonza Parking Garage/Proposed Dwy
 2035 Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	3.2											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	0	0	0	0	0	144	0	216	0	13	12	6
Future Vol, veh/h	0	0	0	0	0	144	0	216	0	13	12	6
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	92	92	92	92	92	92	39	39	92	92	67	67
Heavy Vehicles, %	2	2	2	2	2	2	0	0	2	2	0	0
Mvmt Flow	0	0	0	0	0	157	0	554	0	14	18	9

Major/Minor	Minor2		Minor1		Major1			Major2				
Conflicting Flow All	684	605	23	605	609	554	27	0	0	554	0	0
Stage 1	51	51	-	554	554	-	-	-	-	-	-	-
Stage 2	633	554	-	51	55	-	-	-	-	-	-	-
Critical Hdwy	7.12	6.52	6.22	7.12	6.52	6.22	4.1	-	-	4.12	-	-
Critical Hdwy Stg 1	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.12	5.52	-	6.12	5.52	-	-	-	-	-	-	-
Follow-up Hdwy	3.518	4.018	3.318	3.518	4.018	3.318	2.2	-	-	2.218	-	-
Pot Cap-1 Maneuver	363	412	1054	410	410	532	1600	-	-	1016	-	-
Stage 1	962	852	-	517	514	-	-	-	-	-	-	-
Stage 2	468	514	-	962	849	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	253	406	1054	405	404	532	1600	-	-	1016	-	-
Mov Cap-2 Maneuver	253	406	-	405	404	-	-	-	-	-	-	-
Stage 1	962	840	-	517	514	-	-	-	-	-	-	-
Stage 2	330	514	-	949	837	-	-	-	-	-	-	-

Approach	EB		WB		NB		SB		
HCM Control Delay, s	0		14.6		0		3		
HCM LOS	A		B						

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1	WBLn1	SBL	SBT	SBR
Capacity (veh/h)	1600	-	-	-	-	532	1016	-
HCM Lane V/C Ratio	-	-	-	-	0.294	0.014	-	-
HCM Control Delay (s)	0	-	-	0	14.6	8.6	0	-
HCM Lane LOS	A	-	-	A	B	A	A	-
HCM 95th %tile Q(veh)	0	-	-	-	1.2	0	-	-

208: Granite State Driveway & International Drive
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W	R	T	R	L	T
Traffic Vol, veh/h	8	3	655	1	5	165
Future Vol, veh/h	8	3	655	1	5	165
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	88	88	78	78	76	76
Heavy Vehicles, %	0	0	1	0	0	4
Mvmt Flow	9	3	840	1	7	217

Major/Minor	Minor1	Major1	Major2	Major3	Major4	Major5
Conflicting Flow All	1072	841	0	0	841	0
Stage 1	841	-	-	-	-	-
Stage 2	231	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	246	368	-	-	803	-
Stage 1	426	-	-	-	-	-
Stage 2	812	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	244	368	-	-	803	-
Mov Cap-2 Maneuver	244	-	-	-	-	-
Stage 1	426	-	-	-	-	-
Stage 2	804	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	19	0	0.3
HCM LOS	C		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	269	803
HCM Lane V/C Ratio	-	-	0.046	0.008
HCM Control Delay (s)	-	-	19	9.5
HCM Lane LOS	-	-	C	A
HCM 95th %tile Q(veh)	-	-	0.1	0

209: International Drive & Lonza North Driveway
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	12.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	T		T		T	
Traffic Vol, veh/h	54	166	490	17	15	158
Future Vol, veh/h	54	166	490	17	15	158
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	72	72	67	67	81	81
Heavy Vehicles, %	14	0	1	46	0	3
Mvmt Flow	75	231	731	25	19	195

Major/Minor	Minor1	Major1	Major2		
Conflicting Flow All	977	744	0	0	756
Stage 1	744	-	-	-	-
Stage 2	233	-	-	-	-
Critical Hdwy	6.54	6.2	-	-	4.1
Critical Hdwy Stg 1	5.54	-	-	-	-
Critical Hdwy Stg 2	5.54	-	-	-	-
Follow-up Hdwy	3.626	3.3	-	-	2.2
Pot Cap-1 Maneuver	264	418	-	-	864
Stage 1	449	-	-	-	-
Stage 2	778	-	-	-	-
Platoon blocked, %			-	-	-
Mov Cap-1 Maneuver	257	418	-	-	864
Mov Cap-2 Maneuver	257	-	-	-	-
Stage 1	449	-	-	-	-
Stage 2	759	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	50.6	0	0.8
HCM LOS	F		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	362	864
HCM Lane V/C Ratio	-	-	0.844	0.021
HCM Control Delay (s)	-	-	50.6	9.3
HCM Lane LOS	-	-	F	A
HCM 95th %tile Q(veh)	-	-	7.7	0.1

210: International Drive & Lonza South Driveway
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.3					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations	W		T			T
Traffic Vol, veh/h	0	5	404	0	0	232
Future Vol, veh/h	0	5	404	0	0	232
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	-	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	25	25	68	68	74	74
Heavy Vehicles, %	0	0	3	0	0	7
Mvmt Flow	0	20	594	0	0	314

Major/Minor	Minor1	Major1	Major2			
Conflicting Flow All	908	594	0	0	594	0
Stage 1	594	-	-	-	-	-
Stage 2	314	-	-	-	-	-
Critical Hdwy	6.4	6.2	-	-	4.1	-
Critical Hdwy Stg 1	5.4	-	-	-	-	-
Critical Hdwy Stg 2	5.4	-	-	-	-	-
Follow-up Hdwy	3.5	3.3	-	-	2.2	-
Pot Cap-1 Maneuver	308	509	-	-	992	-
Stage 1	555	-	-	-	-	-
Stage 2	745	-	-	-	-	-
Platoon blocked, %			-	-		
Mov Cap-1 Maneuver	308	509	-	-	992	-
Mov Cap-2 Maneuver	308	-	-	-	-	-
Stage 1	555	-	-	-	-	-
Stage 2	745	-	-	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	12.4	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT
Capacity (veh/h)	-	-	509	992
HCM Lane V/C Ratio	-	-	0.039	-
HCM Control Delay (s)	-	-	12.4	0
HCM Lane LOS	-	-	B	A
HCM 95th %tile Q(veh)	-	-	0.1	0

211: Corporate Dr/New Hampshire Ave & Durham St/International Dr
 2035 Build Condition Weekday PM Peak

Intersection												
Int Delay, s/veh	205.8											
Movement	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		↕			↕			↕			↕	
Traffic Vol, veh/h	30	23	3	314	21	23	1	326	114	3	560	14
Future Vol, veh/h	30	23	3	314	21	23	1	326	114	3	560	14
Conflicting Peds, #/hr	0	0	0	0	0	0	0	0	0	0	0	0
Sign Control	Stop	Stop	Stop	Stop	Stop	Stop	Free	Free	Free	Free	Free	Free
RT Channelized	-	-	None	-	-	None	-	-	None	-	-	None
Storage Length	-	-	-	-	-	-	-	-	-	-	-	-
Veh in Median Storage, #	-	0	-	-	0	-	-	0	-	-	0	-
Grade, %	-	0	-	-	0	-	-	0	-	-	0	-
Peak Hour Factor	54	54	54	85	85	85	84	84	84	88	88	88
Heavy Vehicles, %	0	13	0	0	14	0	0	2	1	0	1	11
Mvmt Flow	56	43	6	369	25	27	1	388	136	3	636	16

Major/Minor	Minor2		Minor1		Major1		Major2					
Conflicting Flow All	1134	1176	644	1133	1116	456	652	0	0	524	0	0
Stage 1	650	650	-	458	458	-	-	-	-	-	-	-
Stage 2	484	526	-	675	658	-	-	-	-	-	-	-
Critical Hdwy	7.1	6.63	6.2	7.1	6.64	6.2	4.1	-	-	4.1	-	-
Critical Hdwy Stg 1	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Critical Hdwy Stg 2	6.1	5.63	-	6.1	5.64	-	-	-	-	-	-	-
Follow-up Hdwy	3.5	4.117	3.3	3.5	4.126	3.3	2.2	-	-	2.2	-	-
Pot Cap-1 Maneuver	181	182	476	~ 182	197	609	944	-	-	1053	-	-
Stage 1	461	448	-	587	547	-	-	-	-	-	-	-
Stage 2	568	511	-	447	443	-	-	-	-	-	-	-
Platoon blocked, %								-	-	-	-	-
Mov Cap-1 Maneuver	155	181	476	~ 147	196	609	944	-	-	1053	-	-
Mov Cap-2 Maneuver	155	181	-	~ 147	196	-	-	-	-	-	-	-
Stage 1	460	446	-	586	546	-	-	-	-	-	-	-
Stage 2	517	510	-	398	441	-	-	-	-	-	-	-

Approach	EB	WB	NB	SB
HCM Control Delay, s	54.1	\$ 820.1	0	0
HCM LOS	F	F		

Minor Lane/Major Mvmt	NBL	NBT	NBR	EBLn1WBLn1	SBL	SBT	SBR
Capacity (veh/h)	944	-	-	171	157	1053	-
HCM Lane V/C Ratio	0.001	-	-	0.606	2.683	0.003	-
HCM Control Delay (s)	8.8	0	-	54.1	\$ 820.1	8.4	0
HCM Lane LOS	A	A	-	F	F	A	A
HCM 95th %tile Q(veh)	0	-	-	3.3	37.3	0	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

212: Corporate Dr & Grafton Rd
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	177.5					
Movement	EBL	EBR	NBL	NBT	SBT	SBR
Lane Configurations	↖	↗	↖	↗	↗	↖
Traffic Vol, veh/h	373	85	267	51	27	870
Future Vol, veh/h	373	85	267	51	27	870
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	0	290	100	-	-	175
Veh in Median Storage, #	0	-	-	0	0	-
Grade, %	0	-	-	0	0	-
Peak Hour Factor	86	86	76	76	83	83
Heavy Vehicles, %	2	2	1	3	0	1
Mvmt Flow	434	99	351	67	33	1048

Major/Minor	Minor2	Major1	Major2			
Conflicting Flow All	802	33	1081	0	-	0
Stage 1	33	-	-	-	-	-
Stage 2	769	-	-	-	-	-
Critical Hdwy	6.42	6.22	4.11	-	-	-
Critical Hdwy Stg 1	5.42	-	-	-	-	-
Critical Hdwy Stg 2	5.42	-	-	-	-	-
Follow-up Hdwy	3.518	3.318	2.209	-	-	-
Pot Cap-1 Maneuver	~ 353	1041	649	-	-	-
Stage 1	989	-	-	-	-	-
Stage 2	457	-	-	-	-	-
Platoon blocked, %				-	-	-
Mov Cap-1 Maneuver	~ 162	1041	649	-	-	-
Mov Cap-2 Maneuver	~ 162	-	-	-	-	-
Stage 1	454	-	-	-	-	-
Stage 2	457	-	-	-	-	-

Approach	EB	NB	SB
HCM Control Delay, s	666.1	14.2	0
HCM LOS	F		

Minor Lane/Major Mvmt	NBL	NBT	EBLn1	EBLn2	SBT	SBR
Capacity (veh/h)	649	-	162	1041	-	-
HCM Lane V/C Ratio	0.541	-	2.677	0.095	-	-
HCM Control Delay (s)	16.9	-	815.9	8.8	-	-
HCM Lane LOS	C	-	F	A	-	-
HCM 95th %tile Q(veh)	3.3	-	38.2	0.3	-	-

Notes
 ~: Volume exceeds capacity \$: Delay exceeds 300s +: Computation Not Defined *: All major volume in platoon

213: Grafton Rd & I-95 SB Off-ramp
 2035 Build Condition Weekday PM Peak

Intersection						
Int Delay, s/veh	0.6					
Movement	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations		↗	↖			↖↗
Traffic Vol, veh/h	0	72	590	0	0	1435
Future Vol, veh/h	0	72	590	0	0	1435
Conflicting Peds, #/hr	0	0	0	0	0	0
Sign Control	Stop	Stop	Free	Free	Free	Free
RT Channelized	-	None	-	None	-	None
Storage Length	-	0	-	-	-	-
Veh in Median Storage, #	0	-	0	-	-	0
Grade, %	0	-	0	-	-	0
Peak Hour Factor	73	73	95	95	89	89
Heavy Vehicles, %	0	13	0	1	0	1
Mvmt Flow	0	99	621	0	0	1612

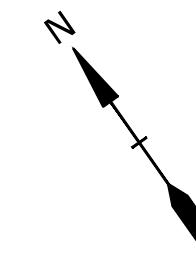
Major/Minor	Minor1	Major1	Major2
Conflicting Flow All	-	621	0
Stage 1	-	-	-
Stage 2	-	-	-
Critical Hdwy	-	6.395	-
Critical Hdwy Stg 1	-	-	-
Critical Hdwy Stg 2	-	-	-
Follow-up Hdwy	-	3.4235	-
Pot Cap-1 Maneuver	0	462	-
Stage 1	0	-	-
Stage 2	0	-	-
Platoon blocked, %	-	-	-
Mov Cap-1 Maneuver	-	462	-
Mov Cap-2 Maneuver	-	-	-
Stage 1	-	-	-
Stage 2	-	-	-

Approach	WB	NB	SB
HCM Control Delay, s	14.9	0	0
HCM LOS	B		

Minor Lane/Major Mvmt	NBTWBLn1	SBT
Capacity (veh/h)	- 462	-
HCM Lane V/C Ratio	- 0.213	-
HCM Control Delay (s)	- 14.9	-
HCM Lane LOS	- B	-
HCM 95th %tile Q(veh)	- 0.8	-

APPENDIX I

Site Development Plan



**PROPOSED ADMINISTRATIVE
APPROVAL MASTER SITE PLAN**
01/09/2023

SITE DATA

LOCATION: TAX MAP 305, LOTS 1 & 2
70 & 80 CORPORATE DRIVE
PORTSMOUTH, NH

TAX MAP 305, LOT 6
101 INTERNATIONAL DRIVE
PORTSMOUTH, NH

ZONING DISTRICT: AIRPORT, BUSINESS & COMMERCIAL (ABC)

DIMENSIONAL REQUIREMENTS:

MINIMUM LOT AREA:	REQUIRED 5 AC	PROVIDED 43.4± AC
MINIMUM STREET FRONTAGE:	200 FT	1,038 FT
MINIMUM FRONT YARD SETBACK:	70 FT	70 FT
SIDE SETBACK:	30 FT	30 FT
REAR SETBACK:	50 FT	51 FT
MINIMUM OPEN SPACE:	25 %	43.3± %

MAXIMUM STRUCTURE HEIGHT SHALL NOT EXCEED FAA CRITERIA.

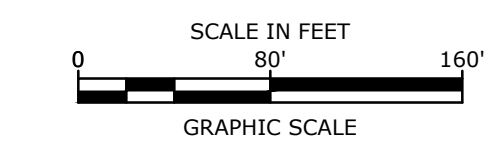
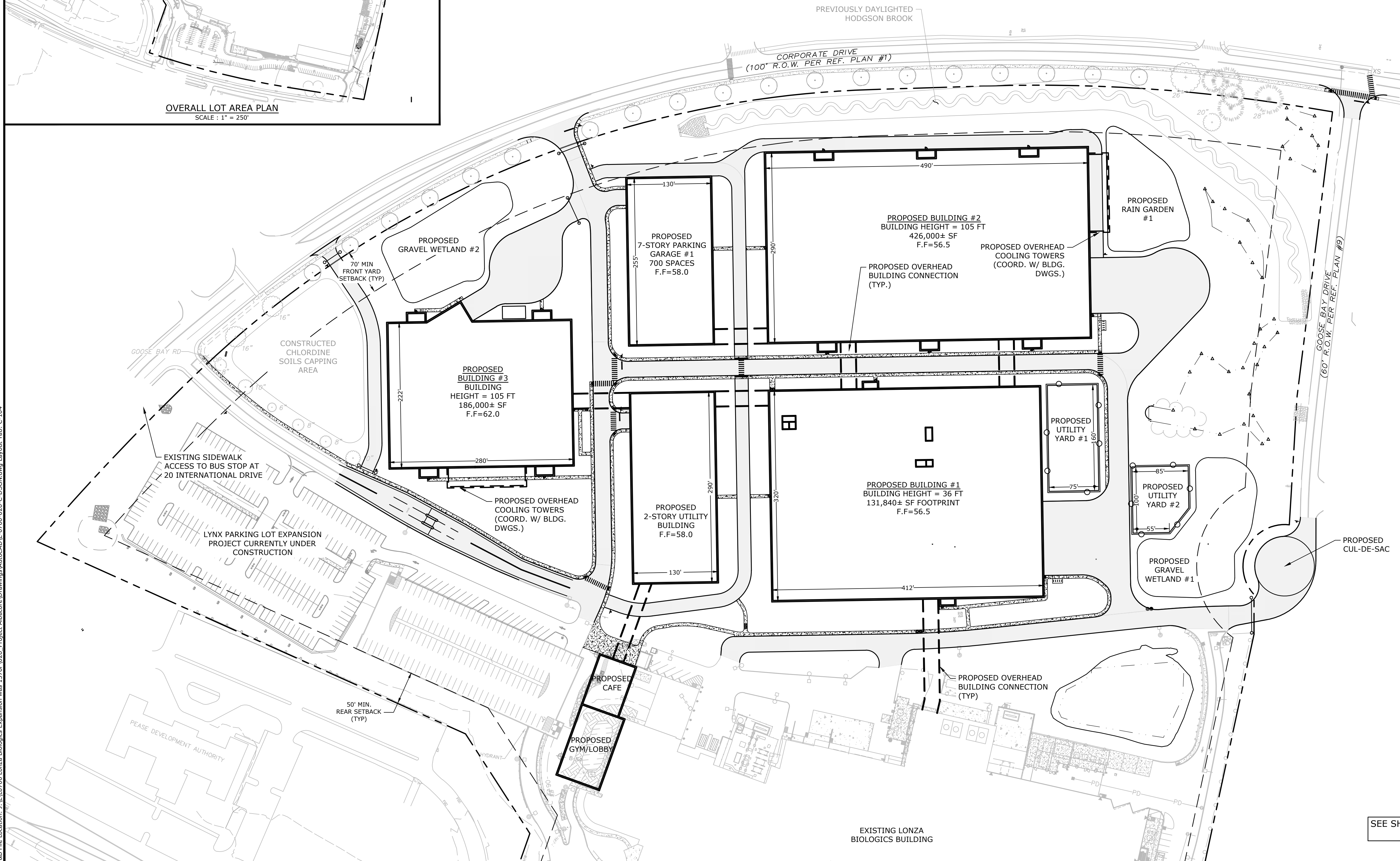
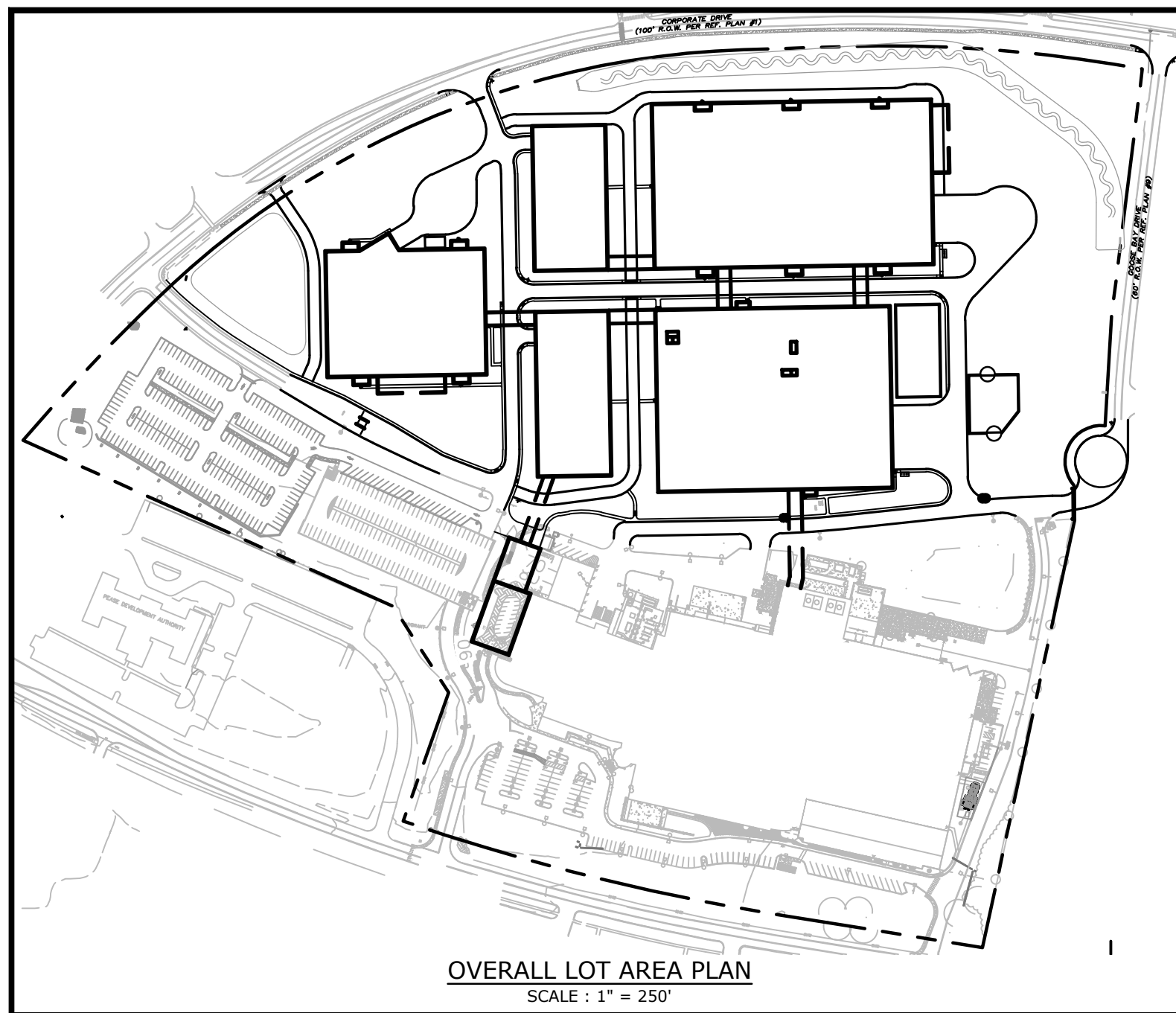
PARKING REQUIREMENTS:

REQUIRED PARKING

2 SPACES PER 3 EMPLOYEES ON LARGEST SHIFT	
740 EXISTING EMPLOYEES	493 SPACES
1250 ANTICIPATED EMPLOYEES	833 SPACES
TOTAL REQUIRED:	1,326 SPACES

PARKING PROVIDED

EXISTING SPACES:	522 SPACES
LYNX PARKING LOT EXPANSION SPACES:	222 SPACES
PROPOSED PARKING GARAGE #1:	700 SPACES
TOTAL:	1,444 SPACES



**Proposed
Industrial
Development**

Lonza Biologics

Portsmouth,
New Hampshire

I	1/9/2023	Admin. Approval Submission
H	12/10/2021	Planning Board Stipulation
G	8/19/2019	Admin. Approval Submission
F	11/6/2018	P.B. Submission
E	8/30/2018	Revised Aot Submission

MARK	DATE	DESCRIPTION
PROJECT NO: L-0700-013		
DATE: 04/03/2018		
FILE: L-0700-026-C-DSGN.dwg		
DRAWN BY: CJK		
CHECKED: NAH		
APPROVED: PMC		

MASTER SITE PLAN

SCALE: AS SHOWN

C-104

SEE SHEET C-105 FOR LEGEND
AND SITE NOTES

Last Save Date: January 6, 2023 3:51 PM By: CKRZCUIK
 Plot Date: Monday, January 09, 2023 Plotted By: Colter Krzoulik
 P&E File Location: J:\110700 Lonza Biologics Expansion.was 12/26/2026 Project Abstract\Drawings\AutoCAD\0700-026-C-DSGN.dwg Layout Tab: C-104

APPENDIX J

Traffic Control Signal Plans

SIGN 9"x 12" 1 EACH
 SIGN 9"x 12" 5 EACH

R10-3A(R) BLACK ON WHITE
 R10-3A(L) BLACK ON WHITE

1 MOUNTED OVER PUSH BUTTON
 5 MOUNTED OVER PUSH BUTTONS

SIGN 24"x 30" 2 EACH
 SIGN 30"x 30" 4 EACH
 SIGN 24"x 30" 2 EACH

R3-5L BLACK ON WHITE
 R3-7L LEFT LANE MUST TURN LEFT BLACK ON WHITE
 R4-7 BLACK ON WHITE

MOUNTED ON MAST ARM NEXT TO LEFT TURN SIGNAL
 1 T.S. POST MOUNTED
 1 T.S. POST MOUNTED (PAIR)

PULL BOX SCHEDULE

49+36 - 42' RT
49+42 - 05' LT
49+01 - 17' LT
50+36 - 11' LT
50+51 - 01' RT (2)
64+55 - 44' RT (SHEET 36)
65+45 - 44' RT (SHEET 34)
66+35 - 44' RT (SHEET 34)
67+25 - 44' RT
68+15 - 44' RT
68+70 - 35' LT
68+93 - 22' RT
68+95 - 85' RT (2)
69+02 - 45' LT
69+01 - 46' RT
69+20 - 54' RT (2)
69+54 - 56' RT (2)



NOTES:

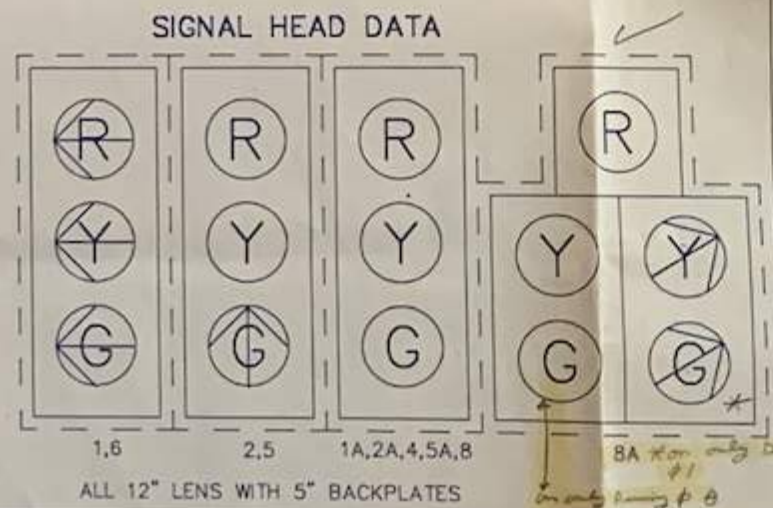
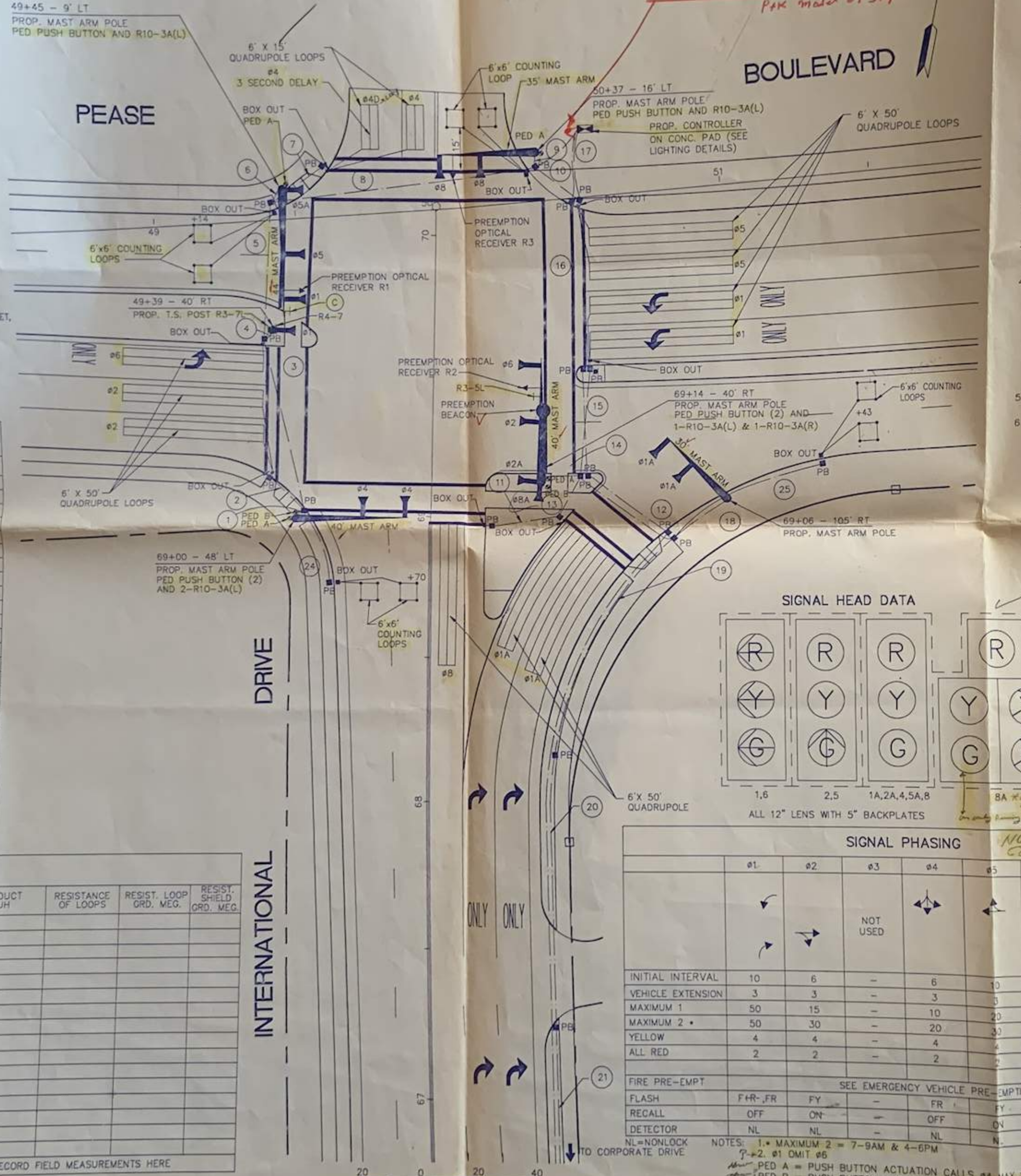
1. SIGNS MOUNTED ON MAST ARMS AND T.S. POSTS SHOWN ON THIS SHEET. OTHER POST MOUNTED SIGNS SHOWN ON SHEET 41.
2. FOR PAVEMENT MARKINGS SEE SHEET 41.
3. QUADRUPOLE LOOPS TO HAVE 2-4-2 LOOP WIRE CONFIGURATION. 6"x6" LOOPS TO HAVE 3 TURNS.

CONDUIT SCHEDULE

I.D.	STATION TO STATION	NO.	LENGTH	SCHEDULE TYPE	REMARKS
1	69+00 - 48' LT - 69+02 - 45' LT	1	4'	40	FROM MAST ARM
2	69+02 - 45' LT - 69+14 - 58' LT	1	16'	40	
3	69+02 - 45' LT - 49+36 - 42' RT	1	61'	80	
4	49+36 - 42' RT - 49+39 - 40' RT	1	4'	40	TO T.S. POST
5	49+39 - 40' RT - 49+42 - 05' LT	1	46'	80	
6	49+42 - 05' LT - 49+45 - 09' LT	1	5'	40	TO MAST ARM
7	49+42 - 05' LT - 49+61 - 17' LT	1	21'	40	
8	49+42 - 05' LT - 50+36 - 11' LT	1	94'	80	
9	50+36 - 11' LT - 50+36 - 11' LT	1	4'	40	FROM MAST ARM
10	50+36 - 11' LT - 50+64 - 22' LT	1	20'	40	TO CONTROLLER
11	68+97 - 22' RT - 69+01 - 46' RT	1	23'	40	1 POWER SERVICE
12	68+95 - 85' RT - 69+20 - 54' RT	2	40'	80	
13	69+01 - 46' RT - 69+20 - 54' RT	1	20'	40	
14	69+17 - 40' RT - 69+20 - 54' RT	1	13'	40	
15	69+20 - 54' RT - 69+54 - 56' RT	2	32'	80	1 POWER SERVICE
16	69+54 - 56' RT - 50+51 - 01' RT	2	59'	80	1 POWER SERVICE
17	50+51 - 01' RT - 50+64 - 22' LT	2	26'	40	1 POWER SERVICE
18	68+95 - 85' RT - 69+06 - 105' RT	1	23'	40	TO MAST ARM
19	68+95 - 85' RT - 68+15 - 44' RT	1	90'	40	
20	68+15 - 44' RT - 67+25 - 44' RT	1	90'	80	*SEE SHT. 8 TRNCH DTL.
21	67+25 - 44' RT - 66+35 - 44' RT	1	90'	40	*SEE SHT. 8 TRNCH DTL.
22	66+35 - 44' RT - 65+45 - 44' RT	1	90'	40	*SEE SHT. 8 TRNCH DTL.
23	65+45 - 44' RT - 64+55 - 44' RT	1	90'	40	*SEE SHT. 8 TRNCH DTL.
24	68+70 - 35' LT - 69+02 - 45' LT	1	35'	40	
25	68+95 - 85' RT - 51+30 - 98' RT	1	60'	40	

DETECTOR SCHEDULE

STREET	DIRECTION	LANE	β	AMPLIFIER NO.	CHANNEL	INDUCT UH	RESISTANCE OF LOOPS	RESIST. LOOP ORD. MEG.	RESIST. SHIELD ORD. MEG.
PEASE BOULEVARD	EASTBOUND	LEFT	6	1	1				
PEASE BOULEVARD	EASTBOUND	CENTER & RIGHT	2	1	2				
PEASE BOULEVARD	WESTBOUND	LEFT & CENTER	1	2	1				
PEASE BOULEVARD	WESTBOUND	CENTER & RIGHT	5	2	2				
INTERNATIONAL DRIVE	NORTHBOUND	LEFT	8	3	1				
INTERNATIONAL DRIVE	NORTHBOUND	CENTER & RIGHT	1	3	2				
DRIVE	SOUTHBOUND	LEFT	4	4	1				
DRIVE	SOUTHBOUND	RIGHT	4	5	2				
PEASE BOULEVARD	EB EGRESS	LEFT	C	6	1				
PEASE BOULEVARD	EB EGRESS	RIGHT	C	6	2				
PEASE BOULEVARD	WB EGRESS	LEFT	C	7	1				
PEASE BOULEVARD	WB EGRESS	RIGHT	C	7	2				
INTERNATIONAL DRIVE	SB EGRESS	LEFT	C	8	1				
INTERNATIONAL DRIVE	SB EGRESS	RIGHT	C	8	2				
DRIVE	NB EGRESS	LEFT	C	9	1				
DRIVE	NB EGRESS	RIGHT	C	9	2				



SIGNAL PHASING

	ø1	ø2	ø3	ø4	ø5	ø6	ø7	ø8
INITIAL INTERVAL	10	6	-	6	10	6	-	6
VEHICLE EXTENSION	3	3	-	3	3	2	-	3
MAXIMUM 1	50	15	-	10	20	10	-	10
MAXIMUM 2	50	30	-	20	30	15	-	20
YELLOW	4	4	-	4	4	3	-	4
ALL RED	2	2	-	2	2	2	-	2

EMERGENCY VEHICLE PRE-EMPTION OPERATION

	F+R-FR	FY	FR	FY	F+R	FR
FLASH						
RECALL	OFF	ON	OFF	ON	OFF	OFF
DETECTOR	NL	NL	NL	NL	NL	NL

NOTES:
 1. MAXIMUM 2 = 7-9AM & 4-6PM
 2. ø1 OMIT ø6
 PED A = PUSH BUTTON ACTUATION CALLS ø4 MAX 2
 PED B = PUSH BUTTON ACTUATION CALLS ø2 MAX 1

PRE-EMPTION PHASING & PRIORITY

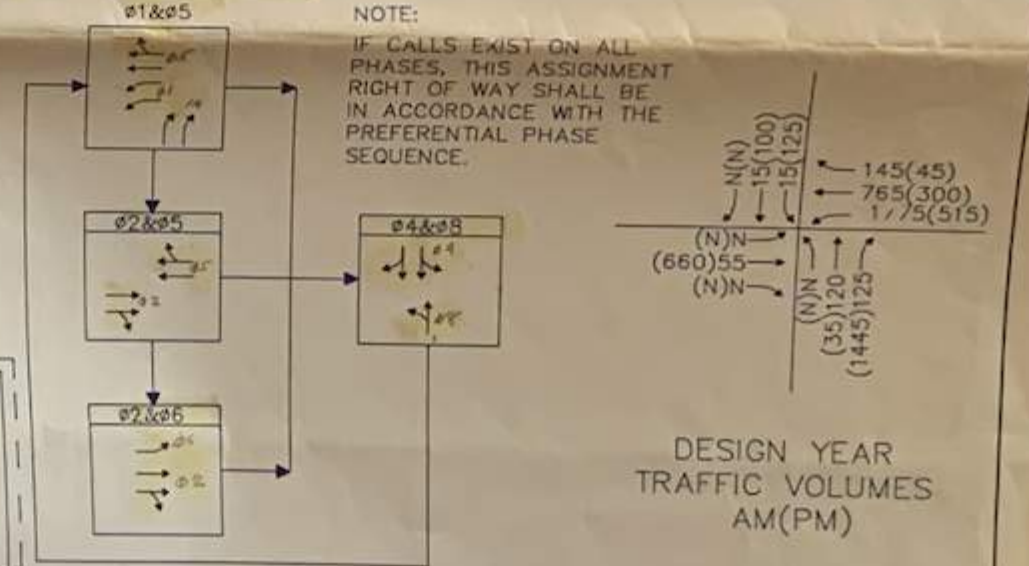
RECEIVER & PRIORITY	PREEMPT PHASE ASSIGNMENT	MOVEMENT	VEHICLE PHASE ASSIGNMENT
R1	1	[Symbol]	1 + 5
R2	2	[Symbol]	2 + 6
R3	3	[Symbol]	8

EMERGENCY VEHICLE PRE-EMPTION OPERATION

1. PRE-EMPTION OPERATION UTILIZES AVAILABLE PHASES IN 8 PHASE TIMER THROUGH THE MSD PRE-EMPT INPUTS TO EFFECT APPROPRIATE SIGNAL DISPLAYS FOR SINGLE APPROACH MOVEMENTS AS SHOWN IN THE PRE-EMPTION PHASING AND PRIORITY CHART.
2. EMERGENCY VEHICLE PRE-EMPTION SIGNALS SHALL BE OPTICALLY TRANSMITTED BY OPTICAL EMITTERS MOUNTED IN EMERGENCY VEHICLES AND RECEIVED BY OPTICAL DETECTORS LOCATED AT EACH INTERSECTION.
3. PRE-EMPTION SIGNALS SHALL BE SERVICED ON A PRIORITY BASIS WITH RECEIVERS 1, 2, OR 3 ASSIGNED DESCENDING PRIORITIES AS FOLLOWS: (1 HIGHEST AND 3 LOWEST)
4. IN RESPONSE TO A PRE-EMPTION SIGNAL RECEIVED AT AN INTERSECTION BY OPTICAL DETECTOR #1 (OR #2, #3) THE CONTROLLER SHALL HOLD OR ADVANCE TO AND HOLD IN EMERGENCY VEHICLE PRE-EMPTION PHASE #1 (OR #2, #3) GREEN FOR A MINIMUM OF TEN (10) SECONDS OR UNTIL PRE-EMPTION SIGNAL CEASES. THE CONTROLLER SHALL THEN TIME PRE-EMPTION PHASE CLEARANCE (4 SECONDS: YELLOW AND 1 SECOND: ALL RED) AND SERVICE EMERGENCY VEHICLE PRE-EMPTION PHASE #2 (OR #1) IF NECESSARY, THEN TIME PHASE PRE-EMPTION CLEARANCE AND RESUME NORMAL SIGNAL OPERATION. EMERGENCY VEHICLE PRE-EMPTION PHASES #3 SHALL BE SIMILARLY SERVED.
5. MINIMUM GREEN & NORMAL VEHICLE CLEARANCE, SHALL BE PROVIDED ON PHASES THAT ARE TO BE TERMINATED BY PRE-EMPTION DEMAND.
6. EMERGENCY VEHICLE PRE-EMPTION SHALL OVERRIDE COORDINATION.

NO COORDINATION

PREFERENTIAL PHASE SEQUENCE



Rev. No. Date Description Made by Chk. by Appd. by

Pease Development Authority
 Portsmouth, New Hampshire

Pease International Tradeport
 Portsmouth, New Hampshire
 E.D.A. No. 01-49-03235

Pease Boulevard and International Drive Signalization Plan

Vanasse Hagen Brustlin, Inc.
 Engineers • Planners • Scientists Six Bedford Farms, Kilton Road
 Bedford, New Hampshire 03110 603 644 0888 • FAX 603 644 2305

Designed by: _____ Drawn by: _____ Checked by: _____

Scale: 1" = 20' Date: **March 10, 1994**

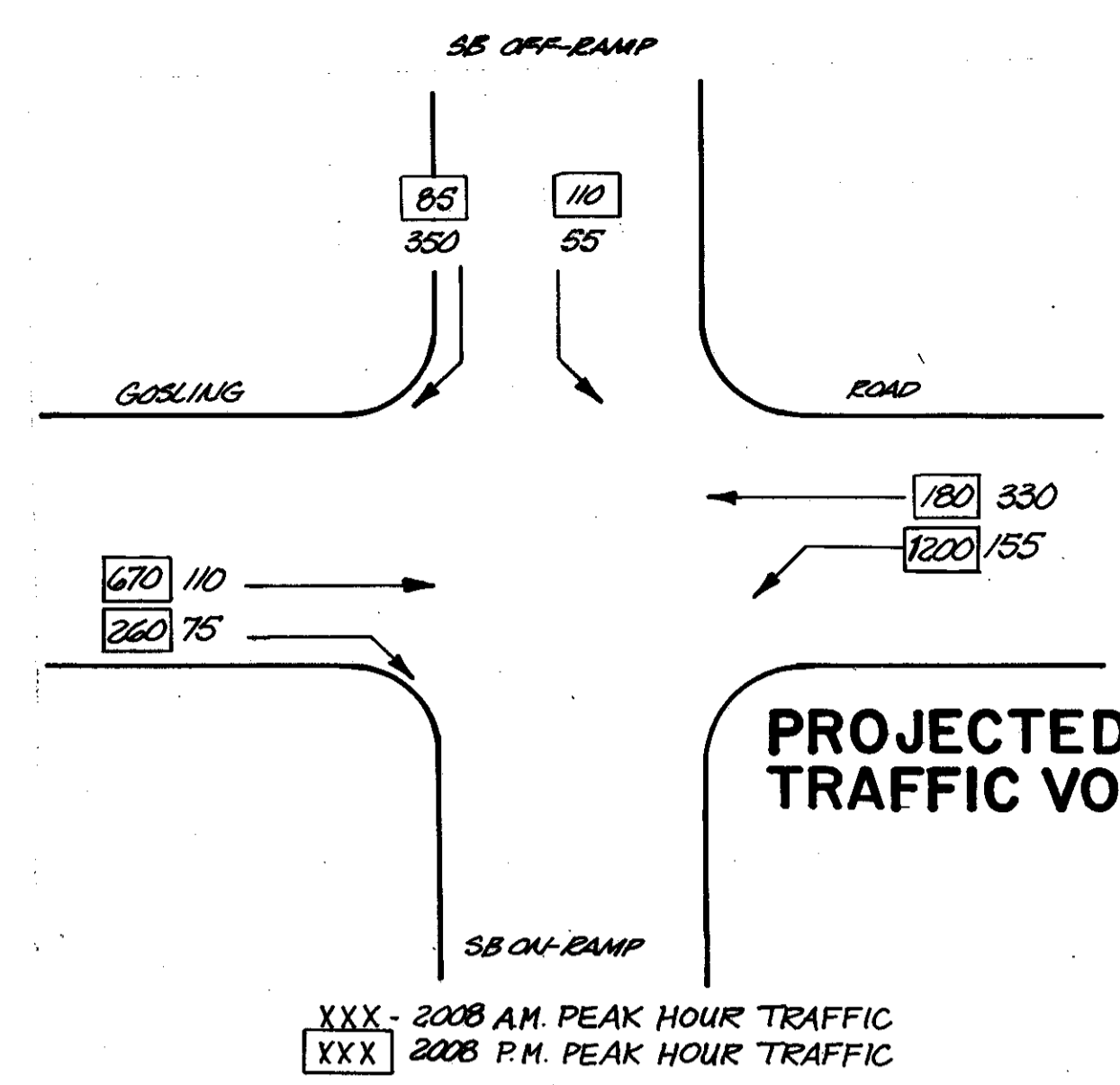
REVISIONS AFTER PROPOSAL

STATION	DATE	NUMBER	DESCRIPTION

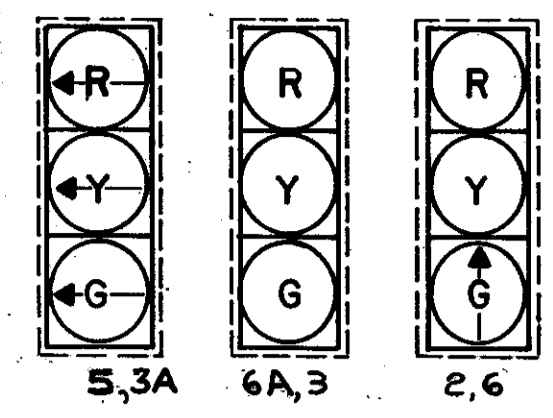
NOTEBOOKS

BOOK	PAGE	BOOK	PAGE

EXISTING DETAIL DATE 10-6-87
 PROPOSED DESIGN DATE 10-6-87
 SHEET CHECKED DATE 10-6-87
 AS BUILT DETAILS



SIGNAL HEADS
 12" LENSES
 5" (NOMINAL) BACKPLATES

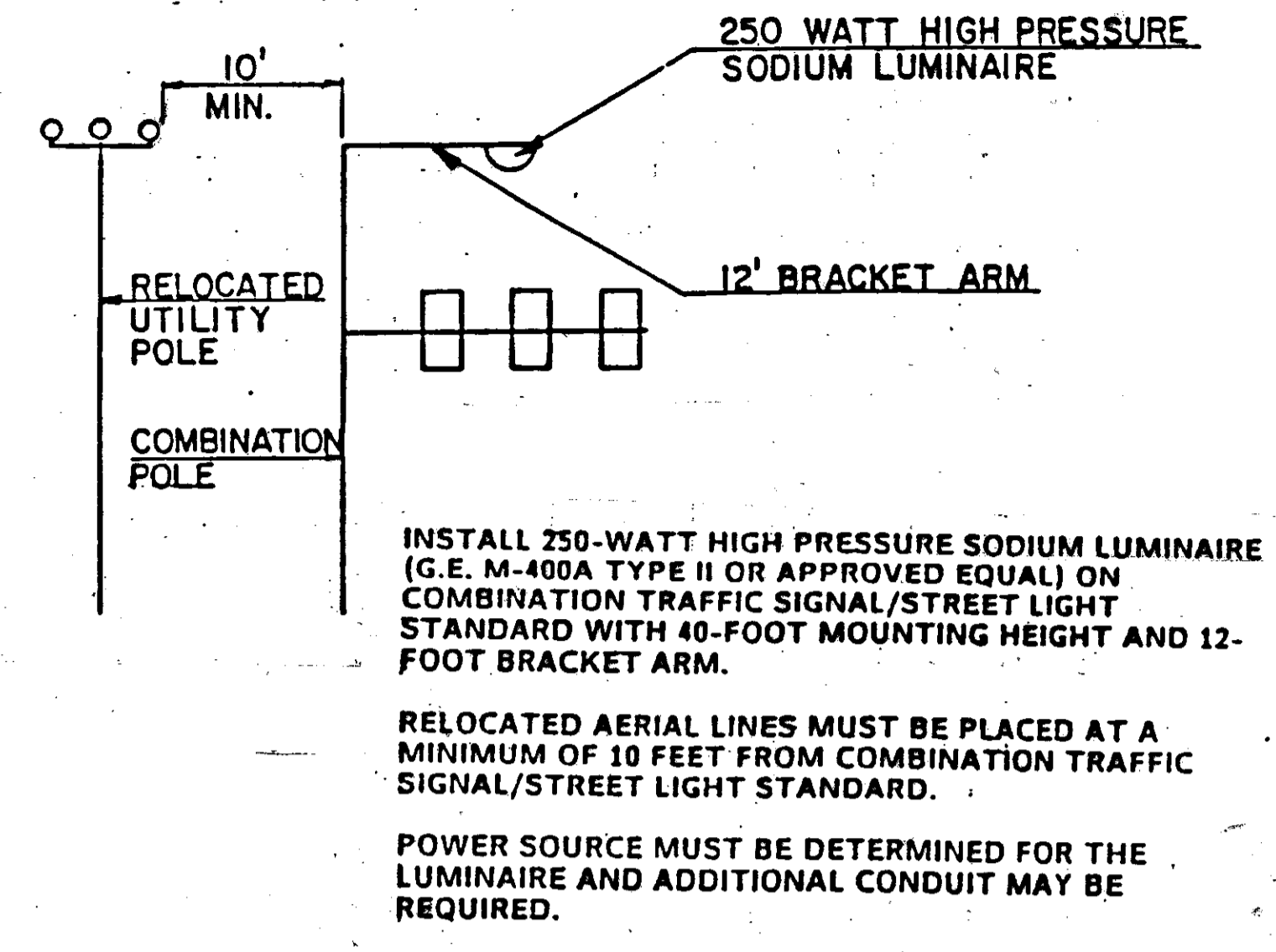


NO TURN ON RED ARROW
 TO BE PLACED ADJACENT TO LEFT TURN SIGNALS 3A, 1A, 5

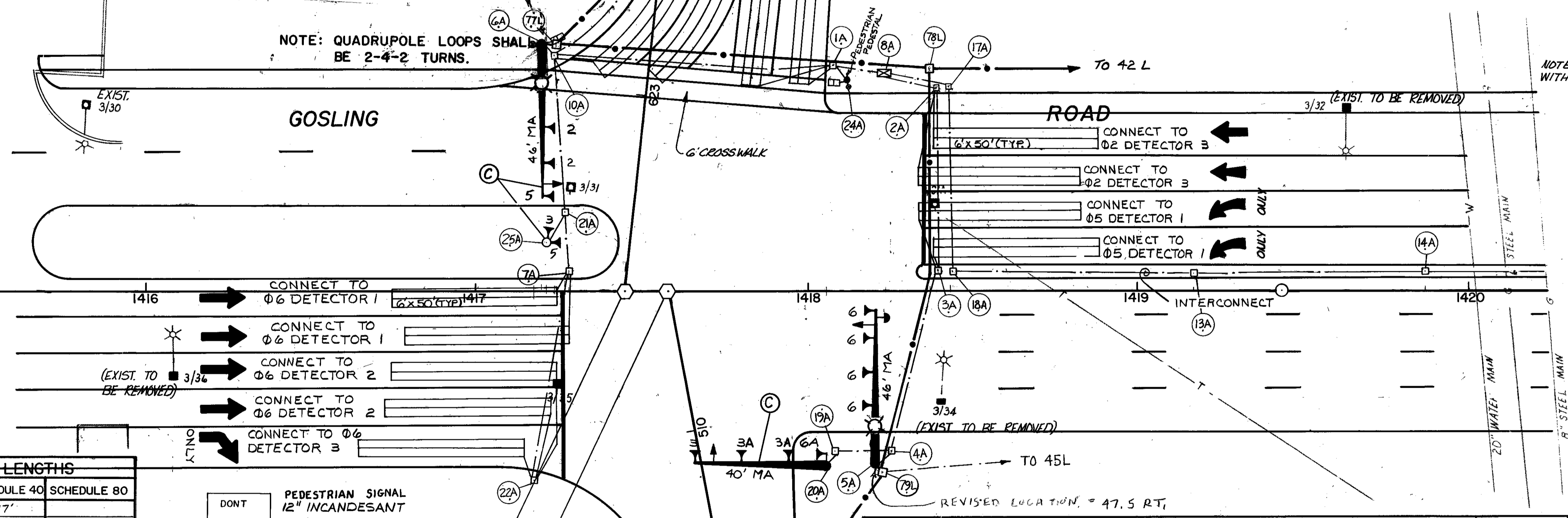
DETECTOR		AMPLIFIER		INDUCT	RESIST. OF LOOP	RESIST. COY/GND SHIELDING	RESIST. SHIELDING
STREET	DIRECTION	LANE	NO.	CHANNEL	μH	MEG. ~	MEG. ~
GOSLING RD.	SB RD.	LEFT TURN	1	1			
GOSLING RD.	W BD.	THRU	2	1			
GOSLING RD.	E BD.	THRU (2)	3	1			
SB OFF-RAMP	SB RD.	LEFT TURN	4	1			

RECORD FIELD MEASUREMENTS HERE

SCHEMATIC COMBINATION POLES

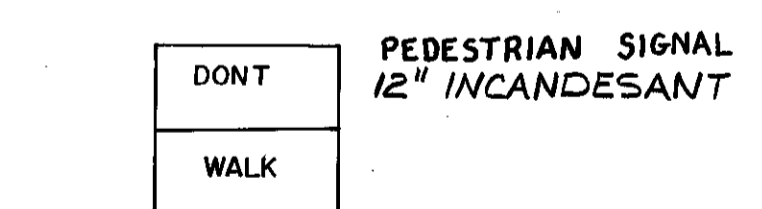


NOTE: QUADRUPOLE LOOPS SHALL BE 2-4-2 TURNS.



FOUNDATIONS			
FOUNDATION LOC. TYPE	STATION	OFFSET	NOTES
1A	PB	1418+08	6'8" LT
2A	PB	1418+39	6'2" LT
3A	PB	1418+39	6' LT
4A	PB	1418+25	48' RT
5A	MA	1418+20	56' RT
6A	SP	1417+20	75' LT
7A	PB	1417+28	6' LT
8A	CC	1418+24	66' LT
24A	SP	1418+12	64' LT
10A	PB	1417+24	72' RT
22A	PB	1417+18	57' RT
13A	PB	1419+17	5' LT
14A	PB	1419+87	5' LT
21A	PB	1417+27	24' LT
17A	PB	1418+43	62' LT
18A	PB	1418+43	6' LT
20A	SP	1418+05	53' RT
26A	PB	622+52	4' RT

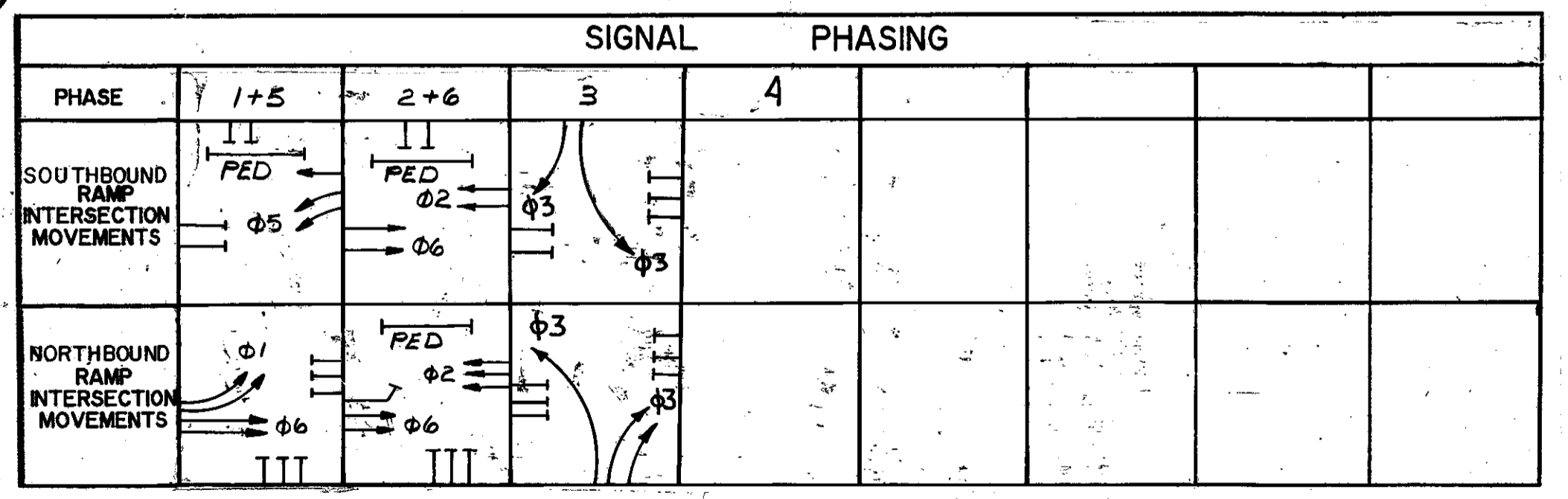
CONDUIT LENGTHS			
FROM	TO	SCHEDULE 40	SCHEDULE 80
1A	8A	17'	
2A	3A		55'
3A	4A		57'
4A	5A	5'	
10A	6A	5'	
10A	21A		48'
8A	2A	16'	
1A	24A	5'	
1A	10A		85'
17A	8A	20'	
17A	18A		56'
21A	7A	18'	
18A	13A	73'	
13A	14A	70'	
4A	19A	17'	
19A	20A	5'	
7A	22A		64'
10A	26A	48'	



POT. 623+59.43 SB OFF RAMP CONST. LINE =
 POT. 1417+45.26 GOS. RD. CONST. LINE

POT. 509+57.35 S.B. ON RAMP CONST. LINE =
 POT. 1417+58.33 GOS. RD. CONST. LINE

PUSH BUTTON FOR WALK SIGNAL
 R10-4
 9" x 12"



SIGNAL TIMING						
	φ 1	φ 2	φ 3	φ 5	φ 6	FLASH
EB GOSLING RD LEFT TURN	G	Y	R	R	R	R
WB GOSLING RD THRU'S	R	R	R	G	Y	R
SB OFF RAMP	R	R	R	R	R	R
WB GOSLING RD LEFT TURN	R	R	R	R	R	R
EB GOSLING RD THRU'S	R	R	R	R	R	R
MIN GREEN	15	8	8	5	8	
EXTENSION	4	5	5	4	5	
YELLOW	4	4	4	4	4	
RED	2	2	2	2	2	
MAX. I	25	35	25	25	35	
WALK	7	7				OUT
DON'T WALK	18	18				OUT

- KEY
- LIGHTING CONDUIT
 - SIGNAL CONDUIT
 - BOX OUT
 - ⊠ CONTROLLER CABINET
 - METER PEDESTAL
 - PEDESTRIAN SIGNAL
 - ⊠ 2 DUCT CONDUIT

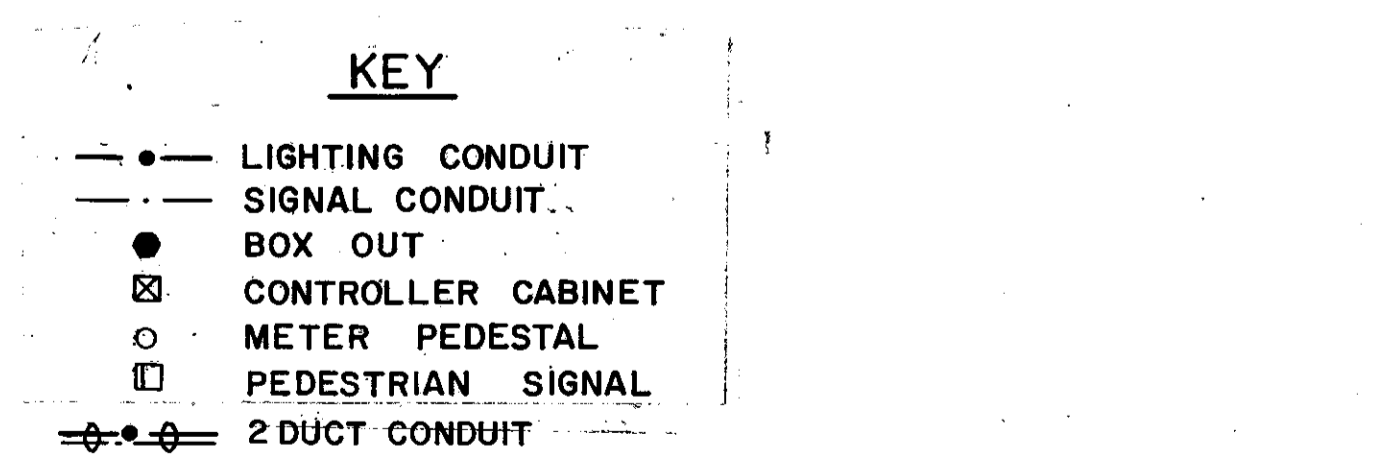
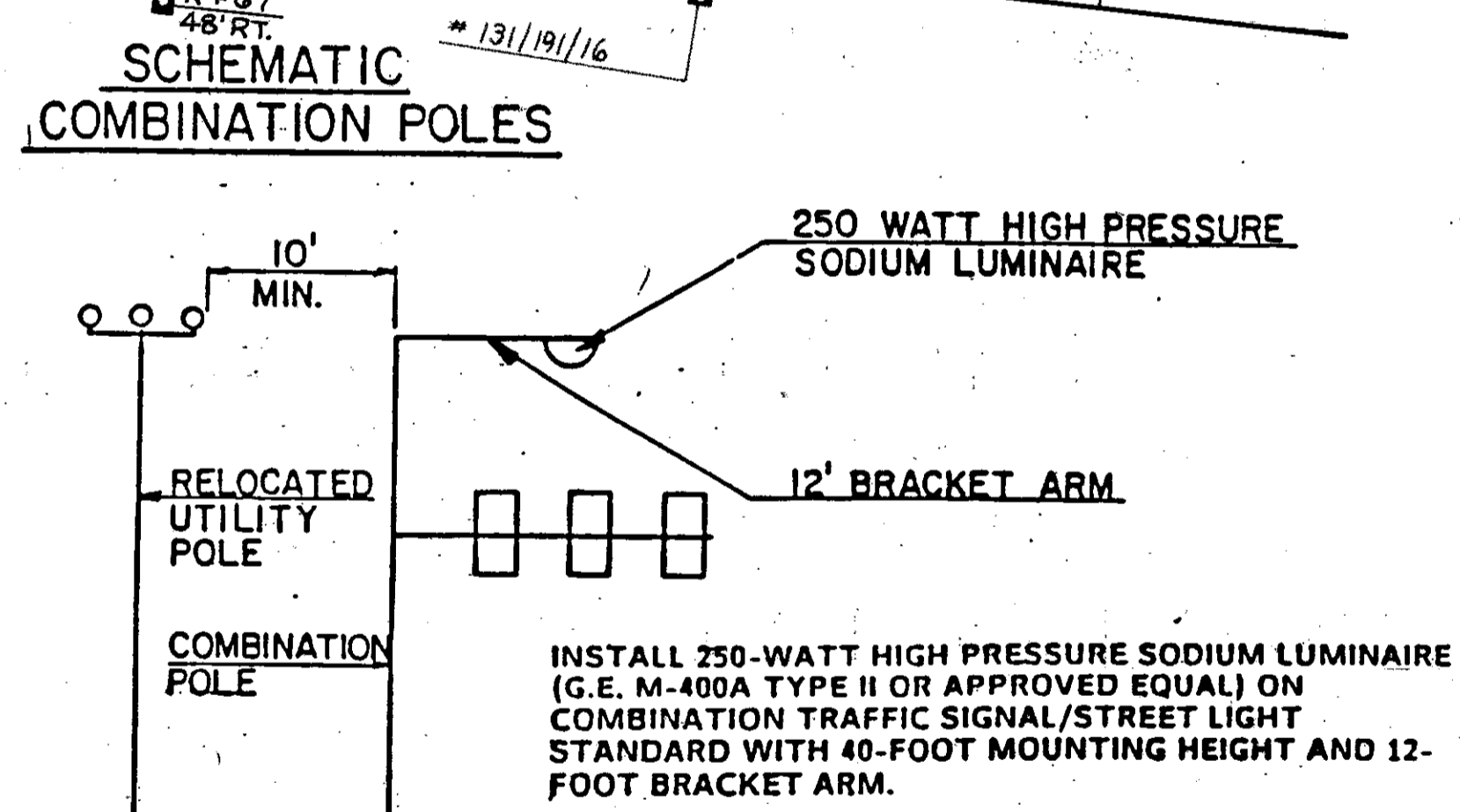
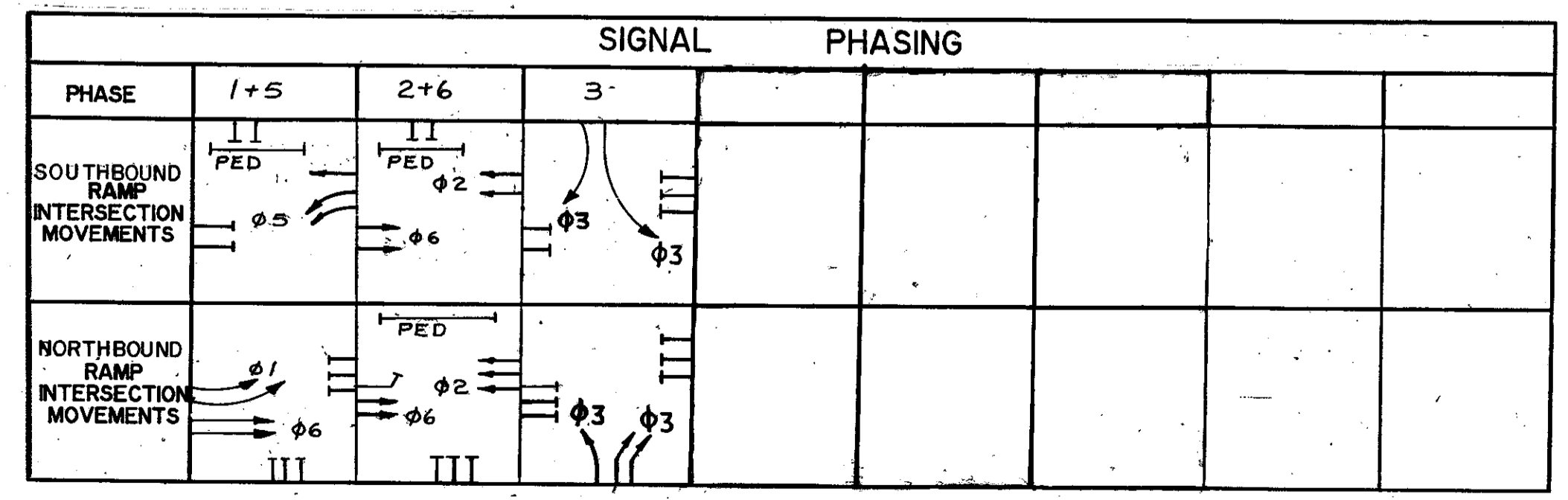
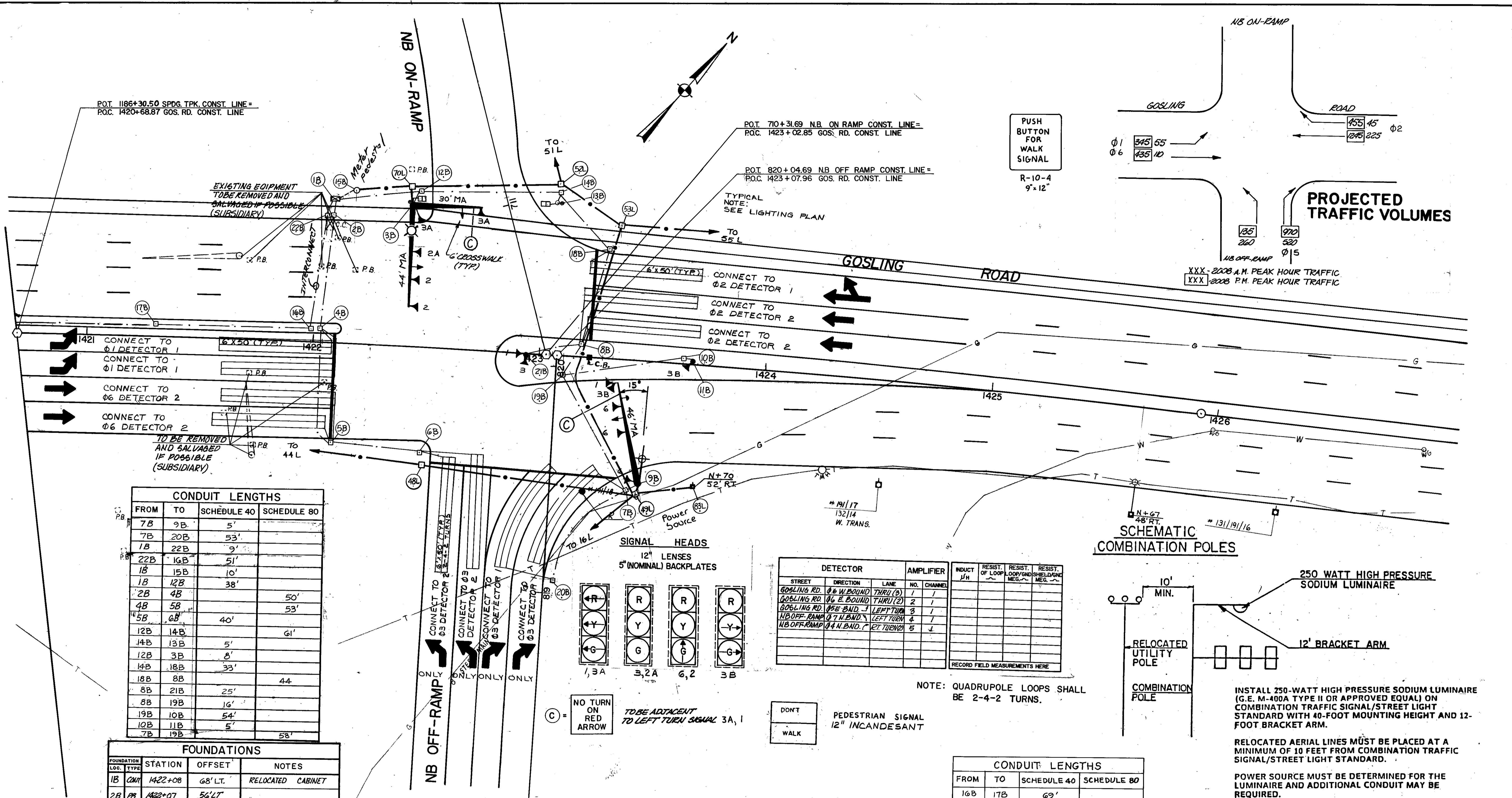
REVISIONS AFTER PROPOSAL

REVISIONS	DATE	DESCRIPTION

EXISTING DETAIL
 PROPOSED DESIGN
 SHEET CHECKED
 AS BUILT DETAILS

DATE 10-6-89
 DATE 10-6-89
 DATE 10-6-89
 DATE 10-6-89

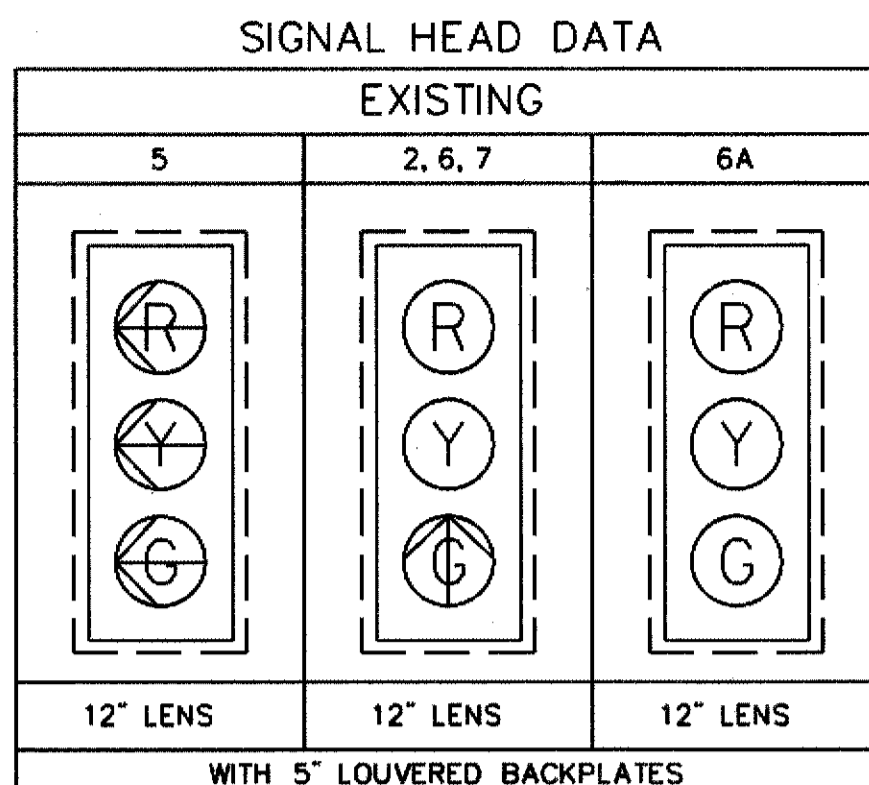
NOTEBOOKS
 BOOK PAGE
 BOOK PAGE
 BOOK PAGE



8 PHASE NEMA DUAL RING QUAD LEFT CONTROLLER

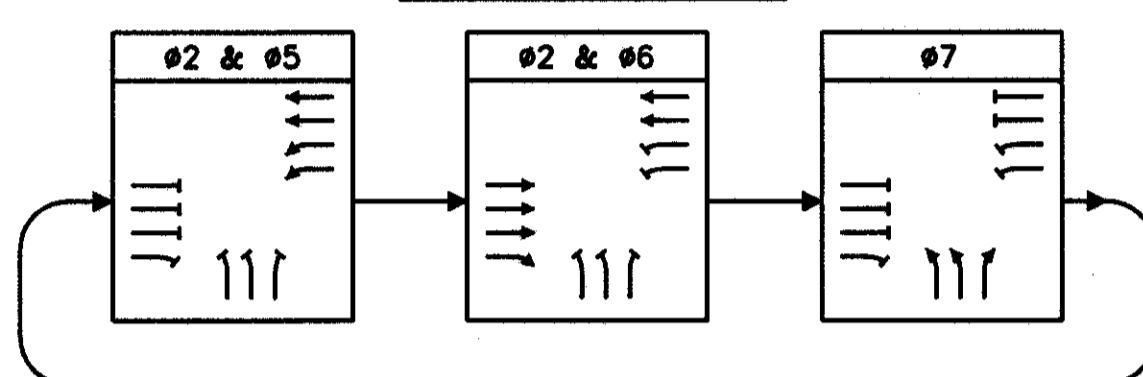
SIGNAL PHASING & TIMING								
	Ø1	Ø2	Ø3	Ø4	Ø5	Ø6	Ø7	Ø8
TIMING IN SECONDS	NOT USED	←	NOT USED	NOT USED	←	→	→	NOT USED
INITIAL INTERVAL	-	8	-	-	5	8	5	-
VEHICLE EXTENSION	-	4	-	-	4	4	4	-
MAXIMUM 1	-	30	-	-	20	30	25	-
MAXIMUM 2	-	30	-	-	20	30	25	-
YELLOW	-	4	-	-	4	4	4	-
ALL RED	-	2	-	-	2	2	2	-
PEDESTRIAN WALK	-	-	-	-	-	-	-	-
PEDESTRIAN CLEAR	-	-	-	-	-	-	-	-
FLASH	-	FY	-	-	FRA	FY	FR	-
RECALL	-	SOFT	-	-	OFF	SOFT	OFF	-
DETECTOR	-	NL	-	-	NL	NL	NL	-
PRE-EMPT PRIORITY	-	2	-	-	2	1	3	-

SYSTEM TO MAXIMUM 2 UNDER COORDINATION



NOTE: ALL SIGNAL HEADS ARE EQUIPPED WITH L.E.D. MODULES.

N.E.M.A. PHASE SEQUENCE



DETECTOR SCHEDULE						INDUCT UH	RESISTANCE OF LOOPS	RESIST. LOOP GRD. MEG.	RESIST. SHIELD GRD. MEG.
STREET	DIRECTION	LANE	Ø	NO.	CHANNEL				
NH ROUTE 33	EASTBOUND	THRU (MEDIAN)	6	1	1				
NH ROUTE 33	EASTBOUND	THRU (CEN-LEFT)	6	1	2				
NH ROUTE 33	EASTBOUND	THRU (CEN-RIGHT)	6	2	1				
NH ROUTE 33	EASTBOUND	RIGHT	6D	2	2				
NH ROUTE 33	EASTBOUND	THRU-BACK (MEDIAN)	6	3	1				
NH ROUTE 33	EASTBOUND	THRU-BACK (CEN-LEFT)	6	3	2				
NH ROUTE 33	EASTBOUND	THRU-BACK (CEN-RIGHT)	6	4	1				
NH ROUTE 33	EASTBOUND	THRU-DEPART (MEDIAN)	S5	10	1				
NH ROUTE 33	EASTBOUND	THRU-DEPART (CENTER)	S8	10	2				
NH ROUTE 33	EASTBOUND	THRU-DEPART (RIGHT)	S7	11	1				
NH ROUTE 33	WESTBOUND	LEFT (MEDIAN)	5	5	1				
NH ROUTE 33	WESTBOUND	LEFT (CEN-LEFT)	5	5	2				
NH ROUTE 33	WESTBOUND	THRU (CEN-RIGHT)	2	6	1				
NH ROUTE 33	WESTBOUND	THRU (RIGHT)	2	6	2				
NH ROUTE 33	WESTBOUND	THRU-BACK (CEN-RIGHT)	2	7	1				
NH ROUTE 33	WESTBOUND	THRU-BACK (CEN-LEFT)	2	7	2				
NH ROUTE 33	WESTBOUND	THRU-DEPART (LEFT)	S8	12	1				
NH ROUTE 33	WESTBOUND	THRU-DEPART (RIGHT)	S9	12	2				
I-95 SB RAMP	NORTHBOUND	LEFT (MEDIAN)	7	8	1				
I-95 SB RAMP	NORTHBOUND	LEFT (CENTER)	7	8	2				
I-95 SB RAMP	NORTHBOUND	RIGHT	7D	9	1				

S = SYSTEM LOOP
Ø6D & Ø7D SHALL BE PROGRAMMED WITH 5 SECOND DELAY

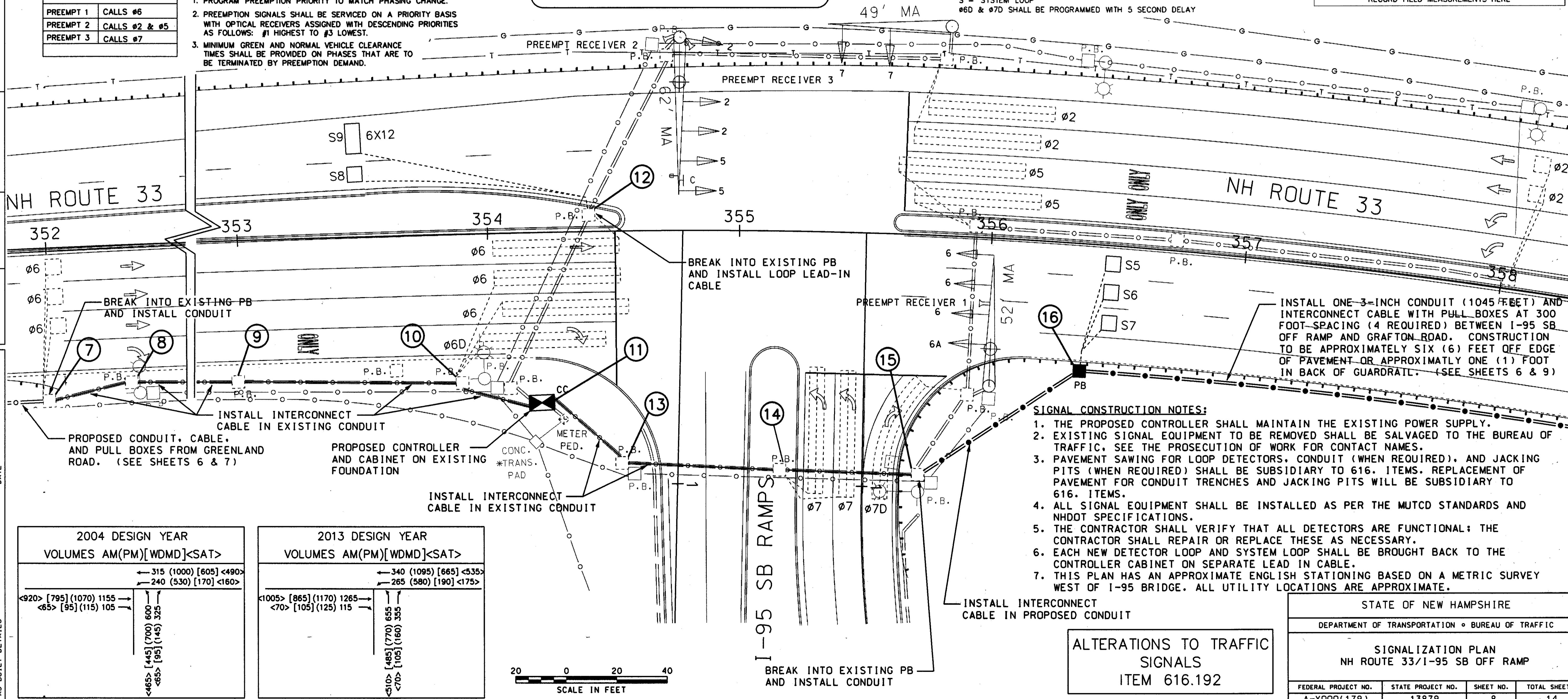
RECORD FIELD MEASUREMENTS HERE

FIRE PREEMPTION

PREEMPT 1	CALLS Ø6
PREEMPT 2	CALLS Ø2 & Ø5
PREEMPT 3	CALLS Ø7

FIRE PREEMPTION NOTES:

- PROGRAM PREEMPTION PRIORITY TO MATCH PHASING CHANGE.
- PREEMPTION SIGNALS SHALL BE SERVICED ON A PRIORITY BASIS WITH OPTICAL RECEIVERS ASSIGNED WITH DESCENDING PRIORITIES AS FOLLOWS: Ø1 HIGHEST TO Ø3 LOWEST.
- MINIMUM GREEN AND NORMAL VEHICLE CLEARANCE TIMES SHALL BE PROVIDED ON PHASES THAT ARE TO BE TERMINATED BY PREEMPTION DEMAND.



SIGNAL CONSTRUCTION NOTES:

- THE PROPOSED CONTROLLER SHALL MAINTAIN THE EXISTING POWER SUPPLY.
- EXISTING SIGNAL EQUIPMENT TO BE REMOVED SHALL BE SALVAGED TO THE BUREAU OF TRAFFIC. SEE THE PROSECUTION OF WORK FOR CONTACT NAMES.
- PAVEMENT SAWING FOR LOOP DETECTORS, CONDUIT (WHEN REQUIRED), AND JACKING PITS (WHEN REQUIRED) SHALL BE SUBSIDIARY TO 616. ITEMS. REPLACEMENT OF PAVEMENT FOR CONDUIT TRENCHES AND JACKING PITS WILL BE SUBSIDIARY TO 616. ITEMS.
- ALL SIGNAL EQUIPMENT SHALL BE INSTALLED AS PER THE MUTCD STANDARDS AND NHDOT SPECIFICATIONS.
- THE CONTRACTOR SHALL VERIFY THAT ALL DETECTORS ARE FUNCTIONAL; THE CONTRACTOR SHALL REPAIR OR REPLACE THESE AS NECESSARY.
- EACH NEW DETECTOR LOOP AND SYSTEM LOOP SHALL BE BROUGHT BACK TO THE CONTROLLER CABINET ON SEPARATE LEAD IN CABLE.
- THIS PLAN HAS AN APPROXIMATE ENGLISH STATIONING BASED ON A METRIC SURVEY WEST OF I-95 BRIDGE. ALL UTILITY LOCATIONS ARE APPROXIMATE.

2004 DESIGN YEAR
VOLUMES AM(PM)[WDM]<SAT>

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← 240 (530) [170] <160>
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2013 DESIGN YEAR
VOLUMES AM(PM)[WDM]<SAT>

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ALTERATIONS TO TRAFFIC SIGNALS
ITEM 616.192

STATE OF NEW HAMPSHIRE			
DEPARTMENT OF TRANSPORTATION • BUREAU OF TRAFFIC			
SIGNALIZATION PLAN			
NH ROUTE 33/I-95 SB OFF RAMP			
FEDERAL PROJECT NO.	STATE PROJECT NO.	SHEET NO.	TOTAL SHEETS
A-X000(179)	13879	8	14

SDR PROCESSED CMB
NEW DESIGN DJD
SHEET CHECKED CMB
AS BUILT DETAILS

DATE 7/7/03
DATE 8/11/03
DATE 8/21/03
DATE

REVISIONS AFTER PROPOSAL

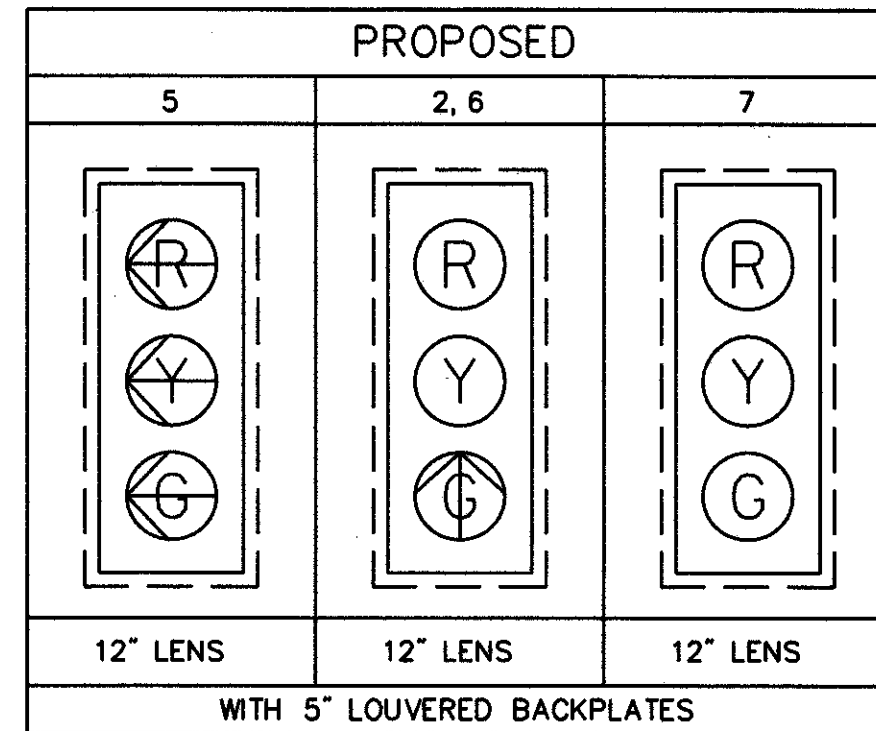
STATION

STATION

DATE

NUMBER

SIGNAL HEAD DATA



NOTE: ALL SIGNAL HEADS SHALL BE EQUIPPED WITH NEW L.E.D. MODULES.

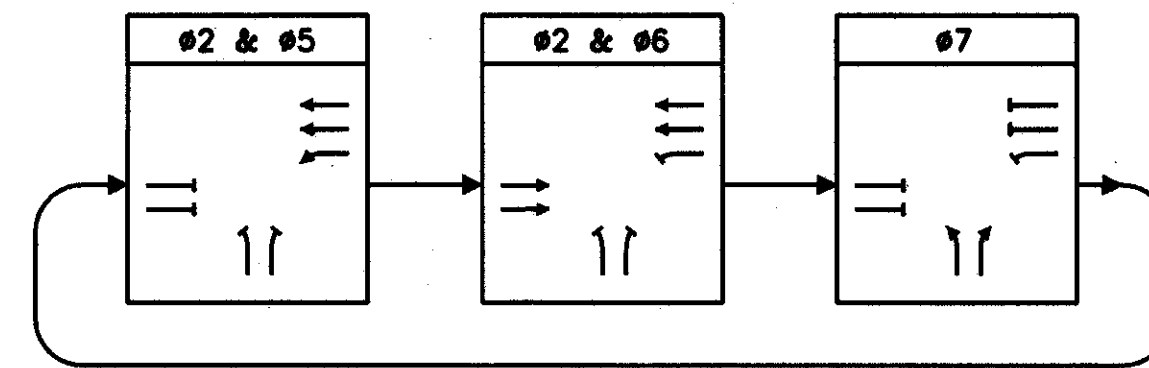
FIRE PREEMPTION

PREEMPT 1	CALLS #6
PREEMPT 2	CALLS #2 & #5
PREEMPT 3	CALLS #7

FIRE PREEMPTION NOTES:

- PREEMPTION SIGNALS SHALL BE SERVICED ON A PRIORITY BASIS WITH OPTICAL RECEIVERS ASSIGNED WITH DESCENDING PRIORITIES AS FOLLOWS: #1 HIGHEST TO #3 LOWEST.
- MINIMUM GREEN AND NORMAL VEHICLE CLEARANCE TIMES SHALL BE PROVIDED ON PHASES THAT ARE TO BE TERMINATED BY PREEMPTION DEMAND.

N.E.M.A. PHASE SEQUENCE



DETECTOR SCHEDULE

STREET	DIRECTION	LANE	Ø	AMPLIFIER		INDUCT UH	RESISTANCE OF LOOPS	RESIST. LOOP GRD. MEG.	RESIST. SHIELD GRD. MEG.
				NO.	CHANNEL				
NH ROUTE 33	EASTBOUND	THRU (LEFT)	6*	*	*				
NH ROUTE 33	EASTBOUND	THRU (RIGHT)	6*	*	*				
NH ROUTE 33	EASTBOUND	THRU-DEPART (LEFT)	S14	3	1				
NH ROUTE 33	EASTBOUND	THRU-DEPART (RIGHT)	S15	3	2				
NH ROUTE 33	WESTBOUND	LEFT (2)	5	1	1				
NH ROUTE 33	WESTBOUND	THRU (CENTER)	2*	*	*				
NH ROUTE 33	WESTBOUND	THRU (RIGHT)	2*	*	*				
NH ROUTE 33	WESTBOUND	THRU-DEPART (LEFT)	S16	4	1				
NH ROUTE 33	WESTBOUND	THRU-DEPART (RIGHT)	S17	4	2				
I-95 OFF RAMP	NORTHBOUND	LEFT	7	2	1				
I-95 OFF RAMP	NORTHBOUND	RIGHT	7D	2	2				

* = MAGNETIC DETECTOR (USE EXISTING AMPLIFIERS)

S = SYSTEM LOOP

Ø7D SHALL BE PROGRAMMED WITH A 5 SECOND DELAY

RECORD FIELD MEASUREMENTS HERE

DESCRIPTION

REVISIONS AFTER PROPOSAL

STATION

DATE

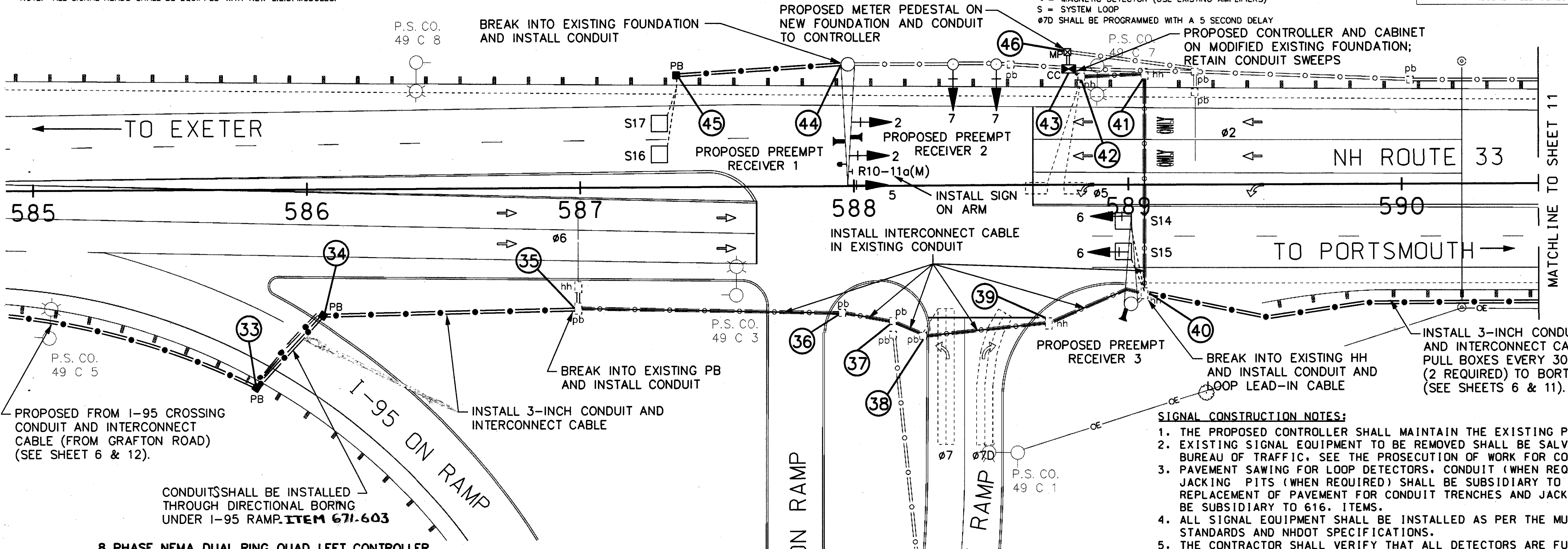
NUMBER

DATE

DATE

DATE

DATE



PROPOSED FROM I-95 CROSSING CONDUIT AND INTERCONNECT CABLE (FROM GRAFTON ROAD) (SEE SHEET 6 & 12).

CONDUITS SHALL BE INSTALLED THROUGH DIRECTIONAL BORING UNDER I-95 RAMP. ITEM 671.603

8 PHASE NEMA DUAL RING QUAD LEFT CONTROLLER

SIGNAL PHASING & TIMING

TIMING IN SECONDS	#1	#2	#3	#4	#5	#6	#7	#8
	NOT USED	←→	NOT USED	NOT USED	←→	←→	↑↑	NOT USED
INITIAL INTERVAL	-	10	-	-	5	10	8	-
VEHICLE EXTENSION	-	4	-	-	4	4	4	-
MAXIMUM 1	-	25	-	-	40	25	50	-
MAXIMUM 2	-	40	-	-	40	40	40	-
YELLOW	-	4	-	-	4	4	4	-
ALL RED	-	2	-	-	2	2	2	-
PEDESTRIAN WALK	-	-	-	-	-	-	-	-
PEDESTRIAN CLEAR	-	-	-	-	-	-	-	-
FLASH	-	FY	-	-	FRA	FY	FR	-
RECALL	-	SOFT	-	-	OFF	SOFT	OFF	-
DETECTOR	-	LOCK	-	-	NL	LOCK	NL	-
PRE-EMPT PRIORITY	-	2	-	-	2	1	3	-

#4 & #8 DUAL ENTRY SYSTEM TO MAXIMUM 2 UNDER COORDINATION

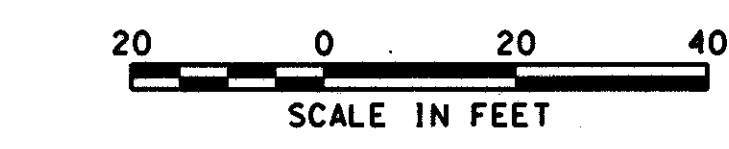
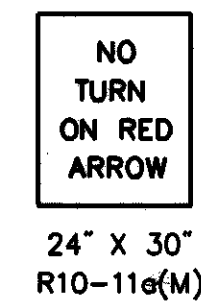
2004 DESIGN YEAR
VOLUMES AM(PM)[WDM]<SAT>

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2013 DESIGN YEAR
VOLUMES AM(PM)[WDM]<SAT>

<430> [565] (770) 760	<540> [420] (815) 535
← 600 (920) [595] <495>	← 65 (430) [145] <135>
<85> [125] (165) 275	<170> [145] (460) 475

PROPOSED SIGN



- SIGNAL CONSTRUCTION NOTES:**
- THE PROPOSED CONTROLLER SHALL MAINTAIN THE EXISTING POWER SUPPLY.
 - EXISTING SIGNAL EQUIPMENT TO BE REMOVED SHALL BE SALVAGED TO THE BUREAU OF TRAFFIC. SEE THE PROSECUTION OF WORK FOR CONTACT NAMES.
 - PAVEMENT SAWING FOR LOOP DETECTORS, CONDUIT (WHEN REQUIRED), AND JACKING PITS (WHEN REQUIRED) SHALL BE SUBSIDIARY TO 616. ITEMS. REPLACEMENT OF PAVEMENT FOR CONDUIT TRENCHES AND JACKING PITS WILL BE SUBSIDIARY TO 616. ITEMS.
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 - THE CONTRACTOR SHALL VERIFY THAT ALL DETECTORS ARE FUNCTIONAL; THE CONTRACTOR SHALL REPAIR OR REPLACE THESE AS NECESSARY.
 - EACH NEW DETECTOR LOOP AND SYSTEM LOOP SHALL BE BROUGHT BACK TO THE CONTROLLER CABINET ON SEPARATE LEAD IN CABLE.
 - INSTALL SIGN R10-11a(M) ADJACENT TO SIGNAL HEAD 5.
 - THE EXISTING MAGNETIC DETECTION AMPLIFIERS SHALL BE REUSED IN THE NEW CONTROLLER.
 - MODIFY THE EXISTING CONTROLLER CABINET FOUNDATION TO ACCOMMODATE THE NEW P-TYPE CABINET WITH TELEMETRY HARNESS AND PANEL, WITH A 12-INCH EXTENSION BASE.
 - THIS PLAN INCLUDED A BASELINE FROM NHDOT PLANS PREPARED IN 1982. THIS BASELINE EXTENDS EAST FROM THE I-95 BRIDGE. THE LOCATIONS OF UTILITIES ARE APPROXIMATE.

ALTERATIONS TO TRAFFIC SIGNALS
ITEM 616.194

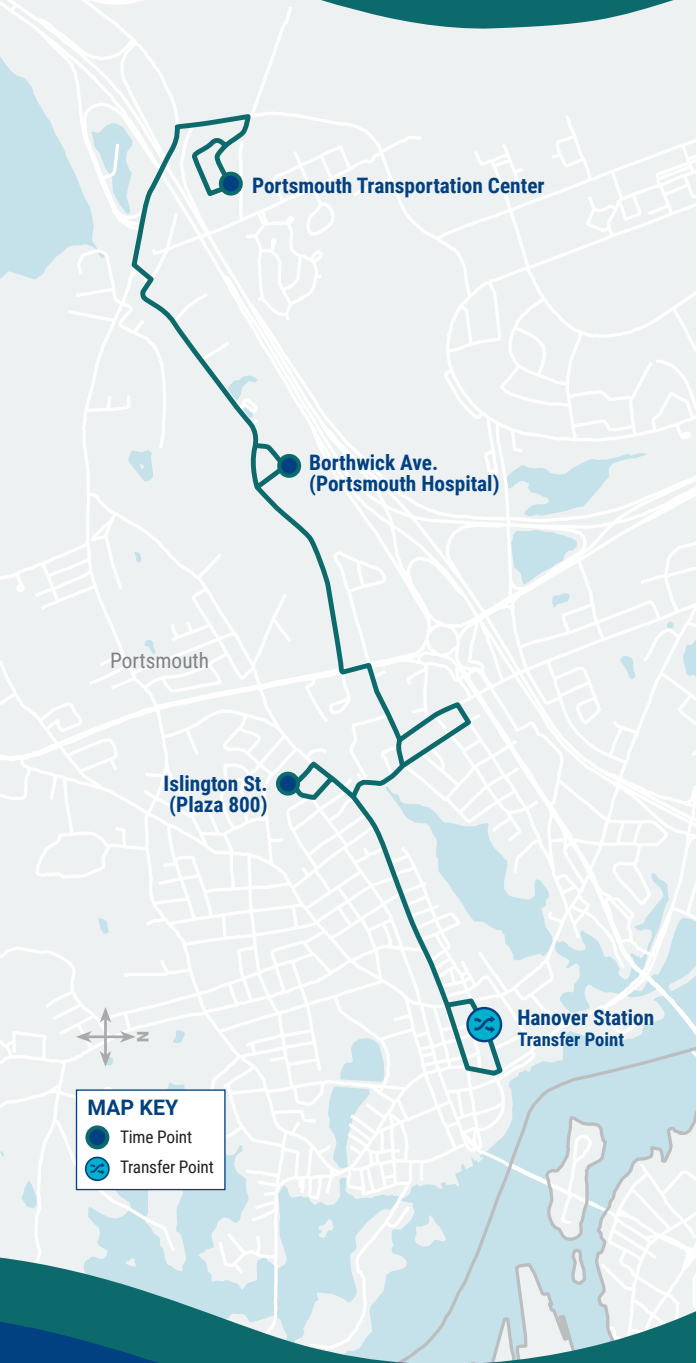
STATE OF NEW HAMPSHIRE			
DEPARTMENT OF TRANSPORTATION • BUREAU OF TRAFFIC			
SIGNALIZATION PLAN NH ROUTE 33/I-95 NB OFF RAMP			
FEDERAL PROJECT NO.	STATE PROJECT NO.	SHEET NO.	TOTAL SHEETS
A-X000(179)	13879	10	14

APPENDIX K
COAST Bus Schedule & Map

40

Route 40 Map

Portsmouth Islington Borthwick



Ride Information

COAST BUS FARES

Base Cash Fare **\$1.50**
All passengers ages 5 and up are required to pay this fare each time they board a COAST bus.

Half-Fare **\$ 0.75**
Passengers 65 and older, or passengers with a disability are entitled to pay half the cash fare. Proof of eligibility is required by showing a Medicare card, photo ID with birth date, COAST ADA Paratransit Card, or COAST Half-Fare Card. Please contact COAST to apply for a Half-Fare Card.

Multi-Ride Tickets and Passes
Available at www.coastbus.org or call 603-743-5777, TTY 711.

Unlimited Monthly Pass **\$ 52**
Unlimited rides on COAST Routes for the month.

YOUR RIGHTS

COAST adheres to all Federal regulations regarding Civil Rights. If you need to request an ADA Reasonable Modification/ Accommodation, or if you believe you have been discriminated against or would like to file a complaint under the ADA or Title VI, please contact COAST's Civil Rights Officer at 603-516-0788, TTY 711 or email CivilRights@coastbus.org.

NO SERVICE DAYS

COAST does not operate on the following holidays:

- New Year's Day
- Martin Luther King Jr./ Civil Rights Day
- Memorial Day
- Independence Day
- Labor Day
- Thanksgiving Day
- Christmas Eve Day
- Christmas Day



42 Sumner Drive • Dover, NH 03820
 603-743-5777 • TTY 711 • www.coastbus.org

This brochure is available in alternative formats upon request.

Bus Schedule & Map 40



Effective
09.17.22

ROUTE
40

Portsmouth Islington Borthwick



Find all of the full COAST schedules online at coastbus.org

MAP OUT YOUR GAME PLAN

Planning your trip has never been easier!

www.coastbus.org



COAST SYSTEM MAP



OUTBOUND • INBOUND

Route 40

Portsmouth • Islington • Borthwick

How to Read the Schedule

Printed bus schedules only show the timepoints ● (major bus stops where the bus will hold until the scheduled departure time). In between those timepoints are many other stops that you can use. For a full listing of bus stops, visit www.coastbus.org, or use the Passio GO! App.

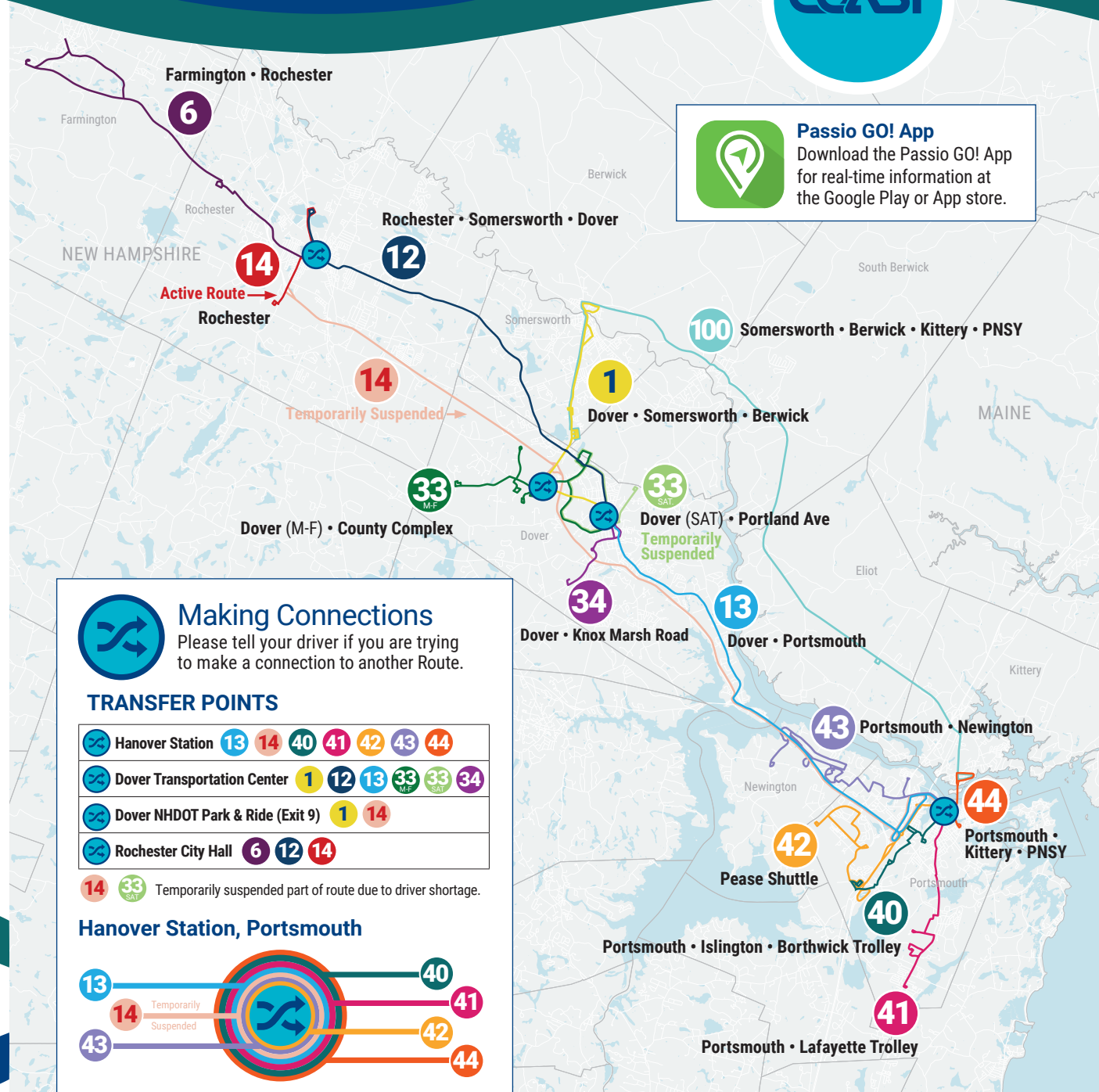
The times shown represent the number of minutes after the hour that the bus will depart from that stop. Last stop times are arrivals. Any exceptions will be noted.

OUTBOUND (M-Sat)	Service On Every Hour		
Hanover Station - Portsmouth Transportation Center	First Bus	Minutes Past Hour	Last Bus
● Hanover Station	6:00am	:00*	7:00pm
● Islington St. (Plaza 800)	6:07am	:07*	7:07pm
● Borthwick Ave. (Ports. Hospital)	6:15am	:15*	7:15pm
● Portsmouth Transportation Center	6:23am	:23*	7:23pm

*No Service during the hour of 3pm.

INBOUND (M-Sat)	Service On Every Hour		
Portsmouth Transportation Center - Hanover Station	First Bus	Minutes Past Hour	Last Bus
● Portsmouth Transportation Center	6:24am	:24*	7:24pm
● Borthwick Ave. (Ports. Hospital)	6:31am	:31*	7:31pm
● Islington St. (Plaza 800)	6:39am	:39*	7:39pm
● Hanover Station	6:47am	:47*	7:47pm

*No Service during the hour of 3pm.



Passio GO! App
 Download the Passio GO! App for real-time information at the Google Play or App store.



Making Connections

Please tell your driver if you are trying to make a connection to another Route.

TRANSFER POINTS

☞ Hanover Station	13	14	40	41	42	43	44
☞ Dover Transportation Center	1	12	13	33 _{M-F}	33 _{SAT}	34	
☞ Dover NHDOT Park & Ride (Exit 9)	1	14					
☞ Rochester City Hall	6	12	14				

14 33_{SAT} Temporarily suspended part of route due to driver shortage.

Hanover Station, Portsmouth

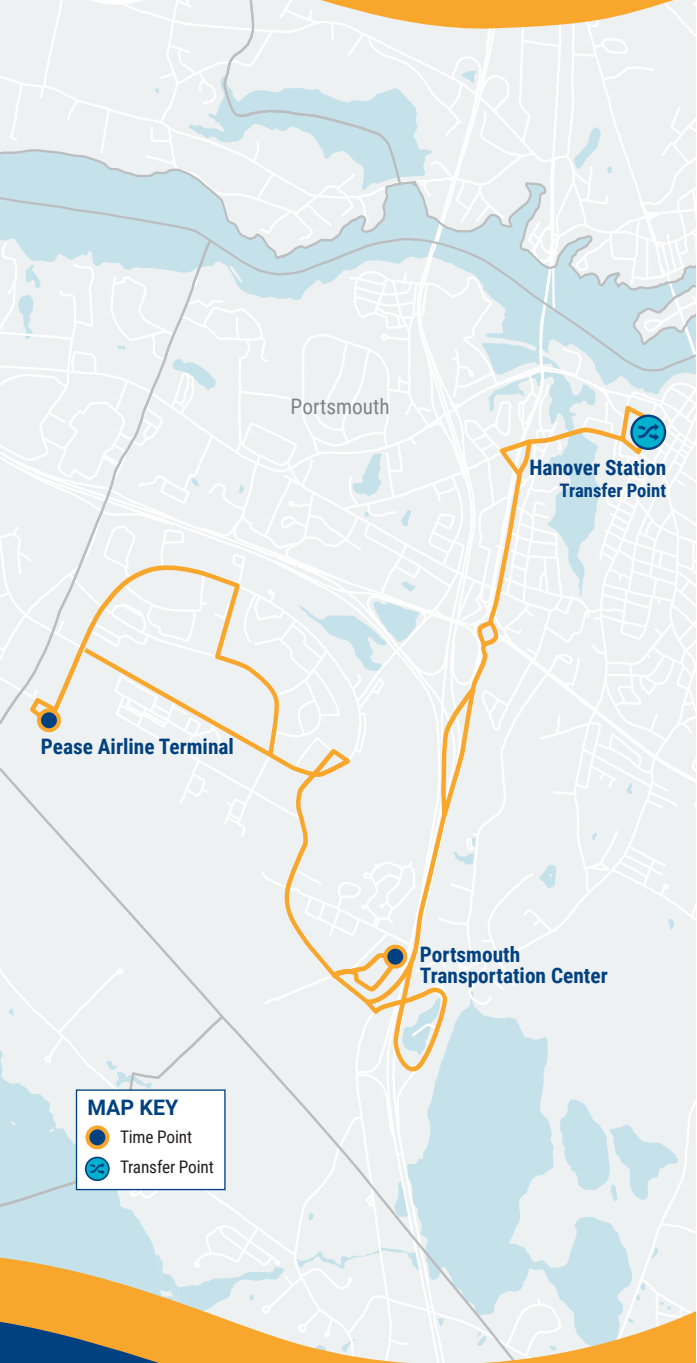


MAP IT!

For a full listing of bus stops, visit www.coastbus.org or use the Passio GO! App.

42

Route 42 Map Portsmouth • Pease Shuttle



Ride Information

COAST BUS FARES

Base Cash Fare **\$1.50**
All passengers ages 5 and up are required to pay this fare each time they board a COAST bus.

Half-Fare **\$ 0.75**
Passengers 65 and older, or passengers with a disability are entitled to pay half the cash fare. Proof of eligibility is required by showing a Medicare card, photo ID with birth date, COAST ADA Paratransit Card, or COAST Half-Fare Card. Please contact COAST to apply for a Half-Fare Card.

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COAST does not operate on the following holidays:

- New Year's Day
- Martin Luther King Jr./ Civil Rights Day
- Memorial Day
- Independence Day
- Labor Day
- Thanksgiving Day
- Christmas Eve Day
- Christmas Day



42 Sumner Drive • Dover, NH 03820
 603-743-5777 • TTY 711 • www.coastbus.org
This brochure is available in alternative formats upon request.

Bus Schedule & Map 42



Effective
07.01.22

ROUTE
42

Portsmouth • Pease Shuttle



Find all of the full COAST schedules online at coastbus.org

MAP OUT YOUR GAME PLAN

Planning your trip has never been easier!

www.coastbus.org



COAST SYSTEM MAP



OUTBOUND • INBOUND

Route 42 Portsmouth • Pease Shuttle

How to Read the Schedule

Printed bus schedules only show the timepoints (major bus stops where the bus will hold until the scheduled departure time). In between those timepoints are many other stops that you can use. For a full listing of bus stops, visit www.coastbus.org, or use the Passio Go! App.

The times shown represent the number of minutes after the hour that the bus will depart from that stop. Last stop times are arrivals. Any exceptions will be noted.

OUTBOUND (M-F)	Service On Every Hour		
Hanover Station - Pease Airline Terminal	First Bus	Minutes Past Hour	Last Bus
Hanover Station	6:22am	:00*	6:00pm
Portsmouth Transportation Center	6:33am	:11*	6:11pm
Pease Airline Terminal	6:42am	:20*	6:20pm

**Regular hourly schedule starts during the hour of 7am and No Service during the hour of 10am.*

INBOUND (M-F)	Service On Every Hour		
Pease Airline Terminal - Hanover Station	First Bus	Minutes Past Hour	Last Bus
Pease Airline Terminal	6:43am	:21*	6:21pm
Portsmouth Transportation Center	6:47am	:25*	6:25pm
Hanover Station	6:57am	:35*	6:35pm

**Regular hourly schedule starts during the hour of 7am and No Service during the hour of 10am.*



MAP IT!

For a full listing of bus stops, visit www.coastbus.org or use the Passio GO! App.



APPENDIX L

Lonza Employee Residential Zip Code
Based Trip Distribution Analysis

LONZA BIOLOGICS
EMPLOYEE RESIDENTIAL ZIP CODE BASED TRIP DISTRIBUTION ANALYSIS

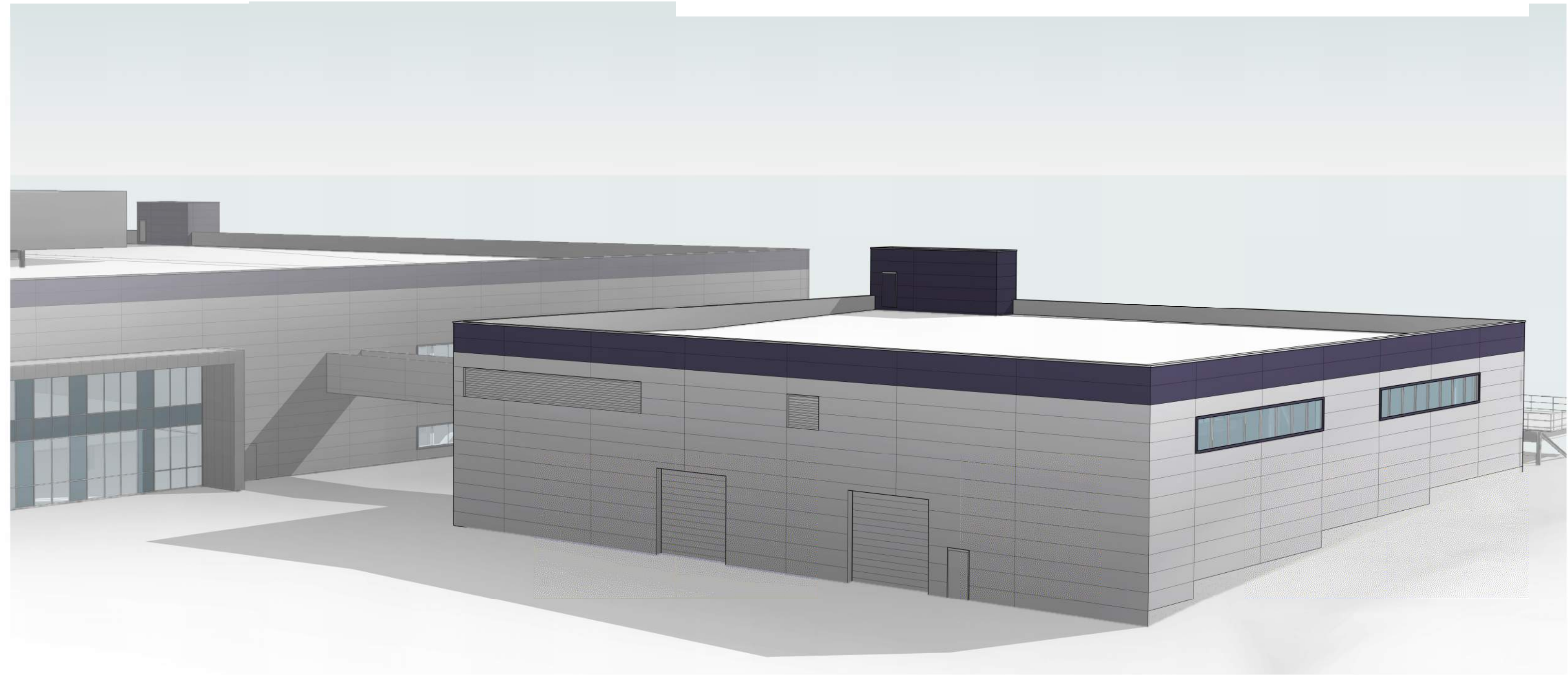
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1	1010.00	Brimfield	MA	1	0.010514			100.00%							OK									
2	1451.00	Harvard	MA	1	0.006399			100.00%							OK									
3	1507.00	Charlton	MA	1	0.012443			100.00%							OK									
4	1522.00	Jefferson	MA	1	0.00476			100.00%							OK									
5	1581.00	Westborough	MA	1	0.005997			100.00%							OK									
6	1730.00	Bedford	MA	2	0.003859			100.00%							OK									
7	1772.00	Southborough	MA	1	0.004393			100.00%							OK									
8	1801.00	Woburn	MA	1	0.00367			100.00%							OK									
9	1810.00	Andover	MA	2	0.009116			100.00%							OK									
10	1826.00	Dracut	MA	2	0.006115			100.00%							OK									
11	1830.00	Haverhill	MA	6	0.004248			100.00%							OK									
12	1832.00	Haverhill	MA	2	0.003408			100.00%							OK									
13	1833.00	Georgetown	MA	1	0.003762			100.00%							OK									
14	1835.00	Haverhill	MA	1	0.002461			100.00%							OK									
15	1844.00	Methuen	MA	10	0.006546			100.00%							OK									
16	1845.00	North Andover	MA	2	0.007855			100.00%							OK									
17	1852.00	Lowell	MA	1	0.001495			100.00%							OK									
18	1854.00	Lowell	MA	2	0.001247			100.00%							OK									
19	1860.00	Merrimac	MA	2	0.002536			100.00%							OK									
20	1876.00	Tewksbury	MA	2	0.006037			100.00%							OK									
21	1880.00	Wakefield	MA	1	0.00226			100.00%							OK									
22	1886.00	Westford	MA	1	0.008731			100.00%							OK									
23	1907.00	Swampscott	MA	1	0.00085			100.00%							OK									
24	1913.00	Amesbury	MA	5	0.003893			100.00%							OK									
25	1915.00	Beverly	MA	1	0.00446			100.00%							OK									
26	1921.00	Boxford	MA	2	0.006996			100.00%							OK									
27	1938.00	Ipswich	MA	1	0.009451			100.00%							OK									
28	1950.00	Newburyport	MA	7	0.003159			100.00%							OK									
29	1951.00	Newburyport	MA	2	0.005088			100.00%							OK									
30	1952.00	Salisbury	MA	3	0.004937			100.00%							OK									
31	1960.00	Peabody	MA	1	0.004791			100.00%							OK									
32	1970.00	Salem	MA	1	0.002453			100.00%							OK									
33	1985.00	West Newbury	MA	1	0.004183			100.00%							OK									
34	2127.00	Boston	MA	1	0.000853			100.00%							OK									
35	2145.00	Somerville	MA	1	0.000407			100.00%							OK									
36	2176.00	Melrose	MA	1	0.001348			100.00%							OK									
37	2180.00	Stoneham	MA	1	0.001849			100.00%							OK									
38	2461.00	Newton Highlands	MA	1	0.000427			100.00%							OK									
39	2472.00	Watertown	MA	3	0.001181			100.00%							OK									
40	2492.00	Needham	MA	1	0.00267			100.00%							OK									
41	3031.00	Amherst	NH	5	0.010143			100.00%							OK									
42	3032.00	Auburn	NH	1	0.008167			100.00%							OK									
43	3034.00	Candia	NH	3	0.01063			100.00%							OK									
44	3037.00	Deerfield	NH	4	0.014317			100.00%							OK									
45	3038.00	Derry	NH	8	0.010857			100.00%							OK									
46	3042.00	Epping	NH	11	0.007973		50.00%						50.00%		OK	5.5	0	0	0	0	0	5.5	0	
47	3044.00	Fremont	NH	4	0.004945		50.00%		50.00%						OK	2	0	2	0	0	0	0	0	
48	3045.00	Goffstown	NH	2	0.010311		100.00%								OK	2	0	0	0	0	0	0	0	
49	3047.00	Greenfield	NH	1	0.008001		100.00%								OK	1	0	0	0	0	0	0	0	
50	3051.00	Hudson	NH	1	0.008357		100.00%								OK	1	0	0	0	0	0	0	0	
51	3052.00	Litchfield	NH	1	0.004289		100.00%								OK	1	0	0	0	0	0	0	0	
52	3053.00	Londonderry	NH	10	0.011616		100.00%								OK	10	0	0	0	0	0	0	0	
53	3054.00	Merrimack	NH	1	0.009547		100.00%								OK	1	0	0	0	0	0	0	0	
54	3055.00	Millford	NH	1	0.007092		75.00%		25.00%						OK	0.75	0	0.25	0	0	0	0	0	
55	3062.00	Nashua	NH	1	0.003368		100.00%								OK	1	0	0	0	0	0	0	0	
56	3070.00	New Boston	NH	2	0.012502		75.00%		25.00%						OK	1.5	0	0.5	0	0	0	0	0	
57	3076.00	Pelham	NH	3	0.007647		100.00%								OK	3	0	0	0	0	0	0	0	
58	3077.00	Raymond	NH	8	0.008318		100.00%								OK	8	0	0	0	0	0	0	0	
59	3079.00	Salem	NH	6	0.007438		100.00%								OK	6	0	0	0	0	0	0	0	
60	3101.00	Manchester	NH	1	0.000226		90.00%						10.00%		OK	0.9	0	0	0	0	0	0.1	0	
61	3102.00	Manchester	NH	9	0.002627		90.00%						10.00%		OK	8.1	0	0	0	0	0	0.9	0	
62	3103.00	Manchester	NH	6	0.002887		90.00%						10.00%		OK	5.4	0	0	0	0	0	0.6	0	
63	3104.00	Manchester	NH	9	0.002441		90.00%						10.00%		OK	8.1	0	0	0	0	0	0.9	0	
64	3106.00	Hooksett	NH	3	0.010556		100.00%								OK	3	0	0	0	0	0	0	0	
65	3109.00	Manchester	NH	1	0.002277		90.00%						10.00%		OK	0.9	0	0	0	0	0	0.1	0	
66	3110.00	Bedford	NH	4	0.009428		100.00%								OK	4	0	0	0	0	0	0	0	
67	3225.00	Center Barnstead	NH	1	0.008176								100.00%		OK	0	0	0	0	0	0	1	0	
68	3234.00	Epsom	NH	1	0.009624								100.00%		OK	0	0	0	0	0	0	1	0	
69	3235.00	Franklin	NH	1	0.009122			50.00%					50.00%		OK	0	0.5	0	0	0	0	0.5	0	
70	3244.00	Hillsborough	NH	1	0.024593		100.00%								OK	1	0	0	0	0	0	0	0	
71	3245.00	Holderness	NH	1	0.010031								100.00%		OK	0	0	0	0	0	0	1	0	
72	3253.00	Meredith	NH	1	0.014683								100.00%		OK	0	0	0	0	0	0	1	0	
73	3255.00	Newbury	NH	1	0.010912		50.00%						50.00%		OK	0.5	0	0	0	0	0	0.5	0	
74	3258.00	Chichester	NH	3	0.005796								100.00%		OK	0	0	0	0	0	0	3	0	
75	3261.00	Northwood	NH	9	0.008624								100.00%		OK	0	0	0	0	0	0	9	0	
76	3263.00	Pittsfield	NH	1	0.007336								100.00%		OK	0	0	0	0	0	0	1	0	
77	3275.00	Suncook	NH	1	0.011764		50.00%						50.00%		OK	0.5	0	0	0	0	0	0.5	0	

LONZA BIOLOGICS
EMPLOYEE RESIDENTIAL ZIP CODE BASED TRIP DISTRIBUTION ANALYSIS

OBJECTID	ZIP_CODE	PO_NAME	STATE	employeeCount	Shape_Area	Direction	I-95 South	I-95 North	Route 33 South	Route 33 East	Route 1 East	Route 1 North	Route 4 West	Gosling Road North	check
78	3280.00	Washington	NH	1	0.013125			100.00%							OK
79	3281.00	Weare	NH	1	0.017189		50.00%						50.00%		OK
80	3290.00	Nottingham	NH	18	0.013032		50.00%						50.00%		OK
81	3301.00	Concord	NH	2	0.014821		50.00%						50.00%		OK
82	3303.00	Concord	NH	1	0.020526		50.00%						50.00%		OK
83	3570.00	Berlin	NH	1	0.023446								100.00%		OK
84	3576.00	Colebrook	NH	1	0.057233			34.00%	33.00%				33.00%		OK
85	3801.00	Portsmouth	NH	116	0.008103				20.00%	20.00%			20.00%	20.00%	OK
86	3809.00	Alton	NH	1	0.014804								100.00%		OK
87	3810.00	Alton Bay	NH	3	0.008575								100.00%		OK
88	3811.00	Atkinson	NH	2	0.003295		100.00%								OK
89	3812.00	Bartlett	NH	1	0.02191								100.00%		OK
90	3819.00	Danville	NH	3	0.003186		50.00%						50.00%		OK
91	3820.00	Dover	NH	116	0.00875								100.00%		OK
92	3823.00	Madbury	NH	5	0.003217								100.00%		OK
93	3824.00	Durham	NH	7	0.007376								100.00%		OK
94	3825.00	Barrington	NH	20	0.014117								100.00%		OK
95	3826.00	East Hampstead	NH	2	0.001192		100.00%								OK
96	3827.00	East Kingston	NH	3	0.00496		100.00%								OK
97	3830.00	East Wakefield	NH	2	0.003238								100.00%		OK
98	3833.00	Exeter	NH	39	0.013793		50.00%		50.00%						OK
99	3835.00	Farmington	NH	15	0.010892								100.00%		OK
100	3839.00	Rochester	NH	9	0.002018								100.00%		OK
101	3840.00	Greenland	NH	24	0.003048				100.00%						OK
102	3841.00	Hampstead	NH	7	0.003098		100.00%								OK
103	3842.00	Hampton	NH	27	0.003921		100.00%								OK
104	3844.00	Hampton Falls	NH	4	0.003506		100.00%								OK
105	3848.00	Kingston	NH	3	0.005907		100.00%								OK
106	3851.00	Milton	NH	10	0.008272								100.00%		OK
107	3852.00	Milton Mills	NH	1	0.001669								100.00%		OK
108	3855.00	New Durham	NH	9	0.012785								100.00%		OK
109	3856.00	Newfields	NH	5	0.00225				100.00%						OK
110	3857.00	Newmarket	NH	25	0.004782		50.00%						50.00%		OK
111	3858.00	Newton	NH	1	0.002836		100.00%								OK
112	3861.00	Lee	NH	7	0.005561								100.00%		OK
113	3862.00	North Hampton	NH	9	0.003932				100.00%						OK
114	3864.00	Ossipee	NH	2	0.01136								100.00%		OK
115	3865.00	Plastow	NH	4	0.002967		100.00%								OK
116	3867.00	Rochester	NH	58	0.009024								100.00%		OK
117	3868.00	Rochester	NH	15	0.002244								100.00%		OK
118	3869.00	Rollinsford	NH	5	0.001979			50.00%				50.00%			OK
119	3870.00	Rye	NH	10	0.003512		50.00%		50.00%						OK
120	3872.00	Sanbornville	NH	3	0.012299								100.00%		OK
121	3873.00	Sandown	NH	4	0.004147		50.00%		50.00%						OK
122	3874.00	Seabrook	NH	5	0.002676		100.00%								OK
123	3878.00	Somersworth	NH	50	0.002836								100.00%		OK
124	3882.00	Eppingham	NH	2	0.011411								100.00%		OK
125	3884.00	Strafford	NH	5	0.014538								100.00%		OK
126	3885.00	Stratham	NH	24	0.004492				100.00%						OK
127	3887.00	Union	NH	7	0.006041								100.00%		OK
128	3894.00	Wolfeboro	NH	1	0.020419								100.00%		OK
129	3901.00	Berwick	ME	10	0.0107			100.00%							OK
130	3902.00	Cape Neddick	ME	9	0.005456			100.00%							OK
131	3903.00	Eliot	ME	13	0.006136			100.00%							OK
132	3904.00	Kittery	ME	10	0.003178			100.00%							OK
133	3905.00	Kittery Point	ME	3	0.002057			100.00%							OK
134	3906.00	North Berwick	ME	7	0.011124			100.00%							OK
135	3907.00	Ogunquit	ME	1	0.0011			100.00%							OK
136	3908.00	South Berwick	ME	13	0.009329			100.00%							OK
137	3909.00	York	ME	9	0.010628			100.00%							OK
138	4005.00	Biddeford	ME	2	0.014128			100.00%							OK
139	4009.00	Bridgton	ME	1	0.018959			100.00%							OK
140	4021.00	Cumberland Center	ME	1	0.005747			100.00%							OK
141	4027.00	Lebanon	ME	5	0.016093			100.00%							OK
142	4038.00	Gorham	ME	1	0.014925			100.00%							OK
143	4042.00	Hollis Center	ME	2	0.009715			100.00%							OK
144	4043.00	Kennebunk	ME	9	0.009994			100.00%							OK
145	4046.00	Kennebunkport	ME	2	0.013092			100.00%							OK
146	4061.00	North Waterboro	ME	1	0.005735			100.00%							OK
147	4062.00	Windham	ME	3	0.014431			100.00%							OK
148	4072.00	Saco	ME	2	0.011271			100.00%							OK
149	4073.00	Sanford	ME	4	0.010941			100.00%							OK
150	4076.00	Shapleigh	ME	3	0.011892			100.00%							OK
151	4083.00	Springvale	ME	2	0.002897			100.00%							OK
152	4087.00	Waterboro	ME	1	0.005467			100.00%							OK
153	4090.00	Wells	ME	2	0.016786			100.00%							OK
154	4105.00	Falmouth	ME	1	0.008846			100.00%							OK
155	4281.00	South Paris	ME	1	0.012843			100.00%							OK
156	4938.00	Farmington	ME	1	0.036329			100.00%							OK
				SUM	1020										
					0										

I-95 South	I-95 North	Route 33 South	Route 33 East	Route 1 East	Route 1 North	Route 4 West	Gosling Road North	
1	0	0	0	0	0	0	0	OK
0.5	0	0	0	0	0	0.5	0	OK
9	0	0	0	0	0	9	0	OK
1	0	0	0	0	0	1	0	OK
0.5	0	0	0	0	0	0.5	0	OK
0	0	0	0	0	0	1	0	OK
0	0.34	0.33	0	0	0	0.33	0	OK
0	0	23.2	23.2	23.2	0	23.2	23.2	OK
0	0	0	0	0	0	1	0	OK
0	0	0	0	0	0	3	0	OK
2	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	1	0	OK
1.5	0	0	0	0	0	1.5	0	OK
0	0	0	0	0	0	116	0	OK
0	0	0	0	0	0	5	0	OK
0	0	0	0	0	0	7	0	OK
0	0	0	0	0	0	20	0	OK
2	0	0	0	0	0	0	0	OK
3	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	2	0	OK
19.5	0	19.5	0	0	0	0	0	OK
0	0	0	0	0	0	15	0	OK
0	0	0	0	0	0	9	0	OK
0	0	24	0	0	0	0	0	OK
7	0	0	0	0	0	0	0	OK
27	0	0	0	0	0	0	0	OK
4	0	0	0	0	0	0	0	OK
3	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	10	0	OK
0	0	0	0	0	0	1	0	OK
0	0	0	0	0	0	9	0	OK
0	0	5	0	0	0	0	0	OK
12.5	0	0	0	0	0	12.5	0	OK
1	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	7	0	OK
0	0	9	0	0	0	0	0	OK
0	0	0	0	0	0	2	0	OK
4	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	58	0	OK
0	0	0	0	0	0	15	0	OK
0	2.5	0	0	0	2.5	0	0	OK
5	0	5	0	0	0	0	0	OK
0	0	0	0	0	0	3	0	OK
2	0	2	0	0	0	0	0	OK
5	0	0	0	0	0	0	0	OK
0	0	0	0	0	0	50	0	OK
0	0	0	0	0	0	2	0	OK
0	0	0	0	0	0	5	0	OK
0	0	24	0	0	0	0	0	OK
0	0	0	0	0	0	7	0	OK
0	0	0	0	0	0	1	0	OK
0	10	0	0	0	0	0	0	OK
0	9	0	0	0	0	0	0	OK
0	13	0	0	0	0	0	0	OK
0	10	0	0	0	0	0	0	OK
0	3	0	0	0	0	0	0	OK
0	7	0	0					





JONES & BEACH ENGINEERS INC.

85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885
603.772.4746 - JonesandBeach.com

July 17, 2023

Portsmouth Technical Advisory Committee
Attn: Board Members
1 Junkins Avenue, Suite 3rd Floor
Portsmouth, NH 03801

RE: Subdivision Application
375 Banfield Road, Portsmouth, NH
Tax Map 266, Lot 7
JBE Project No. 19190.2

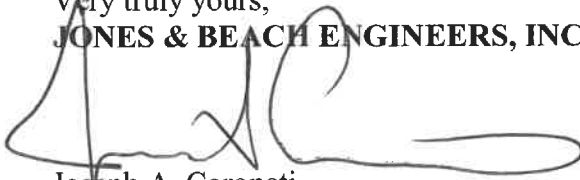
Dear Board Members,

Jones & Beach Engineers, Inc., respectfully submits a Subdivision Plan application on behalf of the applicant, Banfield Realty, LLC. The intent of this application is to subdivide the lot into two separate parcels. The new lot 7-1 will be a non-building lot and is being subdivided for financing reasons. Since this lot will not have any construction proposed on it, we are not applying for a Conditional Use Permit. The following items are provided in support of this application:

1. Completed Subdivision (submitted online) and Checklist.
2. Letter of Authorization.
3. Current Deed.
4. One (1) Full Size Plan (Folded).

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours,
JONES & BEACH ENGINEERS, INC.



Joseph A. Coronati
Vice President

cc: Rob Graham, Banfield Realty, LLC (via email)
Cindy Nix, Banfield Realty, LLC (via email)
Lynn Preston, Esq (via email)
Bill Wilcox, Wilcox & Barton (via email)



City of Portsmouth, New Hampshire

Subdivision Application Checklist

This subdivision application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. A pre-application conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all subdivision review requirements. Please refer to the Subdivision review regulations for full details.

Applicant Responsibilities (Section III.C): Applicable fees are due upon application submittal along with required number of copies of the Preliminary or final plat and supporting documents and studies. Please consult with Planning staff for submittal requirements.

Owner: Banfield Realty LLC Date Submitted: 7/17/2023

Applicant: Same as Owner

Phone Number: 603-479-3666 E-mail: rob@grahm-consult.com

Site Address 1: 375 Banfield Road Map: 266 Lot: 7

Site Address 2: _____ Map: _____ Lot: _____

Application Requirements			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested
<input checked="" type="checkbox"/>	Completed Application form. (III.C.2-3)		N/A
<input checked="" type="checkbox"/>	All application documents, plans, supporting documentation and other materials provided in digital Portable Document Format (PDF) on compact disc, DVD or flash drive. (III.C.4)		N/A

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Name and address of record owner, any option holders, descriptive name of subdivision, engineer and/or surveyor or name of person who prepared the plat. (Section IV.1/V.1)	A1	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	<p>Preliminary Plat Names and addresses of all adjoining property owners. (Section IV.2)</p> <p>Final Plat Names and addresses of all abutting property owners, locations of buildings within one hundred (100) feet of the parcel, and any new house numbers within the subdivision. (Section V.2)</p>	A1	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	North point, date, and bar scale. (Section IV.3/V3)	Required on all Plan Sheets	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	Zoning classification and minimum yard dimensions required. (Section IV.4/V.4)	A1, Note 2	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	<p>Preliminary Plat Scale (not to be smaller than one hundred (100) feet = 1 inch) and location map (at a scale of 1" = 1000'). (Section IV.5)</p> <p>Final Plat Scale (not to be smaller than 1"=100'), Location map (at a scale of 1"=1,000') showing the property being subdivided and its relation to the surrounding area within a radius of 2,000 feet. Said location map shall delineate all streets and other major physical features that may either affect or be affected by the proposed development. (Section V.5)</p>	A1	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input checked="" type="checkbox"/>	Location and approximate dimensions of all existing and proposed property lines including the entire area proposed to be subdivided, the areas of proposed lots, and any adjacent parcels in the same ownership. (Section IV.6)	A1	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input type="checkbox"/>	Dimensions and areas of all lots and any and all property to be dedicated or reserved for schools, parks, playgrounds, or other public purpose. Dimensions shall include radii and length of all arcs and calculated bearing for all straight lines. (Section V.6/ IV.7)		<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	N/A
<input type="checkbox"/>	Location, names, and present widths of all adjacent streets, with a designation as to whether public or private and approximate location of existing utilities to be used. Curbs and sidewalks shall be shown. (Section IV.8/V.7)		<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Location of significant physical features, including bodies of water, watercourses, wetlands, railroads, important vegetation, stone walls and soils types that may influence the design of the subdivision. (Section IV.9/V.8)	A1	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input type="checkbox"/>	Preliminary Plat Proposed locations, widths and other dimensions of all new streets and utilities, including water mains, storm and sanitary sewer mains, catch basins and culverts, street lights, fire hydrants, sewerage pump stations, etc. (Section IV.10) Final Plat Proposed locations and profiles of all proposed streets and utilities, including water mains, storm and sanitary sewer mains, catchbasins and culverts, together with typical cross sections. Profiles shall be drawn to a horizontal scale of 1"=50' and a vertical scale of 1"=5', showing existing centerline grade, existing left and right sideline grades, and proposed centerline grade. (Section V.9)		<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input type="checkbox"/>	When required by the Board, the plat shall be accompanied by profiles of proposed street grades, including extensions for a reasonable distance beyond the subject land; also grades and sizes of proposed utilities. (Section IV.10)		<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Base flood elevation (BFE) for subdivisions involving greater than five (5) acres or fifty (50) lots. (Section IV.11)	A1, Note 4	<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input type="checkbox"/>	For subdivisions of five (5) lots or more, or at the discretion of the Board otherwise, the preliminary plat shall show contours at intervals no greater than two (2) feet. Contours shall be shown in dotted lines for existing natural surface and in solid lines for proposed final grade, together with the final grade elevations shown in figures at all lot corners. If existing grades are not to be changed, then the contours in these areas shall be solid lines. (Section IV.12/ V.12)		<input checked="" type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

Requirements for Preliminary/Final Plat				
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Required for Preliminary / Final Plat	Waiver Requested
<input checked="" type="checkbox"/>	Dates and permit numbers of all necessary permits from governmental agencies from which approval is required by Federal or State law. (Section V.10)	A1, Note 13	<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input type="checkbox"/>	For subdivisions involving greater than five (5) acres or fifty (50) lots, the final plat shall show hazard zones and shall include elevation data for flood hazard zones. (Section V.11)		<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	
<input checked="" type="checkbox"/>	Location of all permanent monuments. (Section V.12)	A1	<input type="checkbox"/> Preliminary Plat <input checked="" type="checkbox"/> Final Plat	

<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input checked="" type="checkbox"/>	15. Easements (VI.15)		
<input checked="" type="checkbox"/>	a. Utilities	A1	
<input checked="" type="checkbox"/>	b. Drainage		
<input checked="" type="checkbox"/>	16. Monuments: (VI.16)	A1	
<input type="checkbox"/>	17. Benchmarks: (VI.17)		
<input type="checkbox"/>	18. House Numbers (VI.18)		

Design Standards			
	Required Items for Submittal	Indicate compliance and/or provide explanation as to alternative design	Waiver Requested
<input type="checkbox"/>	1. Streets have been designed according to the design standards required under Section (VII.1). a. Clearing b. Excavation c. Rough Grade and Preparation of Sub-Grade d. Base Course e. Street Paving f. Side Slopes g. Approval Specifications h. Curbing i. Sidewalks j. Inspection and Methods		
<input type="checkbox"/>	2. Storm water Sewers and Other Drainage Appurtenances have been designed according to the design standards required under Section (VII.2). a. Design b. Standards of Construction		
<input type="checkbox"/>	3. Sanitary Sewers have been designed according to the design standards required under Section (VII.3). a. Design b. Lift Stations c. Materials d. Construction Standards		
<input type="checkbox"/>	4. Water Mains and Fire Hydrants have been designed according to the design standards required under Section (VII.4). a. Connections to Lots b. Design and Construction c. Materials d. Notification Prior to Construction		

Applicant's/Representative's Signature: _____

Date: 7/17/2023

¹ See City of Portsmouth, NH Subdivision Rules and Regulations for details.
Subdivision Application Checklist/January 2018

Letter of Authorization

I, Banfield Realty, LLC, 304 Maplewood Avenue, Portsmouth, NH 03801, owner of property located in Portsmouth, NH, known as Tax Map 266, Lot 7, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on my behalf concerning the previously-mentioned property. The parcel is located on 375 Banfield Road in Portsmouth, NH.

I hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

Cynthia Hix
Witness

[Signature]
Banfield Realty, LLC

7-23-20
Date



Return to:



LCHIP	ROA480986	25.00
TRANSFER TAX	RO094654	18,000.00
RECORDING		30.00
SURCHARGE		2.00

WARRANTY DEED

KNOW ALL PERSONS BY THESE PRESENTS, that we, **William E. Copeland** a married man of 26 Constitution Way, Dover, NH 03820, **Jack Copeland** a single man of 245 Middle Street, Apartment #227, Portsmouth, NH 03801, **Kevin Copeland** a single man of P.O. Box 4213, Valley Village, CA 91617, **Joseph P. Copeland**, married man of 142 Dennett Road, Kittery, ME 03904, and **Roeseland Holdings 5, LLC**, a New Hampshire limited liability company with an address of 21 Moody Point Drive, Newmarket, NH 03857, grant to **Banfield Realty LLC**, a New Hampshire limited liability company with an address of 304 Maplewood Avenue, Portsmouth, NH 03801, with warranty covenants, all our right, title and interest in the following described premises:

A certain lot or parcel of land together with the buildings thereon situated on the Southeasterly sideline of Banfield Road in Portsmouth, County of Rockingham and State of New Hampshire, bounded and described as follows:

Commencing at a point on said Southeasterly sideline of Banfield Road at the intersection of two stone walls and at land now or formerly of one Barratt; thence running in a Southeasterly direction by and along an old stone wall and land now or formerly of said Barratt, Thompson, Pickering, Iafolla, Wood and Myers, a total distance of Two Thousand Six Hundred Sixty-Three feet (2,663') more or less to a point at the intersection of two stone walls; thence turning and running by and along a stone wall and land of Myers N 58° 22' E, a distance of One Hundred Twenty-Eight feet (128') to other land of Iafolla; thence turning and running by and along another stone wall and land of Iafolla, S 18° 21' E, a distance of Three Hundred Twenty feet (320'); thence turning and running by and along another stone wall S 54° 8' 30" W, a distance of Thirty feet (30'); thence turning and running by a stone wall S 47° 49' 30" E, a distance of One Hundred Seven feet (107') to a point adjoining land of Peverly Hill Corp., thence turning and running S 70° 15' W, a distance of Five Hundred Thirty-Three feet (533') to a point; thence turning and running N 25° 11' W, a distance of Three Hundred Twenty-Five feet (325') to a point at an old stone wall; thence turning and running in a Southwesterly direction by and along said stone wall and land of said Peverly Hill Corp. and also by land of Stef, a distance of Four Hundred Forty-Six feet (446') to a point; thence turning and running in a Northwesterly direction by a stone wall and land of Stef, a distance of One Thousand Four Hundred Ninety-Five feet (1,495') more or less to a point; thence turning and running S 65° 16' W, a distance of Ninety-Two feet (92') also by land of Stef to a point adjoining land now or formerly of Dow; thence turning and running N 25° 31' W, a distance of One Hundred Seventy-Five feet (175') to a point; thence continuing N 33° 50' W, a distance of Three Hundred and Eighteen feet (318') to a point; thence continuing N 35° 25' W, a distance of

Four Hundred Five feet (405') to a point adjoining land of Copeland; thence turning and running N 64° 17' E, a distance of Three Hundred Sixty feet (360') to a point; thence turning and running N 33° 21' W, a distance of Two Hundred feet (200'), the last two courses by land of Copeland, to a point at an old stone wall on the Southeasterly sideline of Banfield Road; thence turning and running by said stone wall N 63° 50' E, a distance of One Hundred Twenty-Nine feet (129'); thence continuing N 60° 28' E, a distance of Three Hundred Ten feet (310'); thence continuing N 61° 1' E, a distance of One Hundred Twenty-One feet (121') to the stone wall and point of beginning.

Excepting and excluding from this conveyance that portion of the above-described premises previously conveyed by warranty deed of William H. Copeland and Virginia A. Copeland to John Iafolla Co., Inc. dated September 3, 1963, recorded in Rockingham County Registry of Deeds at Book 1686, Page 133.

Subject to a right of way Fifty feet (50') in width lying along the Northeasterly sideline of the premises herein conveyed, and adjoining a stone wall designating said boundary, for access from Banfield Road to property conveyed by William H. Copeland and Virginia A. Copeland to John Iafolla Co., Inc. by warranty deed dated September 3, 1963, recorded in Rockingham County Registry of Deeds at Book 1686, Page 133.

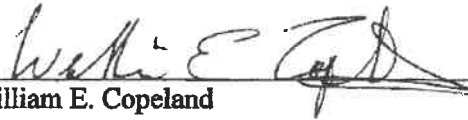
Meaning and intending to describe and convey a portion of the same premises conveyed by Harry Zaitland and Irving Zaitland to William H. Copeland and Virginia A. Copeland by warranty deed dated September 3, 1963, recorded in Rockingham County Registry of Deeds at Book 1686, Page 128. William H. Copeland conveyed his interest in the premises to Virginia A. Copeland by quitclaim deed dated March 15, 2001, recorded in Rockingham County Registry of Deeds at Book 3555, Page 0083. Virginia A. Copeland died on September 10, 2008. See Estate of Virginia A. Copeland, 10th Circuit – Probate Division – Brentwood, Case No. 318-2008-ET-01202. Virginia A. Copeland's interest in the premises passed to the grantors William E. Copeland, Jack Copeland, Kevin Copeland and to James R. Copeland, who died on June 4, 2018. See Estate of James R. Copeland, 10th Circuit – Probate Division – Brentwood, Case No. 318-2018-ET-01138. James R. Copeland's interest in the premises passed to his sons, Joseph P. Copeland and James W. Copeland. James W. Copeland conveyed his portion of the premises to Roeseland Holdings 5, LLC, by Quitclaim Deed dated May 7, 2019, recorded in Rockingham County Registry of Deeds at Book 5998, Page 2778.

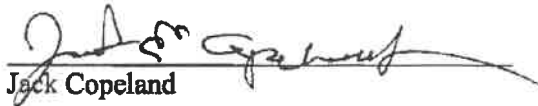
The premises conveyed hereby is not homestead property of the Grantors.

Executed this 5th day of February, 2020.

[Signature Page Attached]

[Signature Page to Warranty Deed]

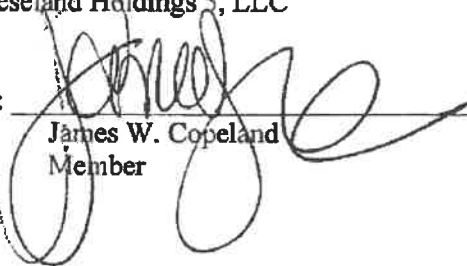

William E. Copeland


Jack Copeland

Kevin Copeland


Joseph P. Copeland

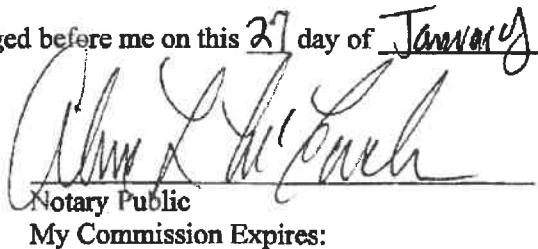
Roeseland Holdings, LLC

By: 
James W. Copeland
Its: Member

STATE OF NEW HAMPSHIRE
COUNTY OF ROCKINGHAM

The foregoing instrument was acknowledged before me on this 27 day of January
2020, by William E. Copeland.




Notary Public
My Commission Expires:

[Signature Page to Warranty Deed]

William E. Copeland

Jack Copeland



Kevin Copeland

Joseph P. Copeland

Roeseland Holdings 5, LLC

By: _____
James W. Copeland

Its: Member

STATE OF NEW HAMPSHIRE
COUNTY OF ROCKINGHAM

The foregoing instrument was acknowledged before me on this ____ day of _____
2020, by William E. Copeland.

~~See attached certificate.~~

Notary Public
My Commission Expires:

STATE OF NEW HAMPSHIRE
COUNTY OF ROCKINGHAM

The foregoing instrument was acknowledged before me on this 28 day of January
2020, by Jack Copeland.



Alec L. McEachern
Notary Public

My Commission Expires:

STATE OF CALIFORNIA
COUNTY OF _____

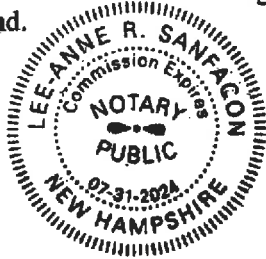
The foregoing instrument was acknowledged before me on this _____ day of _____
2020, by Kevin Copeland.

See attached certificate.

Notary Public
My Commission Expires:

STATE OF NEW HAMPSHIRE
COUNTY OF ROCKINGHAM

The foregoing instrument was acknowledged before me on this 5th day of February
2020, by Joseph P. Copeland.

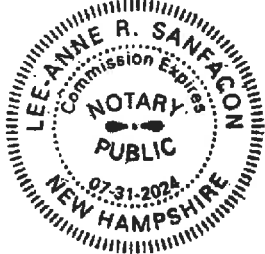


Lee Anne R. Sanfacon
Notary Public

My Commission Expires:

STATE OF NEW HAMPSHIRE
COUNTY OF ROCKINGHAM

The foregoing instrument was acknowledged before me on this 5th day of February
2020, by James W. Copeland in his capacity as Member of Roeseland Holdings 5, LLC.



Lee Anne R. Sanfacon
Notary Public

My Commission Expires:

CALIFORNIA ALL-PURPOSE ACKNOWLEDGMENT

CIVIL CODE § 1180

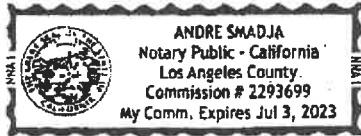
A notary public or other officer completing this certificate verifies only the identity of the individual who signed the document to which this certificate is attached, and not the truthfulness, accuracy, or validity of that document.

State of California)
County of Los Angeles)
On 01/27/2020 before me, ANDRE SMADJA, Notary Public.
Date Here Insert Name and Title of the Officer
personally appeared KEVIN COLEMAN
Name(s) of Signer(s)

who proved to me on the basis of satisfactory evidence to be the person(s) whose name(s) is/are subscribed to the within instrument and acknowledged to me that he/she/they executed the same in his/her/their authorized capacity(ies), and that by his/her/their signature(s) on the instrument the person(s), or the entity upon behalf of which the person(s) acted, executed the instrument.

I certify under PENALTY OF PERJURY under the laws of the State of California that the foregoing paragraph is true and correct.

WITNESS my hand and official seal.



Signature _____
Signature of Notary Public

Place Notary Seal Above

OPTIONAL

Though this section is optional, completing this information can deter alteration of the document or fraudulent reattachment of this form to an unintended document.

Description of Attached Document
Title or Type of Document: WARRANTY DEED
Document Date: 01/27/2020 Number of Pages: 4
Signer(s) Other Than Named Above:

Capacity(ies) Claimed by Signer(s)

Signer's Name: _____
[] Corporate Officer -- Title(s): _____
[] Partner -- [] Limited [] General
[x] Individual [] Attorney in Fact
[] Trustee [] Guardian or Conservator
[] Other: _____
Signer Is Representing: _____

Signer's Name: _____
[] Corporate Officer -- Title(s): _____
[] Partner -- [] Limited [] General
[] Individual [] Attorney in Fact
[] Trustee [] Guardian or Conservator
[] Other: _____
Signer Is Representing: _____

**FEE SCHEDULE
 Planning Department
 Effective 07/01/23 – 06/30/24**

PLANNING BOARD

Subdivision:

Subdivision	
Residential	\$600.00 plus \$200.00 per lot
Non-Residential.....	\$800.00 plus \$300.00 per lot \$1,400.00

Subdivision Amendment:

Administrative approval	\$200.00
TAC or Planning Board approval.....	\$500.00

Lot line revision/verification\$250.00

Lot Line Revision Amendment

Administrative approval	\$200.00
TAC or Planning Board approval.....	\$250.00

Lot Consolidation – No Subdivision.....\$175.00

Restoration of Involuntarily Merged Lots\$300.00

Preliminary Conceptual Consultation\$200.00

Design Review.....\$500.00

Site Plan Review:

All developments.....	\$600.00
	plus \$5.00 per \$1,000 of site costs only
	plus \$10.00 per 1,000 s.f. of site development area

Total fee not to exceed (cap).....\$20,000.00

Site Plan Minor Amendment:

Administrative approval	\$400.00
Administrative approval after	
work has been done	\$500.00
TAC or Planning Board approval.....	\$800.00

Preliminary Conceptual Consultation\$200.00

Design Review.....\$500.00

Planning Department Fee Schedule (Effective 07/01/23 – 06/30/24)

Wetlands Conditional Use Permit:

Area of disturbance in wetland or wetland buffer:

Up to 250 sq. ft.	\$100.00
Up to 1,000 sq. ft.....	\$500.00
Greater than 1,000 sq. ft.....	\$1,300.00

Conditional Use Permit (Non-Wetland):

Conditional Use Permit (Non-Wetland).....	\$500.00
---	----------

Courier Fees:

Mylar Recording.....	\$150.00
Deed Recording.....	\$100.00

BOARD OF ADJUSTMENT

Residential Applications

1-2 dwelling units	\$200.00
3-4 dwelling units	\$300.00 plus \$50.00 for each unit over 4
Total fee not to exceed (cap).....	\$3,000.00

Residential accessory structure only	\$50.00
--	---------

Non-Residential Applications \$400.00 plus \$5.00 per \$1,000 of valuation of new construction

Total fee not to exceed (cap).....	\$3,000.00
------------------------------------	------------

Signs	\$200.00
--------------------	----------

Appeal of Administrative Decision	\$50.00
--	---------

HISTORIC DISTRICT COMMISSION

Work Session (prior to application for approval)	\$200.00 per work session
---	---------------------------

Residential Applications

1 dwelling unit	\$100.00
2 dwelling units	\$100.00
3 dwelling units	\$250.00
4 dwelling units and over.....	\$400.00 plus \$100.00 for each unit over 4
Total fee not to exceed (cap).....	\$5,000.00

Accessory structure, mechanical equipment or replacement of doors/windows only	\$100.00
---	----------

Planning Department Fee Schedule (Effective 07/01/23 – 06/30/24)

Non-Residential Applications	\$500.00 plus \$5.00 per \$1,000 of valuation of new construction
Total fee not to exceed (cap).....	\$5,000.00
Accessory structure, mechanical equipment or replacement of doors/windows only	\$100.00
Signs	\$100.00
Amendment to Certificate of Approval:	
Administrative approval	\$100.00
Administrative approval after work has been done	\$500.00
Commission approval	\$800.00

ZONING PERMITS

Certificate of conformity	\$50.00
Letter of interpretation.....	\$100.00

Please note: Costs associated with third party review and technical assistance may apply, including but not limited to costs associated with review and recordation of documents at the registry.

PLAN REFERENCES:

- "PLAN OF LAND IN PORTSMOUTH, N.H. OWNED BY PEVERLY HILL CORPORATION AND JOHN IAFOLLA COMPANY INC." DATED DECEMBER 1975. PREPARED BY FRANCIS BARRETT. R.C.R.D. 5657.
- "PLAN OF LAND FOR MICHAEL R. IAFOLLA & FERRIS G. BAWCOHL." DATED MAY 2, 1983. PREPARED BY KIMBALL CHASE COMPANY, INC. R.C.R.D. 11561.
- "SUBDIVISION PLAN FOR JOHN IAFOLLA COMPANY, INC. PEVERLY HILL ROAD / BANFIELD ROAD, PORTSMOUTH, N.H." DATED OCTOBER 11, 1996. R.C.R.D. 25153.
- "BOUNDARY PLAN, TAX MAP R66, LOT 4." DATED JUNE 1997. PREPARED BY LITTLE RIVER SURVEY COMPANY. R.C.R.D. 26190.
- "LOT LINE ADJUSTMENT, JOHN IAFOLLA COMPANY, INC. AND CITY OF PORTSMOUTH." DATED NOVEMBER 16, 1997. R.C.R.D. 26202.
- "LOT LINE REVISION PLAN, CAMPUS DRIVE, BANFIELD & PEVERLY HILL ROADS, PORTSMOUTH, NEW HAMPSHIRE." DATED OCTOBER 24, 2016. PREPARED BY JAMES VERRA AND ASSOCIATES. R.C.R.D. 39897.

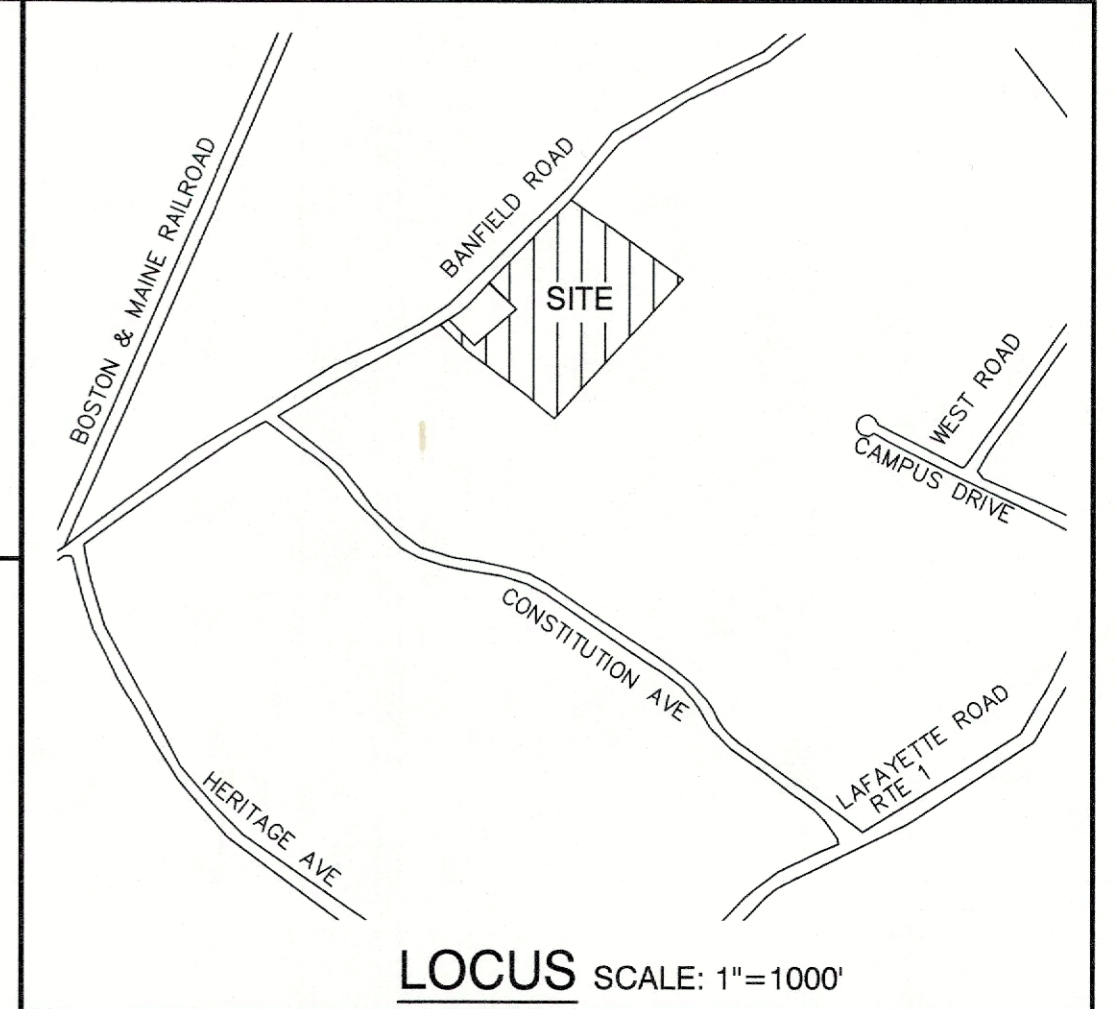
MAP 265 LOT 2A
DAVID W. ECKER
875 BANFIELD RD
PORTSMOUTH, NH 03801
BK 6091 PG 374

MAP 256 LOT 1
SWIFT WATER GIRL SCOUT COUNCIL
ONE COMMERCE DR
BEDFORD, NH 03110

MAP 265 LOT 4
PORTSMOUTH NH GIRL SCOUT COUNCIL
ONE COMMERCE DR
BEDFORD, NH 03110
BK 1602 PG 19

APPROVED - PORTSMOUTH, NH
PLANNING BOARD

DATE:



GENERAL LEGEND

EXISTING	PROPOSED	DESCRIPTION
---	---	PROPERTY LINES
---	---	SETBACK LINES
---	---	CENTERLINE
---	---	FRESHWATER WETLAND LINE
---	---	STONEWALL
---	---	FENCE
---	---	SOIL BOUNDARY
---	---	EASEMENT
---	---	EDGE OF PAVEMENT
---	---	IRON PIPE/IRON ROD
---	---	DRILL HOLE
---	---	IRON ROD/DRILL HOLE
---	---	STONE/GRANITE BOUND
---	---	BENCHMARK (TBM)
---	---	FRESHWATER WETLANDS

APPROVED 1,910 S.F. WETLAND FILL NHDES PERMIT #2021-00240

MAP 266 LOT 5
HOPE FOR TOMORROW FOUNDATION
1 STONERIDGE DR
RYE, NH 03870
BK 5783 PG 602

EXISTING 50' RIGHT OF WAY FOR ACCESS TO BENEFIT TAX MAP 266, LOT 84 BK 1686 PG 133

SUBDIVISION NOTES:

- THE INTENT OF THIS PLAN IS TO SUBDIVIDE MAP 266, LOT 7 INTO TWO (2) LOTS.
- ZONING DISTRICT: INDUSTRIAL
LOT AREA MINIMUM = 2 ACRES
LOT FRONTAGE MINIMUM = 200'
BUILDING SETBACKS (MINIMUM):
FRONT SETBACK = 70'
SIDE SETBACK = 50'
REAR SETBACK = 50'
MAX. BUILDING HEIGHT = 70'
MAX. BUILDING COVERAGE = 50%
MIN. OPEN SPACE = 20%
OPEN SPACE PROVIDED = 161,600 S.F. = 55.8% OF LOT 7; 346,620 S.F. = 100% OF LOT 7-1
BUILDING COVERAGE PROVIDED = 75,000 S.F. = 25.9% OF LOT 7; 0 S.F. = 0% OF LOT 7-1
- THIS PLAN SET HAS BEEN PREPARED BY JONES & BEACH ENGINEERS, INC. FOR MUNICIPAL AND STATE APPROVALS AND FOR CONSTRUCTION BASED ON DATA OBTAINED FROM ON-SITE FIELD SURVEY AND EXISTING MUNICIPAL RECORDS. THROUGHOUT THE CONSTRUCTION PROCESS, THE CONTRACTOR SHALL INFORM THE ENGINEER IMMEDIATELY OF ANY FIELD DISCREPANCY FROM DATA AS SHOWN ON THE DESIGN PLANS, INCLUDING ANY UNFORESEEN CONDITIONS, SUBSURFACE OR OTHERWISE, FOR EVALUATION AND RECOMMENDATIONS. ANY CONTRADICTION BETWEEN ITEMS ON THIS PLAN/PLAN SET, OR BETWEEN THE PLANS AND ON-SITE CONDITIONS, MUST BE RESOLVED BEFORE RELATED CONSTRUCTION HAS BEEN INITIATED.
- THE SUBJECT PARCEL IS NOT LOCATED WITHIN AN AREA HAVING A SPECIAL FLOOD HAZARD AREA DESIGNATION BY THE FEDERAL EMERGENCY MANAGEMENT AGENCY, ON FLOOD INSURANCE RATE MAP NO. 33015C00270E, WITH EFFECTIVE DATE OF MAY 17, 2005.
- ALL MONUMENTS TO BE SET ARE 5/8" IRON RODS WITH ALUMINUM CAPS MARKED "JONES & BEACH ENGINEERS BOUNDARY, DO NOT DISTURB, STRATHAM, N.H." AS SHOWN.
- WETLANDS WERE DELINEATED BY GOVE ENVIRONMENTAL SERVICES, INC., DURING MARCH 2020, AND LOCATED BY THIS OFFICE.
- LANDOWNERS ARE RESPONSIBLE FOR COMPLYING WITH ALL APPLICABLE LOCAL, STATE AND FEDERAL WETLAND REGULATIONS, INCLUDING PERMITTING REQUIRED UNDER THESE REGULATIONS.
- ALL BOOK AND PAGE NUMBERS REFER TO THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
- THE TAX MAP AND LOT NUMBERS AND ADJOINING OWNERS ARE BASED ON THE CITY OF PORTSMOUTH TAX RECORDS AND ARE SUBJECT TO CHANGE.
- RESEARCH WAS PERFORMED AT THE TOWN OF PORTSMOUTH ASSESSORS OFFICE AND THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
- THIS SURVEY IS NOT A CERTIFICATION TO OWNERSHIP OR TITLE OF LANDS SHOWN. OWNERSHIP AND ENCUMBRANCES ARE MATTERS OF TITLE EXAMINATION NOT OF A BOUNDARY SURVEY. THE INTENT OF THIS PLAN IS TO RETRACE THE BOUNDARY LINES OF DEEDS REFERENCED HEREON. OWNERSHIP OF ADJOINING PROPERTIES IS ACCORDING TO ASSESSOR'S RECORDS. THIS PLAN MAY OR MAY NOT INDICATE ALL ENCUMBRANCES EXPRESSED, IMPLIED OR PRESCRIPTIVE.
- ANY USE OF THIS PLAN AND OR ACCOMPANYING DESCRIPTIONS SHOULD BE DONE WITH LEGAL COUNSEL TO BE CERTAIN THAT TITLES ARE CLEAR, THAT INFORMATION IS CURRENT, AND THAT ANY NECESSARY CERTIFICATES ARE IN PLACE FOR A PARTICULAR CONVEYANCE, OR OTHER USES.
- NHDES ALTERATION OF TERRAIN PERMIT NO. A07-2040, DATED 10/28/2021
NHDES SEPTIC SYSTEM APPROVAL FOR CONSTRUCTION NO. ECA2021102913, DATED 10/29/2021
NHDES WETLANDS BUREAU PERMIT NO. 2021-00240, DATED 12/06/2021

CERTIFICATION:

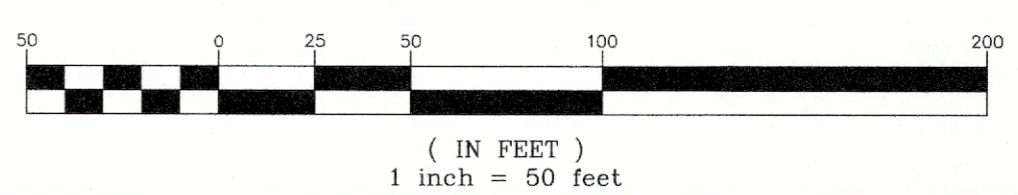
I CERTIFY THAT THIS PLAT WAS PREPARED UNDER MY DIRECT SUPERVISION, THAT IT IS THE RESULT OF A FIELD SURVEY BY THIS OFFICE AND HAS AN UNADJUSTED LINEAR ERROR OF CLOSURE THAT EXCEEDS BOTH THE MINIMUM OF 1:10,000 AS DEFINED IN SECTION 503.04 OF THE NEW HAMPSHIRE CODE OF ADMINISTRATIVE RULES AND THE MINIMUM OF 1:15,000 AS DEFINED IN SECTION 4.2 OF THE N.H.L.S.A. ETHICS AND STANDARDS.

THIS SURVEY CONFORMS TO A CATEGORY 1 SURVEY AS DEFINED IN SECTION 4.1 OF THE N.H.L.S.A. ETHICS AND STANDARDS.

DAVID M. COLLIER, LLS 892
ON BEHALF OF JONES & BEACH ENGINEERS, INC.

DATE: 7/12/2023

GRAPHIC SCALE



TOTAL LOT AREA
636,237 S.F.
14.61 ACRES

F:\CADD\MASTER STANDARD\dwg\JOB-LAYOUTS.dwg 3/12/2015 3:27:29 PM EDT

Design: JAC	Draft: DJM	Date: 04/21/20
Checked: JAC	Scale: AS-NOTED	Project No.: 19190.2
Drawing Name: 19190-PLAN-NEW-LAYOUT.dwg		
THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.		

REV.	DATE	REVISION	BY
0	7/17/23	ISSUED FOR REVIEW	DJM

J/B Jones & Beach Engineers, Inc.
Civil Engineering Services
85 Portsmouth Ave. PO Box 219 Stratham, NH 03885
603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:	SUBDIVISION AND EASEMENT PLAN TAX MAP 266, LOT 7
Project:	INDUSTRIAL WAREHOUSE 375 BANFIELD ROAD, PORTSMOUTH, NH 03801
Owner of Record:	BANFIELD REALTY LLC 304 MAPLEWOOD AVENUE, PORTSMOUTH, NH 03801

DRAWING No.
A1
SHEET 1 OF 1
JBE PROJECT NO. 19190.2



200 Griffin Road, Unit 3, Portsmouth, NH 03801
Phone (603) 430-9282 Fax 436-2315

17 July 2023

Peter Stith, TAC Committee Chair
City of Portsmouth
1 Junkins Avenue
Portsmouth, NH 03801

RE: Request for Site Plan Approval at 700 Peverly Hill Road, Proposed Building Addition

Dear Mr. Stith and TAC Members:

On behalf of JMK Realty, LLC and Portsmouth Auto Body Center we are pleased to submit the attached plan set for **Site Plan Approval** for the above-mentioned project and request that we be placed on the agenda for your **August 1, 2023**, TAC Meeting. The project consists of a 3,385-sf addition to the existing rear commercial building at 700 Peverly Hill Road. The area surrounding the existing building is currently a paved service lot. The pavement will be sawcut to allow the proposed addition to be placed. Existing porous area (open space) to be covered by the addition will be replaced by the creation of a similarly sized area where the pavement will be removed. This results in no change to the impervious surface coverage on the site. The grades will be adjusted to accommodate the new construction. As a result of our review with the TAC Committee in a workshop the plans reflect improvements to the site drainage system. The new construction will require the relocation of the existing gas service. All other utility connections will be internal.

The following plans are included in our submission:

- Cover Sheet – This shows the Development Team, Legend, Site Location, and Site Zoning.
- Boundary Survey Plan – This plan shows the existing property boundaries.
- Existing Conditions and Demolition Plan C1 – This plan shows the existing site conditions at the location of the addition in detail as well as the site features which will be removed.
- Site Plan C2 – This plan shows the proposed building addition placement and proposed setbacks.
- Grading Plan C3 – This plan shows proposed site grading and the proposed drainage improvements.
- Utility Plan C4 – This plan shows the gas service relocation and notes that all other utilities will be unchanged.
- Detail Sheet D1 – This plan shows site details.

Also please find attached the following submission items:

Site Plan Application Checklist
Statement of No Further action from NHDES
Tri Generation Calculations
Parking Demand Memo
Site Drainage Analysis
Building Plans

We look forward to and in person presentation and the review of this submission by Staff and City Department's for this project.

Sincerely,

A handwritten signature in black ink, appearing to read 'J. Chagnon', with a long horizontal flourish extending to the right.

John R. Chagnon, PE



City of Portsmouth, New Hampshire

Site Plan Application Checklist

This site plan application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. The checklist is required to be completed and uploaded to the Site Plan application in the City's online permitting system. A pre-application conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all site plan review requirements. Please refer to the Site Plan review regulations for full details.

Applicant Responsibilities (Section 2.5.2): Applicable fees are due upon application submittal along with required attachments. The application shall be complete as submitted and provide adequate information for evaluation of the proposed site development. Waiver requests must be submitted in writing with appropriate justification.

Name of Applicant: Portsmouth Autobody Center Date Submitted: 7-17-23

Application # (in City's online permitting): TBD

Site Address: 700 Peverly Hill Road Map: 252 Lot: 2-10

Application Requirements			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	Complete application form submitted via the City's web-based permitting program (2.5.2.1(2.5.2.3A))	Online	N/A
<input type="checkbox"/>	All application documents, plans, supporting documentation and other materials uploaded to the application form in viewpoint in digital Portable Document Format (PDF). One hard copy of all plans and materials shall be submitted to the Planning Department by the published deadline. (2.5.2.8)	Online	N/A

Site Plan Review Application Required Information			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	Statement that lists and describes "green" building components and systems. (2.5.3.1B)	Online App	
<input type="checkbox"/>	Existing and proposed gross floor area and dimensions of all buildings and statement of uses and floor area for each floor. (2.5.3.1C)	Building Plans	N/A
<input type="checkbox"/>	Tax map and lot number, and current zoning of all parcels under Site Plan Review. (2.5.3.1D)	Cover Sheet	N/A

Site Plan Review Application Required Information			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	Owner's name, address, telephone number, and signature. Name, address, and telephone number of applicant if different from owner. (2.5.3.1E)	Cover Sheet	N/A
<input type="checkbox"/>	Names and addresses (including Tax Map and Lot number and zoning districts) of all direct abutting property owners (including properties located across abutting streets) and holders of existing conservation, preservation or agricultural preservation restrictions affecting the subject property. (2.5.3.1F)	Existing Conditions Plan	N/A
<input type="checkbox"/>	Names, addresses and telephone numbers of all professionals involved in the site plan design. (2.5.3.1G)	Cover Sheet	N/A
<input type="checkbox"/>	List of reference plans. (2.5.3.1H)	Existing Conditions Plan	N/A
<input type="checkbox"/>	List of names and contact information of all public or private utilities servicing the site. (2.5.3.1I)	Cover Sheet	N/A

Site Plan Specifications			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	Full size plans shall not be larger than 22 inches by 34 inches with match lines as required, unless approved by the Planning Director.. (2.5.4.1A)	Required on all plan sheets	N/A
<input type="checkbox"/>	Scale: Not less than 1 inch = 60 feet and a graphic bar scale shall be included on all plans. (2.5.4.1B)	Required on all plan sheets	N/A
<input type="checkbox"/>	GIS data should be referenced to the coordinate system New Hampshire State Plane, NAD83 (1996), with units in feet. (2.5.4.1C)	Yes	N/A
<input type="checkbox"/>	Plans shall be drawn to scale and stamped by a NH licensed civil engineer. (2.5.4.1D)	Required on all plan sheets	N/A
<input type="checkbox"/>	Wetlands shall be delineated by a NH certified wetlands scientist and so stamped. (2.5.4.1E)	N/A	N/A
<input type="checkbox"/>	Title (name of development project), north point, scale, legend. (2.5.4.2A)	Cover Sheet	N/A
<input type="checkbox"/>	Date plans first submitted, date and explanation of revisions. (2.5.4.2B)	All sheets	N/A
<input type="checkbox"/>	Individual plan sheet title that clearly describes the information that is displayed. (2.5.4.2C)	Required on all plan sheets	N/A
<input type="checkbox"/>	Source and date of data displayed on the plan. (2.5.4.2D)	Boundary & Existing Conditions Plans	N/A

Site Plan Specifications – Required Exhibits and Data

<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	<p>1. Existing Conditions: (2.5.4.3A)</p> <ul style="list-style-type: none"> • Surveyed plan of site showing existing natural and built features; • Existing building footprints and gross floor area; • Existing parking areas and number of parking spaces provided; • Zoning district boundaries; • Existing, required, and proposed dimensional zoning requirements including building and open space coverage, yards and/or setbacks, and dwelling units per acre; • Existing impervious and disturbed areas; • Limits and type of existing vegetation; • Wetland delineation, wetland function and value assessment (including vernal pools); • SFHA, 100-year flood elevation line and BFE data, as required. 	Existing Conditions Plan	
<input type="checkbox"/>	<p>2. Buildings and Structures: (2.5.4.3B)</p> <ul style="list-style-type: none"> • Plan view: Use, size, dimensions, footings, overhangs, 1st fl. elevation; • Elevations: Height, massing, placement, materials, lighting, façade treatments; • Total Floor Area; • Number of Usable Floors; • Gross floor area by floor and use. 	Building Plans	
<input type="checkbox"/>	<p>3. Access and Circulation: (2.5.4.3C)</p> <ul style="list-style-type: none"> • Location/width of access ways within site; • Location of curbing, right of ways, edge of pavement and sidewalks; • Location, type, size and design of traffic signing (pavement markings); • Names/layout of existing abutting streets; • Driveway curb cuts for abutting prop. and public roads; • If subdivision; Names of all roads, right of way lines and easements noted; • AASHTO truck turning templates, description of minimum vehicle allowed being a WB-50 (unless otherwise approved by TAC). 	Existing Conditions Plan	
<input type="checkbox"/>	<p>4. Parking and Loading: (2.5.4.3D)</p> <ul style="list-style-type: none"> • Location of off street parking/loading areas, landscaped areas/buffers; • Parking Calculations (# required and the # provided). 	Existing Conditions Plan	
<input type="checkbox"/>	<p>5. Water Infrastructure: (2.5.4.3E)</p> <ul style="list-style-type: none"> • Size, type and location of water mains, shut-offs, hydrants & Engineering data; • Location of wells and monitoring wells (include protective radii). 	N/A- Existing	
<input type="checkbox"/>	<p>6. Sewer Infrastructure: (2.5.4.3F)</p> <ul style="list-style-type: none"> • Size, type and location of sanitary sewage facilities & Engineering data, including any onsite temporary facilities during construction period. 	N/A- Existing	

<input type="checkbox"/>	7. Utilities: (2.5.4.3G) <ul style="list-style-type: none"> The size, type and location of all above & below ground utilities; Size type and location of generator pads, transformers and other fixtures. 	Existing- No Change	
<input type="checkbox"/>	8. Solid Waste Facilities: (2.5.4.3H) <ul style="list-style-type: none"> The size, type and location of solid waste facilities. 	Existing Conditions Plan	
<input type="checkbox"/>	9. Storm water Management: (2.5.4.3I) <ul style="list-style-type: none"> The location, elevation and layout of all storm-water drainage. The location of onsite snow storage areas and/or proposed off-site snow removal provisions. Location and containment measures for any salt storage facilities Location of proposed temporary and permanent material storage locations and distance from wetlands, water bodies, and stormwater structures. 	Drainage Analysis	
<input type="checkbox"/>	10. Outdoor Lighting: (2.5.4.3J) <ul style="list-style-type: none"> Type and placement of all lighting (exterior of building, parking lot and any other areas of the site) and photometric plan. 	No Change	
<input type="checkbox"/>	11. Indicate where dark sky friendly lighting measures have been implemented. (10.1)		
<input type="checkbox"/>	12. Landscaping: (2.5.4.3K) <ul style="list-style-type: none"> Identify all undisturbed area, existing vegetation and that which is to be retained; Location of any irrigation system and water source. 	N/A	
<input type="checkbox"/>	13. Contours and Elevation: (2.5.4.3L) <ul style="list-style-type: none"> Existing/Proposed contours (2 foot minimum) and finished grade elevations. 	Grading Plan	
<input type="checkbox"/>	14. Open Space: (2.5.4.3M) <ul style="list-style-type: none"> Type, extent and location of all existing/proposed open space. 	Site Plan	
<input type="checkbox"/>	15. All easements, deed restrictions and non-public rights of ways. (2.5.4.3N)	Existing Conditions Plan	
<input type="checkbox"/>	16. Character/Civic District (All following information shall be included): (2.5.4.3P) <ul style="list-style-type: none"> Applicable Building Height (10.5A21.20 & 10.5A43.30); Applicable Special Requirements (10.5A21.30); Proposed building form/type (10.5A43); Proposed community space (10.5A46). 	N/A	
<input type="checkbox"/>	17. Special Flood Hazard Areas (2.5.4.3Q) <ul style="list-style-type: none"> The proposed development is consistent with the need to minimize flood damage; All public utilities and facilities are located and construction to minimize or eliminate flood damage; Adequate drainage is provided so as to reduce exposure to flood hazards. 	N/A	

Other Required Information			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	Traffic Impact Study or Trip Generation Report, as required. (3.2.1-2)	Application Package	
<input type="checkbox"/>	Indicate where Low Impact Development Design practices have been incorporated. (7.1)	Grading Plan	
<input type="checkbox"/>	Indicate whether the proposed development is located in a wellhead protection or aquifer protection area. Such determination shall be approved by the Director of the Dept. of Public Works. (7.3.1)	N/A	
<input type="checkbox"/>	Stormwater Management and Erosion Control Plan. (7.4)	Grading Plan/D1	
<input type="checkbox"/>	Inspection and Maintenance Plan (7.6.5)	Drain Study	

Final Site Plan Approval Required Information			
<input checked="" type="checkbox"/>	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
<input type="checkbox"/>	All local approvals, permits, easements and licenses required, including but not limited to: <ul style="list-style-type: none"> • Waivers; • Driveway permits; • Special exceptions; • Variances granted; • Easements; • Licenses. (2.5.3.2A)	Cover	
<input type="checkbox"/>	Exhibits, data, reports or studies that may have been required as part of the approval process, including but not limited to: <ul style="list-style-type: none"> • Calculations relating to stormwater runoff; • Information on composition and quantity of water demand and wastewater generated; • Information on air, water or land pollutants to be discharged, including standards, quantity, treatment and/or controls; • Estimates of traffic generation and counts pre- and post-construction; • Estimates of noise generation; • A Stormwater Management and Erosion Control Plan; • Endangered species and archaeological / historical studies; • Wetland and water body (coastal and inland) delineations; • Environmental impact studies. (2.5.3.2B)	Online Submission	
<input type="checkbox"/>	A document from each of the required private utility service providers indicating approval of the proposed site plan and indicating an ability to provide all required private utilities to the site. (2.5.3.2D)	Internal Connection	



The State of New Hampshire
DEPARTMENT OF ENVIRONMENTAL SERVICES



Thomas S. Burack, Commissioner

May 8, 2007

Robert F. Fleischmann
P.O. Box 221
Corvallis, Montana 59828

CERTIFICATE OF NO FURTHER ACTION

Subject Site: **Portsmouth - Bob's of Portsmouth, 700 Peverly Hill Road**
DES Site #200107033, Project #11316, Project Type Ether

Dear Mr. Fleischmann:

The New Hampshire Department of Environmental Services (DES) has reviewed the groundwater monitoring analyses completed by Eastern Analytical in 2006. These sample results and the information in the site file were compared with the criteria for issuance of a *Certificate of No Further Action* as contained in New Hampshire Code of Administrative Rules Env-Or 600, *Contaminated Site Management*. These criteria are outlined below:

1. All human health hazards associated with direct exposure to contaminants through dermal contact, ingestion, and inhalation have been eliminated;
2. All necessary activity and use restrictions have been implemented;
3. All sources of groundwater contamination have been eliminated;
4. All on-site and off-site dissolved contamination levels meet groundwater quality criteria as specified in Env-Or 603.01;
5. All recorded release of recordation notices are on file with the DES as required by Env-Or 607.09;
6. All penalty(ies) or fine(s) issued under RSA 146-A, RSA 146-C, RSA 147-A, and RSA 485-C have been paid;
7. All invoices associated with the DES' recoverable cost pursuant to RSA 146-A, RSA 146-C, RSA 147-A, and RSA 485-C have been paid (payment was received at DES offices on April 26, 2007 via check #240337960-1),
8. All fees or costs due under RSA 147-F have been paid.

The DES has concluded that the conditions at this site meet the above closure criteria. Therefore, in accordance with Env-Or 609.02, DES hereby issues this *Certificate of No Further Action* for this site. Through issuance of this *Certificate of No Further Action*,

Robert Fleischmann
DES #200107033
May 8, 2007
Page 2 of 2

DES certifies that no additional investigation, remedial measures, or groundwater monitoring will be required by the DES for this site. Accordingly, DES will remove this site from our active project list and close the regulatory site file.

The DES reserves the right, under New Hampshire Code of Administrative Rules Env-Or 600 *Contaminated Site Management*, to require additional investigations, remedial measures, or groundwater monitoring if further information indicating the need for such work becomes known.

Monitoring Wells

As previously discussed in the April 6, 2007 intent to close letter, DES recommends that the groundwater monitoring wells be decommissioned. If the monitoring wells are not decommissioned, they need to be properly maintained in accordance with the requirements discussed in Env-Or 610.04(a).

If you should have any questions, please contact me immediately.

Sincerely,



Gary S. Lynn, P.E.
Oil Remediation and Compliance Bureau
Tel: (603) 271-8873
Fax: (603) 271-2181
Email: glynn@des.state.nh.us

cc: Portsmouth Health Officer
Robert Bradfield, Esq.
Glen Graper, Esq.



200 Griffin Road, Unit 3, Portsmouth, NH 03801
Phone (603) 430-9282 Fax 436-2315

16 July, 2023

Trip Generation Calculation
Proposed Site Improvements: Portsmouth Auto Body
700 Peverly Hill Road
Portsmouth, NH

Introduction

Ambit Engineering - Haley Ward has prepared this *Trip Generation Calculation* for the proposed site improvements at 700 Peverly Hill Road (Portsmouth Auto Body) in Portsmouth, NH. The site is accessed via West Road and is located at the intersection of West and Peverly Hill Roads. The purpose of this calculation is to identify the net change in vehicle trips expected to be generated by the building addition at the project site. Currently, the site contains two buildings, a 9,627 square foot building fronting Peverly Hill Road and a 12,066 square foot building fronting West Road. The project proposes to expand the West Road building with six additional service bay lifts in a proposed 3,456 square foot addition. The six-service bay lifts addition will be constructed on top of the existing parking lot on the east side of the building. No changes to ingress, egress, or directional traffic flow are proposed.

Existing Conditions

The subject property is owned by JMK Realty, LLC. The parcel is 4.20 acres and located in the Industrial Zoning District. The property is separated from Peverly Hill Road and West Roads by a landscaped area with planted trees. Portsmouth Public Works is located on the west side of the property. Located to the south is a commercial building housing multiple business. There are two paved entrances located on West Road to access the property. There is no history of fatal accidents at this location in the last ten years.

The subject property's immediate neighborhood is a moderately-high trafficked area close to the Lafayette Road (US Route 1) intersection. Peverly Hill Road connects US Route 1 and NH Route 33 – Greenland Road. According to the NH-DOT Transportation Data Management System, the average daily traffic count 1/2 mile north on Lafayette Road is approximately 24,000 vehicles, and at the northwesterly end of Peverly Hill Road the daily traffic count is approximately 8,600 vehicles.

Proposed Condition

The project proposes to expand the West Road building with six additional service bay lifts in a proposed 3,456 square foot addition. The six-service bay footprint addition will be constructed on top of the existing parking lot (and over some existing open space) on the east side of the building. Some pavement will be removed to mimic the existing impervious surface coverage at the site. No changes to ingress, egress, or directional traffic flow are proposed.

Trip Generation

In developing the expected trips Ambit Engineering – Haley Ward considered the standard trip generation rates and equations published in the Institute of Transportation Engineers (ITE) Trip Generation Manual. The calculations are provided for the AM and PM Peak hour of Generator. The trips for the existing Peverly Hill building remain the same in the pre and post analysis. The land use category that best correlates with the use is “Automobile Care Center” (ITE Land Use Code 942), applied to the site in the existing condition (combined 9,627 square foot and 12,066 square foot buildings for a total square footage of 21, 693). The land use category that best correlates with the six additional service bay addition is “Tire Store” (ITE Land Use Code 848), due to the addition being car lift stations. This code is applied to the proposed 3,456 square foot addition on the east side of the West Road building. The trip rates, based upon the square footage of the buildings are calculated using the ITE Trip Generation Software (see attached printouts). The results are summarized below for the **Weekday AM and PM Peak Hour**:

Trip Generation Summary

Current Use

Automobile Care Center (2.83 trips X 21.693 S.F.)	<u>62 trips AM Peak</u>
Automobile Care Center (3.51 trips X 21.693 S.F.)	<u>76 trips PM Peak</u>

Total 62 AM and 76 PM Trips

Proposed Use

Automobile Care Center (2.83 trips X 21.693 S.F.)	<u>62 trips AM Peak</u>
Automobile Care Center (3.51 trips X 21.693 S.F.)	<u>76 trips PM Peak</u>

Tire Store (3.56 trips X 3.456 S.F.)	<u>12 trips AM Peak</u>
Tire Store (3.72 trips X 3.456 S.F.)	<u>13 trips PM Peak</u>

Total 74 AM and 89 PM Trips

Trip Generation Impact

The increase trip generation anticipated with this project is **12 new AM trips and 13 new PM trips**. When compared to the existing traffic conditions, this results in a modest increase in proposed trips. The anticipated increase in trips is negligible and does not substantially alter the traffic conditions in the adjacent roadway system. The corridor is designed and zoned for uses such as the proposed project.

Conclusions

- Currently, the site contains a 9,627 square foot and 12,066 square foot auto body repair buildings (Portsmouth Auto Body).
- The project proposes to expand the West Road building with six additional service bay lifts with a 3,456 square foot building addition. The six-service bay lift addition will be constructed on top of the existing parking lot on the east side of the building.

- According to the NH-DOT Transportation Data Management System, the average daily traffic count at the northwesterly end of Peverly Hill Road is approximately 8,600 vehicles
- The increase trip generation anticipated with this project is **12 new AM trips and 13 new PM trips**. When compared to the existing Peverly Hill Road traffic conditions, this results in a modest 0.3 % increase in proposed trips. The local road network surrounding the site can easily accommodate the increase trips generated.

Based on the findings above, the proposed Service Bay Addition can be safely and efficiently accommodated along the existing roadway network without off-site improvements. Please feel free to call if you have any questions or comments.

Sincerely,



John Chagnon, PE
Vice President
Ambit Engineering – Haley Ward

Land Use: 942

Automobile Care Center

Description

An automobile care center houses numerous businesses that provide automobile-related services, such as repair and servicing, stereo installation, and seat cover upholstery. Quick lubrication vehicle shop (Land Use 941) and automobile parts and service center (Land Use 943) are related uses.

Additional Data

The sites were surveyed in the 1980s and the 1990s in California and Florida.

Source Numbers

267, 273, 439, 715

Automobile Care Center (942)

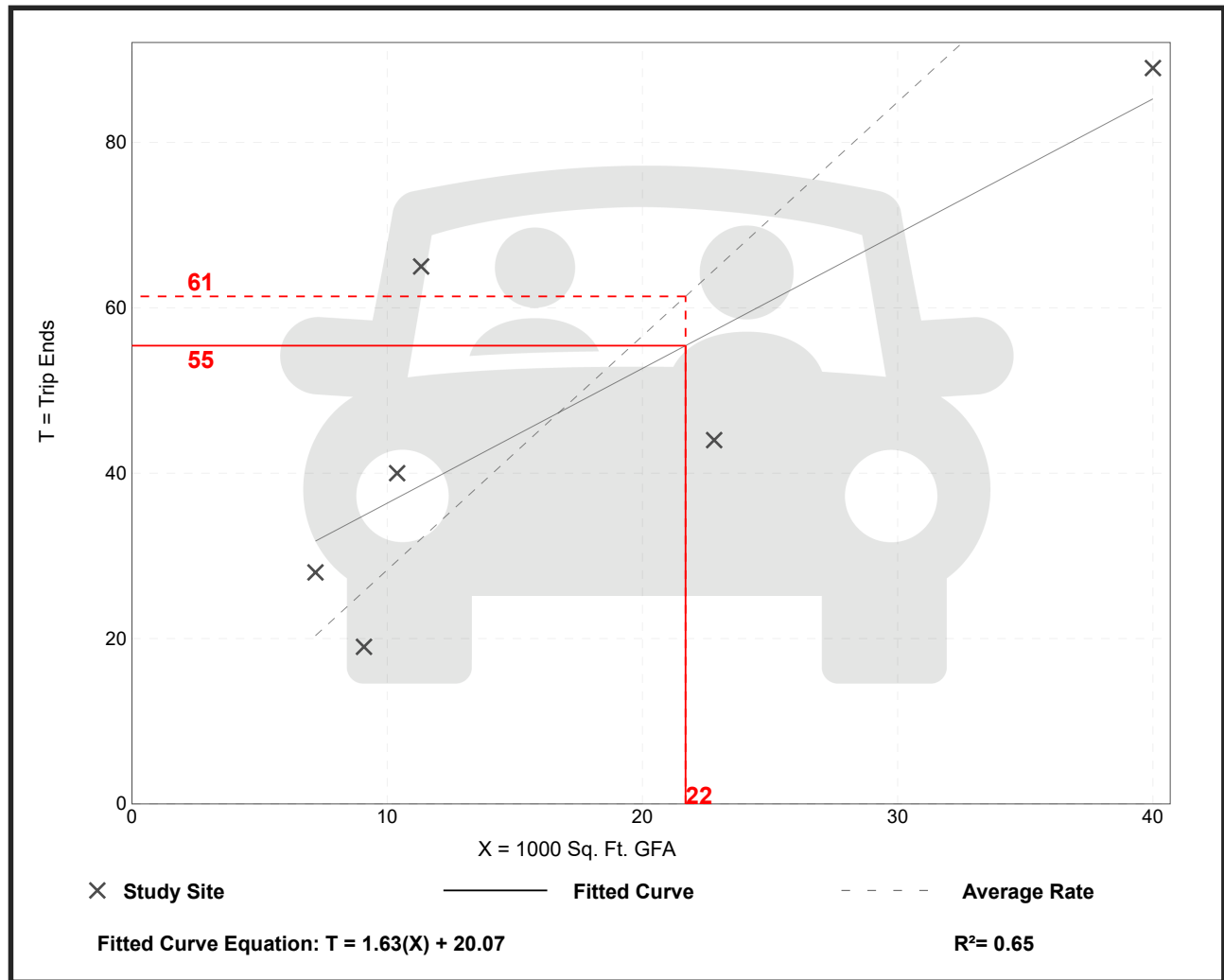
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
AM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 6
 Avg. 1000 Sq. Ft. GFA: 17
 Directional Distribution: 56% entering, 44% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
2.83	1.93 - 5.74	1.35

Data Plot and Equation



Automobile Care Center (942)

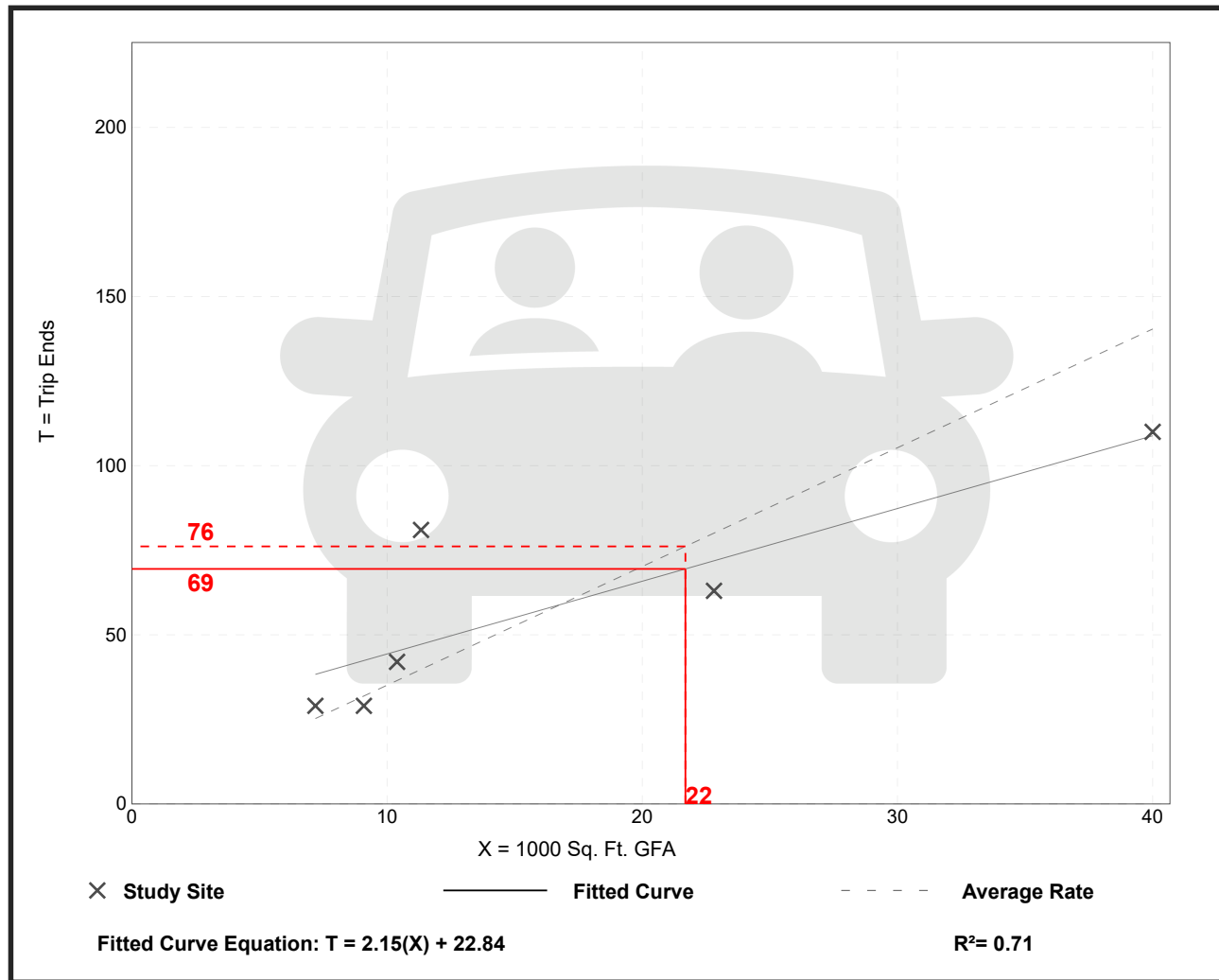
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
PM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 6
 Avg. 1000 Sq. Ft. GFA: 17
 Directional Distribution: 49% entering, 51% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
3.51	2.75 - 7.15	1.51

Data Plot and Equation



Automobile Care Center (942)

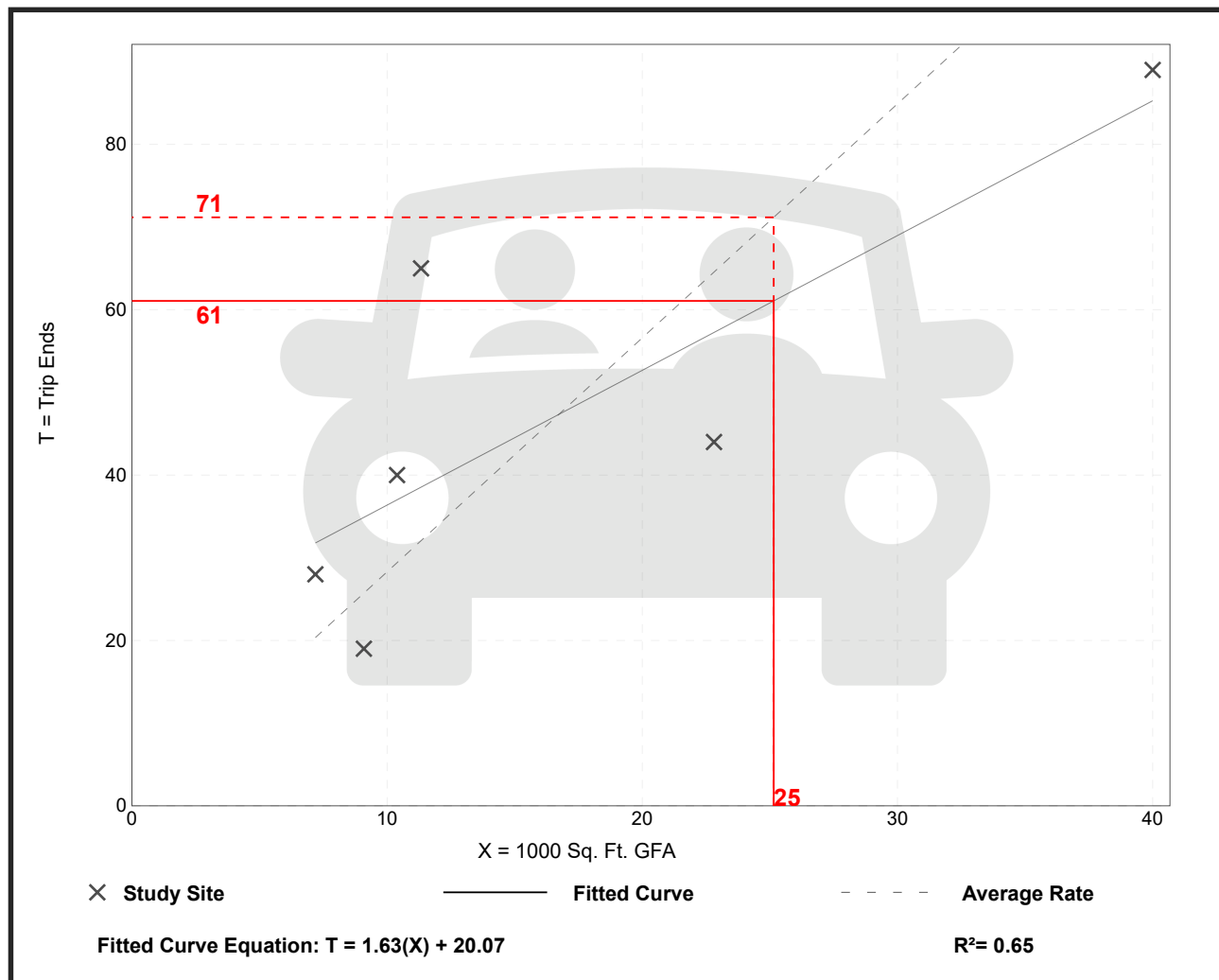
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
AM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 6
 Avg. 1000 Sq. Ft. GFA: 17
 Directional Distribution: 56% entering, 44% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
2.83	1.93 - 5.74	1.35

Data Plot and Equation



Automobile Care Center (942)

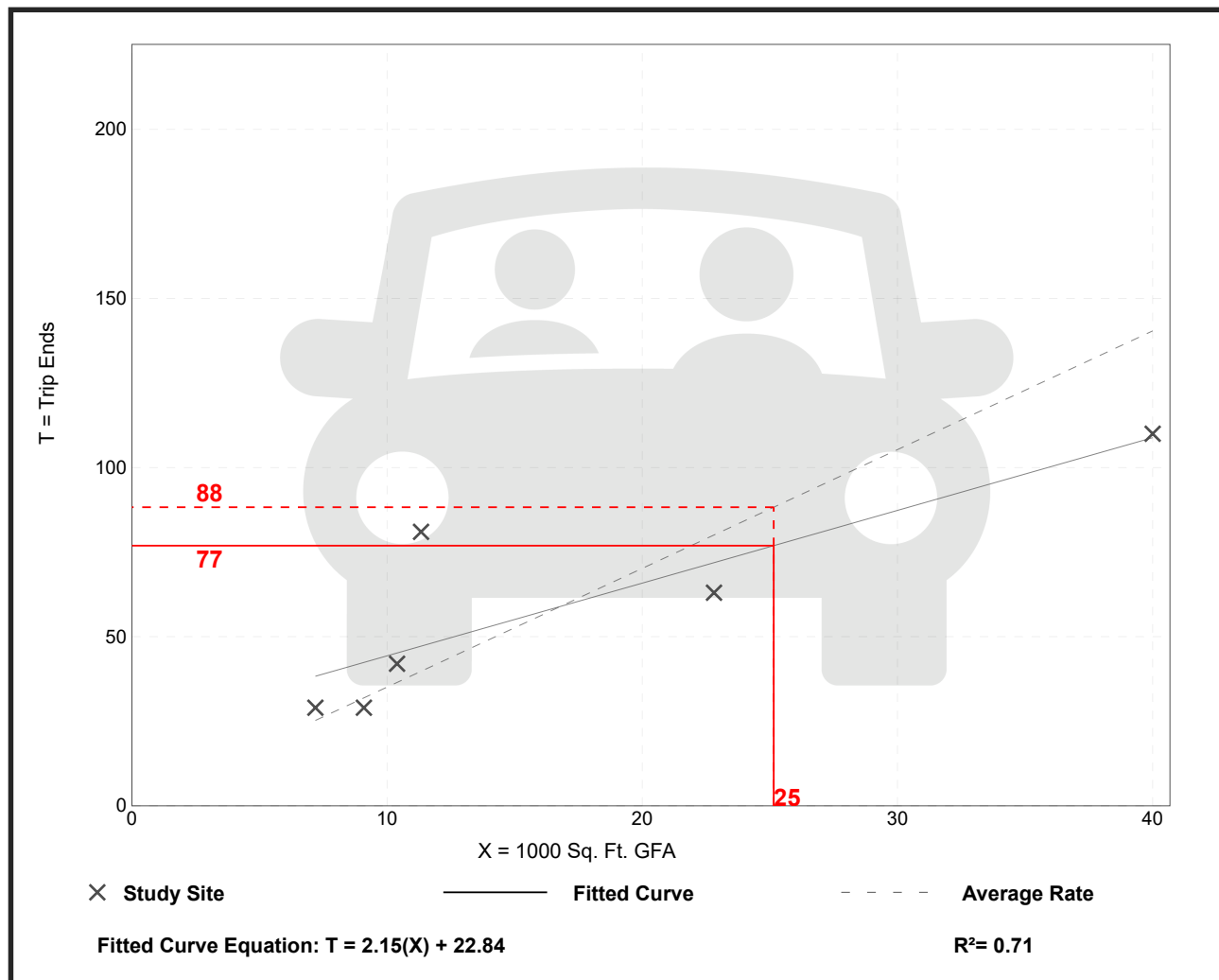
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
PM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 6
 Avg. 1000 Sq. Ft. GFA: 17
 Directional Distribution: 49% entering, 51% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
3.51	2.75 - 7.15	1.51

Data Plot and Equation



Land Use: 848

Tire Store

Description

The primary business associated with a tire store is the sale of tires for automotive vehicles. Services offered by these stores usually include tire installation and repair, as well as other automotive maintenance or repair services and customer assistance. These stores generally do not contain large storage or warehouse areas. Automobile parts sales (Land Use 843), tire superstore (Land Use 849), and automobile parts and service center (Land Use 943) are related uses.

Additional Data

The technical appendices provide supporting information on time-of-day distributions for this land use. The appendices can be accessed through either the ITETripGen web app or the trip generation resource page on the ITE website (<https://www.ite.org/technical-resources/topics/trip-and-parking-generation/>).

The sites were surveyed in the 1980s, the 1990s, the 2000s, and the 2010s in Florida, Minnesota, New Jersey, New York, Oregon, Pennsylvania, South Dakota, Texas, and Wisconsin.

Source Numbers

328, 359, 438, 555, 571, 583, 599, 870, 886, 887, 959, 1049

Tire Store (848)

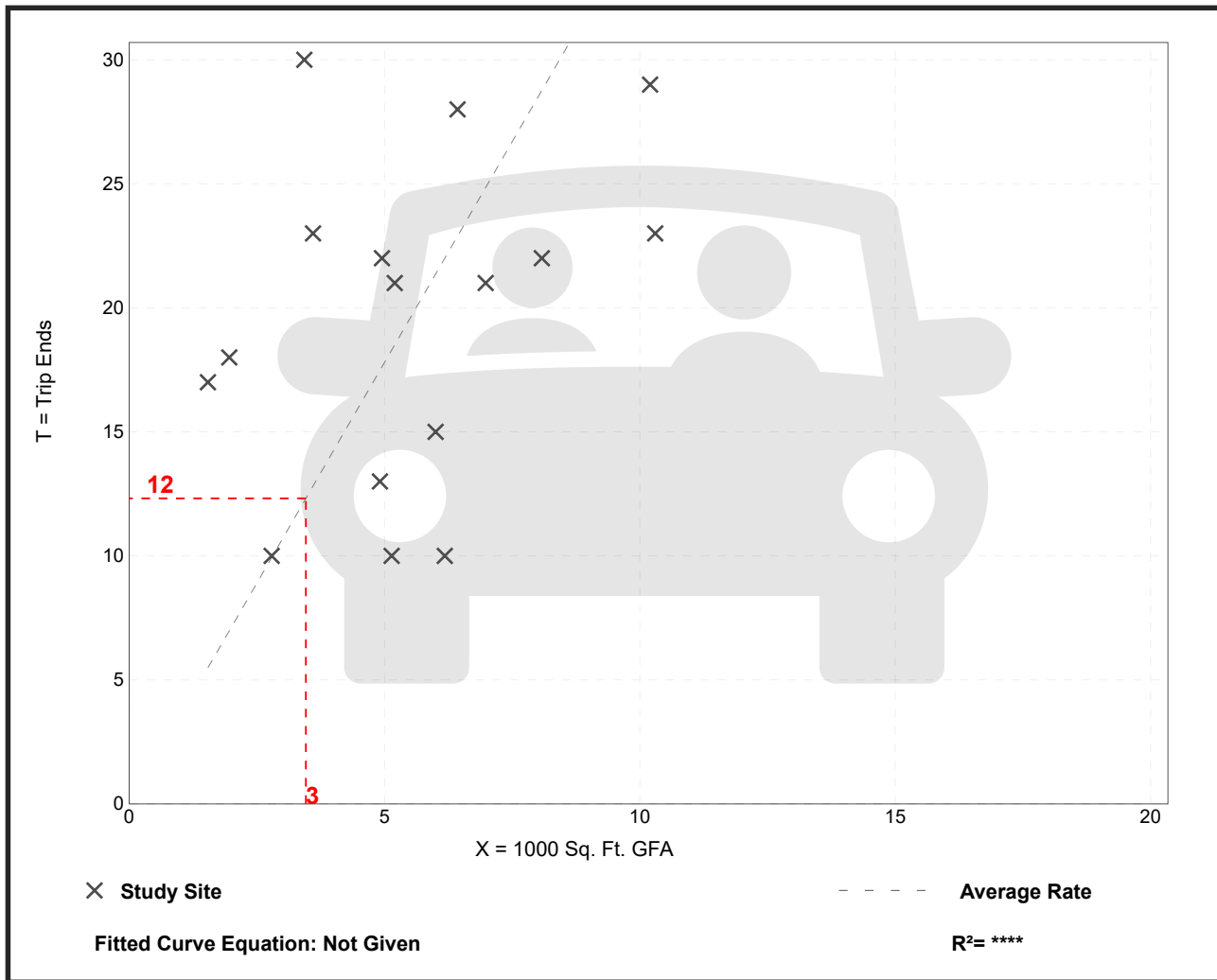
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
AM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 16
 Avg. 1000 Sq. Ft. GFA: 5
 Directional Distribution: 51% entering, 49% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
3.56	1.62 - 11.02	2.08

Data Plot and Equation



Tire Store (848)

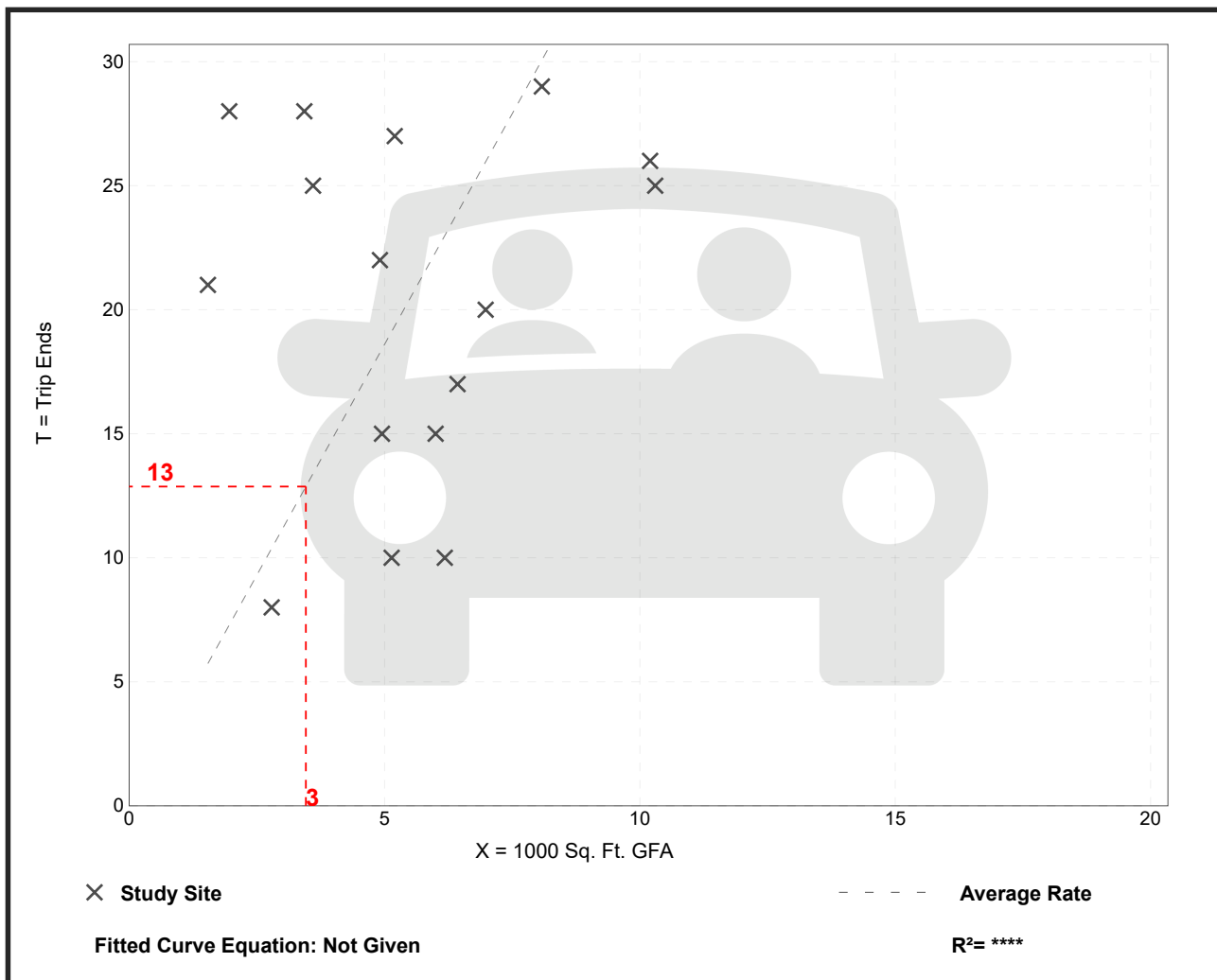
Vehicle Trip Ends vs: 1000 Sq. Ft. GFA
On a: Weekday,
PM Peak Hour of Generator

Setting/Location: General Urban/Suburban
 Number of Studies: 16
 Avg. 1000 Sq. Ft. GFA: 5
 Directional Distribution: 46% entering, 54% exiting

Vehicle Trip Generation per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	Standard Deviation
3.72	1.62 - 14.29	2.68

Data Plot and Equation





200 Griffin Road, Unit 3, Portsmouth, NH 03801
 Phone (603) 430-9282 Fax 436-2315

16 July, 2023

**Parking Demand
 Proposed Site Improvements
 Portsmouth Auto Body
 700 Peverly Hill Road
 Portsmouth, NH**

The purpose of this calculation is to identify the existing and proposed parking demand expected to be generated by the site improvements at 700 Peverly Hill Road. Currently, the site contains two buildings, a 9,627 square foot building fronting Peverly Hill Road and a 12,066 square foot building fronting West Road. The project proposes to expand the West Road building with six additional service bay lifts in a proposed 3,456 square foot addition.

In developing the expected parking demand Ambit Engineering considered the standard Parking Demand rates and equations published in the Institute of Transportation Engineers (ITE) Parking Generation Manual, 5th Edition. The land use category that best correlates with the proposed uses are Automobile Parts and Service Center (ITE Land Use Code 943) and Tire Store (ITE Land Use Code 848). Please note that there is no Parking Demand ITE Rate for an Automobile Care Center. The ITE Rates of peak parking demand are for non-overlapping peak periods of demand; the Automobile Parts and Service Center being 10:00 AM to 4:00 PM and the Tire Store 11:00 AM to 2:00 PM. This makes the total numbers calculated more conservative. The parking demand, based upon the GFA of the existing and proposed buildings are summarized below for the **Average Peak Period of Parking Demand:**

Parking Demand Summary - EXISTING

Peak Period of Demand

Automobile Parts and Service Center (1.69 vehicles per 1,000 SF GFA)	<u>1.69 x 21.693 KSF = 37 vehicles</u>
---	--

Total Parking Spaces required	<u>37 vehicles</u>
-------------------------------	--------------------

Parking Demand Summary - PROPOSED

Peak Period of Demand

Automobile Parts and Service Center (1.69 vehicles per 1,000 SF GFA)	<u>1.69 x 21.693 KSF = 37 vehicles</u>
---	--

Tire Store (2.85 vehicles per 1,000 SF GFA)	<u>2.85 x 3.456 KSF = 10 vehicles</u>
--	---------------------------------------

Total Parking Spaces required	<u>47 vehicles</u>
-------------------------------	--------------------

Based on the calculation there is an anticipated minor increase in parking demand of 10 vehicles with this project. The site can easily accommodate the additional parking requirement.

Please feel free to call if you have any questions or comments.

Sincerely,

A handwritten signature in black ink, appearing to read 'JRC', with a long horizontal flourish extending to the right.

John R. Chagnon, PE
Ambit Engineering – Haley Ward

Automobile Parts and Service Center (943)

Peak Period Parking Demand vs: 1000 Sq. Ft. GFA

On a: **Weekday (Monday - Friday)**

Setting/Location: General Urban/Suburban

Peak Period of Parking Demand: 10:00 a.m. - 4:00 p.m

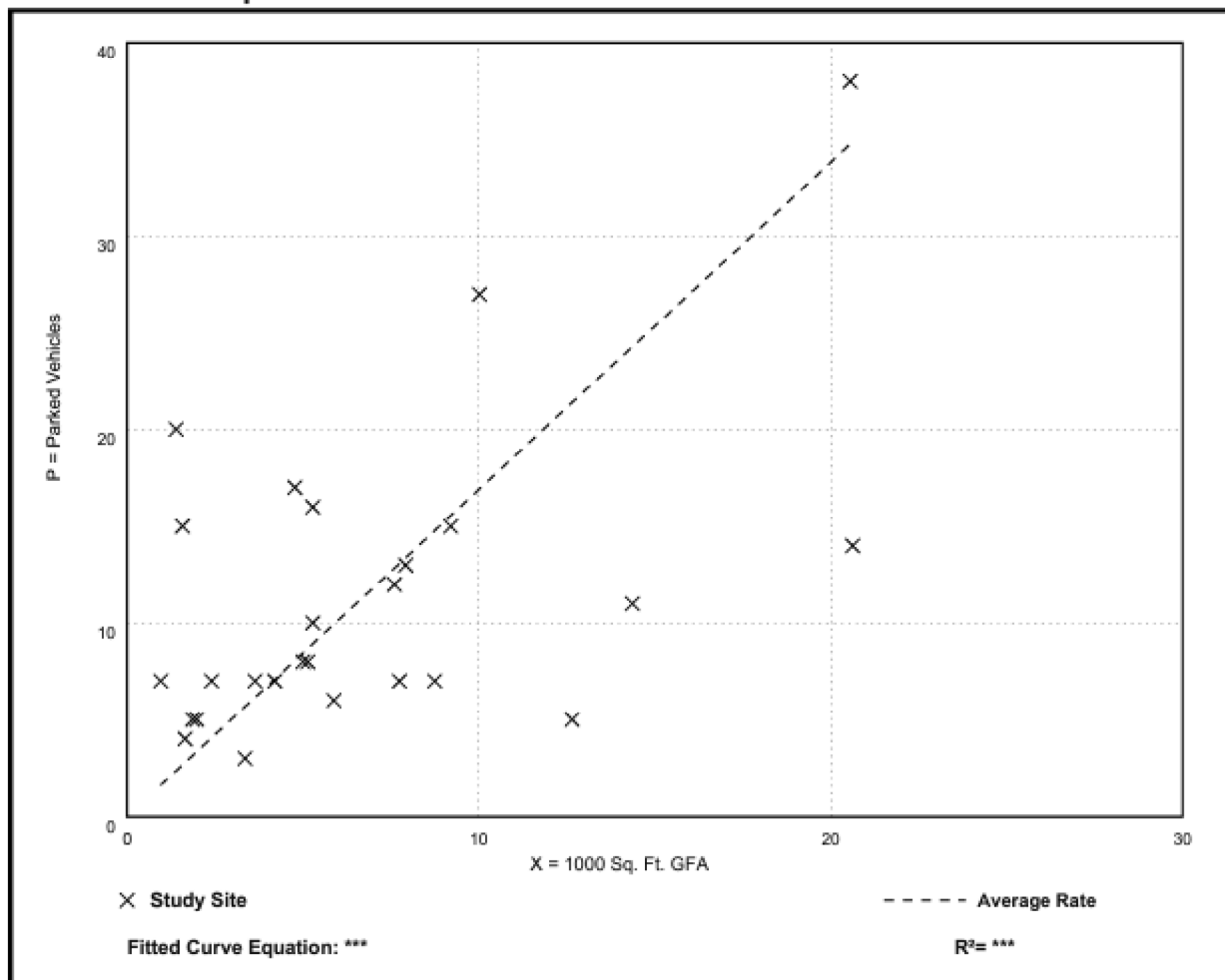
Number of Studies: 26

Avg. 1000 Sq. Ft. GFA: 6.7

Peak Period Parking Demand per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	33rd / 85th Percentile	95% Confidence Interval	Standard Deviation (Coeff. of Variation)
1.69	0.40 - 14.37	1.58 / 3.54	1.05 - 2.33	1.67 (99%)

Data Plot and Equation



Tire Store (848)

Peak Period Parking Demand vs: 1000 Sq. Ft. GFA

On a: Weekday (Monday - Friday)

Setting/Location: General Urban/Suburban

Peak Period of Parking Demand: 11:00 a.m. - 2:00 p.m.

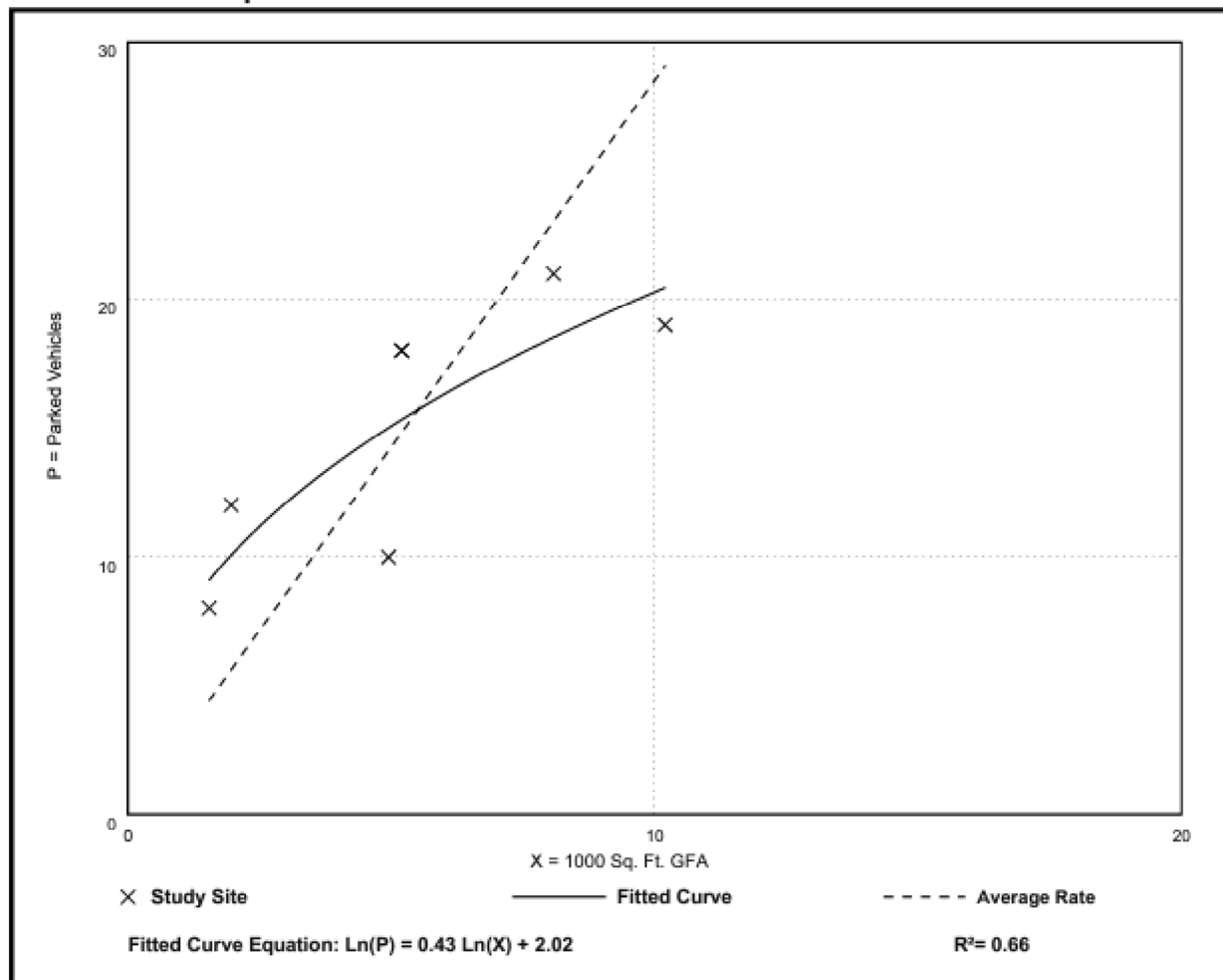
Number of Studies: 7

Avg. 1000 Sq. Ft. GFA: 5.3

Peak Period Parking Demand per 1000 Sq. Ft. GFA

Average Rate	Range of Rates	33rd / 85th Percentile	95% Confidence Interval	Standard Deviation (Coeff. of Variation)
2.85	1.86 - 6.12	2.39 / 5.94	***	1.22 (43%)

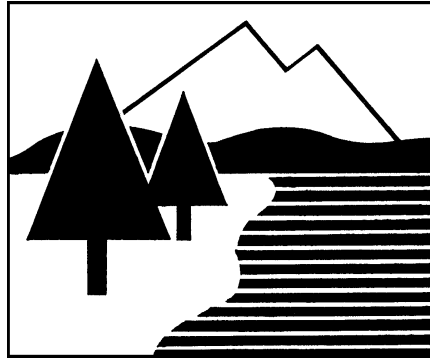
Data Plot and Equation



DRAINAGE ANALYSIS

PROPOSED BUILDING ADDITION

**700 PEVERLY HILL ROAD
PORTSMOUTH, NH**



**PREPARED FOR
PORTSMOUTH AUTO BODY CENTER**

17 JULY 2023



200 Griffin Road, Unit 3
Portsmouth, NH 03801
Phone: 603.430.9282; Fax: 603.436.2315
E-mail: jchagnon@haleyward.com
(Ambit Job Number 5010265.3576)

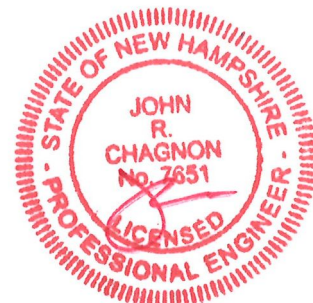


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EXECUTIVE SUMMARY

This drainage analysis examines the pre-development (existing) and post-development (proposed) stormwater drainage patterns for the Building Addition at the property known as 700 Peverly Hill Road in Portsmouth, NH. The site is shown on the City of Portsmouth Assessor's Tax Map 252 as Lot 2-10. The total size of the combined lots and drainage area is 297,341± square feet (6.826 acres).

The development will provide for a building addition, parking, and associated utilities. The development has the potential to increase stormwater runoff to adjacent properties and should be designed in a manner to prevent that occurrence. The site addition will result in no net increase in impervious area. The site contains two existing buildings which will be maintained through development. The proposed stormwater BMPs will offset any potential impact caused by the development.

The hydrologic modeling utilized for this analysis uses the "Extreme Precipitation" values for rainfall from The Northeast Regional Climate Center (Cornell University), with a 15% increase to comply with local ordinance. The drainage design uses the 10-Year storm in accordance with the New Hampshire Stormwater Manual, but was designed for anticipated inundation in excess of the 50-Year storm.

INTRODUCTION / PROJECT DESCRIPTION

This drainage report is designed to assist the owner, contractor, regulatory reviewer, and others in understanding the impact of the proposed development project on local surface water runoff and quality. The project site is shown on the City of Portsmouth Assessor's Tax Map 252 as Lot 2-10. Bounding the site to the west is City property (DPW Facility). Bounding the site to the North is Peverly Hill Road and commercial property. Bounding the site to the east is West Road followed by commercial property. Bounding the site to the south is commercial property. A vicinity map is included in the Appendix to this report. The proposed project includes a building addition with associated paving and utilities. This report uses the plans of the future improvements on the proposed lot to design the site drainage, as required by the City.

This report includes information about the existing site and the proposed site necessary to analyze stormwater runoff and to design the mitigation. The report includes impervious surface analyses and the associated operations and maintenance manual. The report will provide a narrative of the stormwater runoff. Proposed stormwater management and treatment structures and methods will also be described, as well as erosion and sediment control practices. To fully understand the proposed site development the reader should also review a complete site plan set in addition to this report.

METHODOLOGY

"Extreme Precipitation" values from The Northeast Regional Climate Center (Cornell University) have been used for modeling purposes. These values have been used in this analysis, with a 15% addition to comply with local ordinances.

This report uses the US Soil Conservation Service (SCS) Method for estimating stormwater runoff. The SCS method is published in The National Engineering Handbook (NEH), Section 4 "Hydrology" and includes the Technical Release No. 20, (TR-20) "Computer Program for Project Formulation Hydrology", and Technical Release No. 55 (TR-55) "Urban Hydrology for Small Watersheds" methods. This report uses the HydroCAD version 10.20 program, written by HydroCAD Software Solutions LLC, Chocorua, N.H., to apply these methods for

the calculation of runoff and for pond modeling. Rainfall data and runoff curve numbers are taken from “The Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire.”

Time of Concentration (Tc) is calculated by entering measured flow path data such as flow path type, length, slope and surface characteristics into the HydroCAD program. For the purposes of this report, a minimum time of concentration of 5 minutes is used.

The storm events used for the calculations in this report are the 2-year, 10-year, 25-year, and 50-year (24-hour) storms. Watershed basin boundaries have been delineated using topographic maps prepared by Ambit-Haley Ward and field observations to confirm.

SITE SPECIFIC INFORMATION

Based on the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS), Soil Survey of Rockingham County, New Hampshire the location of development is made up of one soil type:

Soil Symbol	Soil Name and Slopes
299	Udorthents, smoothed

Udorthents is stated to be excessively drained with a depth to water table and restrictive feature of more than 80 inches. There is no Hydrologic Soil Group (HSG) given, so an HSG of B was assumed. These are known disturbed soils.

The physical characteristics of the site consist of flat (0-8%) grades that generally slope from east to west of the property. Elevations on the site range from 40 to 52 feet above sea level. The existing site is developed and includes two existing buildings near the center of the lot. Vegetation consists of established grasses and shrubs.

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) number 33015C0270F (effective date January 29, 2021), the proposed development is located in Zone X and is outside the flood hazard zone. A copy of the FIRM map is included in the Appendix.

PRE-DEVELOPMENT DRAINAGE

In the pre-development condition, the site has been analyzed as three subcatchment basins (E1, E1a and E2) based on localized topography and discharge location. All subcatchments flow toward the southwest corner of the property and either infiltrate into the native soil or are discharged through two overflow pipes (Discharge Point 1, or DP1). The height and volume of the depression is substantial enough to contain the 50-Year storm without overflowing. Subcatchment E1 contains the majority of the property including the proposed development as well as off-site drainage (DPW). Subcatchment E1a is a subsection of E1 modelled to estimate the capacity of the onsite drainage network. Subcatchment E2 contains some offsite street drainage area which drains through the onsite drainage network through city drainage infrastructure.

Table 1: Pre-Development Watershed Basin Summary

Watershed Basin ID	Basin Area (SF)	Tc (MIN)	CN	10-Year Runoff (CFS)	50-Year Runoff (CFS)	To Design Point
E1	256,358	13.8	90	33.61	53.47	DP1
E1a	28,397	5.0	98	5.30	8.06	DP1
E2	12,598	5.0	98	2.35	3.57	DP1

POST-DEVELOPMENT DRAINAGE

Proposed subcatchments P1, P1a and P2 occupy the same approximate space as subcatchments E1, E1a, and E2. All subcatchments flow to the same discharge point (DP1). Under the proposed design, there is no increase in impervious area. The existing detention pond has been expanded to increase its infiltrative capacity. Additionally, the on-site swales and drainage network will be updated to meet the conveyance needs of the site. The subcatchments were analyzed for peak discharges using HydroCAD.

Table 2: Post-Development Watershed Basin Summary

Watershed Basin ID	Basin Area (SF)	Tc (MIN)	CN	10-Year Runoff (CFS)	50-Year Runoff (CFS)	Design Point
P1	256,358	13.8	90	33.61	53.47	DP1
P1a	28,397	5.0	98	5.30	8.06	DP1
P2	12,598	5.0	98	2.35	3.57	DP1

The overall impervious coverage of the subcatchment areas analyzed in this report remains **approximately the same** at 140,263 square-feet (76.7%) in the pre-development and post-development conditions. The purpose of this design is to update the on-site drainage from the current inadequate system. Table 3 shows a summary of the comparison between pre-developed flows and post-developed flows for each design point. The comparison shows the reduced flows as a result of the increase in detention pond capacity.

Table 3: Pre-Development to Post-Development Comparison

Design Point	Q2 (CFS)		Q10 (CFS)		Q50 (CFS)		Description
	Pre	Post	Pre	Post	Pre	Post	
DP1	10.02	8.39	11.72	11.05	13.26	12.95	SW Corner

The proposed development has been designed to match the pre-development drainage patterns to the greatest extent feasible. A plan sheet detailing the subcatchments and direction of runoff are included in the Attachments. Discharge Point 1 will experience peak discharge flows and treatment in line with an up-to-date drainage system for all design storms in the proposed condition.

OFFSITE INFRASTRUCTURE CAPACITY

The proposed drainage system update experiences adequate performance due to the increase in detention pond capacity. As a result, there is no anticipated negative impact to City infrastructure.

EROSION AND SEDIMENT CONTROL PRACTICES

The erosion potential for this site as it exists is moderate due to the presence of construction areas that are highly erodible. During construction, the major potential for erosion is wind and stormwater runoff. The contractor will be required to inspect and maintain all necessary erosion control measures, as well as installing any additional measures as required. All erosion control practices shall conform to "The Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire." Some examples of erosion and sediment control measures to be utilized for this project during construction may include:

- Silt Soxx (or approved alternative) located at the toe of disturbed slopes
- Stabilized construction entrance at access point to the site
- Temporary mulching and seeding for disturbed areas
- Spraying water over disturbed areas to minimize wind erosion

After construction, permanent stabilization will be accomplished by permanent seeding, landscaping, compacting/surfacing the access drives with gravel, and the installation of sediment forebays in the detention pond.

CONCLUSION

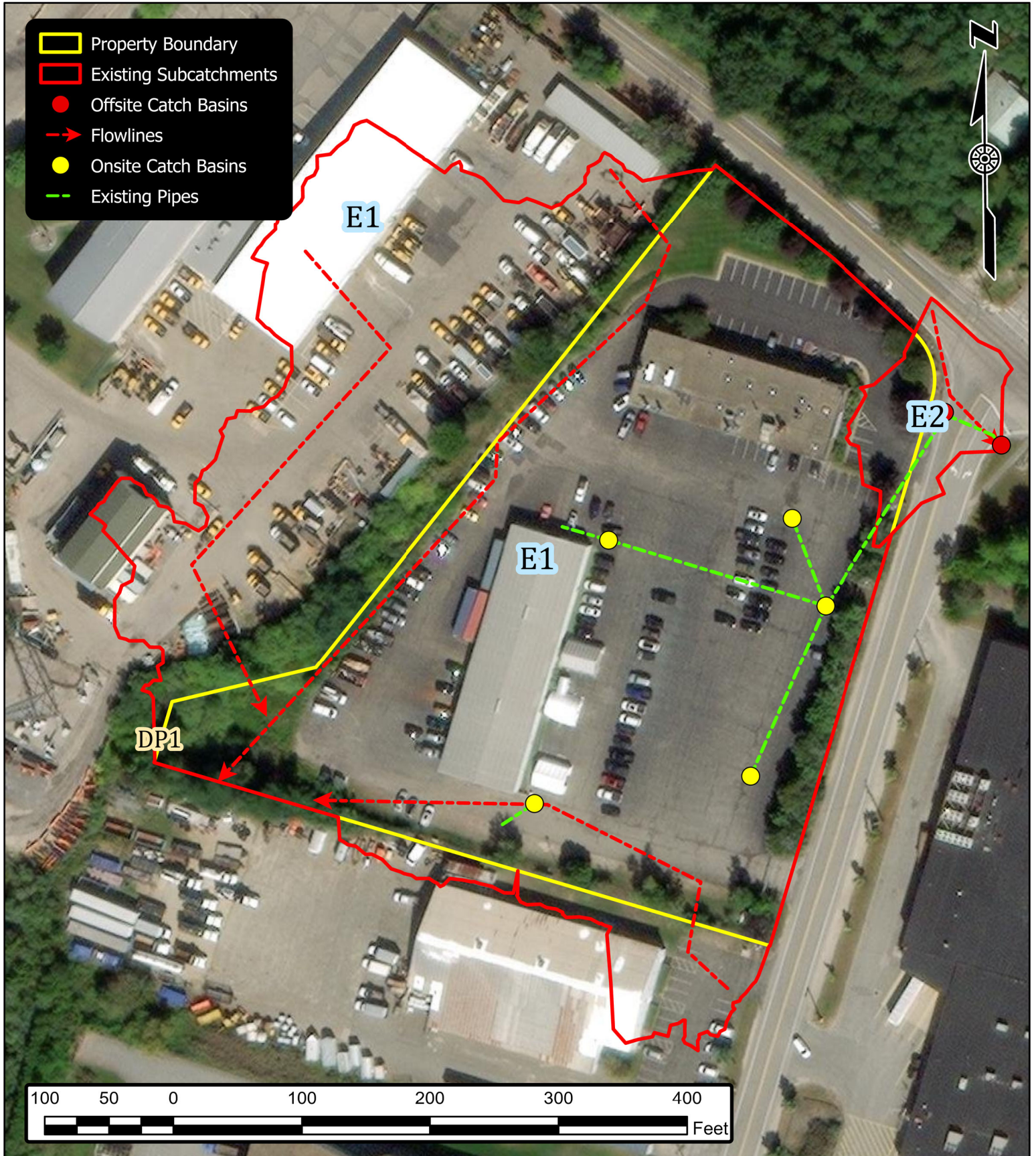
The proposed development has been designed to match the pre-development drainage patterns to the greatest extent feasible. With the increased capacity of the detention pond, and update to the drainage network, the post-development runoff will be sufficiently restored to the condition of a working drainage system. Erosion and sediment control practices will be implemented for both the temporary condition during construction and for final stabilization after construction. Therefore, there are no negative impacts to downstream receptors or adjacent properties anticipated as a result of this project.

REFERENCES

1. Comprehensive Environmental Inc. and New Hampshire Department of Environmental Services. *New Hampshire Stormwater Manual (Volumes 1, 2 and 3)*, December 2008 (Revision 1.0).
2. Minnick, E.L. and H.T. Marshall. *Stormwater Management and Erosion and Sediment Control Handbook for Urban and Developing Areas in New Hampshire*, prepared by Rockingham County Conservation District, prepared for New Hampshire Department of Environmental Services, in cooperation with USDA Soil Conservation Service, August 1992.
3. HydroCAD Software Solution, LLC. *HydroCAD Stormwater Modeling System Version 10.20* copyright 2022.

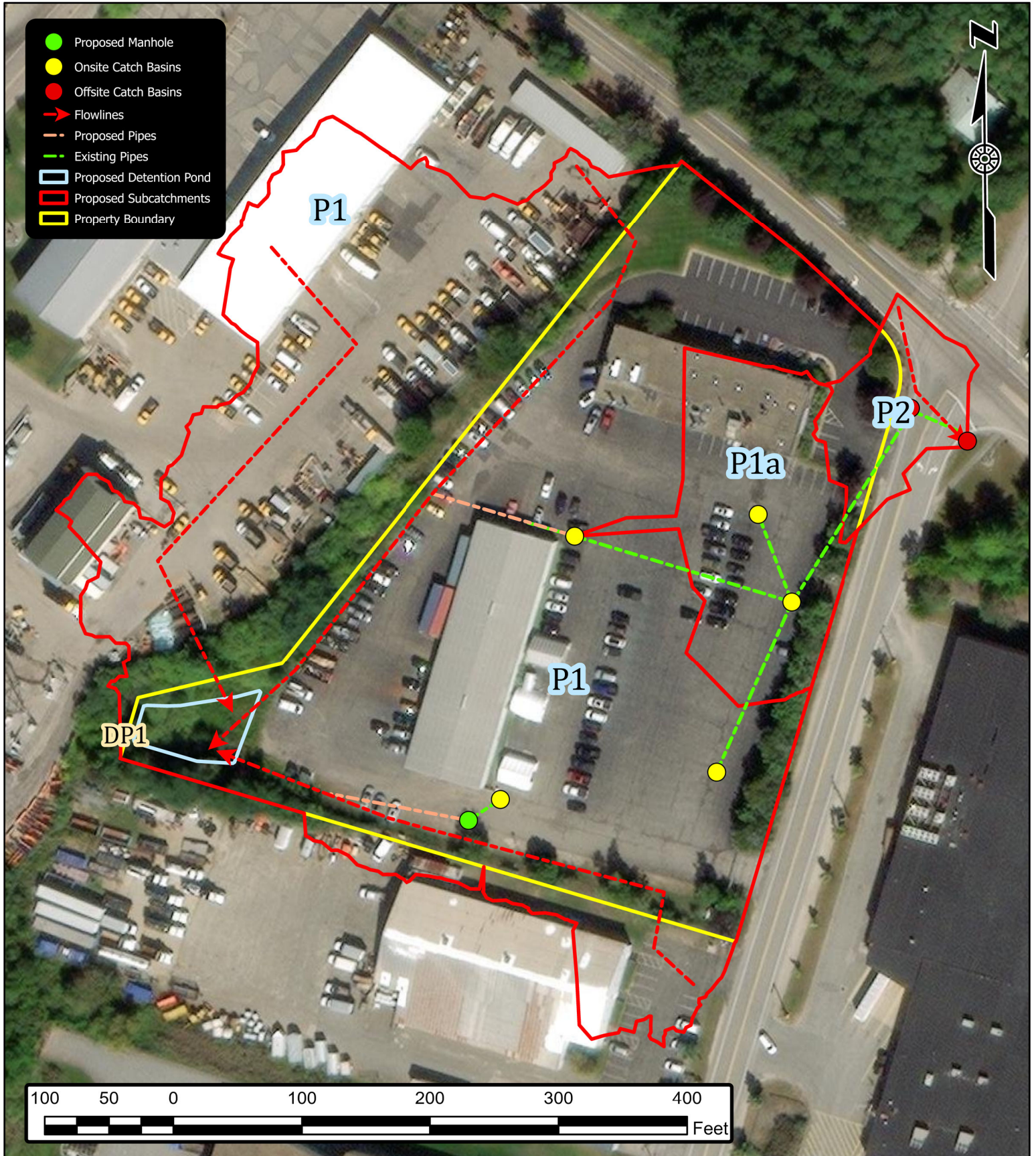
PORTSMOUTH AUTOBODY CENTER
700 PEVERLY HILL ROAD
PORTSMOUTH, NH

JOB NUMBER: 5010265.3576
SCALE: 1" = 100'
SUBMITTED: 07-13-2023



PORTSMOUTH AUTOBODY CENTER
700 PEVERLY HILL ROAD
PORTSMOUTH, NH

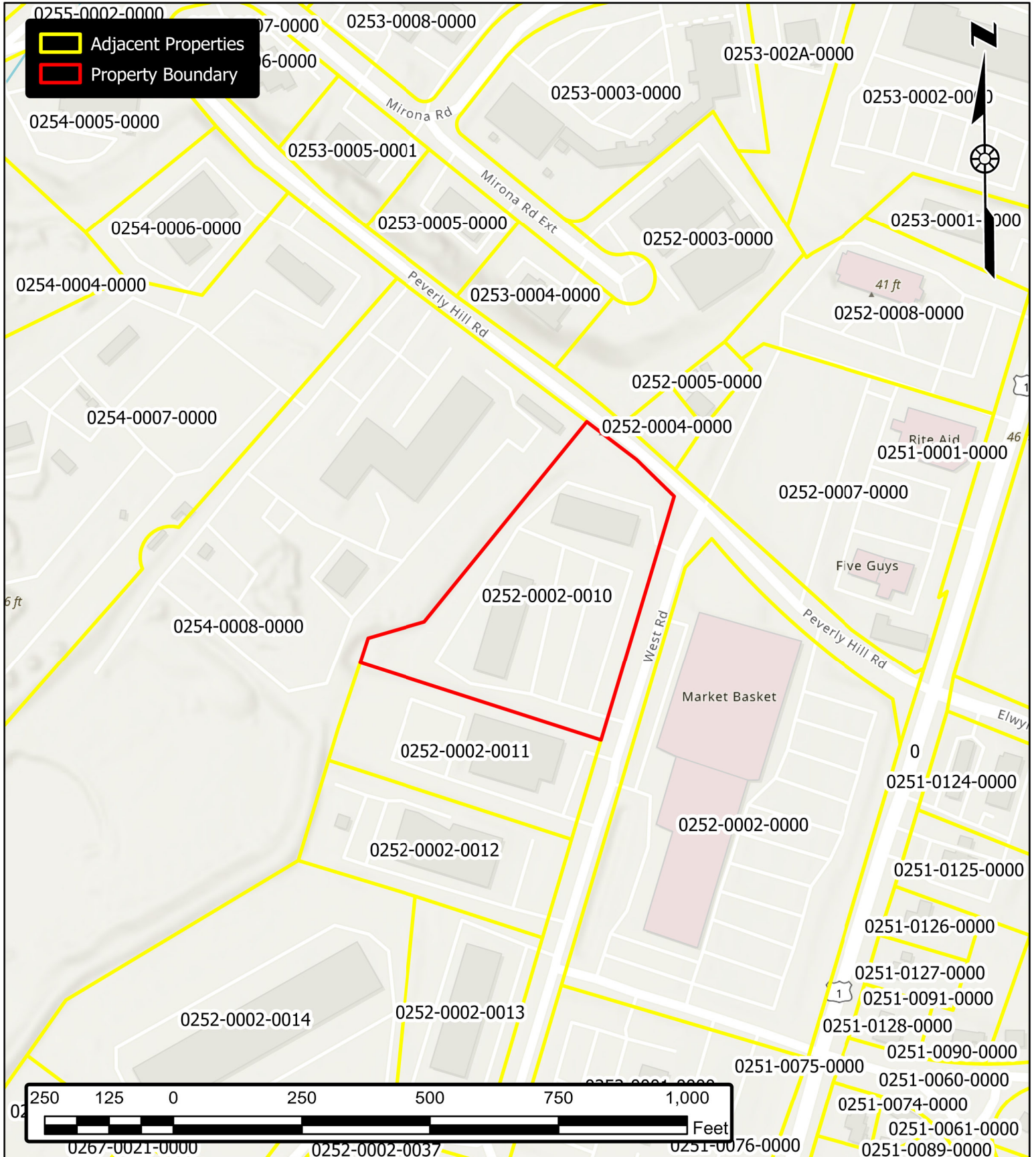
JOB NUMBER: 5010265.3576
SCALE: 1" = 100'
SUBMITTED: 07-13-2023



APPENDIX A
VICINITY (TAX) MAP

PORTSMOUTH AUTOBODY CENTER
700 PEVERLY HILL ROAD
PORTSMOUTH, NH

JOB NUMBER: 5010265.3576
SCALE: 1" = 250'
SUBMITTED: 2023-07-13



PORTSMOUTH AUTOBODY CENTER
700 PEVERLY HILL ROAD
PORTSMOUTH, NH

JOB NUMBER: 5010265.3576
SCALE: 1" = 100'
SUBMITTED: 07-13-2023



APPENDIX B
TABLES, CHARTS, ETC.

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point	
Smoothing State	Yes
Location	
Latitude	43.046 degrees North
Longitude	70.775 degrees West
Elevation	10 feet
Date/Time	Wed Jun 21 2023 11:46:34 GMT-0400 (Eastern Daylight Time)

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.66	0.82	1.04	1yr	0.71	0.98	1.22	1.57	2.04	2.67	2.94	1yr	2.37	2.83	3.24	3.96	4.58	1yr
2yr	0.32	0.50	0.62	0.82	1.02	1.30	2yr	0.88	1.18	1.52	1.94	2.50	3.23	3.59	2yr	2.86	3.45	3.96	4.71	5.36	2yr
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5yr	1.08	1.47	1.89	2.44	3.16	4.09	4.61	5yr	3.62	4.43	5.08	5.97	6.74	5yr
10yr	0.41	0.65	0.82	1.12	1.45	1.90	10yr	1.26	1.73	2.24	2.90	3.77	4.90	5.57	10yr	4.34	5.35	6.13	7.16	8.03	10yr
25yr	0.48	0.76	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.77	6.21	7.15	25yr	5.50	6.87	7.87	9.09	10.12	25yr
50yr	0.54	0.86	1.10	1.54	2.08	2.77	50yr	1.79	2.53	3.30	4.35	5.70	7.44	8.64	50yr	6.59	8.31	9.51	10.90	12.06	50yr
100yr	0.60	0.97	1.25	1.78	2.43	3.27	100yr	2.09	2.99	3.92	5.19	6.81	8.92	10.45	100yr	7.89	10.05	11.49	13.08	14.38	100yr
200yr	0.68	1.11	1.43	2.05	2.84	3.85	200yr	2.45	3.53	4.64	6.17	8.14	10.69	12.64	200yr	9.46	12.16	13.90	15.69	17.16	200yr
500yr	0.80	1.32	1.72	2.50	3.49	4.79	500yr	3.02	4.40	5.80	7.75	10.29	13.59	16.27	500yr	12.03	15.64	17.87	19.97	21.67	500yr

Lower Confidence Limits

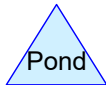
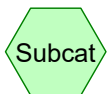
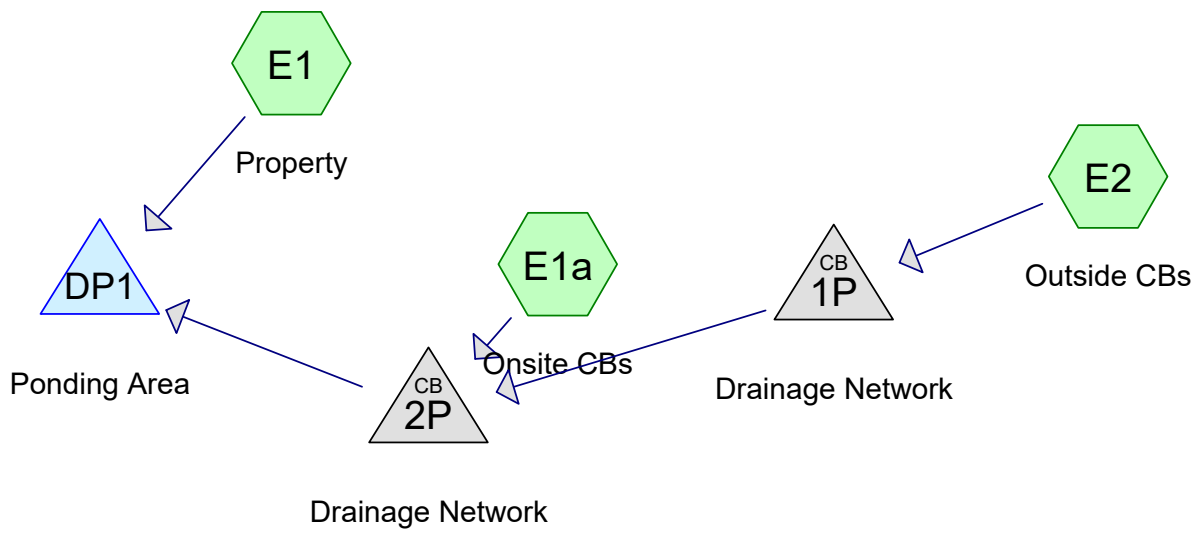
	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.63	0.87	0.92	1.33	1.68	2.25	2.54	1yr	1.99	2.45	2.88	3.18	3.92	1yr
2yr	0.32	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	2.33	3.08	3.48	2yr	2.72	3.35	3.85	4.58	5.11	2yr
5yr	0.35	0.54	0.67	0.92	1.17	1.41	5yr	1.01	1.38	1.61	2.12	2.73	3.82	4.24	5yr	3.38	4.07	4.76	5.59	6.30	5yr
10yr	0.39	0.60	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.81	2.39	3.06	4.41	4.92	10yr	3.91	4.74	5.52	6.49	7.27	10yr
25yr	0.44	0.67	0.84	1.19	1.57	1.91	25yr	1.36	1.86	2.10	2.75	3.53	4.76	5.99	25yr	4.21	5.76	6.77	7.91	8.79	25yr
50yr	0.49	0.74	0.92	1.32	1.78	2.17	50yr	1.54	2.13	2.35	3.07	3.93	5.38	6.93	50yr	4.77	6.66	7.89	9.20	10.16	50yr
100yr	0.54	0.82	1.02	1.48	2.03	2.48	100yr	1.75	2.42	2.63	3.41	4.35	6.06	8.02	100yr	5.36	7.71	9.21	10.72	11.74	100yr
200yr	0.60	0.90	1.14	1.65	2.31	2.83	200yr	1.99	2.76	2.94	3.77	4.79	6.80	9.28	200yr	6.02	8.92	10.75	12.50	13.59	200yr
500yr	0.70	1.04	1.33	1.94	2.75	3.38	500yr	2.38	3.31	3.42	4.31	5.46	7.93	11.25	500yr	7.02	10.82	13.20	15.34	16.47	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.29	0.44	0.54	0.72	0.89	1.09	1yr	0.77	1.06	1.26	1.74	2.20	3.00	3.17	1yr	2.66	3.05	3.60	4.39	5.08	1yr
2yr	0.34	0.52	0.64	0.86	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.51	3.44	3.72	2yr	3.05	3.57	4.10	4.86	5.66	2yr
5yr	0.40	0.62	0.77	1.05	1.34	1.62	5yr	1.16	1.59	1.88	2.53	3.25	4.36	4.97	5yr	3.86	4.78	5.41	6.39	7.18	5yr
10yr	0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.93	2.28	3.10	3.95	5.37	6.20	10yr	4.75	5.97	6.81	7.85	8.77	10yr
25yr	0.58	0.88	1.09	1.56	2.05	2.57	25yr	1.77	2.52	2.95	4.07	5.14	7.82	8.33	25yr	6.92	8.01	9.12	10.35	11.42	25yr
50yr	0.67	1.02	1.27	1.83	2.47	3.14	50yr	2.13	3.07	3.59	4.99	6.30	9.79	10.42	50yr	8.66	10.02	11.37	12.73	13.97	50yr
100yr	0.79	1.20	1.50	2.16	2.97	3.82	100yr	2.56	3.73	4.37	6.15	7.74	12.24	13.04	100yr	10.84	12.54	14.19	15.69	17.08	100yr
200yr	0.93	1.39	1.77	2.56	3.56	4.66	200yr	3.08	4.56	5.33	7.57	9.50	15.36	16.33	200yr	13.59	15.70	17.72	19.32	20.90	200yr
500yr	1.15	1.71	2.20	3.19	4.54	6.05	500yr	3.92	5.92	6.92	10.01	12.49	20.74	21.99	500yr	18.36	21.15	23.77	25.45	27.30	500yr



APPENDIX C
HYDROCAD DRAINAGE
ANALYSIS CALCULATIONS



Project Notes

Defined 5 rainfall events from extreme_precipitation IDF

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	Type II 24-hr		Default	24.00	1	3.71	2
2	10-yr	Type II 24-hr		Default	24.00	1	5.64	2
3	25-yr	Type II 24-hr		Default	24.00	1	7.14	2
4	50-yr	Type II 24-hr		Default	24.00	1	8.56	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.821	61	>75% Grass cover, Good, HSG B (E1)
0.062	96	Gravel surface, HSG B (E1)
4.713	98	Paved parking, HSG B (E1, E1a)
0.498	98	Roofs, HSG B (E1)
0.210	98	Unconnected pavement, HSG B (E2)
0.079	98	Water Surface, 0% imp, HSG B (E2)
0.443	55	Woods, Good, HSG B (E1)
6.826	91	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
6.826	HSG B	E1, E1a, E2
0.000	HSG C	
0.000	HSG D	
0.000	Other	
6.826		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.821	0.000	0.000	0.000	0.821	>75% Grass cover, Good	E1
0.000	0.062	0.000	0.000	0.000	0.062	Gravel surface	E1
0.000	4.713	0.000	0.000	0.000	4.713	Paved parking	E1, E1a
0.000	0.498	0.000	0.000	0.000	0.498	Roofs	E1
0.000	0.210	0.000	0.000	0.000	0.210	Unconnected pavement	E2
0.000	0.079	0.000	0.000	0.000	0.079	Water Surface, 0% imp	E2
0.000	0.443	0.000	0.000	0.000	0.443	Woods, Good	E1
0.000	6.826	0.000	0.000	0.000	6.826	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Node Name
1	1P	47.60	47.50	51.5	0.0019	0.012	0.0	10.0	0.0	
2	1P	47.50	46.80	173.0	0.0040	0.012	0.0	12.0	0.0	
3	2P	46.60	45.10	294.0	0.0051	0.010	0.0	12.0	0.0	
4	DP1	41.35	40.35	192.0	0.0052	0.010	0.0	12.0	0.0	
5	DP1	39.45	38.45	192.0	0.0052	0.010	0.0	12.0	0.0	

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Type II 24-hr 2-yr Rainfall=3.71"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>2.47"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=20.32 cfs 1.211 af

Subcatchment E1a: Onsite CBs Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>3.21"
Tc=5.0 min CN=98 Runoff=3.47 cfs 0.174 af

Subcatchment E2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>3.21"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=1.54 cfs 0.077 af

Pond 1P: Drainage Network Peak Elev=48.11' Inflow=1.54 cfs 0.077 af
Outflow=1.54 cfs 0.077 af

Pond 2P: Drainage Network Peak Elev=50.49' Inflow=5.00 cfs 0.251 af
12.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=5.00 cfs 0.251 af

Pond DP1: Ponding Area Peak Elev=43.93' Storage=12,526 cf Inflow=22.84 cfs 1.462 af
Discarded=1.05 cfs 0.069 af Primary=10.02 cfs 1.393 af Secondary=0.00 cfs 0.000 af Outflow=11.07 cfs 1.462 af

Total Runoff Area = 6.826 ac Runoff Volume = 1.462 af Average Runoff Depth = 2.57"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Summary for Subcatchment E1: Property

Runoff = 20.32 cfs @ 12.05 hrs, Volume= 1.211 af, Depth> 2.47"
 Routed to Pond DP1 : Ponding Area

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Type II 24-hr 2-yr Rainfall=3.71"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
175,532	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment E1a: Onsite CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.47 cfs @ 11.95 hrs, Volume= 0.174 af, Depth> 3.21"
 Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Type II 24-hr 2-yr Rainfall=3.71"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment E2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af, Depth> 3.21"
 Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Type II 24-hr 2-yr Rainfall=3.71"

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Type II 24-hr 2-yr Rainfall=3.71"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 48.11' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 3.21" for 2-yr event
 Inflow = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af
 Outflow = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af, Atten= 0%, Lag= 0.0 min
 Primary = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.11' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=1.54 cfs @ 11.95 hrs HW=48.11' (Free Discharge)

1=Culvert (Barrel Controls 0.51 cfs @ 2.08 fps)

2=Culvert (Barrel Controls 1.02 cfs @ 2.91 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 50.49' (Flood elevation advised)

[81] Warning: Exceeded Pond 1P by 2.37' @ 11.95 hrs

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Type II 24-hr 2-yr Rainfall=3.71"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 3.21" for 2-yr event
 Inflow = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af
 Outflow = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af, Atten= 0%, Lag= 0.0 min
 Primary = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af
 Routed to Pond DP1 : Ponding Area

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 50.49' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	12.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=5.00 cfs @ 11.95 hrs HW=50.49' (Free Discharge)
 ↑1=Culvert (Barrel Controls 5.00 cfs @ 6.37 fps)

Summary for Pond DP1: Ponding Area

[82] Warning: Early inflow requires earlier time span

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 2.57" for 2-yr event
 Inflow = 22.84 cfs @ 12.03 hrs, Volume= 1.462 af
 Outflow = 11.07 cfs @ 12.21 hrs, Volume= 1.462 af, Atten= 52%, Lag= 10.7 min
 Discarded = 1.05 cfs @ 12.21 hrs, Volume= 0.069 af
 Primary = 10.02 cfs @ 12.21 hrs, Volume= 1.393 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 43.93' @ 12.21 hrs Surf.Area= 9,097 sf Storage= 12,526 cf

Plug-Flow detention time= 7.1 min calculated for 1.457 af (100% of inflow)
 Center-of-Mass det. time= 7.0 min (769.1 - 762.1)

Volume	Invert	Avail.Storage	Storage Description
#1	39.45'	231,724 cf	Custom Stage Data (Prismatic) Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.45	5	0	0
40.00	47	14	14
41.00	641	344	358
42.00	1,927	1,284	1,642
43.00	5,876	3,902	5,544
44.00	9,329	7,603	13,146
45.00	14,297	11,813	24,959
46.00	21,234	17,766	42,725
47.00	29,155	25,195	67,919
48.00	40,152	34,654	102,573
49.00	62,815	51,484	154,056
50.00	92,520	77,668	231,724

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Type II 24-hr 2-yr Rainfall=3.71"

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Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' / ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' / ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	39.45'	5.000 in/hr Exfiltration over Surface area below 44.00'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.05 cfs @ 12.21 hrs HW=43.93' (Free Discharge)↑ **3=Exfiltration** (Exfiltration Controls 1.05 cfs)**Primary OutFlow** Max=10.01 cfs @ 12.21 hrs HW=43.93' (Free Discharge)↑ **1=Culvert** (Inlet Controls 4.30 cfs @ 5.48 fps)↑ **2=Culvert** (Barrel Controls 5.70 cfs @ 7.26 fps)**Secondary OutFlow** Max=0.00 cfs @ 5.00 hrs HW=39.54' (Free Discharge)↑ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

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Type II 24-hr 10-yr Rainfall=5.64"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>4.21"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=33.61 cfs 2.064 af

Subcatchment E1a: Onsite CBs Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>4.95"
Tc=5.0 min CN=98 Runoff=5.30 cfs 0.269 af

Subcatchment E2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>4.95"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=2.35 cfs 0.119 af

Pond 1P: Drainage Network Peak Elev=48.28' Inflow=2.35 cfs 0.119 af
Outflow=2.35 cfs 0.119 af

Pond 2P: Drainage Network Peak Elev=56.34' Inflow=7.64 cfs 0.388 af
12.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=7.64 cfs 0.388 af

Pond DP1: Ponding Area Peak Elev=45.17' Storage=27,559 cf Inflow=37.54 cfs 2.452 af
Discarded=1.08 cfs 0.133 af Primary=11.72 cfs 2.319 af Secondary=0.00 cfs 0.000 af Outflow=12.80 cfs 2.452 af

Total Runoff Area = 6.826 ac Runoff Volume = 2.452 af Average Runoff Depth = 4.31"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

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Type II 24-hr 10-yr Rainfall=5.64"

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Summary for Subcatchment E1: Property

Runoff = 33.61 cfs @ 12.05 hrs, Volume= 2.064 af, Depth> 4.21"
Routed to Pond DP1 : Ponding Area

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
175,532	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment E1a: Onsite CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.30 cfs @ 11.95 hrs, Volume= 0.269 af, Depth> 4.95"
Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment E2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af, Depth> 4.95"
Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

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Type II 24-hr 10-yr Rainfall=5.64"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 48.28' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 4.95" for 10-yr event
 Inflow = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af
 Outflow = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.28' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=2.35 cfs @ 11.95 hrs HW=48.28' (Free Discharge)

1=Culvert (Barrel Controls 0.83 cfs @ 2.40 fps)

2=Culvert (Barrel Controls 1.52 cfs @ 3.20 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 56.34' (Flood elevation advised)

[81] Warning: Exceeded Pond 1P by 8.07' @ 11.95 hrs

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Type II 24-hr 10-yr Rainfall=5.64"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 4.95" for 10-yr event
 Inflow = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af
 Outflow = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af, Atten= 0%, Lag= 0.0 min
 Primary = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af
 Routed to Pond DP1 : Ponding Area

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 56.34' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	12.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=7.64 cfs @ 11.95 hrs HW=56.34' (Free Discharge)
 ↑**1=Culvert** (Barrel Controls 7.64 cfs @ 9.73 fps)

Summary for Pond DP1: Ponding Area

[82] Warning: Early inflow requires earlier time span
 [79] Warning: Submerged Pond 2P Primary device # 1 OUTLET by 0.07'

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 4.31" for 10-yr event
 Inflow = 37.54 cfs @ 12.03 hrs, Volume= 2.452 af
 Outflow = 12.80 cfs @ 12.26 hrs, Volume= 2.452 af, Atten= 66%, Lag= 14.1 min
 Discarded = 1.08 cfs @ 12.00 hrs, Volume= 0.133 af
 Primary = 11.72 cfs @ 12.26 hrs, Volume= 2.319 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 45.17' @ 12.26 hrs Surf.Area= 15,507 sf Storage= 27,559 cf

Plug-Flow detention time= 13.6 min calculated for 2.444 af (100% of inflow)
 Center-of-Mass det. time= 13.5 min (766.0 - 752.5)

Volume	Invert	Avail.Storage	Storage Description
#1	39.45'	231,724 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Existing Conditions 2023-06-21 David T

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Type II 24-hr 10-yr Rainfall=5.64"

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Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.45	5	0	0
40.00	47	14	14
41.00	641	344	358
42.00	1,927	1,284	1,642
43.00	5,876	3,902	5,544
44.00	9,329	7,603	13,146
45.00	14,297	11,813	24,959
46.00	21,234	17,766	42,725
47.00	29,155	25,195	67,919
48.00	40,152	34,654	102,573
49.00	62,815	51,484	154,056
50.00	92,520	77,668	231,724

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	39.45'	5.000 in/hr Exfiltration over Surface area below 44.00'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.08 cfs @ 12.00 hrs HW=44.08' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.08 cfs)

Primary OutFlow Max=11.72 cfs @ 12.26 hrs HW=45.17' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 5.27 cfs @ 6.71 fps)
 ↳ **2=Culvert** (Barrel Controls 6.45 cfs @ 8.21 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=39.65' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Existing Conditions 2023-06-21 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>5.58"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=43.85 cfs 2.735 af

Subcatchment E1a: Onsite CBs Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>6.29"
Tc=5.0 min CN=98 Runoff=6.71 cfs 0.342 af

Subcatchment E2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>6.29"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=2.98 cfs 0.152 af

Pond 1P: Drainage Network Peak Elev=48.40' Inflow=2.98 cfs 0.152 af
Outflow=2.98 cfs 0.152 af

Pond 2P: Drainage Network Peak Elev=62.57' Inflow=9.69 cfs 0.493 af
12.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=9.69 cfs 0.493 af

Pond DP1: Ponding Area Peak Elev=45.90' Storage=40,734 cf Inflow=48.87 cfs 3.228 af
Discarded=1.08 cfs 0.181 af Primary=12.60 cfs 3.047 af Secondary=0.00 cfs 0.000 af Outflow=13.68 cfs 3.228 af

Total Runoff Area = 6.826 ac Runoff Volume = 3.228 af Average Runoff Depth = 5.67"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Existing Conditions 2023-06-21 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Summary for Subcatchment E1: Property

Runoff = 43.85 cfs @ 12.05 hrs, Volume= 2.735 af, Depth> 5.58"
Routed to Pond DP1 : Ponding Area

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
175,532	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment E1a: Onsite CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 6.71 cfs @ 11.95 hrs, Volume= 0.342 af, Depth> 6.29"
Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment E2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af, Depth> 6.29"
Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Existing Conditions 2023-06-21 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 48.40' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 6.29" for 25-yr event
 Inflow = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af
 Outflow = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.40' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=2.98 cfs @ 11.95 hrs HW=48.40' (Free Discharge)

1=Culvert (Barrel Controls 1.08 cfs @ 2.58 fps)

2=Culvert (Barrel Controls 1.89 cfs @ 3.36 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 62.57' (Flood elevation advised)

[81] Warning: Exceeded Pond 1P by 14.17' @ 11.95 hrs

Existing Conditions 2023-06-21 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 6.29" for 25-yr event
 Inflow = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af
 Outflow = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af, Atten= 0%, Lag= 0.0 min
 Primary = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af
 Routed to Pond DP1 : Ponding Area

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 62.57' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	12.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=9.69 cfs @ 11.95 hrs HW=62.55' (Free Discharge)
 ↑1=Culvert (Barrel Controls 9.69 cfs @ 12.34 fps)

Summary for Pond DP1: Ponding Area

[82] Warning: Early inflow requires earlier time span
 [79] Warning: Submerged Pond 2P Primary device # 1 OUTLET by 0.80'

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 5.67" for 25-yr event
 Inflow = 48.87 cfs @ 12.03 hrs, Volume= 3.228 af
 Outflow = 13.68 cfs @ 12.30 hrs, Volume= 3.228 af, Atten= 72%, Lag= 16.4 min
 Discarded = 1.08 cfs @ 11.95 hrs, Volume= 0.181 af
 Primary = 12.60 cfs @ 12.30 hrs, Volume= 3.047 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 45.90' @ 12.30 hrs Surf.Area= 20,573 sf Storage= 40,734 cf

Plug-Flow detention time= 19.3 min calculated for 3.217 af (100% of inflow)
 Center-of-Mass det. time= 19.2 min (767.3 - 748.1)

Volume	Invert	Avail.Storage	Storage Description
#1	39.45'	231,724 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Existing Conditions 2023-06-21 David T

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Type II 24-hr 25-yr Rainfall=7.14"

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Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.45	5	0	0
40.00	47	14	14
41.00	641	344	358
42.00	1,927	1,284	1,642
43.00	5,876	3,902	5,544
44.00	9,329	7,603	13,146
45.00	14,297	11,813	24,959
46.00	21,234	17,766	42,725
47.00	29,155	25,195	67,919
48.00	40,152	34,654	102,573
49.00	62,815	51,484	154,056
50.00	92,520	77,668	231,724

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	39.45'	5.000 in/hr Exfiltration over Surface area below 44.00'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.08 cfs @ 11.95 hrs HW=44.11' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.08 cfs)

Primary OutFlow Max=12.60 cfs @ 12.30 hrs HW=45.90' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 5.75 cfs @ 7.32 fps)
 ↳ **2=Culvert** (Barrel Controls 6.85 cfs @ 8.72 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=39.71' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Existing Conditions 2023-06-21 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment E1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>6.87"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=53.47 cfs 3.371 af

Subcatchment E1a: Onsite CBs Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>7.56"
Tc=5.0 min CN=98 Runoff=8.06 cfs 0.411 af

Subcatchment E2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>7.56"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=3.57 cfs 0.182 af

Pond 1P: Drainage Network Peak Elev=48.52' Inflow=3.57 cfs 0.182 af
Outflow=3.57 cfs 0.182 af

Pond 2P: Drainage Network Peak Elev=69.80' Inflow=11.63 cfs 0.593 af
12.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=11.63 cfs 0.593 af

Pond DP1: Ponding Area Peak Elev=46.48' Storage=53,918 cf Inflow=59.52 cfs 3.964 af
Discarded=1.08 cfs 0.226 af Primary=13.26 cfs 3.737 af Secondary=0.00 cfs 0.000 af Outflow=14.34 cfs 3.964 af

Total Runoff Area = 6.826 ac Runoff Volume = 3.964 af Average Runoff Depth = 6.97"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Existing Conditions 2023-06-21 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Summary for Subcatchment E1: Property

Runoff = 53.47 cfs @ 12.05 hrs, Volume= 3.371 af, Depth> 6.87"

Routed to Pond DP1 : Ponding Area

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
175,532	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment E1a: Onsite CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 8.06 cfs @ 11.95 hrs, Volume= 0.411 af, Depth> 7.56"

Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment E2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af, Depth> 7.56"

Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

Existing Conditions 2023-06-21 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 48.52' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 7.56" for 50-yr event
 Inflow = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af
 Outflow = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af, Atten= 0%, Lag= 0.0 min
 Primary = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.52' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=3.57 cfs @ 11.95 hrs HW=48.52' (Free Discharge)

1=Culvert (Barrel Controls 1.32 cfs @ 2.73 fps)

2=Culvert (Barrel Controls 2.25 cfs @ 3.48 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span

[57] Hint: Peaked at 69.80' (Flood elevation advised)

[81] Warning: Exceeded Pond 1P by 21.28' @ 11.95 hrs

Existing Conditions 2023-06-21 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 7.56" for 50-yr event
 Inflow = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af
 Outflow = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af, Atten= 0%, Lag= 0.0 min
 Primary = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af
 Routed to Pond DP1 : Ponding Area

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 69.80' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	12.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=11.62 cfs @ 11.95 hrs HW=69.78' (Free Discharge)
 ↑1=Culvert (Barrel Controls 11.62 cfs @ 14.80 fps)

Summary for Pond DP1: Ponding Area

[82] Warning: Early inflow requires earlier time span
 [79] Warning: Submerged Pond 2P Primary device # 1 OUTLET by 1.38'

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 6.97" for 50-yr event
 Inflow = 59.52 cfs @ 12.03 hrs, Volume= 3.964 af
 Outflow = 14.34 cfs @ 12.33 hrs, Volume= 3.964 af, Atten= 76%, Lag= 18.2 min
 Discarded = 1.08 cfs @ 11.95 hrs, Volume= 0.226 af
 Primary = 13.26 cfs @ 12.33 hrs, Volume= 3.737 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 46.48' @ 12.33 hrs Surf.Area= 25,064 sf Storage= 53,918 cf

Plug-Flow detention time= 25.0 min calculated for 3.950 af (100% of inflow)
 Center-of-Mass det. time= 24.8 min (770.0 - 745.2)

Volume	Invert	Avail.Storage	Storage Description
#1	39.45'	231,724 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Existing Conditions 2023-06-21 David T

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Type II 24-hr 50-yr Rainfall=8.56"

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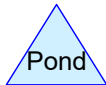
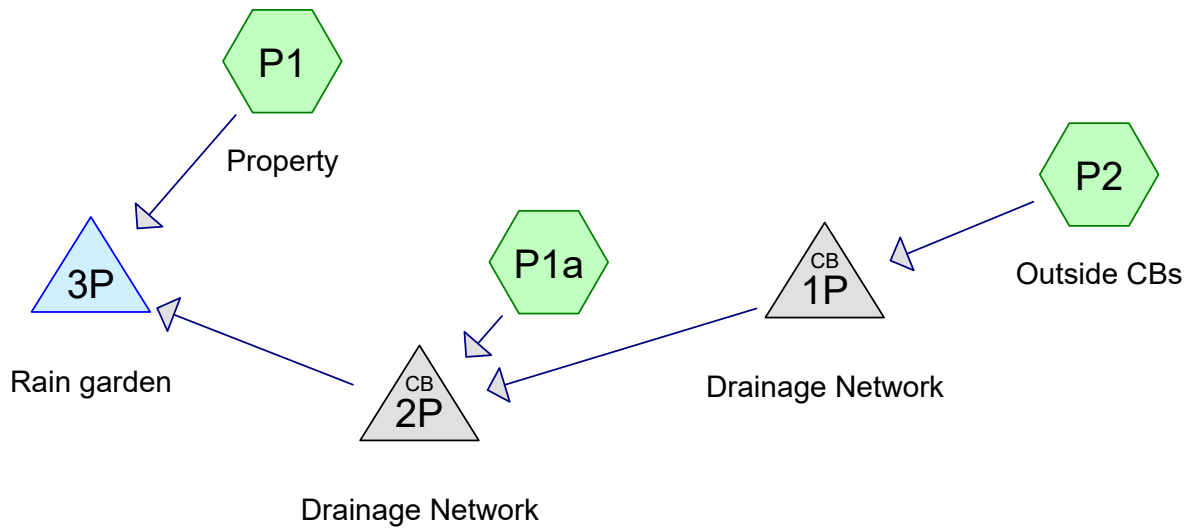
Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
39.45	5	0	0
40.00	47	14	14
41.00	641	344	358
42.00	1,927	1,284	1,642
43.00	5,876	3,902	5,544
44.00	9,329	7,603	13,146
45.00	14,297	11,813	24,959
46.00	21,234	17,766	42,725
47.00	29,155	25,195	67,919
48.00	40,152	34,654	102,573
49.00	62,815	51,484	154,056
50.00	92,520	77,668	231,724

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	39.45'	5.000 in/hr Exfiltration over Surface area below 44.00'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.08 cfs @ 11.95 hrs HW=44.53' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.08 cfs)

Primary OutFlow Max=13.25 cfs @ 12.33 hrs HW=46.48' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 6.11 cfs @ 7.77 fps)
 ↳ **2=Culvert** (Barrel Controls 7.15 cfs @ 9.10 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=39.78' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)



Project Notes

Defined 5 rainfall events from extreme_precipitation IDF

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	Type II 24-hr		Default	24.00	1	3.71	2
2	10-yr	Type II 24-hr		Default	24.00	1	5.64	2
3	25-yr	Type II 24-hr		Default	24.00	1	7.14	2
4	50-yr	Type II 24-hr		Default	24.00	1	8.56	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.821	61	>75% Grass cover, Good, HSG B (P1)
0.062	96	Gravel surface, HSG B (P1)
4.634	98	Paved parking, HSG B (P1, P1a)
0.577	98	Roofs, HSG B (P1)
0.210	98	Unconnected pavement, HSG B (P2)
0.079	98	Water Surface, 0% imp, HSG B (P2)
0.443	55	Woods, Good, HSG B (P1)
6.826	91	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
6.826	HSG B	P1, P1a, P2
0.000	HSG C	
0.000	HSG D	
0.000	Other	
6.826		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
0.000	0.821	0.000	0.000	0.000	0.821	>75% Grass cover, Good	P1
0.000	0.062	0.000	0.000	0.000	0.062	Gravel surface	P1
0.000	4.634	0.000	0.000	0.000	4.634	Paved parking	P1, P1a
0.000	0.577	0.000	0.000	0.000	0.577	Roofs	P1
0.000	0.210	0.000	0.000	0.000	0.210	Unconnected pavement	P2
0.000	0.079	0.000	0.000	0.000	0.079	Water Surface, 0% imp	P2
0.000	0.443	0.000	0.000	0.000	0.443	Woods, Good	P1
0.000	6.826	0.000	0.000	0.000	6.826	TOTAL AREA	

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Pipe Listing (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Width (inches)	Diam/Height (inches)	Inside-Fill (inches)	Node Name
1	1P	47.60	47.50	51.5	0.0019	0.012	0.0	10.0	0.0	
2	1P	47.50	46.80	173.0	0.0040	0.012	0.0	12.0	0.0	
3	2P	46.60	45.10	294.0	0.0051	0.010	0.0	18.0	0.0	
4	3P	41.35	40.35	192.0	0.0052	0.010	0.0	12.0	0.0	
5	3P	39.45	38.45	192.0	0.0052	0.010	0.0	12.0	0.0	

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Type II 24-hr 2-yr Rainfall=3.71"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>2.47"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=20.32 cfs 1.211 af

Subcatchment P1a: Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>3.21"
Tc=5.0 min CN=98 Runoff=3.47 cfs 0.174 af

Subcatchment P2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>3.21"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=1.54 cfs 0.077 af

Pond 1P: Drainage Network Peak Elev=48.11' Inflow=1.54 cfs 0.077 af
Outflow=1.54 cfs 0.077 af

Pond 2P: Drainage Network Peak Elev=47.71' Inflow=5.00 cfs 0.251 af
18.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=5.00 cfs 0.251 af

Pond 3P: Rain garden Peak Elev=43.05' Storage=19,718 cf Inflow=22.84 cfs 1.462 af
Discarded=0.91 cfs 0.476 af Primary=8.39 cfs 0.951 af Secondary=0.00 cfs 0.000 af Outflow=9.30 cfs 1.427 af

Total Runoff Area = 6.826 ac Runoff Volume = 1.462 af Average Runoff Depth = 2.57"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Proposed Conditions 2023-07-12 David T

Type II 24-hr 2-yr Rainfall=3.71"

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Summary for Subcatchment P1: Property

Runoff = 20.32 cfs @ 12.05 hrs, Volume= 1.211 af, Depth> 2.47"
Routed to Pond 3P : Rain garden

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 2-yr Rainfall=3.71"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
172,076	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
3,456	98	Roofs, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment P1a:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.47 cfs @ 11.95 hrs, Volume= 0.174 af, Depth> 3.21"
Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 2-yr Rainfall=3.71"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment P2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af, Depth> 3.21"
Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 2-yr Rainfall=3.71"

Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.11' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 3.21" for 2-yr event
 Inflow = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af
 Outflow = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af, Atten= 0%, Lag= 0.0 min
 Primary = 1.54 cfs @ 11.95 hrs, Volume= 0.077 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.11' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=1.54 cfs @ 11.95 hrs HW=48.11' (Free Discharge)

- 1=Culvert (Barrel Controls 0.51 cfs @ 2.08 fps)
- 2=Culvert (Barrel Controls 1.02 cfs @ 2.91 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 47.71' (Flood elevation advised)
 [79] Warning: Submerged Pond 1P Primary device # 1 INLET by 0.11'
 [79] Warning: Submerged Pond 1P Primary device # 2 INLET by 0.21'

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Type II 24-hr 2-yr Rainfall=3.71"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 3.21" for 2-yr event
 Inflow = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af
 Outflow = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af, Atten= 0%, Lag= 0.0 min
 Primary = 5.00 cfs @ 11.95 hrs, Volume= 0.251 af
 Routed to Pond 3P : Rain garden

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 47.71' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	18.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 ' / Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=5.00 cfs @ 11.95 hrs HW=47.71' (Free Discharge)
 ↑1=Culvert (Inlet Controls 5.00 cfs @ 3.58 fps)

Summary for Pond 3P: Rain garden

[82] Warning: Early inflow requires earlier time span

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 2.57" for 2-yr event
 Inflow = 22.84 cfs @ 12.03 hrs, Volume= 1.462 af
 Outflow = 9.30 cfs @ 12.23 hrs, Volume= 1.427 af, Atten= 59%, Lag= 12.4 min
 Discarded = 0.91 cfs @ 12.23 hrs, Volume= 0.476 af
 Primary = 8.39 cfs @ 12.23 hrs, Volume= 0.951 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 43.05' @ 12.23 hrs Surf.Area= 7,898 sf Storage= 19,718 cf

Plug-Flow detention time= 33.3 min calculated for 1.427 af (98% of inflow)
 Center-of-Mass det. time= 23.4 min (785.5 - 762.1)

Volume	Invert	Avail.Storage	Storage Description
#1	37.00'	247,674 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

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Type II 24-hr 2-yr Rainfall=3.71"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
37.00	0	0.0	0	0
37.01	3,608	20.0	4	4
39.99	3,608	20.0	2,150	2,154
40.00	3,608	100.0	36	2,190
41.00	4,915	100.0	4,262	6,452
42.00	6,494	100.0	5,705	12,156
43.00	7,815	100.0	7,155	19,311
44.00	9,422	100.0	8,619	27,929
45.00	14,471	100.0	11,947	39,876
46.00	21,491	100.0	17,981	57,857
47.00	29,440	100.0	25,466	83,322
48.00	40,464	100.0	34,952	118,274
49.00	63,016	100.0	51,740	170,014
50.00	92,304	100.0	77,660	247,674

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' / Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' / Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	37.00'	5.000 in/hr Exfiltration over Surface area below 44.00' Phase-In= 0.01'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=0.91 cfs @ 12.23 hrs HW=43.05' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 0.91 cfs)

Primary OutFlow Max=8.38 cfs @ 12.23 hrs HW=43.05' (Free Discharge)
 ↳ **1=Culvert** (Inlet Controls 3.26 cfs @ 4.16 fps)
 ↳ **2=Culvert** (Barrel Controls 5.11 cfs @ 6.51 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=37.00' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

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Type II 24-hr 10-yr Rainfall=5.64"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>4.21"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=33.61 cfs 2.064 af

Subcatchment P1a: Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>4.95"
Tc=5.0 min CN=98 Runoff=5.30 cfs 0.269 af

Subcatchment P2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>4.95"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=2.35 cfs 0.119 af

Pond 1P: Drainage Network Peak Elev=48.28' Inflow=2.35 cfs 0.119 af
Outflow=2.35 cfs 0.119 af

Pond 2P: Drainage Network Peak Elev=48.16' Inflow=7.64 cfs 0.388 af
18.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=7.64 cfs 0.388 af

Pond 3P: Rain garden Peak Elev=44.65' Storage=35,174 cf Inflow=37.54 cfs 2.452 af
Discarded=1.09 cfs 0.581 af Primary=11.05 cfs 1.828 af Secondary=0.00 cfs 0.000 af Outflow=12.14 cfs 2.409 af

Total Runoff Area = 6.826 ac Runoff Volume = 2.452 af Average Runoff Depth = 4.31"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

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Type II 24-hr 10-yr Rainfall=5.64"

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Summary for Subcatchment P1: Property

Runoff = 33.61 cfs @ 12.05 hrs, Volume= 2.064 af, Depth> 4.21"

Routed to Pond 3P : Rain garden

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
172,076	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
3,456	98	Roofs, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment P1a:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 5.30 cfs @ 11.95 hrs, Volume= 0.269 af, Depth> 4.95"

Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment P2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af, Depth> 4.95"

Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 10-yr Rainfall=5.64"

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Type II 24-hr 10-yr Rainfall=5.64"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.28' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 4.95" for 10-yr event
 Inflow = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af
 Outflow = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.35 cfs @ 11.95 hrs, Volume= 0.119 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.28' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=2.35 cfs @ 11.95 hrs HW=48.28' (Free Discharge)

- 1=Culvert (Barrel Controls 0.83 cfs @ 2.40 fps)
- 2=Culvert (Barrel Controls 1.52 cfs @ 3.20 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.16' (Flood elevation advised)
 [79] Warning: Submerged Pond 1P Primary device # 1 INLET by 0.56'
 [79] Warning: Submerged Pond 1P Primary device # 2 INLET by 0.66'

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Type II 24-hr 10-yr Rainfall=5.64"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 4.95" for 10-yr event
 Inflow = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af
 Outflow = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af, Atten= 0%, Lag= 0.0 min
 Primary = 7.64 cfs @ 11.95 hrs, Volume= 0.388 af
 Routed to Pond 3P : Rain garden

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.16' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	18.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=7.64 cfs @ 11.95 hrs HW=48.16' (Free Discharge)
 ↑1=Culvert (Inlet Controls 7.64 cfs @ 4.32 fps)

Summary for Pond 3P: Rain garden

[82] Warning: Early inflow requires earlier time span

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 4.31" for 10-yr event
 Inflow = 37.54 cfs @ 12.03 hrs, Volume= 2.452 af
 Outflow = 12.14 cfs @ 12.27 hrs, Volume= 2.409 af, Atten= 68%, Lag= 14.6 min
 Discarded = 1.09 cfs @ 12.10 hrs, Volume= 0.581 af
 Primary = 11.05 cfs @ 12.27 hrs, Volume= 1.828 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 44.65' @ 12.27 hrs Surf.Area= 12,725 sf Storage= 35,174 cf

Plug-Flow detention time= 35.2 min calculated for 2.401 af (98% of inflow)
 Center-of-Mass det. time= 27.7 min (780.2 - 752.5)

Volume	Invert	Avail.Storage	Storage Description
#1	37.00'	247,674 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Proposed Conditions 2023-07-12 David T

Type II 24-hr 10-yr Rainfall=5.64"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
37.00	0	0.0	0	0
37.01	3,608	20.0	4	4
39.99	3,608	20.0	2,150	2,154
40.00	3,608	100.0	36	2,190
41.00	4,915	100.0	4,262	6,452
42.00	6,494	100.0	5,705	12,156
43.00	7,815	100.0	7,155	19,311
44.00	9,422	100.0	8,619	27,929
45.00	14,471	100.0	11,947	39,876
46.00	21,491	100.0	17,981	57,857
47.00	29,440	100.0	25,466	83,322
48.00	40,464	100.0	34,952	118,274
49.00	63,016	100.0	51,740	170,014
50.00	92,304	100.0	77,660	247,674

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' / Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' / Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	37.00'	5.000 in/hr Exfiltration over Surface area below 44.00' Phase-In= 0.01'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.09 cfs @ 12.10 hrs HW=44.18' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.09 cfs)

Primary OutFlow Max=11.04 cfs @ 12.27 hrs HW=44.65' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 4.89 cfs @ 6.23 fps)
 ↳ **2=Culvert** (Barrel Controls 6.15 cfs @ 7.82 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=37.00' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Proposed Conditions 2023-07-12 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>5.58"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=43.85 cfs 2.735 af

Subcatchment P1a: Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>6.29"
Tc=5.0 min CN=98 Runoff=6.71 cfs 0.342 af

Subcatchment P2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>6.29"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=2.98 cfs 0.152 af

Pond 1P: Drainage Network Peak Elev=48.40' Inflow=2.98 cfs 0.152 af
Outflow=2.98 cfs 0.152 af

Pond 2P: Drainage Network Peak Elev=48.79' Inflow=9.69 cfs 0.493 af
18.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=9.69 cfs 0.493 af

Pond 3P: Rain garden Peak Elev=45.54' Storage=48,774 cf Inflow=48.87 cfs 3.228 af
Discarded=1.09 cfs 0.636 af Primary=12.17 cfs 2.547 af Secondary=0.00 cfs 0.000 af Outflow=13.26 cfs 3.183 af

Total Runoff Area = 6.826 ac Runoff Volume = 3.228 af Average Runoff Depth = 5.67"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Proposed Conditions 2023-07-12 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Summary for Subcatchment P1: Property

Runoff = 43.85 cfs @ 12.05 hrs, Volume= 2.735 af, Depth> 5.58"
Routed to Pond 3P : Rain garden

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
172,076	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
3,456	98	Roofs, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment P1a:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 6.71 cfs @ 11.95 hrs, Volume= 0.342 af, Depth> 6.29"
Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment P2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af, Depth> 6.29"
Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 25-yr Rainfall=7.14"

Proposed Conditions 2023-07-12 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.40' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 6.29" for 25-yr event
 Inflow = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af
 Outflow = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af, Atten= 0%, Lag= 0.0 min
 Primary = 2.98 cfs @ 11.95 hrs, Volume= 0.152 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.40' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1/' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1/' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=2.98 cfs @ 11.95 hrs HW=48.40' (Free Discharge)

- 1=Culvert (Barrel Controls 1.08 cfs @ 2.58 fps)
- 2=Culvert (Barrel Controls 1.89 cfs @ 3.36 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.79' (Flood elevation advised)
 [81] Warning: Exceeded Pond 1P by 0.39' @ 11.95 hrs

Proposed Conditions 2023-07-12 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 6.29" for 25-yr event
 Inflow = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af
 Outflow = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af, Atten= 0%, Lag= 0.0 min
 Primary = 9.69 cfs @ 11.95 hrs, Volume= 0.493 af
 Routed to Pond 3P : Rain garden

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.79' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	18.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 ' S= 0.0051 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=9.69 cfs @ 11.95 hrs HW=48.79' (Free Discharge)
 ↑1=Culvert (Barrel Controls 9.69 cfs @ 5.48 fps)

Summary for Pond 3P: Rain garden

[82] Warning: Early inflow requires earlier time span
 [79] Warning: Submerged Pond 2P Primary device # 1 OUTLET by 0.44'

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 5.67" for 25-yr event
 Inflow = 48.87 cfs @ 12.03 hrs, Volume= 3.228 af
 Outflow = 13.26 cfs @ 12.30 hrs, Volume= 3.183 af, Atten= 73%, Lag= 16.7 min
 Discarded = 1.09 cfs @ 12.05 hrs, Volume= 0.636 af
 Primary = 12.17 cfs @ 12.30 hrs, Volume= 2.547 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 45.54' @ 12.30 hrs Surf.Area= 18,285 sf Storage= 48,774 cf

Plug-Flow detention time= 39.4 min calculated for 3.172 af (98% of inflow)
 Center-of-Mass det. time= 33.3 min (781.4 - 748.1)

Volume	Invert	Avail.Storage	Storage Description
#1	37.00'	247,674 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Proposed Conditions 2023-07-12 David T

Type II 24-hr 25-yr Rainfall=7.14"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
37.00	0	0.0	0	0
37.01	3,608	20.0	4	4
39.99	3,608	20.0	2,150	2,154
40.00	3,608	100.0	36	2,190
41.00	4,915	100.0	4,262	6,452
42.00	6,494	100.0	5,705	12,156
43.00	7,815	100.0	7,155	19,311
44.00	9,422	100.0	8,619	27,929
45.00	14,471	100.0	11,947	39,876
46.00	21,491	100.0	17,981	57,857
47.00	29,440	100.0	25,466	83,322
48.00	40,464	100.0	34,952	118,274
49.00	63,016	100.0	51,740	170,014
50.00	92,304	100.0	77,660	247,674

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	37.00'	5.000 in/hr Exfiltration over Surface area below 44.00' Phase-In= 0.01'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.09 cfs @ 12.05 hrs HW=44.57' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.09 cfs)

Primary OutFlow Max=12.17 cfs @ 12.30 hrs HW=45.54' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 5.52 cfs @ 7.03 fps)
 ↳ **2=Culvert** (Barrel Controls 6.65 cfs @ 8.47 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=37.01' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

Proposed Conditions 2023-07-12 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Time span=5.00-20.00 hrs, dt=0.05 hrs, 301 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment P1: Property Runoff Area=256,358 sf 77.47% Impervious Runoff Depth>6.87"
Flow Length=879' Slope=0.0213 '/' Tc=13.8 min CN=90 Runoff=53.47 cfs 3.371 af

Subcatchment P1a: Runoff Area=28,397 sf 100.00% Impervious Runoff Depth>7.56"
Tc=5.0 min CN=98 Runoff=8.06 cfs 0.411 af

Subcatchment P2: Outside CBs Runoff Area=12,598 sf 72.77% Impervious Runoff Depth>7.56"
Flow Length=135' Slope=0.0286 '/' Tc=5.0 min CN=98 Runoff=3.57 cfs 0.182 af

Pond 1P: Drainage Network Peak Elev=48.52' Inflow=3.57 cfs 0.182 af
Outflow=3.57 cfs 0.182 af

Pond 2P: Drainage Network Peak Elev=49.75' Inflow=11.63 cfs 0.593 af
18.0" Round Culvert n=0.010 L=294.0' S=0.0051 '/' Outflow=11.63 cfs 0.593 af

Pond 3P: Rain garden Peak Elev=46.21' Storage=62,535 cf Inflow=59.52 cfs 3.964 af
Discarded=1.09 cfs 0.674 af Primary=12.95 cfs 3.243 af Secondary=0.00 cfs 0.000 af Outflow=14.04 cfs 3.918 af

Total Runoff Area = 6.826 ac Runoff Volume = 3.964 af Average Runoff Depth = 6.97"
20.58% Pervious = 1.405 ac 79.42% Impervious = 5.422 ac

Proposed Conditions 2023-07-12 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Summary for Subcatchment P1: Property

Runoff = 53.47 cfs @ 12.05 hrs, Volume= 3.371 af, Depth> 6.87"

Routed to Pond 3P : Rain garden

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

Area (sf)	CN	Description
1,375	98	Paved parking, HSG B
172,076	98	Paved parking, HSG B
21,694	98	Roofs, HSG B
35,764	61	>75% Grass cover, Good, HSG B
2,687	96	Gravel surface, HSG B
19,306	55	Woods, Good, HSG B
3,456	98	Roofs, HSG B
256,358	90	Weighted Average
57,757		22.53% Pervious Area
198,601		77.47% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
13.8	879	0.0213	1.06		Lag/CN Method,

Summary for Subcatchment P1a:

[49] Hint: Tc<2dt may require smaller dt

Runoff = 8.06 cfs @ 11.95 hrs, Volume= 0.411 af, Depth> 7.56"

Routed to Pond 2P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

Area (sf)	CN	Description
28,397	98	Paved parking, HSG B
28,397		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment P2: Outside CBs

[49] Hint: Tc<2dt may require smaller dt

Runoff = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af, Depth> 7.56"

Routed to Pond 1P : Drainage Network

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Type II 24-hr 50-yr Rainfall=8.56"

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Type II 24-hr 50-yr Rainfall=8.56"

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Area (sf)	CN	Description
3,431	98	Water Surface, 0% imp, HSG B
171	98	Unconnected pavement, HSG B
8,996	98	Unconnected pavement, HSG B
12,598	98	Weighted Average
3,431		27.23% Pervious Area
9,167		72.77% Impervious Area
9,167		100.00% Unconnected

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	135	0.0286	1.25		Lag/CN Method,
1.8	135	Total, Increased to minimum Tc = 5.0 min			

Summary for Pond 1P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 48.52' (Flood elevation advised)

Inflow Area = 0.289 ac, 72.77% Impervious, Inflow Depth > 7.56" for 50-yr event
 Inflow = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af
 Outflow = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af, Atten= 0%, Lag= 0.0 min
 Primary = 3.57 cfs @ 11.95 hrs, Volume= 0.182 af
 Routed to Pond 2P : Drainage Network

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 48.52' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	47.60'	10.0" Round Culvert L= 51.5' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.60' / 47.50' S= 0.0019 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.55 sf
#2	Primary	47.50'	12.0" Round Culvert L= 173.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 47.50' / 46.80' S= 0.0040 1/1' Cc= 0.900 n= 0.012 Steel, smooth, Flow Area= 0.79 sf

Primary OutFlow Max=3.57 cfs @ 11.95 hrs HW=48.52' (Free Discharge)

- 1=Culvert (Barrel Controls 1.32 cfs @ 2.73 fps)
- 2=Culvert (Barrel Controls 2.25 cfs @ 3.48 fps)

Summary for Pond 2P: Drainage Network

[82] Warning: Early inflow requires earlier time span
 [57] Hint: Peaked at 49.75' (Flood elevation advised)
 [81] Warning: Exceeded Pond 1P by 1.23' @ 11.95 hrs

Proposed Conditions 2023-07-12 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Inflow Area = 0.941 ac, 91.63% Impervious, Inflow Depth > 7.56" for 50-yr event
 Inflow = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af
 Outflow = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af, Atten= 0%, Lag= 0.0 min
 Primary = 11.63 cfs @ 11.95 hrs, Volume= 0.593 af
 Routed to Pond 3P : Rain garden

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 49.75' @ 11.95 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	46.60'	18.0" Round Culvert L= 294.0' CMP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 46.60' / 45.10' S= 0.0051 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf

Primary OutFlow Max=11.62 cfs @ 11.95 hrs HW=49.75' (Free Discharge)
 ↑1=Culvert (Barrel Controls 11.62 cfs @ 6.58 fps)

Summary for Pond 3P: Rain garden

[82] Warning: Early inflow requires earlier time span
 [79] Warning: Submerged Pond 2P Primary device # 1 OUTLET by 1.11'

Inflow Area = 6.826 ac, 79.42% Impervious, Inflow Depth > 6.97" for 50-yr event
 Inflow = 59.52 cfs @ 12.03 hrs, Volume= 3.964 af
 Outflow = 14.04 cfs @ 12.33 hrs, Volume= 3.918 af, Atten= 76%, Lag= 18.5 min
 Discarded = 1.09 cfs @ 12.00 hrs, Volume= 0.674 af
 Primary = 12.95 cfs @ 12.33 hrs, Volume= 3.243 af
 Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
 Peak Elev= 46.21' @ 12.33 hrs Surf.Area= 23,157 sf Storage= 62,535 cf

Plug-Flow detention time= 44.4 min calculated for 3.918 af (99% of inflow)
 Center-of-Mass det. time= 39.3 min (784.5 - 745.2)

Volume	Invert	Avail.Storage	Storage Description
#1	37.00'	247,674 cf	Custom Stage Data (Prismatic) Listed below (Recalc)

Proposed Conditions 2023-07-12 David T

Type II 24-hr 50-yr Rainfall=8.56"

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Elevation (feet)	Surf.Area (sq-ft)	Voids (%)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
37.00	0	0.0	0	0
37.01	3,608	20.0	4	4
39.99	3,608	20.0	2,150	2,154
40.00	3,608	100.0	36	2,190
41.00	4,915	100.0	4,262	6,452
42.00	6,494	100.0	5,705	12,156
43.00	7,815	100.0	7,155	19,311
44.00	9,422	100.0	8,619	27,929
45.00	14,471	100.0	11,947	39,876
46.00	21,491	100.0	17,981	57,857
47.00	29,440	100.0	25,466	83,322
48.00	40,464	100.0	34,952	118,274
49.00	63,016	100.0	51,740	170,014
50.00	92,304	100.0	77,660	247,674

Device	Routing	Invert	Outlet Devices
#1	Primary	41.35'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 41.35' / 40.35' S= 0.0052 ' / S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#2	Primary	39.45'	12.0" Round Culvert L= 192.0' CMP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 39.45' / 38.45' S= 0.0052 ' / S= 0.0052 ' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.79 sf
#3	Discarded	37.00'	5.000 in/hr Exfiltration over Surface area below 44.00' Phase-In= 0.01'
#4	Secondary	48.00'	Custom Weir/Orifice, Cv= 2.62 (C= 3.28) Head (feet) 0.00 1.00 2.00 Width (feet) 24.10 75.20 155.70

Discarded OutFlow Max=1.09 cfs @ 12.00 hrs HW=44.60' (Free Discharge)
 ↳ **3=Exfiltration** (Exfiltration Controls 1.09 cfs)

Primary OutFlow Max=12.95 cfs @ 12.33 hrs HW=46.21' (Free Discharge)
 ↳ **1=Culvert** (Barrel Controls 5.94 cfs @ 7.56 fps)
 ↳ **2=Culvert** (Barrel Controls 7.01 cfs @ 8.92 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=37.01' (Free Discharge)
 ↳ **4=Custom Weir/Orifice** (Controls 0.00 cfs)

APPENDIX D
SOIL SURVEY INFORMATION



United States
Department of
Agriculture

NRCS

Natural
Resources
Conservation
Service

A product of the National
Cooperative Soil Survey,
a joint effort of the United
States Department of
Agriculture and other
Federal agencies, State
agencies including the
Agricultural Experiment
Stations, and local
participants

Custom Soil Resource Report for Rockingham County, New Hampshire

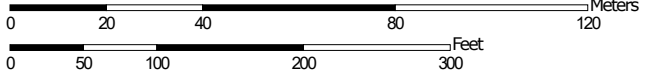


Custom Soil Resource Report Soil Map



Soil Map may not be valid at this scale.


Map Scale: 1:1,570 if printed on A landscape (11" x 8.5") sheet.



Map projection: Web Mercator Corner coordinates: WGS84 Edge tics: UTM Zone 19N WGS84

MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines


 Soil Map Unit Points

Special Point Features






-  Blowout
-  Borrow Pit
-  Clay Spot
-  Closed Depression
-  Gravel Pit
-  Gravelly Spot
-  Landfill
-  Lava Flow
-  Marsh or swamp
-  Mine or Quarry
-  Miscellaneous Water
-  Perennial Water
-  Rock Outcrop
-  Saline Spot
-  Sandy Spot
-  Severely Eroded Spot
-  Sinkhole
-  Slide or Slip
-  Sodic Spot

-  Spoil Area
-  Stony Spot
-  Very Stony Spot
-  Wet Spot
-  Other
-  Special Line Features

Water Features

 Streams and Canals

Transportation

-  Rails
-  Interstate Highways
-  US Routes
-  Major Roads
-  Local Roads

Background

 Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service
 Web Soil Survey URL:
 Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Rockingham County, New Hampshire
 Survey Area Data: Version 25, Sep 12, 2022

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 19, 2020—Sep 20, 2020

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
140C	Chatfield-Hollis-Canton complex, 8 to 15 percent slopes, rocky	0.4	10.4%
299	Udorthents, smoothed	3.8	89.6%
Totals for Area of Interest		4.2	100.0%

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however,

Custom Soil Resource Report

onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An *association* is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Rockingham County, New Hampshire

140C—Chatfield-Hollis-Canton complex, 8 to 15 percent slopes, rocky

Map Unit Setting

National map unit symbol: 2w82s

Elevation: 0 to 980 feet

Mean annual precipitation: 36 to 71 inches

Mean annual air temperature: 39 to 55 degrees F

Frost-free period: 145 to 240 days

Farmland classification: Not prime farmland

Map Unit Composition

Chatfield, very stony, and similar soils: 35 percent

Canton, very stony, and similar soils: 25 percent

Hollis, very stony, and similar soils: 25 percent

Minor components: 15 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Chatfield, Very Stony

Setting

Landform: Ridges, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

O_i - 0 to 1 inches: slightly decomposed plant material

A - 1 to 2 inches: fine sandy loam

B_w - 2 to 30 inches: gravelly fine sandy loam

2R - 30 to 40 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 20 to 41 inches to lithic bedrock

Drainage class: Well drained

Runoff class: High

Capacity of the most limiting layer to transmit water (K_{sat}): Very low (0.00 to 0.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 4.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Custom Soil Resource Report

Hydric soil rating: No

Description of Hollis, Very Stony

Setting

Landform: Ridges, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex

Across-slope shape: Linear, convex

Parent material: Coarse-loamy melt-out till derived from granite, gneiss, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 7 inches: gravelly fine sandy loam

Bw - 7 to 16 inches: gravelly fine sandy loam

2R - 16 to 26 inches: bedrock

Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 8 to 23 inches to lithic bedrock

Drainage class: Somewhat excessively drained

Runoff class: Very high

Capacity of the most limiting layer to transmit water (Ksat): Very low (0.00 to 0.00 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Very low (about 2.7 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: D

Ecological site: F144AY033MA - Shallow Dry Till Uplands

Hydric soil rating: No

Description of Canton, Very Stony

Setting

Landform: Ridges, moraines, hills

Landform position (two-dimensional): Summit, shoulder, backslope

Landform position (three-dimensional): Nose slope, side slope, crest

Down-slope shape: Convex, linear

Across-slope shape: Convex

Parent material: Coarse-loamy over sandy melt-out till derived from gneiss, granite, and/or schist

Typical profile

Oi - 0 to 2 inches: slightly decomposed plant material

A - 2 to 5 inches: fine sandy loam

Bw1 - 5 to 16 inches: fine sandy loam

Bw2 - 16 to 22 inches: gravelly fine sandy loam

2C - 22 to 67 inches: gravelly loamy sand

Custom Soil Resource Report

Properties and qualities

Slope: 8 to 15 percent

Surface area covered with cobbles, stones or boulders: 1.6 percent

Depth to restrictive feature: 19 to 39 inches to strongly contrasting textural stratification

Drainage class: Well drained

Runoff class: Low

Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)

Depth to water table: More than 80 inches

Frequency of flooding: None

Frequency of ponding: None

Maximum salinity: Nonsaline (0.0 to 1.9 mmhos/cm)

Available water supply, 0 to 60 inches: Low (about 3.4 inches)

Interpretive groups

Land capability classification (irrigated): None specified

Land capability classification (nonirrigated): 6s

Hydrologic Soil Group: B

Ecological site: F144AY034CT - Well Drained Till Uplands

Hydric soil rating: No

Minor Components

Newfields, very stony

Percent of map unit: 5 percent

Landform: Moraines, hills, ground moraines

Landform position (two-dimensional): Footslope

Landform position (three-dimensional): Base slope

Down-slope shape: Linear

Across-slope shape: Concave

Hydric soil rating: No

Freetown

Percent of map unit: 5 percent

Landform: Swamps, marshes, kettles, depressions, bogs

Down-slope shape: Concave

Across-slope shape: Concave

Hydric soil rating: Yes

Scarboro, very stony

Percent of map unit: 3 percent

Landform: Outwash deltas, outwash terraces, drainageways, depressions

Landform position (three-dimensional): Tread

Down-slope shape: Concave

Across-slope shape: Concave, linear

Hydric soil rating: Yes

Rock outcrop

Percent of map unit: 2 percent

Landform: Ridges, hills

Hydric soil rating: Unranked

299—Udorthents, smoothed

Map Unit Setting

National map unit symbol: 9cmt

Elevation: 0 to 840 feet

Mean annual precipitation: 44 to 49 inches

Mean annual air temperature: 48 degrees F

Frost-free period: 155 to 165 days

Farmland classification: Not prime farmland

Map Unit Composition

Udorthents and similar soils: 100 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Udorthents

Properties and qualities

Depth to restrictive feature: More than 80 inches

Drainage class: Excessively drained

Depth to water table: More than 80 inches

Frequency of flooding: None

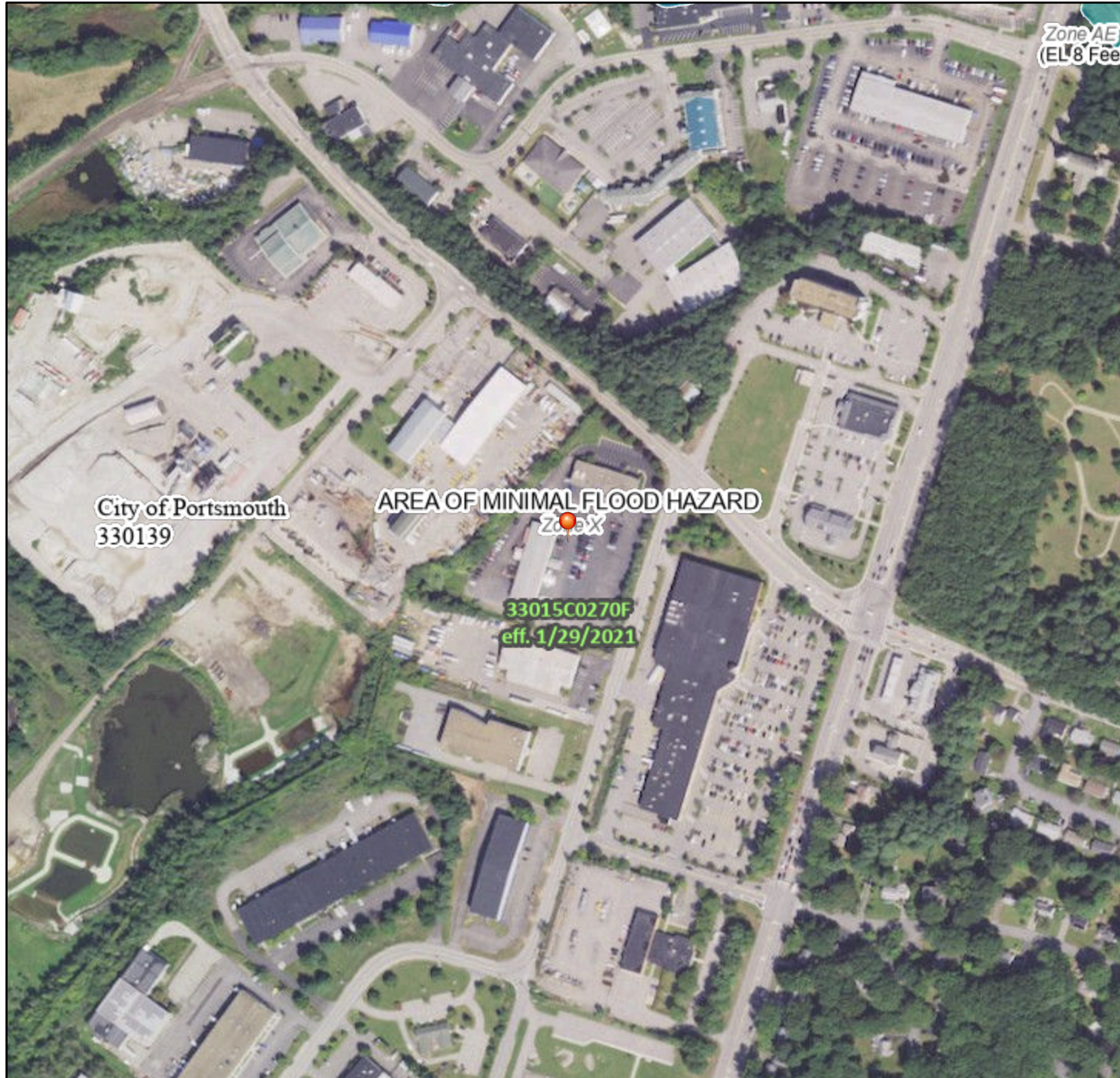
Frequency of ponding: None

APPENDIX E
FEMA FIRM MAP

National Flood Hazard Layer FIRMMette



70°46'51"W 43°2'58"N



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

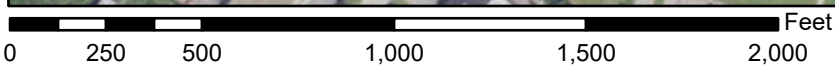
SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
OTHER FEATURES		Levee, Dike, or Floodwall
		20.2 Cross Sections with 1% Annual Chance Water Surface Elevation
MAP PANELS		17.5 Coastal Transect
		Base Flood Elevation Line (BFE)
		Limit of Study
		Jurisdiction Boundary
		Coastal Transect Baseline
		Profile Baseline
		Hydrographic Feature
MAP PANELS		Digital Data Available
		No Digital Data Available
		Unmapped
		The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **6/21/2023 at 11:41 AM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

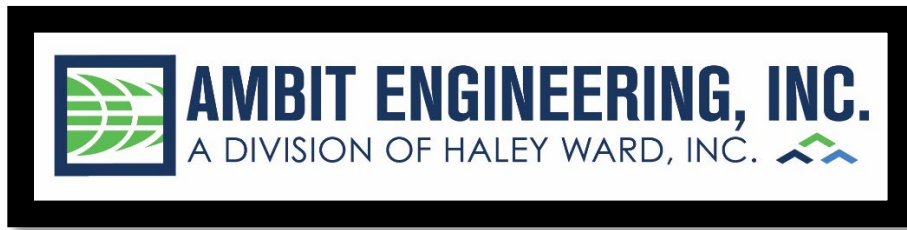


1:6,000

70°46'13"W 43°2'31"N

Basemap Imagery Source: USGS National Map 2023

APPENDIX F
INSPECTION & LONG TERM
MAINTENANCE PLAN



***INSPECTION & LONG-TERM MAINTENANCE PLAN
FOR
BUILDING ADDITION***

**700 PEVERLY HILL ROAD
PORTSMOUTH, NH**

Introduction

The intent of this plan is to provide Portsmouth Auto Body Center (herein referred to as “owner”) with a list of procedures that document the inspection and maintenance requirements of the stormwater management system for this development. Specifically, the Bioretention system other and Best Management Practices (collectively referred to as the “Stormwater Management System”). The contact information for the owner shall be kept current, and if there is a change of ownership of the property this plan must be transferred to the new owner.

The following inspection and maintenance program is necessary to keep the stormwater management system functioning properly and will help in maintaining a high quality of stormwater runoff to minimize potential environmental impacts. By following the enclosed procedures, the owner will be able to maintain the functional design of the stormwater management system and maximize its ability to remove sediment and other contaminants from site generated stormwater runoff.

Annual Report

The owner shall prepare an annual Inspection & Maintenance Report. The report shall include a summary of the system’s maintenance and repair by transmission of the Inspection & Maintenance Log and other information as required. A copy of the report shall be delivered annually to the Portsmouth DPW, if required.

Inspection & Maintenance Checklist/Log

The following pages contain the Stormwater Management System Inspection & Maintenance Requirements and a blank copy of the Stormwater Management System Inspection & Maintenance Log. These forms are provided to the owner as a guideline for performing the inspection and maintenance of the Stormwater Management System. This is a guideline and should be periodically reviewed for conformance with current practice and standards.

Stormwater Management System Components

The Stormwater Management System is designed to mitigate the quality of site-generated stormwater runoff. As a result, the design includes the following elements:

Non-Structural BMPs

Non-Structural best management practices (BMP's) include temporary and permanent measures that typically require less labor and capital inputs and are intended to provide protection against erosion of soils. Examples of non-structural BMP's on this project include but are not limited to:

- Temporary and Permanent mulching
- Temporary and Permanent grass cover
- Trees
- Shrubs and ground covers
- Miscellaneous landscape plantings
- Dust control
- Tree protection
- Topsoiling
- Sediment barriers
- Stabilized construction entrance

Inspection and Maintenance Requirements

The following summarizes the inspection and maintenance requirements for the various BMP's that may be found on this project.

1. **Grassed areas and swales (until established):** After each rain event of 0.5" or more during a 24-hour period, inspect grassed areas for signs of disturbance, such as erosion. If damaged areas are discovered, immediately repair the damage. Repairs may include adding new topsoil, lime, seed, fertilizer and mulch.
2. **Plantings:** Planting and landscaping (trees, shrubs) shall be monitored bi-monthly during the first year to insure viability and vigorous growth. Replace dead or dying vegetation with new stock and make adjustments to the conditions that caused the dead or dying vegetation. During dryer times of the year, provide weekly watering or irrigation during the establishment period of the first year. Make the necessary adjustments to ensure long-term health of the vegetated covers, i.e. provide more permanent mulch or compost or other means of protection.
3. **Storm Drain and Catch Basin Inlets/Outlets:** Monitor drain inlets and outlet aprons for excessive accumulation of sediments, in excess of 1 foot in the sump, or missing stone/riprap, monthly for the first year following construction, every other month thereafter. Remove sediments as required to maintain filtering capabilities of the stone—replace missing riprap. Prior to the end of construction, inspect the drains and basins for accumulations and remove and clean by jet-vacuuming.
4. **Detention Pond:** After installation of the infiltration detention pond, perform the following inspections weekly until vegetation is established after construction, then on a bi-annual basis

and after heavy rains thereafter:

- a. Monitor for excessive or concentrated accumulations of debris, or erosion in excess of 2 inches below the various pipe inlets. Remove debris as required and replace or augment inlet fabric strips.
- b. Monitor the outfall structure for problems with uneven flow or clogged pipes. Repair or remove clogs as required.
- c. Monitor vegetation on pond and replace dead or dying vegetation as required.
- d. Monitor rodent screens and repair or replace as required.
- e. Monitor side slopes of ponds for damage or erosion in excess of 2 inches—repair, as necessary.
- f. If surface ponds for longer than 24 hours following a storm, remove and replace the top 6 inches of soil.
- g. Monitor any sediment forebays for sediment accumulation and remove sediments and dead and dying vegetation where necessary.

Pollution Prevention

The following pollution prevention activities shall be undertaken to minimize potential impacts on stormwater runoff quality. The Contractor is responsible for all activities during construction. The Owner is responsible thereafter.

Spill Procedures

Any discharge of waste oil or other pollutant shall be reported immediately to the New Hampshire Department of Environmental Services (NHDES). The Contractor/Owner will be responsible for any incident of groundwater contamination resulting from the improper discharge of pollutants to the stormwater system, and may be required by NHDES to remediate incidents that may impact groundwater quality. If the property ownership is transferred, the new owner will be informed of the legal responsibilities associated with operation of the stormwater system, as indicated above.

Sanitary Facilities

Sanitary facilities shall be provided during all phases of construction.

Material Storage

No on site trash facility is provided until site is constructed. The contractors are required to remove trash from the site. Hazardous material storage is prohibited.

Material Disposal

All waste material, trash, sediment, and debris shall be removed from the site and disposed of in accordance with applicable local, state, and federal guidelines and regulations. Removed sediments shall be if necessary dewatered prior to disposal.

Invasive Species

Monitor the Stormwater Management System for signs of invasive species growth. If caught early, their eradication is much easier. The most likely places where invasions start is in wetter, disturbed soils or detention ponds. Species such as phragmites and purple loose-strife are common invaders in these wetter areas. If they are found, the owner shall refer to the fact-sheet created by the University of New Hampshire Cooperative Extension or contact a wetlands scientist with experience in invasive species control to implement a plan of action for eradication. Measures that do not require the application of chemical herbicides should be the first line of defense.



Figure 1: *Lythrum salicaria*, Purple Loosestrife. Photo by Liz West.

Figure 2: *Phragmites australis*. Photo by Le Loup Gris

CATCH BASIN BASKET CONSTRUCTION MAINTENANCE SHEET

INSPECTION REQUIREMENTS		
ACTION TAKEN	FREQUENCY	MAINTENANCE REQUIREMENTS
-Check for damage to basket -Remove sediment from basket	Within 24 hours of rainfall, Daily during extended rainfall	<i>-Repair basket as necessary to prevent particles from reaching drainage system, or to prevent flooding.</i> <i>-Empty basket after every storm, or if clogged.</i>

MAINTENANCE LOG	
PROJECT NAME	
INSPECTOR NAME	INSPECTOR CONTACT INFO
DATE OF INSPECTION	REASON FOR INSPECTION <input type="checkbox"/> LARGE STORM EVENT <input type="checkbox"/> PERIODIC CHECK-IN
IS CORRECTIVE ACTION NEEDED? <input type="checkbox"/> YES <input type="checkbox"/> NO	DESCRIBE ANY PROBLEMS, NEEDED MAINTENANCE
DATE OF MAINTENANCE	PERFORMED BY
NOTES	

CLOSED DRAINAGE STRUCTURE LONG-TERM MAINTENANCE SHEET

INSPECTION REQUIREMENTS		
ACTION TAKEN	FREQUENCY	MAINTENANCE REQUIREMENTS
<ul style="list-style-type: none"> -Outlet Control Structures -Drain Manholes -Catch Basins 	Every other Month	<ul style="list-style-type: none"> <i>Check for erosion or short-circuiting</i> <i>Check for sediment accumulation</i> <i>Check for floatable contaminants</i>
<ul style="list-style-type: none"> -Drainage Pipes 	1 time per 2 years	<ul style="list-style-type: none"> <i>Check for sediment accumulation/clogging, or soiled runoff.</i> <i>Check for erosion at outlets.</i>

MAINTENANCE LOG	
PROJECT NAME	
INSPECTOR NAME	INSPECTOR CONTACT INFO
DATE OF INSPECTION	REASON FOR INSPECTION <input type="checkbox"/> LARGE STORM EVENT <input type="checkbox"/> PERIODIC CHECK-IN
IS CORRECTIVE ACTION NEEDED? <input type="checkbox"/> YES <input type="checkbox"/> NO	DESCRIBE ANY PROBLEMS, NEEDED MAINTENANCE
DATE OF MAINTENANCE	PERFORMED BY
NOTES	

DETENTION POND LONG-TERM MAINTENANCE SHEET

INSPECTION REQUIREMENTS		
ACTION TAKEN	FREQUENCY	MAINTENANCE REQUIREMENTS
POND SURFACE -Check for sediment accumulation/clogging of filter. -Check for ponding water > 24 hours over the filter.	Weekly until vegetation is established, then bi-annually and after heavy rains	-Replace dead or dying vegetation -Remove sediments when required -Mow grasses at least twice yearly -If system ponds longer than 24 hours, then a qualified professional should assess the condition of the facility to determine measures required to restore infiltration function.
FOREBAY -Monitor Sediment Accumulation	Bi-annually	-Replace dead or dying vegetation -Remove Sediments When Required

MAINTENANCE LOG	
PROJECT NAME	
INSPECTOR NAME	INSPECTOR CONTACT INFO
DATE OF INSPECTION	REASON FOR INSPECTION <input type="checkbox"/> LARGE STORM EVENT <input type="checkbox"/> PERIODIC CHECK-IN
IS CORRECTIVE ACTION NEEDED? <input type="checkbox"/> YES <input type="checkbox"/> NO	DESCRIBE ANY PROBLEMS, NEEDED MAINTENANCE
DATE OF MAINTENANCE	PERFORMED BY
NOTES	

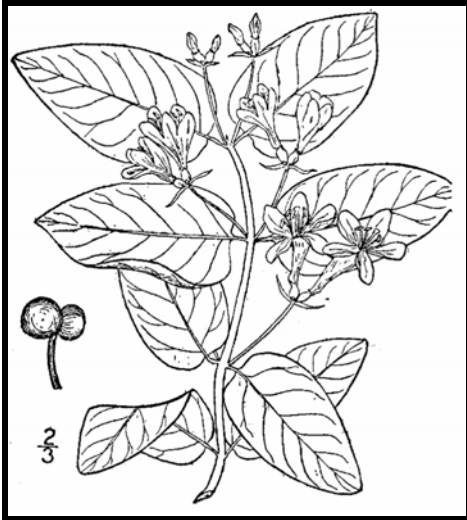
STABILIZED CONSTRUCTION ENTRANCE CONSTRUCTION MAINTENANCE SHEET

INSPECTION REQUIREMENTS		
ACTION TAKEN	FREQUENCY	MAINTENANCE REQUIREMENTS
ENTRANCE SURFACE <i>-Check for sediment accumulation/clogging of stone</i> <i>-Check Vegetative filter strips</i>	After heavy rains, as necessary	<i>-Top dress pad with new stone.</i> <i>-Replace stone completely if completely clogged.</i> <i>-Maintain vigorous stand of vegetation.</i>
WASHING FACILITIES (if applicable) <i>-Monitor Sediment Accumulation</i>	As often as necessary	<i>-Remove Sediments from traps.</i>

MAINTENANCE LOG	
PROJECT NAME	
INSPECTOR NAME	INSPECTOR CONTACT INFO
DATE OF INSPECTION	REASON FOR INSPECTION <input type="checkbox"/> LARGE STORM EVENT <input type="checkbox"/> PERIODIC CHECK-IN
IS CORRECTIVE ACTION NEEDED? <input type="checkbox"/> YES <input type="checkbox"/> NO	DESCRIBE ANY PROBLEMS, NEEDED MAINTENANCE
DATE OF MAINTENANCE	PERFORMED BY
NOTES	

Methods for Disposing Non-Native Invasive Plants

Prepared by the Invasives Species Outreach Group, volunteers interested in helping people control invasive plants. Assistance provided by the Piscataquog Land Conservancy and the NH Invasives Species Committee. Edited by Karen Bennett, Extension Forestry Professor and Specialist.



Tatarian honeysuckle

Lonicera tatarica

USDA-NRCS PLANTS Database / Britton, N.L., and A. Brown. 1913. *An illustrated flora of the northern United States, Canada and the British Possessions*. Vol. 3: 282.

Non-native invasive plants crowd out natives in natural and managed landscapes. They cost taxpayers billions of dollars each year from lost agricultural and forest crops, decreased biodiversity, impacts to natural resources and the environment, and the cost to control and eradicate them.

Invasive plants grow well even in less than desirable conditions such as sandy soils along roadsides, shaded wooded areas, and in wetlands. In ideal conditions, they grow and spread even faster. There are many ways to remove these non-native invasives, but once removed, care is needed to dispose the removed plant material so the plants don't grow where disposed.

Knowing how a particular plant reproduces indicates its method of spread and helps determine the appropriate disposal method. Most are spread by seed and are dispersed by wind, water, animals, or people. Some reproduce by vegetative means from pieces of stems or roots forming new plants. Others spread through both seed and vegetative means.

Because movement and disposal of viable plant parts is restricted (see NH Regulations), viable invasive parts can't be brought to most transfer stations in the state. Check with your transfer station to see if there is an approved, designated area for invasives disposal. This fact sheet gives recommendations for rendering plant parts non-viable.

Control of invasives is beyond the scope of this fact sheet. For information about control visit www.nhinvasives.org or contact your UNH Cooperative Extension office.

New Hampshire Regulations

Prohibited invasive species shall only be disposed of in a manner that renders them nonliving and nonviable. (Agr. 3802.04)

No person shall collect, transport, import, export, move, buy, sell, distribute, propagate or transplant any living and viable portion of any plant species, which includes all of their cultivars and varieties, listed in Table 3800.1 of the New Hampshire prohibited invasive species list. (Agr. 3802.01)

How and When to Dispose of Invasives?

To prevent seed from spreading remove invasive plants before seeds are set (produced). Some plants continue to grow, flower and set seed even after pulling or cutting. Seeds can remain viable in the ground for many years. If the plant has flowers or seeds, place the flowers and seeds in a heavy plastic bag “head first” at the weeding site and transport to the disposal site. The following are general descriptions of disposal methods. See the chart for recommendations by species.

Burning: Large woody branches and trunks can be used as firewood or burned in piles. For outside burning, a written fire permit from the local forest fire warden is required unless the ground is covered in snow. Brush larger than 5 inches in diameter can't be burned. Invasive plants with easily airborne seeds like black swallow-wort with mature seed pods (indicated by their brown color) shouldn't be burned as the seeds may disperse by the hot air created by the fire.

Bagging (solarization): Use this technique with softer-tissue plants. Use heavy black or clear plastic bags (contractor grade), making sure that no parts of the plants poke through. Allow the bags to sit in the sun for several weeks and on dark pavement for the best effect.

Tarping and Drying: Pile material on a sheet of plastic and cover with a tarp, fastening the tarp to the ground and monitoring it for escapes. Let the material dry for several weeks, or until it is clearly nonviable.

Chipping: Use this method for woody plants that don't reproduce vegetatively.

Burying: This is risky, but can be done with watchful diligence. Lay thick plastic in a deep pit before placing the cut up plant material in the hole. Place the material away from the edge of the plastic before covering it with more heavy plastic. Eliminate as much air as possible and toss in soil to weight down the material in the pit. Note that the top of the buried material should be at least three feet underground. Japanese knotweed should be at least 5 feet underground!

Drowning: Fill a large barrel with water and place soft-tissue plants in the water. Check after a few weeks and look for rotted plant material (roots, stems, leaves, flowers). Well-rotted plant material may be composted. A word of caution- seeds may still be viable after using this method. Do this before seeds are set. This method isn't used often. Be prepared for an awful stink!

Composting: Invasive plants can take root in compost. Don't compost any invasives unless you know there is no viable (living) plant material left. Use one of the above techniques (bagging, tarping, drying, chipping, or drowning) to render the plants nonviable before composting. Closely examine the plant before composting and avoid composting seeds.






Japanese knotweed
Polygonum cuspidatum
USDA-NRCS PLANTS Database /
Britton, N.L., and A. Brown. 1913. *An illustrated flora of the northern United States, Canada and the British Possessions*. Vol. 1: 676.

Be diligent looking for seedlings for years in areas where removal and disposal took place.

Suggested Disposal Methods for Non-Native Invasive Plants

This table provides information concerning the disposal of removed invasive plant material. If the infestation is treated with herbicide and left in place, these guidelines don't apply. Don't bring invasives to a local transfer station, unless there is a designated area for their disposal, or they have been rendered non-viable. This listing includes wetland and upland plants from the New Hampshire Prohibited Invasive Species List. The disposal of aquatic plants isn't addressed.

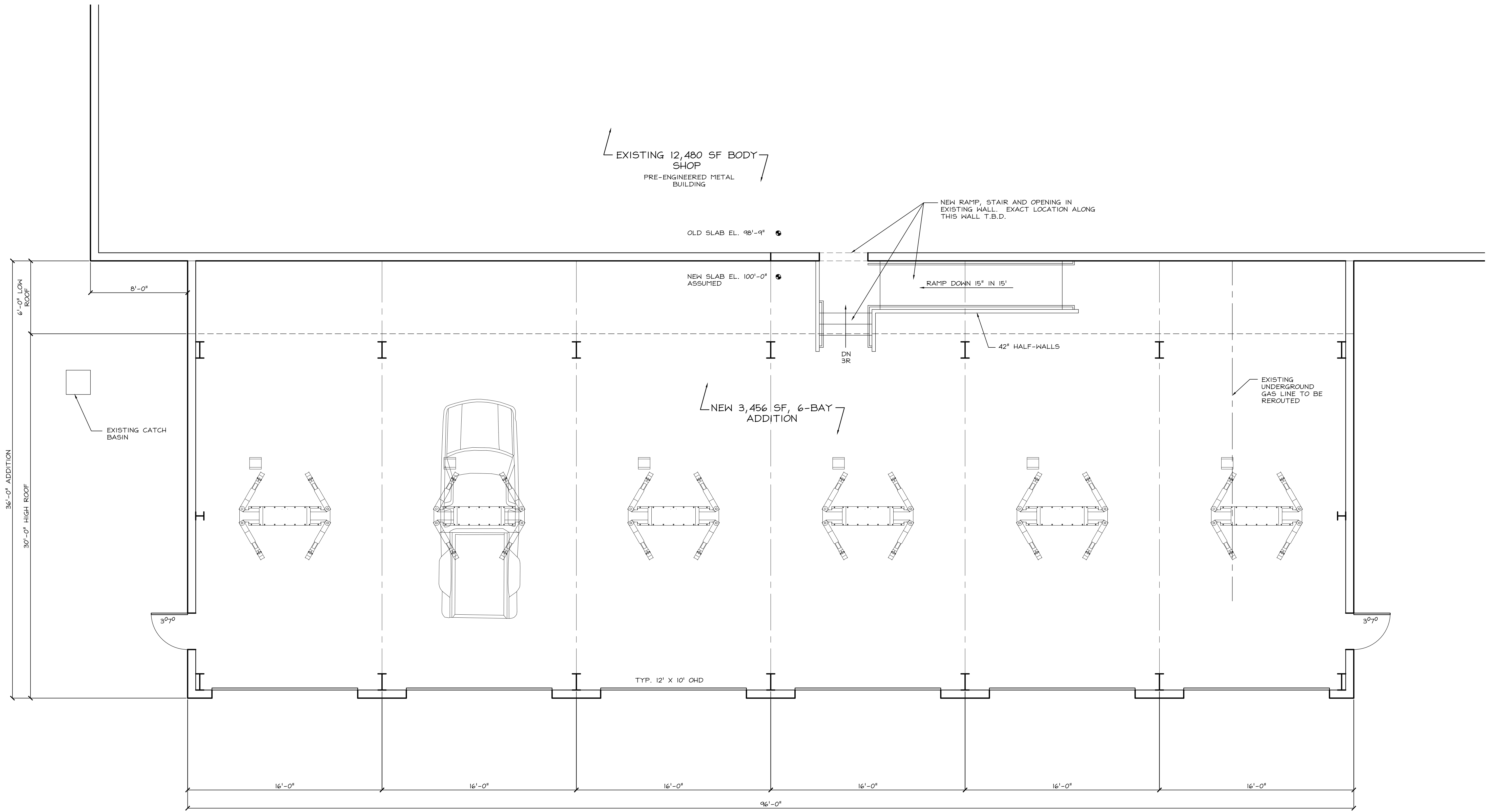
Woody Plants	Method of Reproducing	Methods of Disposal
Norway maple <i>(Acer platanoides)</i> European barberry <i>(Berberis vulgaris)</i> Japanese barberry <i>(Berberis thunbergii)</i> autumn olive <i>(Elaeagnus umbellata)</i> burning bush <i>(Euonymus alatus)</i> Morrow's honeysuckle <i>(Lonicera morrowii)</i> Tatarian honeysuckle <i>(Lonicera tatarica)</i> showy bush honeysuckle <i>(Lonicera x bella)</i> common buckthorn <i>(Rhamnus cathartica)</i> glossy buckthorn <i>(Frangula alnus)</i>		<p>Prior to fruit/seed ripening</p> <p>Seedlings and small plants</p> <ul style="list-style-type: none"> ▪ Pull or cut and leave on site with roots exposed. No special care needed. <p>Larger plants</p> <ul style="list-style-type: none"> ▪ Use as firewood. ▪ Make a brush pile. ▪ Chip. ▪ Burn.
		<p>After fruit/seed is ripe</p> <p>Don't remove from site.</p> <ul style="list-style-type: none"> ▪ Burn. ▪ Make a covered brush pile. ▪ Chip once all fruit has dropped from branches. ▪ Leave resulting chips on site and monitor.
oriental bittersweet <i>(Celastrus orbiculatus)</i> multiflora rose <i>(Rosa multiflora)</i>		<p>Prior to fruit/seed ripening</p> <p>Seedlings and small plants</p> <ul style="list-style-type: none"> ▪ Pull or cut and leave on site with roots exposed. No special care needed. <p>Larger plants</p> <ul style="list-style-type: none"> ▪ Make a brush pile. ▪ Burn.
		<p>After fruit/seed is ripe</p> <p>Don't remove from site.</p> <ul style="list-style-type: none"> ▪ Burn. ▪ Make a covered brush pile. ▪ Chip – only after material has fully dried (1 year) and all fruit has dropped from branches. Leave resulting chips on site and monitor.

Non-Woody Plants	Method of Reproducing	Methods of Disposal
<p>garlic mustard (<i>Alliaria petiolata</i>)</p> <p>spotted knapweed (<i>Centaurea maculosa</i>)</p> <ul style="list-style-type: none"> ▪ Sap of related knapweed can cause skin irritation and tumors. Wear gloves when handling. <p>black swallow-wort (<i>Cynanchum nigrum</i>)</p> <ul style="list-style-type: none"> ▪ May cause skin rash. Wear gloves and long sleeves when handling. <p>pale swallow-wort (<i>Cynanchum rossicum</i>)</p> <p>giant hogweed (<i>Heracleum mantegazzianum</i>)</p> <ul style="list-style-type: none"> ▪ Can cause major skin rash. Wear gloves and long sleeves when handling. <p>dame's rocket (<i>Hesperis matronalis</i>)</p> <p>perennial pepperweed (<i>Lepidium latifolium</i>)</p> <p>purple loosestrife (<i>Lythrum salicaria</i>)</p> <p>Japanese stilt grass (<i>Microstegium vimineum</i>)</p> <p>mile-a-minute weed (<i>Polygonum perfoliatum</i>)</p>	<p>Fruits and Seeds</p> 	<p>Prior to flowering</p> <p>Depends on scale of infestation</p> <p>Small infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and leave on site with roots exposed. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and pile. (You can pile onto or cover with plastic sheeting). ▪ Monitor. Remove any re-sprouting material. <hr/> <p>During and following flowering</p> <p>Do nothing until the following year or remove flowering heads and bag and let rot.</p> <p>Small infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and leave on site with roots exposed. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Pull or cut plant and pile remaining material. (You can pile onto plastic or cover with plastic sheeting). ▪ Monitor. Remove any re-sprouting material.
<p>common reed (<i>Phragmites australis</i>)</p> <p>Japanese knotweed (<i>Polygonum cuspidatum</i>)</p> <p>Bohemian knotweed (<i>Polygonum x bohemicum</i>)</p>	<p>Fruits, Seeds, Plant Fragments</p> <p>Primary means of spread in these species is by plant parts. Although all care should be given to preventing the dispersal of seed during control activities, the presence of seed doesn't materially influence disposal activities.</p>	<p>Small infestation</p> <ul style="list-style-type: none"> ▪ Bag all plant material and let rot. ▪ Never pile and use resulting material as compost. ▪ Burn. <p>Large infestation</p> <ul style="list-style-type: none"> ▪ Remove material to unsuitable habitat (dry, hot and sunny or dry and shaded location) and scatter or pile. ▪ Monitor and remove any sprouting material. ▪ Pile, let dry, and burn.

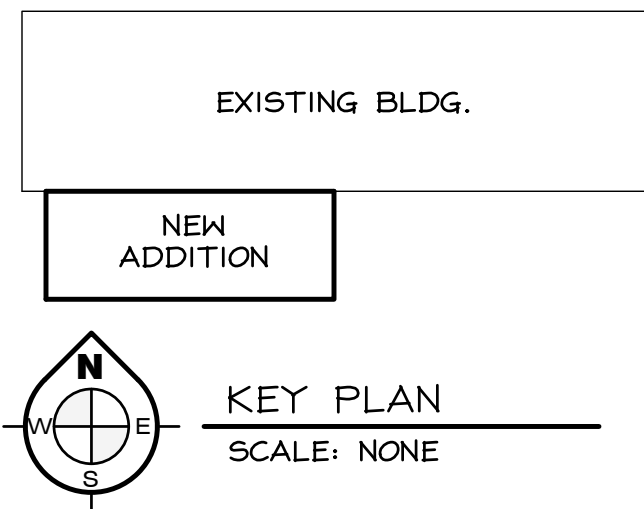
January 2010

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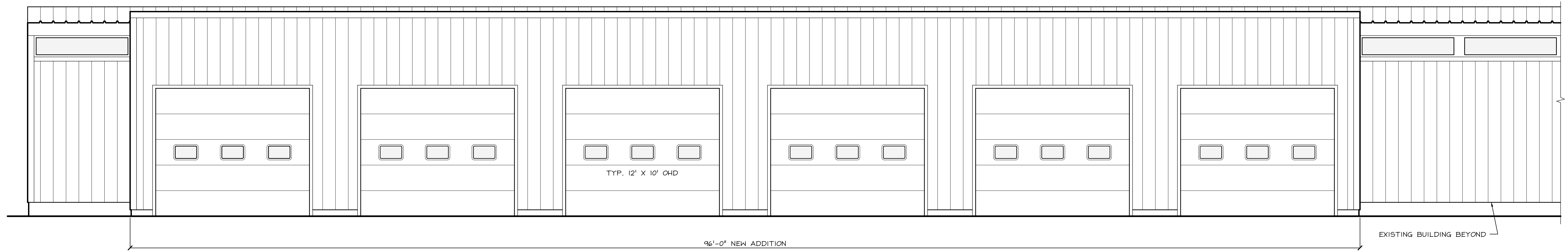
Revisions



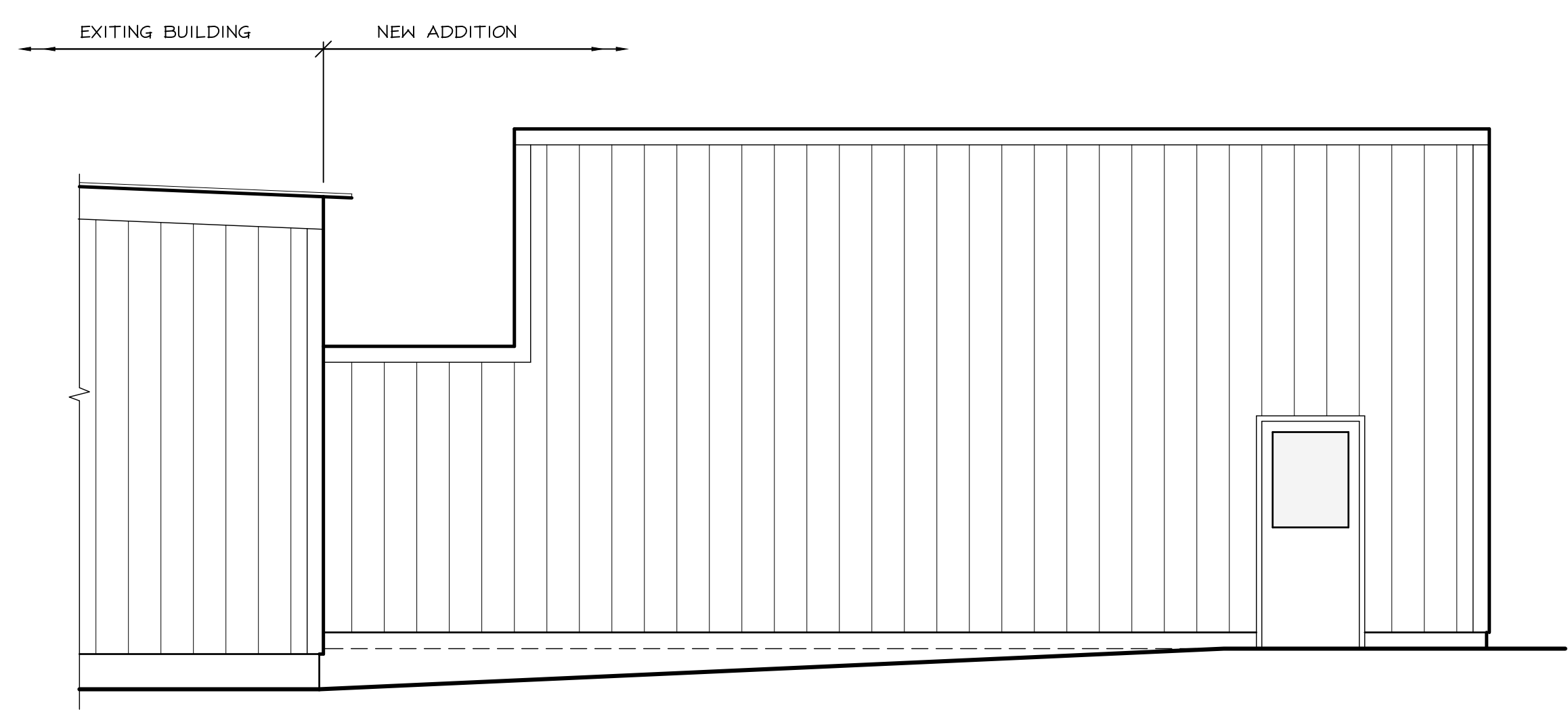
FLOOR PLAN
 SCALE: 1/4" = 1'-0"



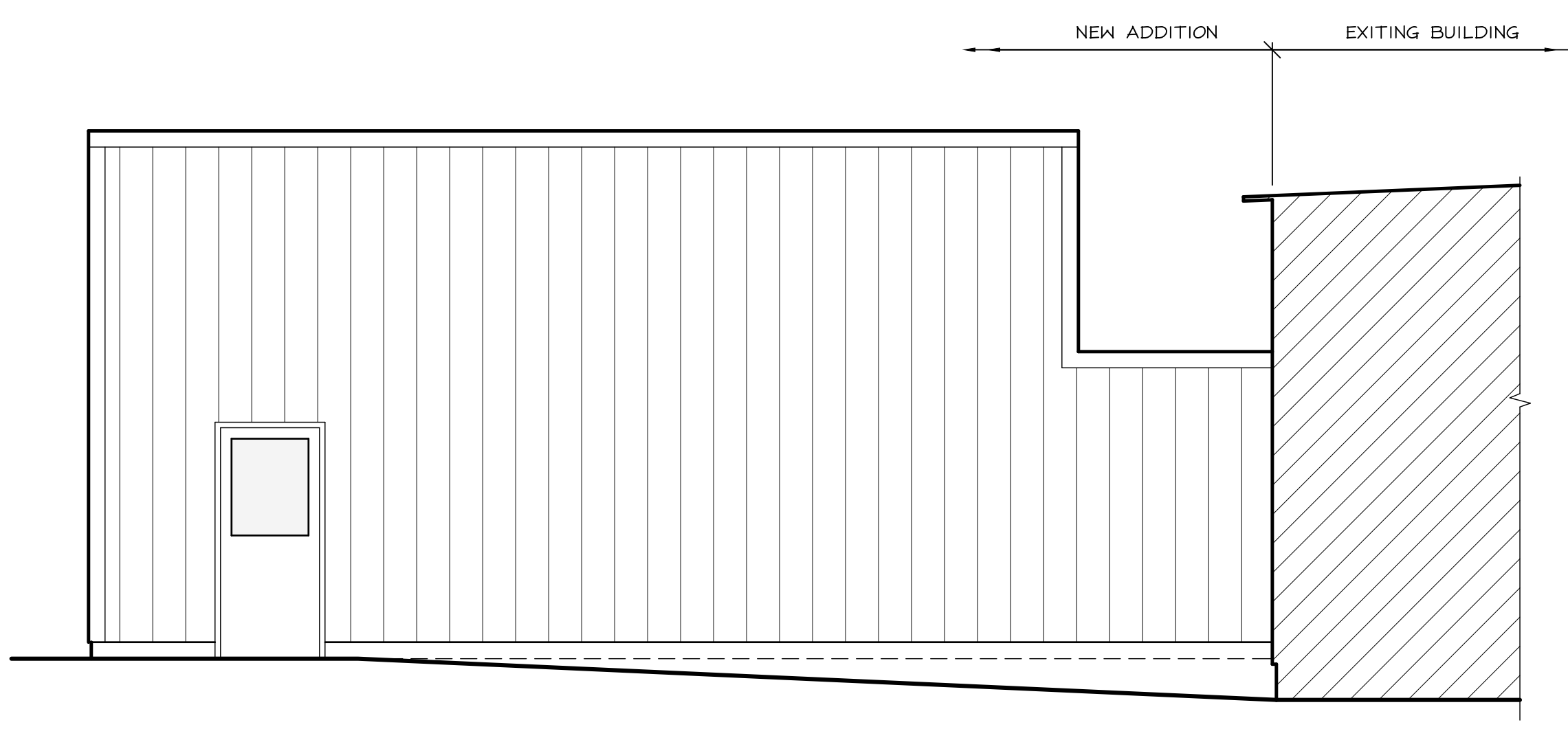
Revisions



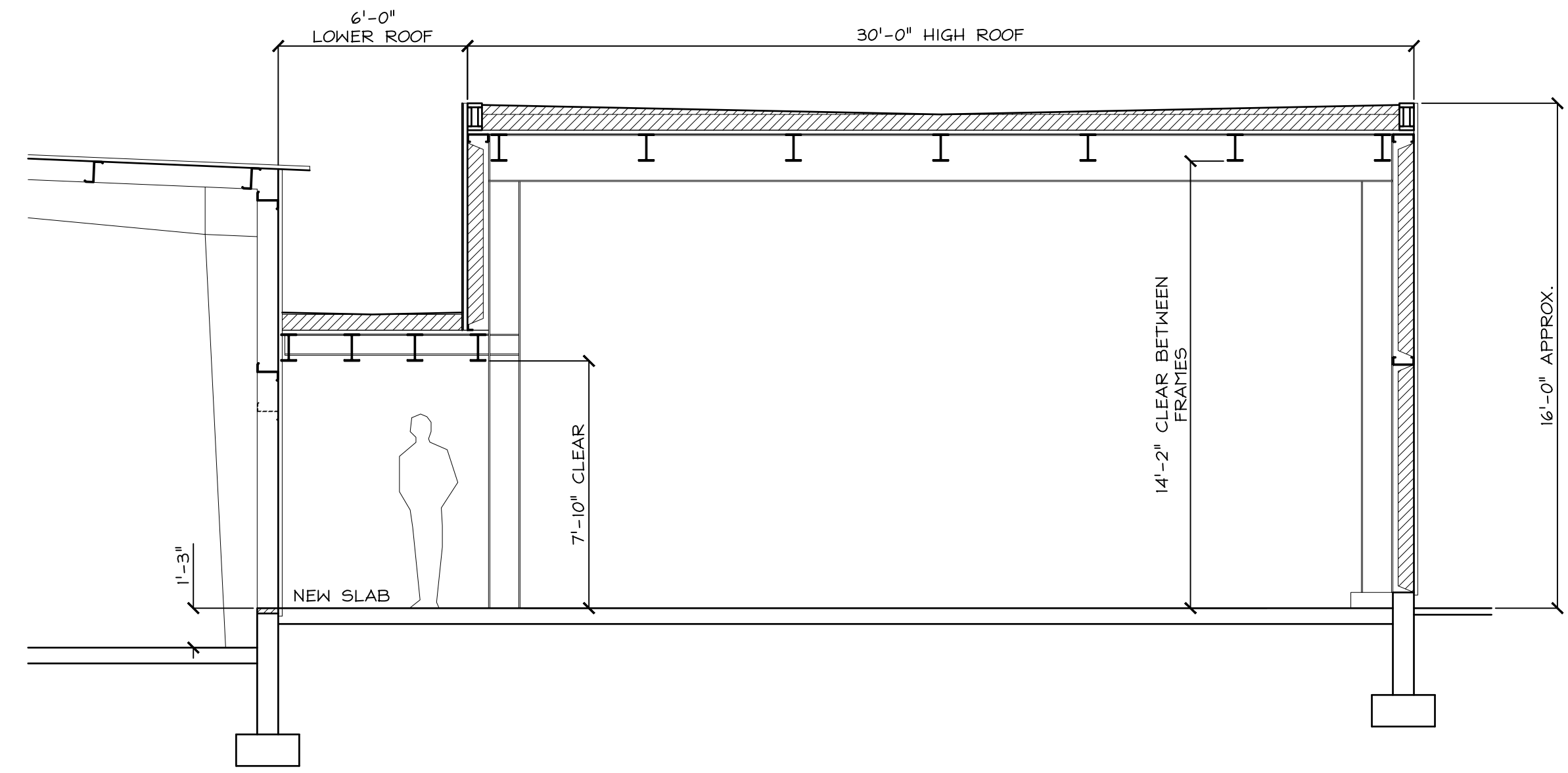
SOUTH ELEVATION
 SCALE: 1/4" = 1'-0"



WEST ELEVATION
 SCALE: 1/4" = 1'-0"



EAST ELEVATION
 SCALE: 1/4" = 1'-0"



SCHEMATIC SECTION
 SCALE: 1/4" = 1'-0"

PROPOSED BUILDING ADDITION PORTSMOUTH AUTO BODY CENTER 700 PEVERLY HILL ROAD PORTSMOUTH NEW HAMPSHIRE SITE PERMIT PLANS

PROJECT PERMITS:
PORTSMOUTH SITE PLAN: PENDING

OWNER AND APPLICANT:

JMK REALTY, LLC
PO BOX 971
PORTSMOUTH, NH 03801
TEL. (603) 431-5533

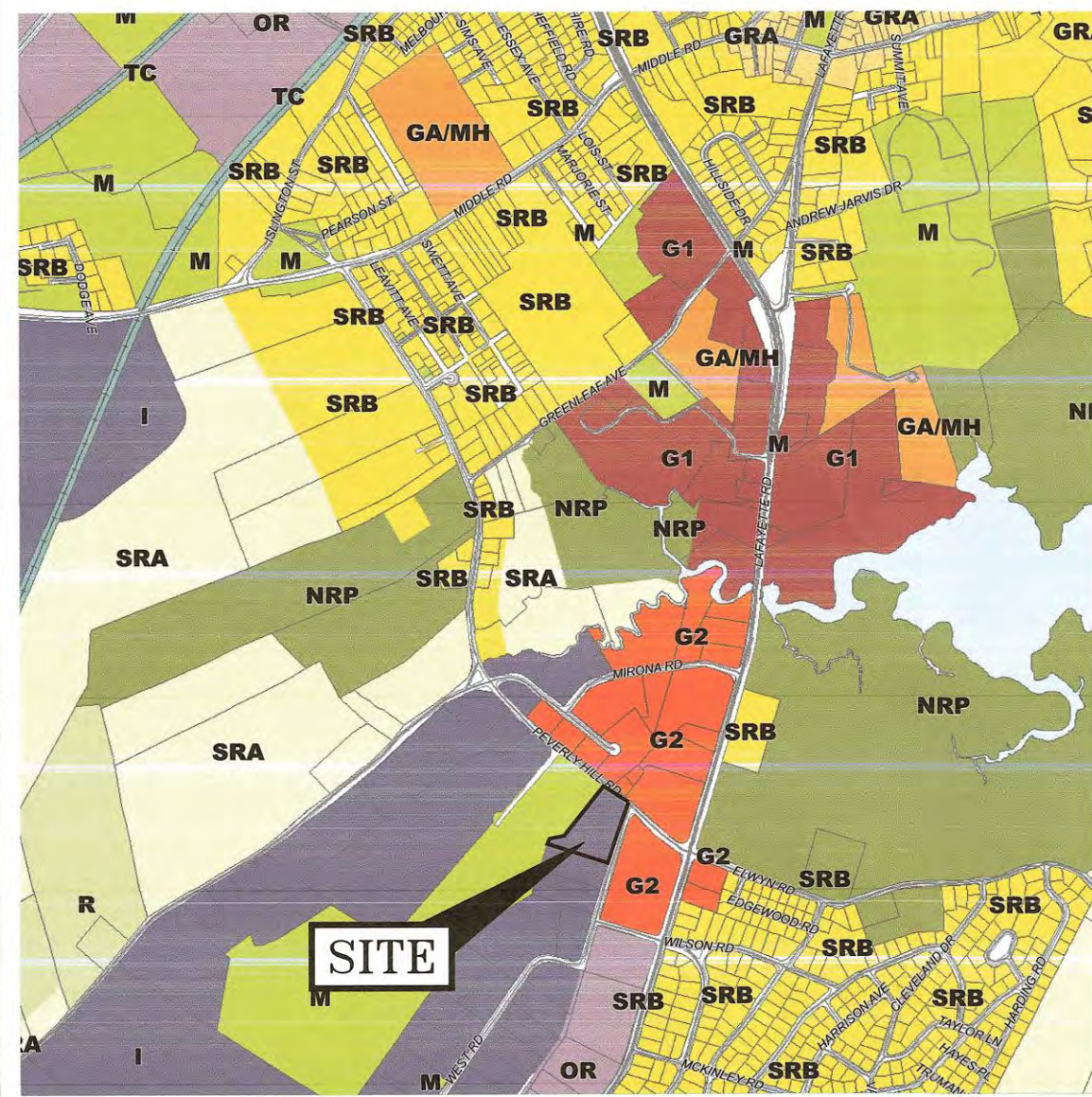
CIVIL ENGINEER & LAND SURVEYOR:

AMBIT ENGINEERING, INC.
A DIVISION OF HALEY WARD, INC.
200 GRIFFIN ROAD, UNIT 3
PORTSMOUTH, NH 03801
TEL. (603) 430-9282
FAX (603) 436-2315

CONSTRUCTION MANAGEMENT:

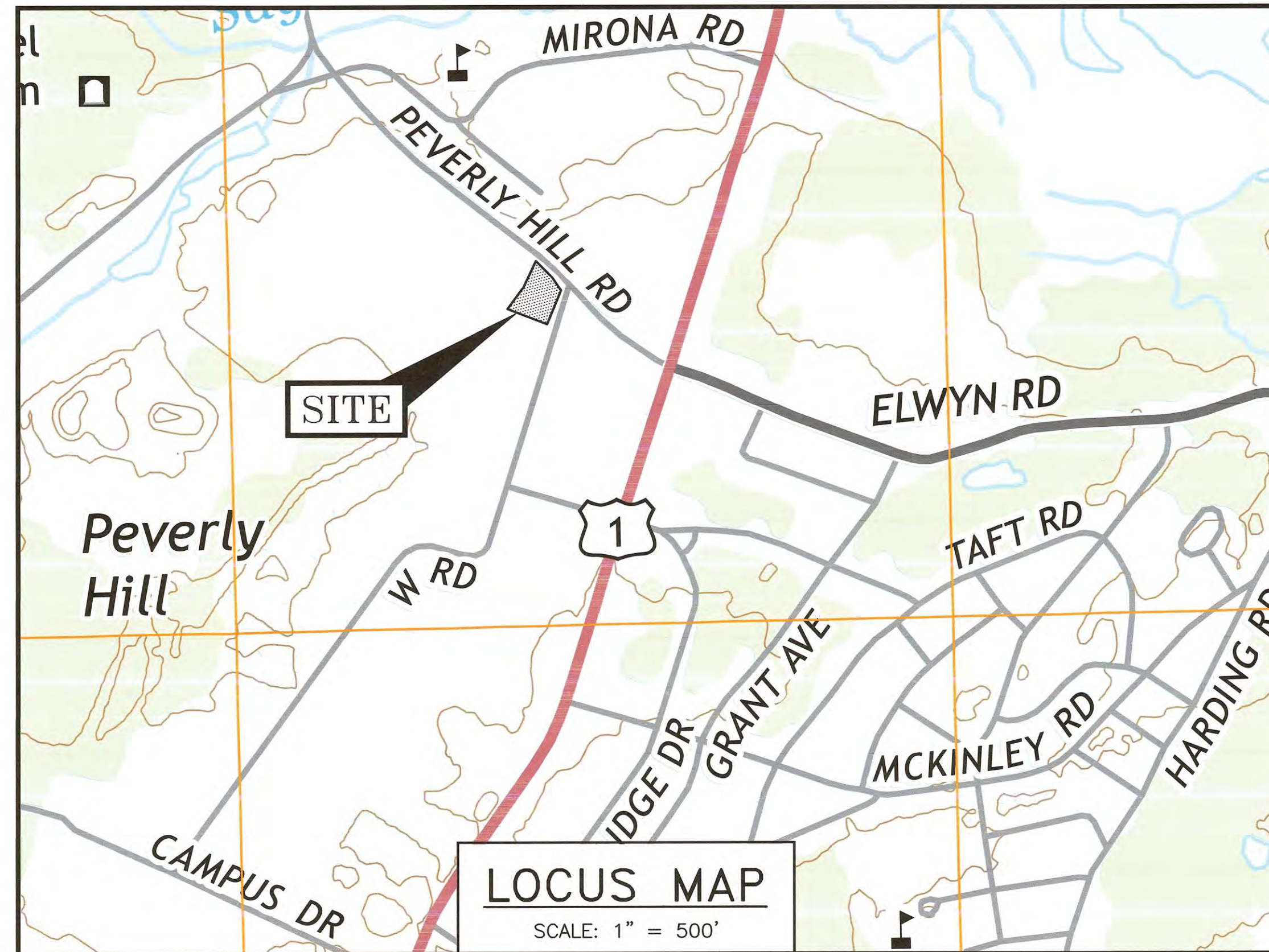
SJM CONSTRUCTION
MANAGEMENT
25 GREENVIEW LANE
SANFORD, ME 04073
TEL. (603) 235-5984

PORTSMOUTH ZONING MAP



Legend

- Character Districts**
--- Character-Based Zoning Area
(Refer to Zoning Map Sheet 2 of 2
Character Districts Regulating Plan)
- Residential Districts**
- R Rural
 - SRA Single Residence A
 - SRB Single Residence B
 - GRA General Residence A
 - GRB General Residence B
 - GRC General Residence C
 - GA/MH Garden Apartment/Mobile Home Park
- Mixed Residential Districts**
- MRO Mixed Residential Office
 - MRB Mixed Residential Business
 - G1 Gateway Corridor
 - G2 Gateway Center
- Business Districts**
- GB General Business
 - B Business
 - WB Waterfront Business
- Industrial Districts**
- OR Office Research
 - I Industrial
 - WI Waterfront Industrial



PROJECT SITE:
TAX MAP 252, LOT 2-10

PORTSMOUTH APPROVAL CONDITIONS NOTE:
ALL CONDITIONS ON THIS PLAN SET SHALL REMAIN IN EFFECT IN
PERPETUITY PURSUANT TO THE REQUIREMENTS OF THE CITY OF
PORTSMOUTH SITE PLAN REVIEW REGULATIONS.

APPROVED BY THE PORTSMOUTH PLANNING BOARD

CHAIRMAN _____ DATE _____

INDEX OF SHEETS

DWG No.	Description
-	BOUNDARY SURVEY PLAN
C1	EXISTING CONDITIONS & DEMOLITION PLAN
C2	SITE PLAN
C3	GRADING PLAN
C4	UTILITY PLAN
D1-D2	DETAILS & EROSION CONTROL

UTILITY CONTACTS

ELECTRIC:
EVERSOURCE
1700 LAFAYETTE ROAD
PORTSMOUTH, N.H. 03801
Tel. (603) 436-7708, Ext. 555.5678
ATTN: MICHAEL BUSBY, P.E. (MANAGER)

NATURAL GAS:
UNITIL
325 WEST ROAD
PORTSMOUTH, N.H. 03801
Tel. (603) 294-5144
ATTN: DAVE BEAULIEU

CABLE:
COMCAST
155 COMMERCE WAY
PORTSMOUTH, N.H. 03801
Tel. (603) 679-5695 (X1037)
ATTN: MIKE COLLINS

SEWER & WATER:
PORTSMOUTH DEPARTMENT OF PUBLIC WORKS
680 PEVERLY HILL ROAD
PORTSMOUTH, N.H. 03801
Tel. (603) 427-1530
ATTN: JIM TOW

COMMUNICATIONS:
CONSOLIDATED
COMMUNICATIONS
JOE CONSIDINE
1575 GREENLAND ROAD
GREENLAND, N.H. 03840
Tel. (603) 427-5525

LEGEND:

EXISTING	PROPOSED	DESCRIPTION
---	---	PROPERTY LINE
---	---	SETBACK
S	S	SEWER PIPE
SL	SL	SEWER LATERAL
G	G	GAS LINE
D	D	STORM DRAIN
W	W	WATER LINE
WS	WS	WATER SERVICE
---	---	UNDERGROUND ELECTRIC
---	---	OVERHEAD ELECTRIC/WIRES
FD	FD	FOUNDATION DRAIN
---	---	EDGE OF PAVEMENT (EP)
100	100	CONTOUR
97x3	98x0	SPOT ELEVATION
⊙	⊙	UTILITY POLE
⊙	⊙	WALL MOUNTED EXTERIOR LIGHTS
⊙	⊙	TRANSFORMER ON CONCRETE PAD
⊙	⊙	ELECTRIC HANDHOLD
⊙	⊙	SHUT OFFS (WATER/GAS)
⊙	⊙	GATE VALVE
⊙	⊙	HYDRANT
⊙	⊙	CATCH BASIN
⊙	⊙	SEWER MANHOLE
⊙	⊙	DRAIN MANHOLE
⊙	⊙	TELEPHONE MANHOLE
⊙	⊙	PARKING SPACE COUNT
⊙	⊙	PARKING METER
LSA	⊙	LANDSCAPED AREA
TBD	TBD	TO BE DETERMINED
CI	CI	CAST IRON PIPE
COP	COP	COPPER PIPE
DI	DI	DUCTILE IRON PIPE
PVC	PVC	POLYVINYL CHLORIDE PIPE
RCP	RCP	REINFORCED CONCRETE PIPE
AC	-	ASBESTOS CEMENT PIPE
VC	VC	VITRIFIED CLAY PIPE
EP	EP	EDGE OF PAVEMENT
EL	EL	ELEVATION
FF	FF	FINISHED FLOOR
INV	INV	INVERT
S =	S =	SLOPE FT/FT
TBM	TBM	TEMPORARY BENCH MARK
TYP	TYP	TYPICAL
W.W.	W.W.	WINDOW WELL
①	①	PHOTO LOCATION



**PROPOSED BUILDING ADDITION
PORTSMOUTH AUTO BODY CENTER
700 PEVERLY HILL ROAD
PORTSMOUTH, N.H.**



WWW.HALEYWARD.COM

PLAN SET SUBMITTAL DATE: 17 JULY 2023

ALTA/ACSM CERTIFICATION:

TO: JMK REALTY, LLC; FORD MOTOR CREDIT COMPANY & LAWYERS TITLE INSURANCE CORPORATION:

THIS TO CERTIFY THAT THIS MAP OR PLAT AND THE SURVEY ON WHICH IT IS BASED WERE MADE IN ACCORDANCE WITH THE "MINIMUM STANDARD DETAILED REQUIREMENTS FOR ALTA/ACSM LAND TITLE SURVEYS," JOINTLY ESTABLISHED AND ADOPTED BY ALTA, ACSM AND NSPS IN 1999, AND INCLUDES ITEMS 2,3,4,6,7A,7C,8,9,10 & 11 OF TABLE A THEREOF. PURSUANT TO THE ACCURACY STANDARDS AS ADOPTED BY ALTA, NSPS AND ACSM AND IN EFFECT ON THE DATE OF THIS CERTIFICATION, UNDERSIGNED FURTHER CERTIFIES THAT THE POSITIONAL UNCERTAINTIES RESULTING FROM THE SURVEY MEASUREMENTS MADE ON THE SURVEY DO NOT EXCEED THE ALLOWABLE POSITIONAL TOLERANCE.

JAMES VERRA LS NO. 625 DATE

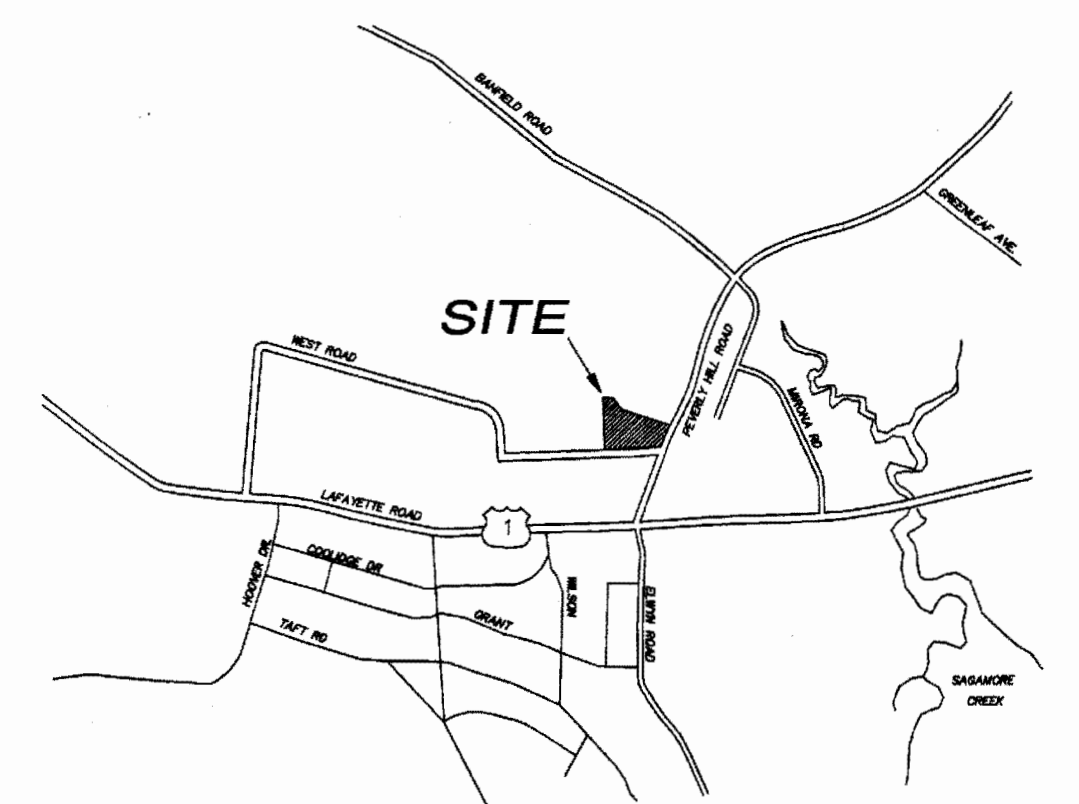
254/8 CITY OF PORTSMOUTH JUNKINS AVE PORTSMOUTH, NH 03801 3276/2986

NOTES:

- 1. OWNER OF RECORD..... ROBERT F. FLEISCHMANN ADDRESS..... 700 PEVERLY HILL ROAD, PORTSMOUTH, N.H., 03801 DEED REFERENCE..... BOOK 2466 PG 1308 RCRD TAX SHEET / LOT..... 252/2-10
2. ZONED..... INDUSTRIAL MINIMUM LOT AREA 2 ACRES FRONTAGE..... 200' MAX. STRUCTURE HEIGHT..... 70' MAX. STRUCTURE COVERAGE..... 50% EXISTING STRUCT. COVERAGE..... 12%
3. THE RELATIVE ERROR OF CLOSURE WAS LESS THAN 1 FOOT IN 15,000 FEET.
4. THE LOCATION OF ALL UNDERGROUND UTILITIES SHOWN HEREON ARE APPROXIMATE AND ARE BASED UPON THE FIELD LOCATION OF ALL VISIBLE STRUCTURES (IE CATCH BASINS, MANHOLES, WATER GATES ETC.) AND INFORMATION COMPILED FROM PLANS PROVIDED BY UTILITY COMPANIES AND GOVERNMENTAL AGENCIES. ALL CONTRACTORS SHOULD NOTIFY, IN WRITING, SAID AGENCIES PRIOR TO ANY EXCAVATION WORK AND CALL DIG-SAFE @ 1-888-DIG-SAFE.
5. THE PARCEL SHOWN HEREON DOES NOT LIE WITHIN THE 100-YEAR FLOOD HAZARD ZONE AS DEPICTED ON FLOOD INSURANCE RATE MAP CITY OF PORTSMOUTH, NEW HAMPSHIRE, ROCKINGHAM COUNTY, COMMUNITY-PANEL NO. 330139 0018 B, EFFECTIVE DATE MAY 17, 1982, BY THE FEDERAL EMERGENCY MANAGEMENT AGENCY.

REFERENCE PLANS:

- 1. LAFAYETTE WEST, PHASE II, LAFAYETTE WEST CORP., SUBDIVISION PLAN, DATED 5/12/83, RCRD #D-11744.
2. SUBDIVISION & LOT LINE RELOCATION PLAN for PIKE INDUSTRIES, INC. & JOHN AFOLLA COMPANY, INC., PEVERLY HILL ROAD / BANFIELD ROAD, PORTSMOUTH, NH, DATED JULY 28, 1997, REV 11/21/97, RCRD # D-26136.
3. EASEMENT PLAN, OVER LAND OF ROBERT F. FLEISCHMANN, WEST ROAD, PORTSMOUTH, N.H., for NEW ENGLAND TELEPHONE and TELEGRAPH COMPANY, DATED 7/17/97, PLAN NO. 20756, by JAMES VERRA and ASSOCIATES, INC.
4. LAFAYETTE WEST, PHASE II, LAFAYETTE WEST CORPORATION, PLAN OF LAND ON PEVERLY HILL ROAD, PORTSMOUTH, N.H., DATED 6/20/83, RCRD #C 11625.



LOCUS

(SCALE: 1" = 1500'±)

LEGAL DESCRIPITON

A CERTAIN TRACT OR PARCEL OF LAND LOCATED ON THE SOUTHWESTERLY SIDE OF PEVERLY HILL ROAD AND THE NORTHWESTERLY SIDE OF WEST ROAD, IN THE CITY OF PORTSMOUTH, COUNTY OF ROCKINGHAM, STATE OF NEW HAMPSHIRE, BOUNDED AND DESCRIBED AS FOLLOWS:

BEGINNING AT AN IRON BOLT ON THE WESTERLY SIDE OF WEST ROAD AT THE SOUTHEAST CORNER OF THE SUBJECT TRACT AT LAND OF SAMUEL J. & MARILYN J. HANSCOM, THENCE BY LAND OF SAID HANSCOM NORTH 55°45'32" WEST 500.02 FEET TO AN IRON ROD AND CAP AT LAND OF THE CITY OF PORTSMOUTH;

THENCE BY LAND OF THE CITY OF PORTSMOUTH ON THE FOLLOWING COURSES:

NORTH 34°25'35" EAST 48.95 FEET TO AN IRON ROD AND CAP; SOUTH 85°43'05" EAST 114.96 FEET TO AN IRON ROD AND CAP; NORTH 56°10'00" EAST 500.01 FEET TO AN IRON ROD ON THE SOUTHERLY SIDE OF PEVERLY HILL ROAD;

THENCE BY PEVERLY HILL ROAD ON THE FOLLOWING COURSES:

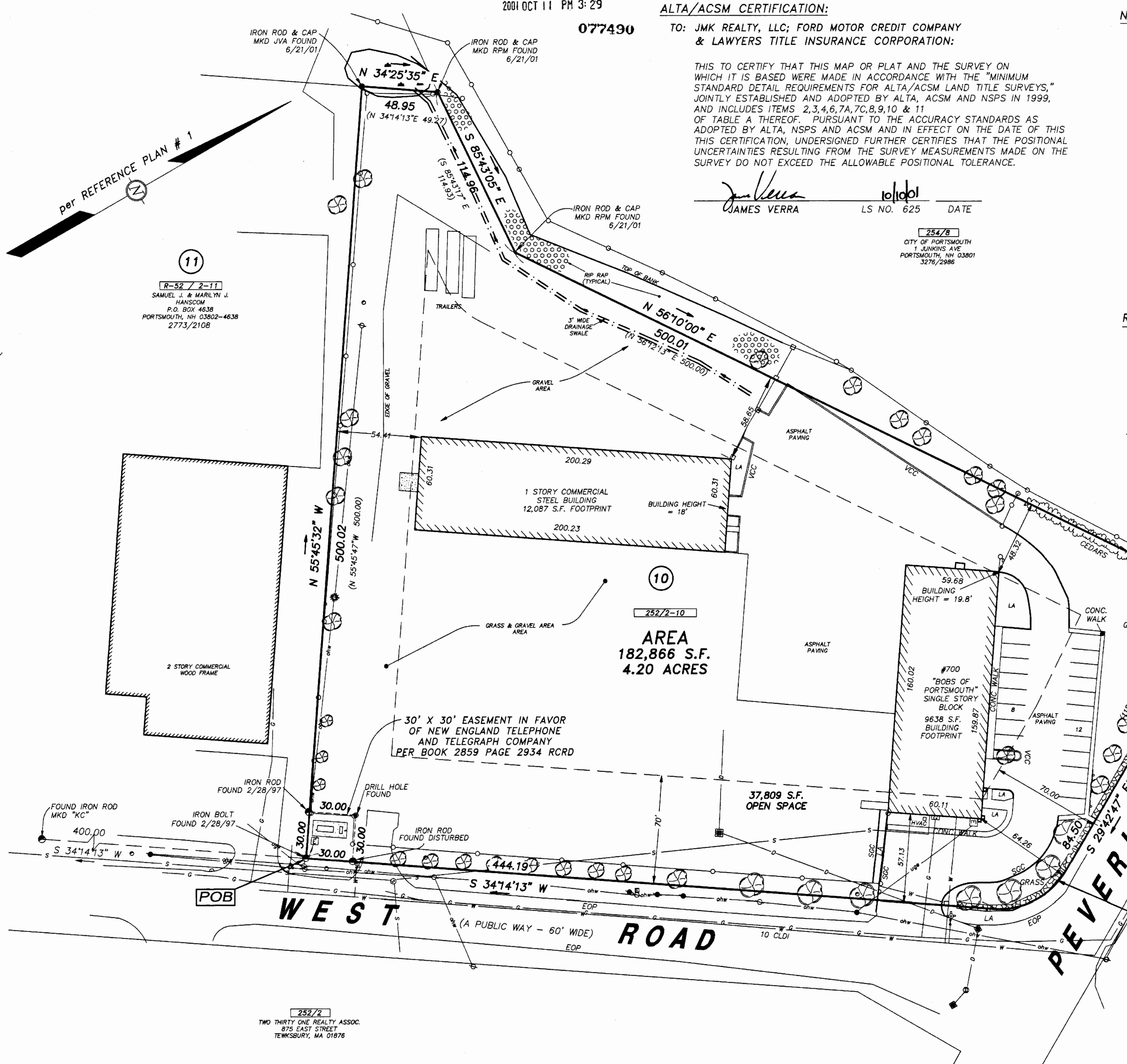
SOUTH 33°53'06" EAST 118.06 FEET TO A POINT; SOUTH 29°42'47" EAST 84.50 FEET TO A POINT;

THENCE SOUTHERLY BY A CURVE CONCAVE TO THE WEST HAVING A RADIUS OF 50.00 FEET AND AN ARC OF 55.81 FEET TO A POINT ON THE WESTERLY SIDE OF WEST ROAD;

THENCE BY THE WEST SIDE OF WEST ROAD SOUTH 34°14'13" WEST 444.19 FEET TO THE POINT OF BEGINNING. SAID TRACT CONTAINS 182,866 SQUARE FEET (4.20 ACRES)

LEGEND:

- IRON ROD, DRILL HOLE, CHAIN LINK FENCE, MORTARED STONE WALL, SEWER MANHOLE, CATCH BASIN, HYDRANT, WATER GATE VALVE, GAS METER, CEMENT CONCRETE PAD, UTILITY POLE, LIGHT POLE, UTILITY POLE W/T TRANSFORMER, GUY, ELECTRICAL MANHOLE, ELECTRIC METER, SEWER LINE, WATER LINE, GAS LINE, OVERHEAD WIRES, OVERHEAD TELEPHONE WIRES, UNDERGROUND ELECTRIC, UNDERGROUND TELEPHONE, ROCKINGHAM COUNTY REGISTRY OF DEEDS, LOT NUMBER PER REFERENCE PLAN NO. 1, JAMES VERRA AND ASSOCIATES, INC., KIMBAL CHASE CO., RICHARD P. MILLETTE, ASSOC., VERTICAL CONCRETE CURB, SLOPED GRANITE CURB, EDGE OF PAVEMENT, LANDSCAPED AREA, DECIDUOUS TREE, WOOD FENCE, WET AREA (PONDED), RECORD PER REFERENCE PLAN NO. 1

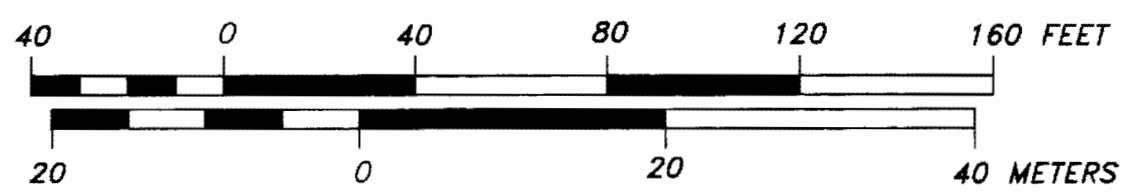


252/2 TWO THIRTY ONE REALTY ASSOC. 875 EAST STREET TEWKSBURY, MA 01876

PURSUANT TO RSA 676:18,III AND RSA 672:14

I CERTIFY THAT THIS SURVEY PLAT IS NOT A SUBDIVISION PURSUANT TO THIS TITLE AND THAT THE LINES OF STREETS AND WAYS SHOWN ARE THOSE OF PUBLIC OR PRIVATE STREETS OR WAYS ALREADY ESTABLISHED AND THAT NO NEW WAYS ARE SHOWN.

JAMES VERRA LS NO. 625 DATE



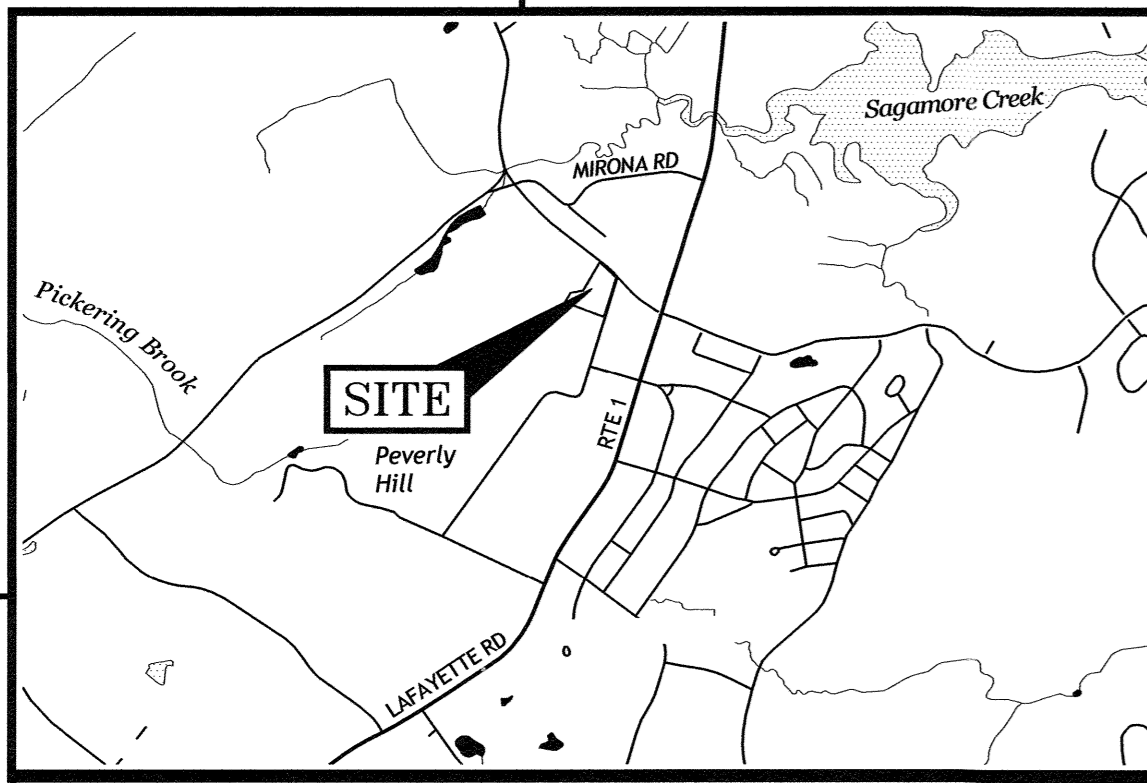
DELTA=63°57'00" RAD =50.00 ARC =55.81 CHORD =S 2°15'43" W 52.95

252/8 MACLEOD ENTERPRISES INC. P.O. BOX 328 PORTSMOUTH, NH 03802-0328

Table with 4 columns: REV. NO., DATE, DESCRIPTION, APPR'D. Row 1: 2, 7-17-01, ADDED OFFSETS, JV. Row 2: 1, 7/5/01, ADDED OPEN SPACE, JV.

ALTA/ACSM LAND TITLE SURVEY 700 PEVERLY HILL ROAD PORTSMOUTH, NEW HAMPSHIRE for JMK REALTY, LLC. JAMES VERRA and ASSOCIATES, INC. DATE: 6/28/01 JOB NO: 21384 SCALE: 1" = 40' DWG NAME: 21384 PLAN NO: 21384 SHEET: 1 of 1

D-29313

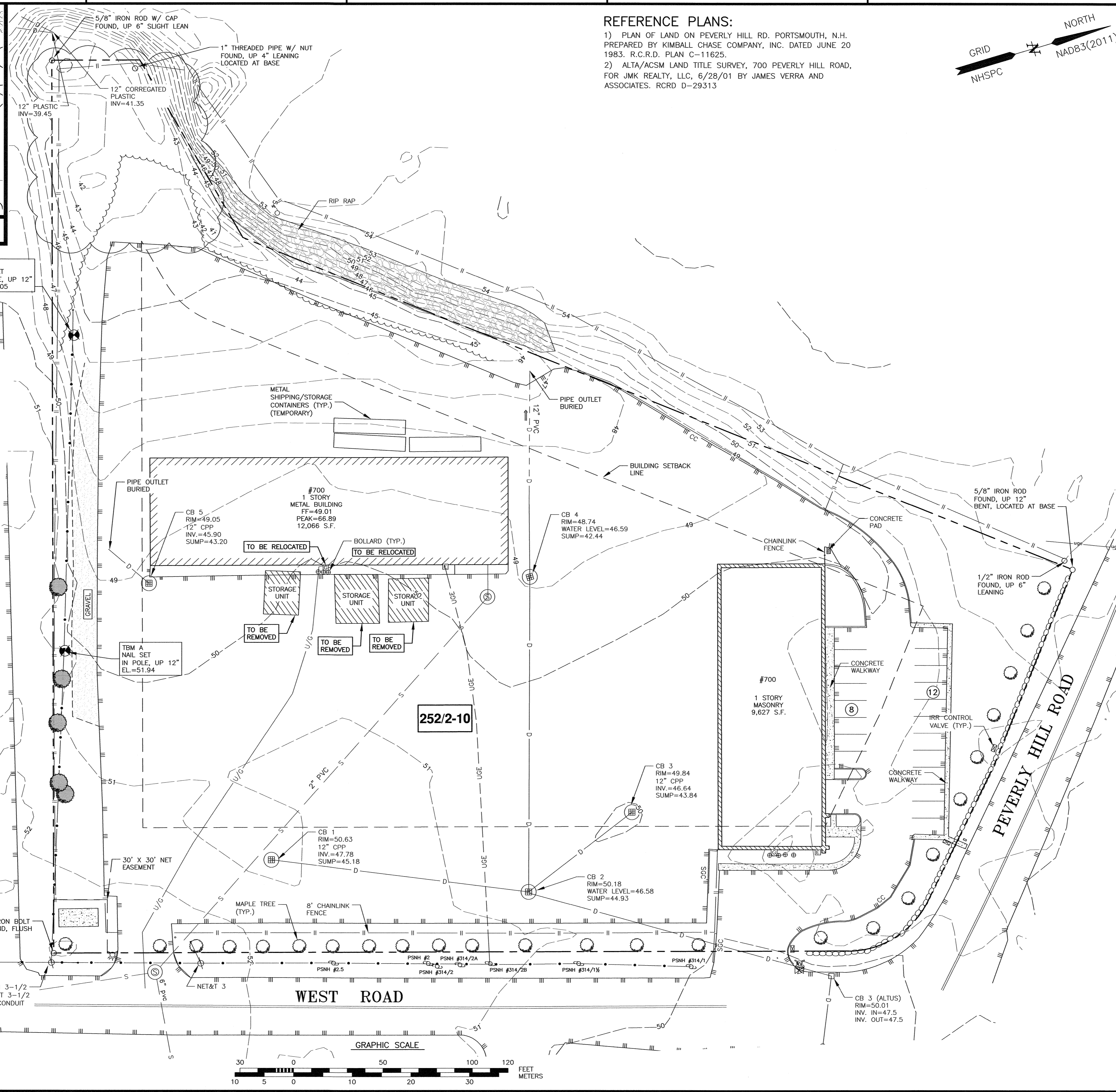


LOCATION MAP SCALE: 1" = 2000'

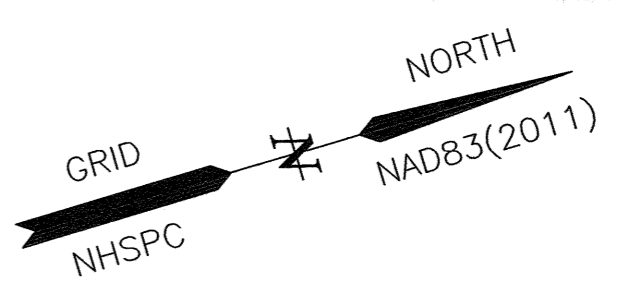
LEGEND: SEE COVER SHEET

DEMOLITION NOTES

- A) THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE DESIGNER. IT IS THE CONTRACTORS' RESPONSIBILITY TO LOCATE UTILITIES AND ANTICIPATE CONFLICTS. CONTRACTOR SHALL REPAIR EXISTING UTILITIES DAMAGED BY THEIR WORK AND RELOCATE EXISTING UTILITIES THAT ARE REQUIRED TO BE RELOCATED PRIOR TO COMMENCING ANY WORK IN THE IMPACTED AREA OF THE PROJECT.
- B) ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTORS UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES. THE CONTRACTOR SHALL COORDINATE REMOVAL, RELOCATION, DISPOSAL, OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY.
- C) ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO THE ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- D) THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES AND CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
- E) SAWCUT AND REMOVE PAVEMENT ONE FOOT OFF PROPOSED EDGE OF PAVEMENT TRENCH IN AREAS WHERE PAVEMENT IS TO BE REMOVED.
- F) IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL THE PERMIT APPROVALS.
- G) THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL CONSTRUCTION PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR ANY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY ADDITIONAL AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK.
- H) THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE, UTILITIES, VEGETATION, PAVEMENT, AND CONTAMINATED SOIL WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ANY EXISTING DOMESTIC / IRRIGATION SERVICE WELLS IN THE PROJECT AREA IDENTIFIED DURING THE CONSTRUCTION AND NOT CALLED OUT ON THE PLANS SHALL BE BROUGHT TO THE ATTENTION OF THE OWNER AND ENGINEER FOR PROPER CAPPING / RE-USE.
- I) PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS WITHIN CONSTRUCTION LIMITS AND MAINTAIN FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE HIGH FLOW SILT SACK BY ACF ENVIRONMENTAL OR APPROVED EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF WARRANTED OR FABRIC BECOMES CLOGGED. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
- J) THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFETY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
- K) ANY CONTAMINATED MATERIAL REMOVED DURING THE COURSE OF THE WORK WILL REQUIRE HANDLING IN ACCORDANCE WITH NHDES REGULATIONS. CONTRACTOR SHALL HAVE A HEALTH AND SAFETY PLAN IN PLACE, AND COMPLY WITH ALL APPLICABLE PERMITS, APPROVALS, AUTHORIZATIONS, AND REGULATIONS



REFERENCE PLANS:
 1) PLAN OF LAND ON PEVERLY HILL RD. PORTSMOUTH, N.H. PREPARED BY KIMBALL CHASE COMPANY, INC. DATED JUNE 20 1983. R.C.R.D. PLAN C-11625.
 2) ALTA/ACSM LAND TITLE SURVEY, 700 PEVERLY HILL ROAD, FOR JMK REALTY, LLC, 6/28/01 BY JAMES VERRA AND ASSOCIATES. RCRD D-29313



- NOTES:**
- 1) PARCEL IS SHOWN ON THE CITY OF PORTSMOUTH MAP 252 AS LOT 2-10.
 - 2) OWNER OF RECORD:
JMK REALTY LLC
PO BOX 971
PORTSMOUTH, NH, 03801
3656 / 0744
 - 3) PARCEL IS NOT IN A SPECIAL FLOOD HAZARD ZONE. (ZONE X) AS SHOWN ON FIRM PANEL 33015C0270F. EFFECTIVE DATE 1/29/2021
 - 4) EXISTING LOT AREA:
4.20 ACRES
 - 5) PARCEL IS LOCATED IN THE INDUSTRIAL DISTRICT.
 - 6) DIMENSIONAL REQUIREMENTS:
MIN. LOT AREA: 2 ACRES
FRONTAGE: 200 FT
SETBACKS:
FRONT: 70 FT
SIDE: 50 FT
REAR: 50 FT

MAXIMUM STRUCTURE HEIGHT: 70 FT
MAXIMUM BUILDING COVERAGE: 50%
MINIMUM OPEN SPACE: 20%
 - 7) THE PURPOSE OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS ON A PORTION OF ASSESSOR'S MAP 252 LOT 2-10 IN THE CITY OF PORTSMOUTH.
 - 8) VERTICAL DATUM IS NAVD88. BASIS OF VERTICAL DATUM IS REDUNDANT RTN GNSS OBSERVATIONS.
 - 9) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.

No.	DATE	DESCRIPTION	BY	CHK.
1	7/17/23	UPDATE TOPOGRAPHY	OS	JC
0	5/2/23	ISSUED FOR COMMENT	OS	JC

DRAWING ISSUE STATUS
NOT FOR CONSTRUCTION

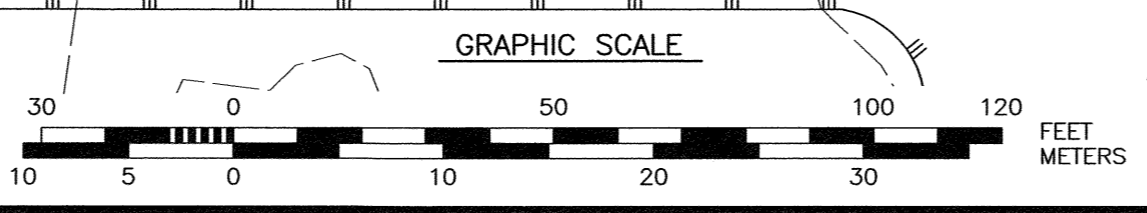
AMBIT ENGINEERING, INC.
 A DIVISION OF HALEY WARD, INC.
 200 Griffin Road, Unit 3
 Portsmouth, NH 03801
 603.430.9282
 WWW.HALEYWARD.COM

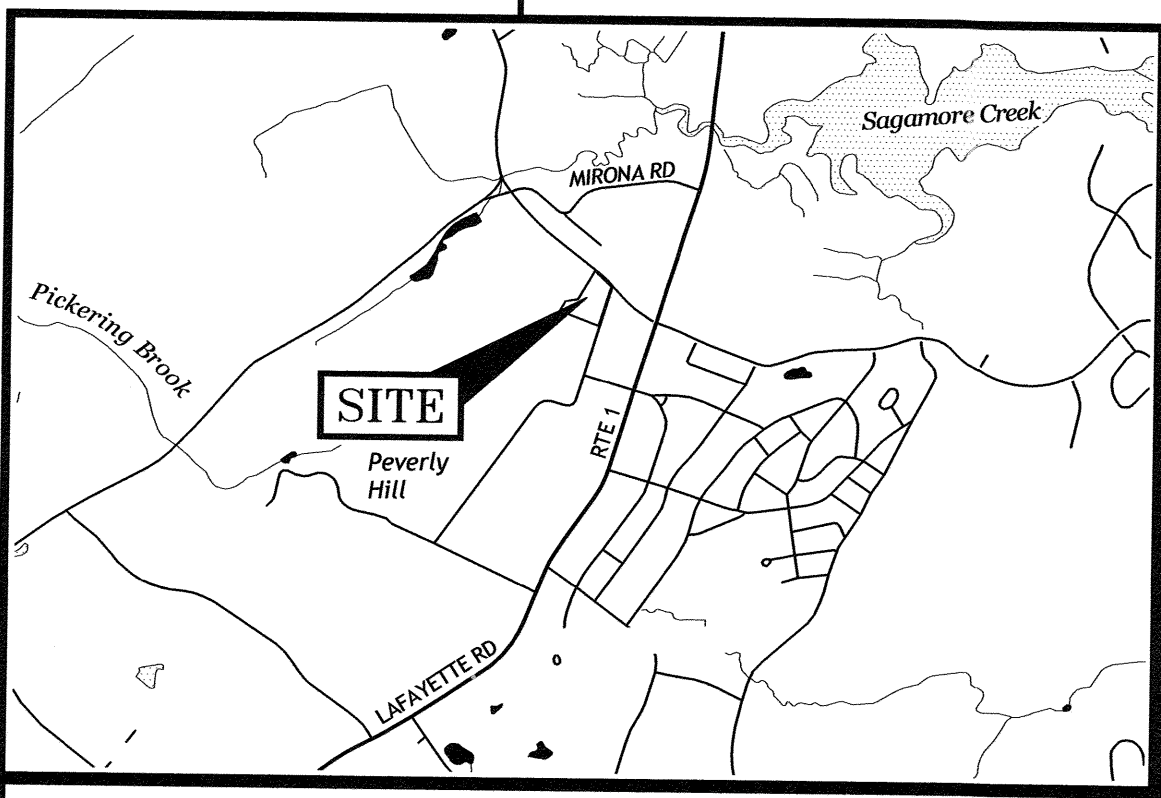
PROJECT
BUILDING ADDITION
 PORTSMOUTH AUTO BODY CENTER
 700 PEVERLY HILL ROAD, PORTSMOUTH, NH

TITLE
EXISTING CONDITIONS & DEMOLITION PLAN

DATE: APRIL 2023 SCALE: 1" = 30'
 DRAWN BY: OS DESIGNED BY: JC CHECKED BY: JC
 PROJECT No: 5010265-3576 FIELD BOOK & PAGE: FB 389 PG 18
 DRAWING No: **SHEET 2** C1

"I CERTIFY THAT THIS PLAN WAS PREPARED UNDER MY DIRECT SUPERVISION, THAT IT IS THE RESULT OF A FIELD SURVEY BY THIS OFFICE AND HAS AN ACCURACY OF THE CLOSED TRAVERSE THAT EXCEEDS THE PRECISION OF 1:15,000."
 JOHN R. CHAGNON, LLS #738 DATE: 7.17.23



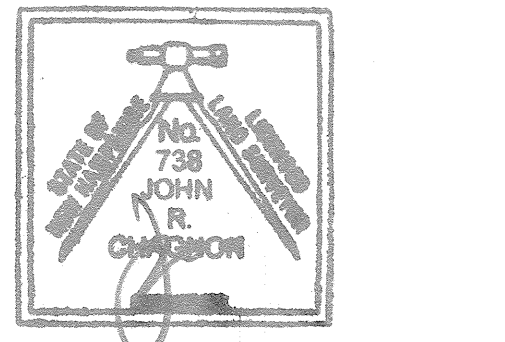


LOCATION MAP SCALE: 1" = 2000'

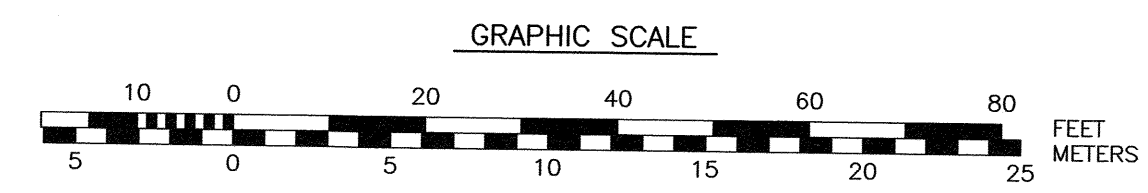
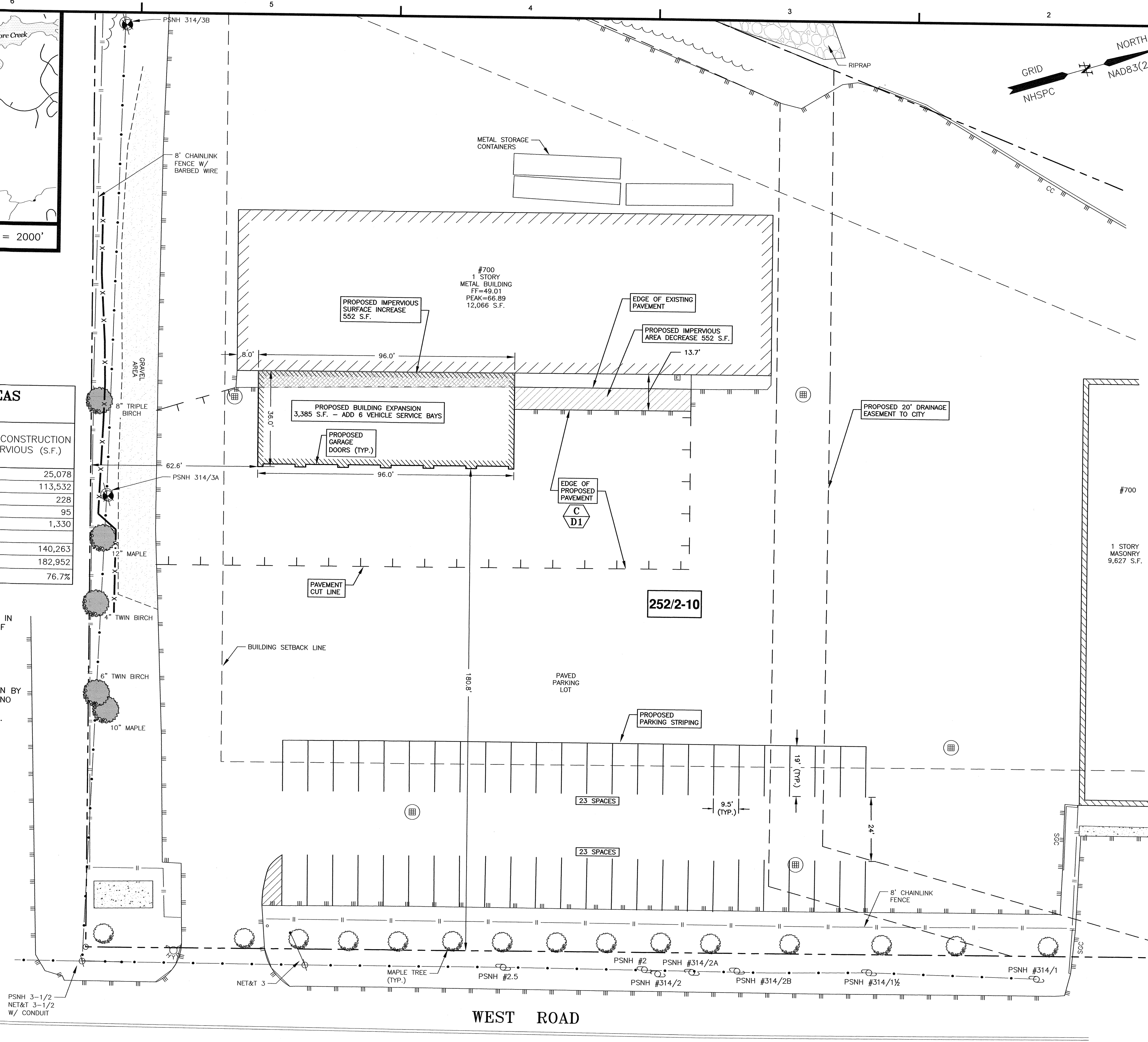
LEGEND: SEE COVER SHEET

IMPERVIOUS SURFACE AREAS (TO PROPERTY LINE)		
STRUCTURE	PRE-CONSTRUCTION IMPERVIOUS (S.F.)	POST-CONSTRUCTION IMPERVIOUS (S.F.)
STRUCTURES	21,693	25,078
PAVEMENT	116,917	113,532
CONCRETE PADS	228	228
CURBING	95	95
CONCRETE WALKWAY	1,330	1,330
TOTAL	140,263	140,263
LOT SIZE	182,952	182,952
% LOT COVERAGE	76.7%	76.7%

PORTSMOUTH APPROVAL CONDITIONS NOTE:
 ALL CONDITIONS ON THIS PLAN SET SHALL REMAIN IN EFFECT IN PERPETUITY PURSUANT TO THE REQUIREMENTS OF THE CITY OF PORTSMOUTH SITE PLAN REVIEW REGULATIONS.
 THIS SITE SHALL BE RECORDED IN THE ROCKINGHAM COUNTY REGISTRY OF DEEDS.
 ALL IMPROVEMENTS SHOWN ON THIS SITE PLAN SHALL BE CONSTRUCTED AND MAINTAINED IN ACCORDANCE WITH THE PLAN BY THE PROPERTY OWNER AND ALL FUTURE PROPERTY OWNERS. NO CHANGES SHALL BE MADE ON THIS SITE PLAN WITHOUT THE EXPRESS APPROVAL OF THE PORTSMOUTH PLANNING DIRECTOR.



"I CERTIFY THAT THIS PLAN WAS PREPARED UNDER MY DIRECT SUPERVISION, THAT IT IS THE RESULT OF A FIELD SURVEY BY THIS OFFICE AND HAS AN ACCURACY OF THE CLOSED TRAVERSE THAT EXCEEDS THE PRECISION OF 1:15,000."
 JOHN R. CHAGNON, LLS #738
 DATE 7-17-23



- NOTES:**
- 1) PARCEL IS SHOWN ON THE CITY OF PORTSMOUTH ASSESSOR'S MAP 252 AS LOT 2-10.
 - 2) OWNER OF RECORD:
JMK REALTY LLC
PO BOX 971
PORTSMOUTH, NH, 03801
3656 / 0744
 - 3) PARCEL IS NOT IN A SPECIAL FLOOD HAZARD ZONE. (ZONE X) AS SHOWN ON FIRM PANEL 33015C0270F. EFFECTIVE DATE 1/29/2021
 - 4) EXISTING LOT AREA:
4.20 ACRES
 - 5) PARCEL IS LOCATED IN THE INDUSTRIAL DISTRICT.
 - 6) DIMENSIONAL REQUIREMENTS:
MIN. LOT AREA: 2 ACRES
FRONTAGE: 200 FT
SETBACKS:
FRONT: 70 FT
SIDE: 50 FT
REAR: 50 FT
MAXIMUM STRUCTURE HEIGHT: 70 FT
MAXIMUM BUILDING COVERAGE: 50%
MINIMUM OPEN SPACE: 20%
 - 7) THE PURPOSE OF THIS PLAN IS TO SHOW THE PROPOSED SITE IMPROVEMENTS ON A PORTION OF ASSESSOR'S MAP 252 LOT 2-10 IN THE CITY OF PORTSMOUTH.
 - 8) VERTICAL DATUM IS NAVD88. BASIS OF VERTICAL DATUM IS REDUNDANT RTN GNSS OBSERVATIONS.
 - 9) ALL PROPOSED UTILITY CONNECTIONS WILL BE INTERNAL FROM THE EXISTING SERVICES.
 - 10) PARKING ANALYSIS:
REQUIRED (PER ARTICLE II SECTION 10.1112.321)-11.20 MOTOR VEHICLE REPAIR SPACE
EXISTING: 21,693 S.F. (400 S.F. GFA + 2) = 57 SPACES
PROPOSED: 25,075 S.F. (400 S.F. GFA + 2) = 65 SPACES
PROVIDED: 66 SPACES

No.	DATE	DESCRIPTION	BY	CHK
1	7/17/23	REV. BUILDING EXPANSION & PARKING	OS	JC
0	5/2/23	ISSUED FOR COMMENT	OS	JC

NOT FOR CONSTRUCTION

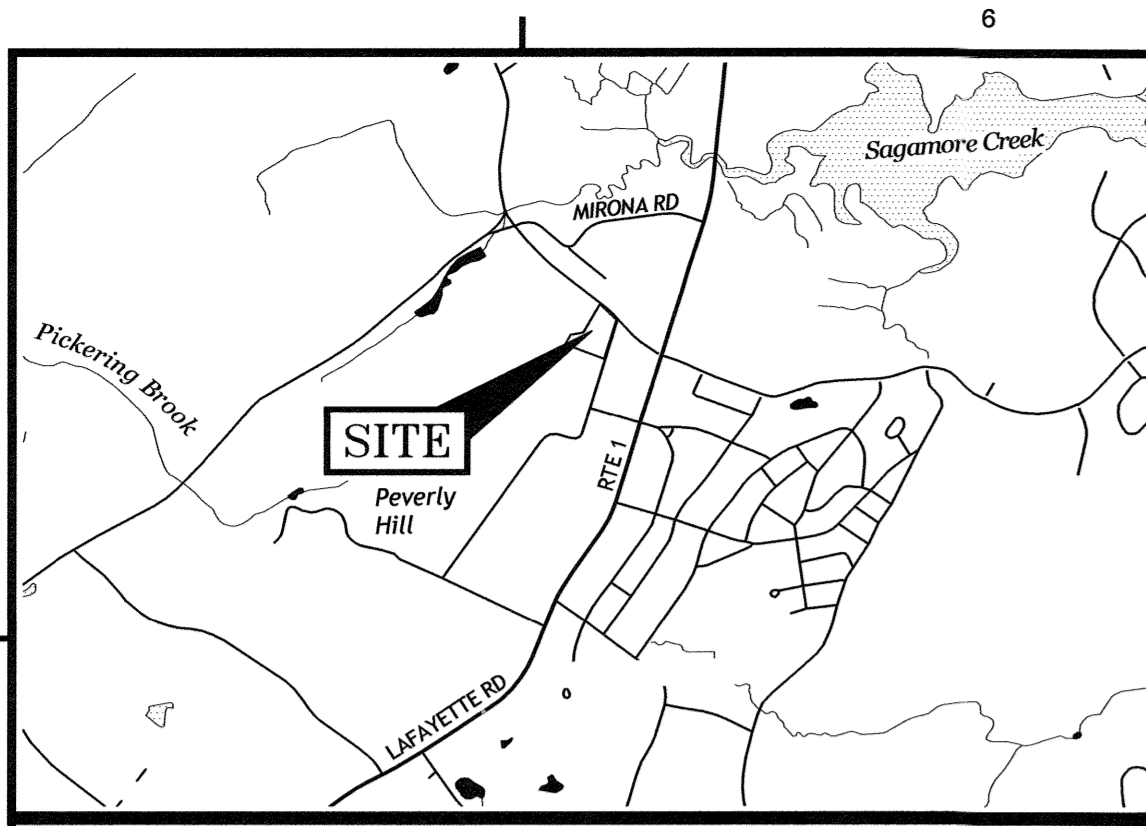
AMBIT ENGINEERING, INC.
 A DIVISION OF HALEY WARD, INC.

200 Griffin Road, Unit 3
 Portsmouth, NH 03801
 603.430.9282

WWW.HALEYWARD.COM
 PROJECT
BUILDING EXPANSION PLAN
 PORTSMOUTH AUTO BODY CENTER
 700 PEVERLY HILL ROAD, PORTSMOUTH, NH

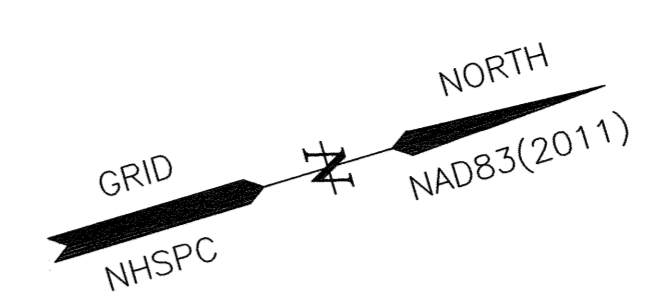
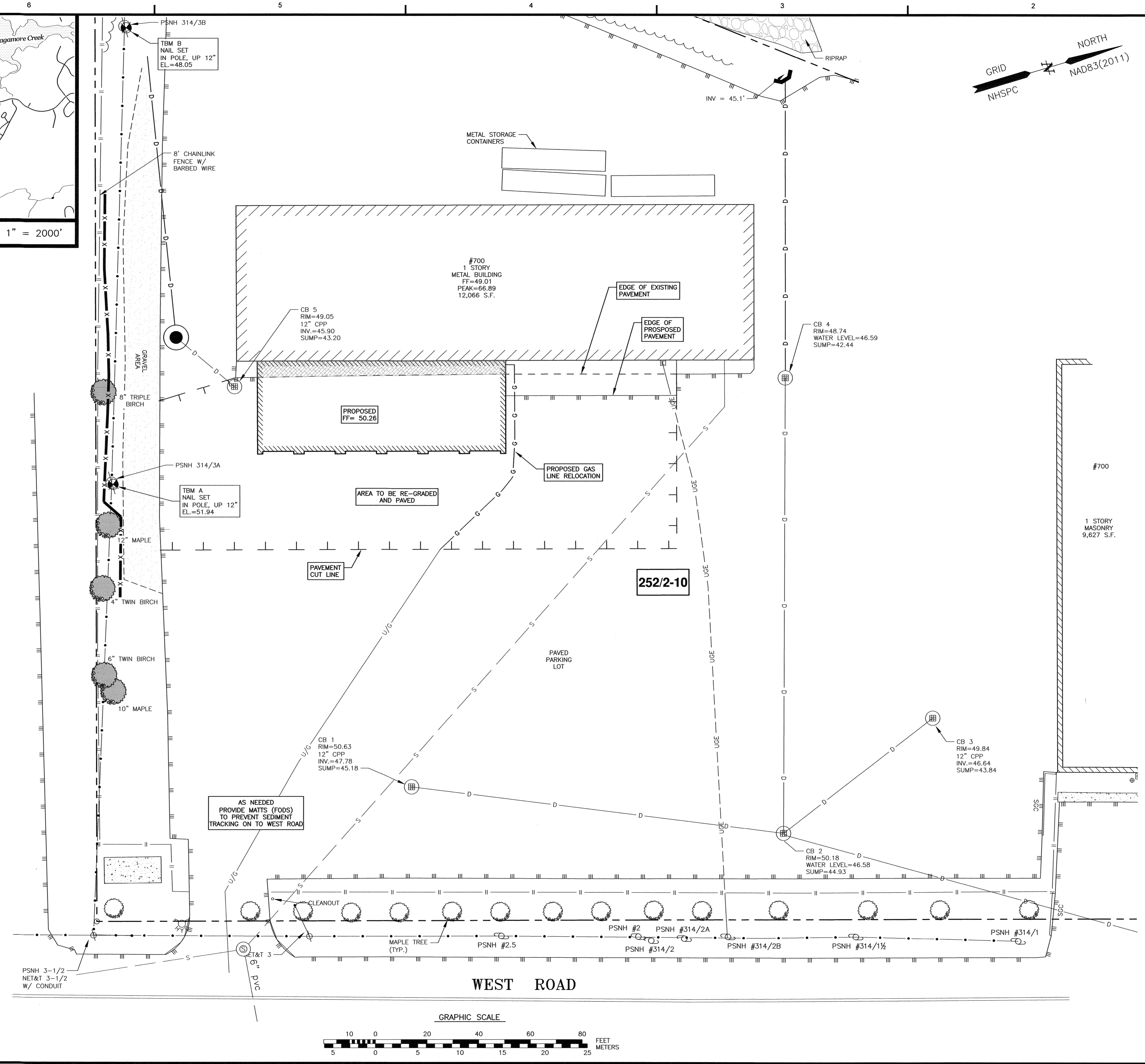
TITLE
SITE PLAN

DATE APRIL 2023	SCALE SCALE: 1" = 20'
DRAWN BY OS	DESIGNED BY JC
CHECKED BY JC	
PROJECT No. 5010265-3576	FIELD BOOK & PAGE FB 389 PG 18
DRAWING No. SHEET 3 C2	



LOCATION MAP SCALE: 1" = 2000'

LEGEND: SEE COVER SHEET



- NOTES:**
- 1) PARCEL IS SHOWN ON THE CITY OF PORTSMOUTH ASSESSOR'S MAP 252 AS LOT 2-10.
 - 2) OWNER OF RECORD:
JMK REALTY LLC
PO BOX 971
PORTSMOUTH, NH, 03801
3656 / 0744
 - 3) PARCEL IS NOT IN A SPECIAL FLOOD HAZARD ZONE. (ZONE X) AS SHOWN ON FIRM PANEL 33015C0270F. EFFECTIVE DATE 1/29/2021
 - 4) EXISTING LOT AREA:
4.20 ACRES
 - 5) THE PURPOSE OF THIS PLAN IS TO SHOW THE PROPOSED SITE IMPROVEMENTS ON A PORTION OF ASSESSOR'S MAP 252 LOT 2-10 IN THE CITY OF PORTSMOUTH.
 - 6) VERTICAL DATUM IS NAVD88. BASIS OF VERTICAL DATUM IS REDUNDANT RTN GNSS OBSERVATIONS.
 - 7) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY WITHIN 100 FEET OF UNDERGROUND UTILITIES. THE EXCAVATOR IS RESPONSIBLE TO MAINTAIN MARKS. DIG SAFE TICKETS EXPIRE IN THIRTY DAYS.
 - 8) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.
 - 9) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL, VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008).

No.	DATE	DESCRIPTION	BY	CHK.
7	7/17/23	REV BUILDING EXPANSION	OS	JC
0	5/2/23	ISSUED FOR COMMENT	OS	JC

NOT FOR CONSTRUCTION

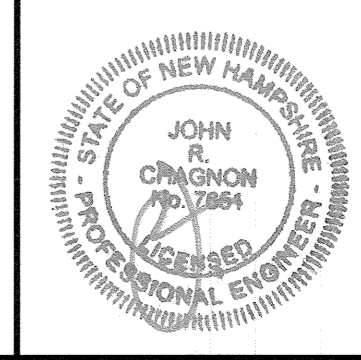


200 Griffin Road, Unit 3
Portsmouth, NH 03801
603.430.9282

PROJECT
BUILDING EXPANSION PLAN
PORTSMOUTH AUTO BODY CENTER
700 PEVERLY HILL ROAD, PORTSMOUTH, NH

TITLE
UTILITY PLAN

DATE APRIL 2023	SCALE SCALE: 1" = 20'	
DRAWN BY OS	DESIGNED BY JC	CHECKED BY JC
PROJECT NO. 5010265-3576	FIELD BOOK & PAGE FB 389 PG 18	
DRAWING No. SHEET 5		C4



EROSION CONTROL NOTES

CONSTRUCTION SEQUENCE

DO NOT BEGIN CONSTRUCTION UNTIL ALL LOCAL, STATE AND FEDERAL PERMITS HAVE BEEN APPLIED FOR AND RECEIVED.

INSTALL INLET PROTECTION CATCH BASIN FILTER BEFORE ANY EARTH MOVING OPERATIONS.

CUT AND GRUB ALL TREES, SHRUBS, SAPLINGS, BRUSH, VINES AND REMOVE OTHER DEBRIS AND RUBBISH AS REQUIRED.

REMOVE EXISTING TEMPORARY BUILDINGS AND OTHER SITE FEATURES TO BE REMOVED.

CONSTRUCT SITE IMPROVEMENTS.

REMOVE TRAPPED SEDIMENTS FROM COLLECTION DEVICES AS APPROPRIATE, AND THEN REMOVE TEMPORARY EROSION CONTROL MEASURES UPON COMPLETION OF FINAL STABILIZATION OF THE SITE.

PROJECT DESCRIPTION

THE PROJECT CONSISTS OF A BUILDING ADDITION WITH ASSOCIATED UTILITIES, GRADING, AND SITE IMPROVEMENTS.

THE TOTAL AREA TO BE DISTURBED IS APPROXIMATELY 14,000 S.F.

BASED ON SITE OBSERVATIONS THE SOILS ON SITE CONSIST OF UDORTHENTS, SMOOTHED WHICH ARE EXCESSIVELY DRAINED, AND CHATFIELD-HOLLIS-CANTON COMPLEX, 8 TO 15% SLOPE, ROCKY WHICH ARE WELL DRAINED SOILS WITH A HYDROLOGIC SOIL GROUP RATING OF B/D.

THE STORMWATER RUNOFF FROM THE SITE WILL BE DISCHARGED TO PROPERTY WHICH ULTIMATELY FLOWS TO THE DRAINAGE COLLECTION SYSTEM FLOWING TO SAGAMORE CREEK.

GENERAL CONSTRUCTION NOTES

THE EROSION CONTROL PROCEDURES SHALL CONFORM TO SECTION 645 OF THE "STANDARD SPECIFICATION FOR ROAD AND BRIDGE CONSTRUCTION" OF THE NHDOT, AND "STORM WATER MANAGEMENT AND EROSION AND SEDIMENT CONTROL HANDBOOK FOR URBAN AND DEVELOPING AREAS IN NEW HAMPSHIRE". THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.

DURING CONSTRUCTION AND THEREAFTER, EROSION CONTROL MEASURES ARE TO BE IMPLEMENTED AS NOTED. THE SMALLEST PRACTICAL AREA OF LAND SHOULD BE EXPOSED AT ANY ONE TIME DURING DEVELOPMENT. NO DISTURBED AREA SHALL BE LEFT UNSTABILIZED FOR MORE THAN 45 DAYS.

ANY DISTURBED AREAS WHICH ARE TO BE LEFT TEMPORARILY, AND WHICH WILL BE REGRADED LATER DURING CONSTRUCTION SHALL BE MACHINE HAY MULCHED AND SEEDED WITH RYE GRASS TO PREVENT EROSION.

THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.

DUST CONTROL: DUST CONTROL MEASURES SHALL INCLUDE BUT ARE NOT LIMITED TO SPRINKLING WATER ON EXPOSED AREAS, COVERING LOADED DUMP TRUCKS LEAVING THE SITE, AND TEMPORARY MULCHING.

DUST CONTROL MEASURES SHALL BE UTILIZED SO AS TO PREVENT THE MIGRATION OF DUST FROM THE SITE TO ADJACENT AREAS.

IF TEMPORARY STABILIZATION PRACTICES, SUCH AS TEMPORARY VEGETATION AND MULCHING, DO NOT ADEQUATELY REDUCE DUST GENERATION, APPLICATION OF WATER OR CALCIUM CHLORIDE SHALL BE APPLIED IN ACCORDANCE WITH BEST MANAGEMENT PRACTICES.

SILTSOXX SHALL BE PERIODICALLY INSPECTED DURING THE LIFE OF THE PROJECT AND AFTER EACH STORM. ALL DAMAGED SILTSOXX SHALL BE REPAIRED. SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED AND DISPOSED IN A SECURED LOCATION.

ALL FILLS SHALL BE PLACED AND COMPACTED TO REDUCE EROSION, SLIPPAGE, SETTLEMENT, SUBSIDENCE OR OTHER RELATED PROBLEMS.

ALL NON-STRUCTURAL, SITE-FILL SHALL BE PLACED AND COMPACTED TO 90% MODIFIED PROCTOR DENSITY IN LAYERS NOT EXCEEDING 18 INCHES IN THICKNESS UNLESS OTHERWISE NOTED.

FROZEN MATERIAL OR SOFT, MUCKY OR HIGHLY COMPRESSIBLE MATERIAL, TRASH, WOODY DEBRIS, LEAVES, BRUSH OR ANY DELETERIOUS MATTER SHALL NOT BE INCORPORATED INTO FILLS.

FILL MATERIAL SHALL NOT BE PLACED ON FROZEN FOUNDATION SUBGRADE.

DURING CONSTRUCTION AND UNTIL ALL DEVELOPED AREAS ARE FULLY STABILIZED, ALL EROSION CONTROL MEASURES SHALL BE INSPECTED WEEKLY AND AFTER EACH ONE HALF INCH OF RAINFALL.

THE CONTRACTOR SHALL MODIFY OR ADD EROSION CONTROL MEASURES AS NECESSARY TO ACCOMMODATE PROJECT CONSTRUCTION.

ALL ROADWAYS AND PARKING AREAS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOADED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.

AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:

- BASE COURSE GRAVELS HAVE BEEN INSTALLED ON AREAS TO BE PAVED
- A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED
- A MINIMUM OF 3 INCHES OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED
- EROSION CONTROL BLANKETS HAVE BEEN INSTALLED.
- IN AREAS TO BE PAVED, "STABLE" MEANS THAT BASE COURSE GRAVELS MEETING THE REQUIREMENTS OF NHDOT STANDARD FOR ROAD AND BRIDGE CONSTRUCTION, 2016, ITEM 304.2 HAVE BEEN INSTALLED.

STABILIZATION SHALL BE INITIATED ON ALL LOAM STOCKPILES, AND DISTURBED AREAS, WHERE CONSTRUCTION ACTIVITY SHALL NOT OCCUR FOR MORE THAN TWENTY-ONE (21) CALENDAR DAYS BY THE FOURTEENTH (14TH) DAY AFTER CONSTRUCTION ACTIVITY HAS PERMANENTLY OR TEMPORARILY CEASED IN THAT AREA.

STABILIZATION MEASURES TO BE USED INCLUDE:

- TEMPORARY SEEDING;
- MULCHING.

1. ALL AREAS SHALL BE STABILIZED WITHIN 45 DAYS OF INITIAL DISTURBANCE.
2. WHEN CONSTRUCTION ACTIVITY PERMANENTLY OR TEMPORARILY CEASES WITHIN 100 FEET OF NEARBY SURFACE WATERS OR DELINEATED WETLANDS, THE AREA SHALL BE STABILIZED WITHIN SEVEN (7) DAYS OR PRIOR TO A RAIN EVENT. ONCE CONSTRUCTION ACTIVITY CEASES PERMANENTLY IN THESE AREAS, SILTSOXX, MULCH BERMS, HAY BALE BARRIERS AND ANY EARTH/DIKES SHALL BE REMOVED ONCE PERMANENT MEASURES ARE ESTABLISHED.
3. DURING CONSTRUCTION, RUNOFF WILL BE DIVERTED AROUND THE SITE WITH EARTH DIKES, PIPING OR STABILIZED CHANNELS WHERE POSSIBLE. SHEET RUNOFF FROM THE SITE WILL BE FILTERED THROUGH SILTSOXX, MULCH BERMS, HAY BALE BARRIERS, OR SILT SOCKS. ALL STORM DRAIN BASIN INLETS SHALL BE PROVIDED WITH FLARED END SECTIONS AND TRASH RACKS. THE SITE SHALL BE STABILIZED FOR THE WINTER BY OCTOBER 15.

MAINTENANCE AND PROTECTION

THE SILTSOXX BARRIER SHALL BE CHECKED AFTER EACH RAINFALL AND AT LEAST DAILY DURING PROLONGED RAINFALL.

SILTSOXX SHALL BE REMOVED ONCE SITE IS STABILIZED, AND DISTURBED AREAS RESULTING FROM SILTSOXX REMOVAL SHALL BE PERMANENTLY SEEDED.

THE CATCH BASIN INLET BASKET SHALL BE INSPECTED WITHIN 24 HOURS AFTER EACH RAINFALL OR DAILY DURING EXTENDED PERIODS OF PRECIPITATION. REPAIRS SHALL BE MADE IMMEDIATELY, AS NECESSARY, TO PREVENT PARTICLES FROM REACHING THE DRAINAGE SYSTEM AND/OR CAUSING SURFACE FLOODING. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT, OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED.

WINTER NOTES

ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85% VEGETATED GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.

ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS;

AFTER OCTOBER 15, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3, OR IF CONSTRUCTION IS TO CONTINUE THROUGH THE WINTER SEASON BE CLEARED OF ANY ACCUMULATED SNOW AFTER EACH STORM EVENT;

STOCKPILES

1. LOCATE STOCKPILES A MINIMUM OF 50 FEET AWAY FROM CATCH BASINS, SWALES, AND CULVERTS.
2. ALL STOCKPILES SHOULD BE SURROUNDED WITH TEMPORARY EROSION CONTROL MEASURES PRIOR TO THE ONSET OF PRECIPITATION.
3. PERIMETER BARRIERS SHOULD BE MAINTAINED AT ALL TIMES, AND ADJUSTED AS NEEDED TO ACCOMMODATE THE DELIVERY AND REMOVAL OF MATERIALS FROM THE STOCKPILE. THE INTEGRITY OF THE BARRIER SHOULD BE INSPECTED AT THE END OF EACH WORKING DAY.
4. PROTECT ALL STOCKPILES FROM STORMWATER RUN-OFF USING TEMPORARY EROSION CONTROL MEASURES SUCH AS BERMS, SILT SOCK, OR OTHER APPROVED PRACTICE TO PREVENT MIGRATION OF MATERIAL BEYOND THE IMMEDIATE CONFINES OF THE STOCKPILES.

CONCRETE WASHOUT AREA

THE FOLLOWING ARE THE ONLY NON-STORMWATER DISCHARGES ALLOWED. ALL OTHER NON-STORMWATER DISCHARGES ARE PROHIBITED ON SITE:

1. THE CONCRETE DELIVERY TRUCKS SHALL, WHENEVER POSSIBLE, USE WASHOUT FACILITIES AT THEIR OWN PLANT OR DISPATCH FACILITY;
2. IF IT IS NECESSARY, SITE CONTRACTOR SHALL DESIGNATE SPECIFIC WASHOUT AREAS AND DESIGN FACILITIES TO HANDLE ANTICIPATED WASHOUT WATER;
3. CONTRACTOR SHALL LOCATE WASHOUT AREAS AT LEAST 150 FEET AWAY FROM STORM DRAINS, SWALES AND SURFACE WATERS OR DELINEATED WETLANDS;
4. INSPECT WASHOUT FACILITIES DAILY TO DETECT LEAKS OR TEARS AND TO IDENTIFY WHEN MATERIALS NEED TO BE REMOVED.

ALLOWABLE NON-STORMWATER DISCHARGES

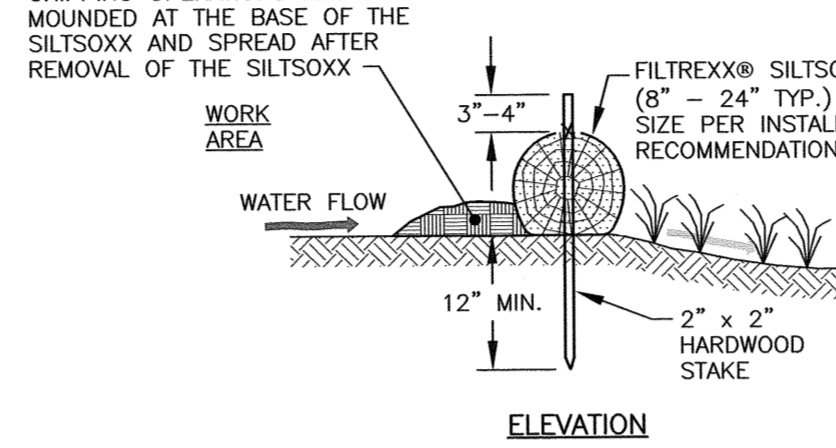
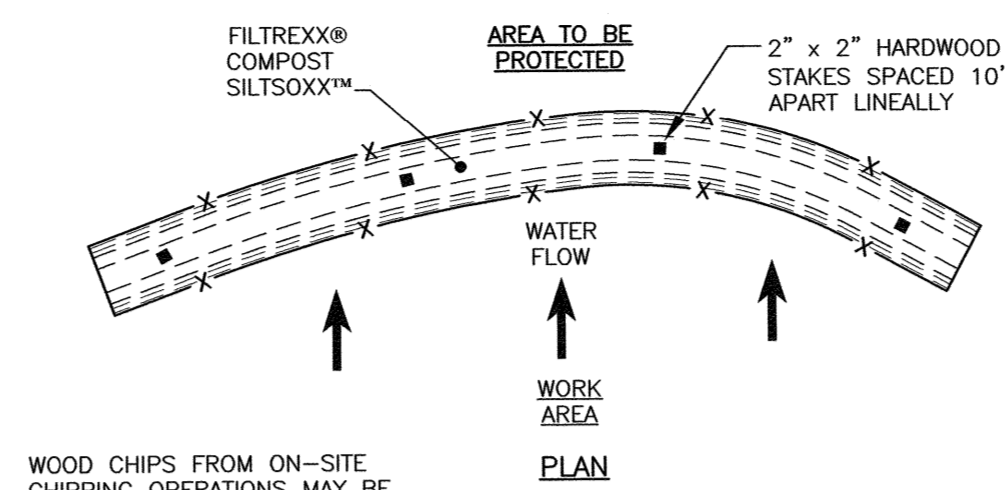
1. FIRE-FIGHTING ACTIVITIES;
2. FIRE HYDRANT FLUSHING;
3. WATERS USED TO WASH VEHICLES WHERE DETERGENTS ARE NOT USED;
4. WATER USED TO CONTROL DUST;
5. POTABLE WATER INCLUDING UNCONTAMINATED WATER LINE FLUSHING;
6. ROUTINE EXTERNAL BUILDING WASH DOWN WHERE DETERGENTS ARE NOT USED;
7. PAVEMENT WASH WATERS WHERE DETERGENTS ARE NOT USED;
8. UNCONTAMINATED AIR CONDITIONING/COMPRESSOR CONDENSATION;
9. UNCONTAMINATED GROUND WATER OR SPRING WATER;
10. FOUNDATION OR FOOTING DRAINS WHICH ARE UNCONTAMINATED;
11. UNCONTAMINATED EXCAVATION DEWATERING;
12. LANDSCAPE IRRIGATION.

WASTE DISPOSAL

1. WASTE MATERIAL
 - ALL WASTE MATERIALS SHALL BE COLLECTED AND STORED IN SECURELY LIDDED RECEPTACLES. ALL TRASH AND CONSTRUCTION DEBRIS FROM THE SITE SHALL BE DEPOSITED IN A DUMPSTER;
 - NO CONSTRUCTION WASTE MATERIALS SHALL BE BURIED ON SITE;
 - ALL PERSONNEL SHALL BE INSTRUCTED REGARDING THE CORRECT PROCEDURE FOR WASTE DISPOSAL BY THE SUPERINTENDENT.
2. HAZARDOUS WASTE
 - ALL HAZARDOUS WASTE MATERIALS SHALL BE DISPOSED OF IN THE MANNER SPECIFIED BY LOCAL OR STATE REGULATION OR BY THE MANUFACTURER;
 - SITE PERSONNEL SHALL BE INSTRUCTED IN THESE PRACTICES BY THE SUPERINTENDENT.
3. SANITARY WASTE
 - ALL SANITARY WASTE SHALL BE COLLECTED FROM THE PORTABLE UNITS A MINIMUM OF ONCE PER WEEK BY A LICENSED SANITARY WASTE MANAGEMENT CONTRACTOR.

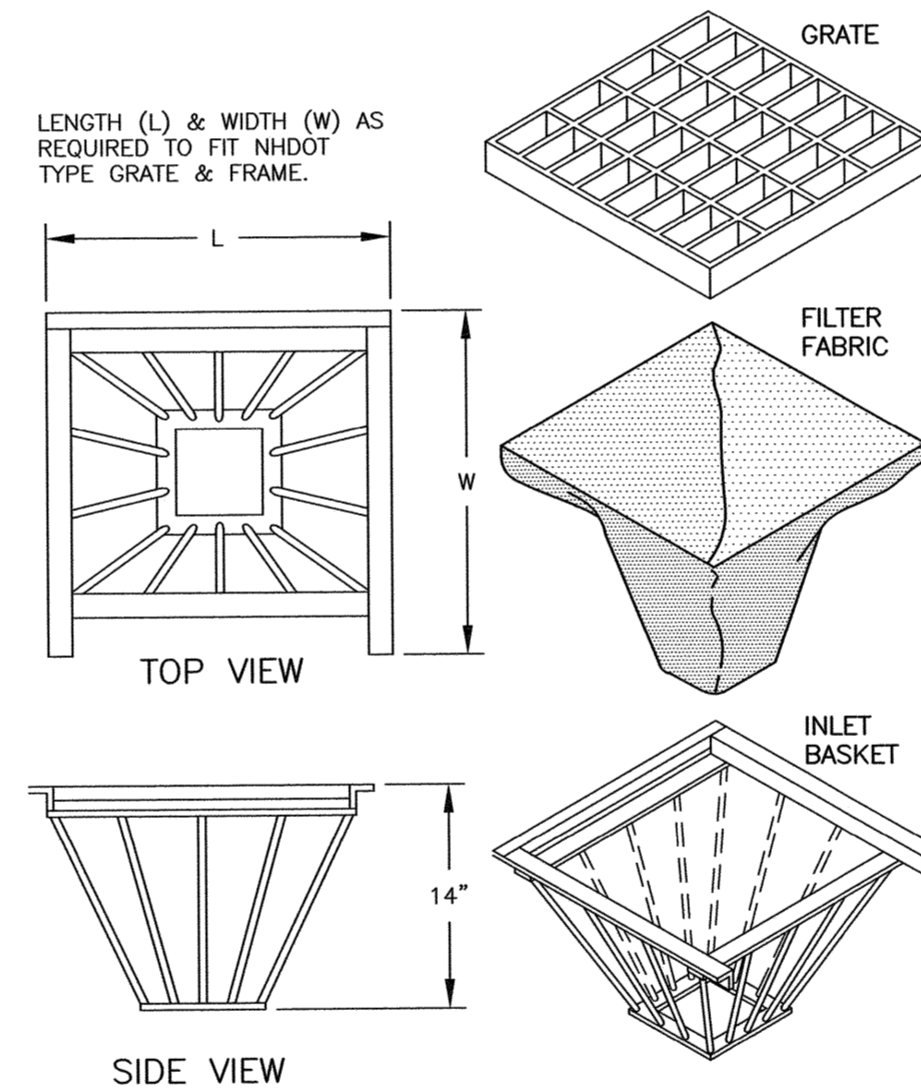
BLASTING NOTES

1. CONTRACTOR SHALL CONTACT THE NHDES AND/OR LOCAL JURISDICTION PRIOR TO COMMENCING ANY BLASTING ACTIVITIES.
2. FOR ANY PROJECT FOR WHICH BLASTING OF BEDROCK IS ANTICIPATED, THE APPLICANT SHALL SUBMIT A BLASTING PLAN THAT IDENTIFIES:
 - WHERE THE BLASTING ACTIVITIES ARE ANTICIPATED TO OCCUR;
 - THE ESTIMATED QUANTITY OF BLAST ROCK IN CUBIC YARDS; AND
 - SITE-SPECIFIC BLASTING BEST MANAGEMENT PRACTICES.



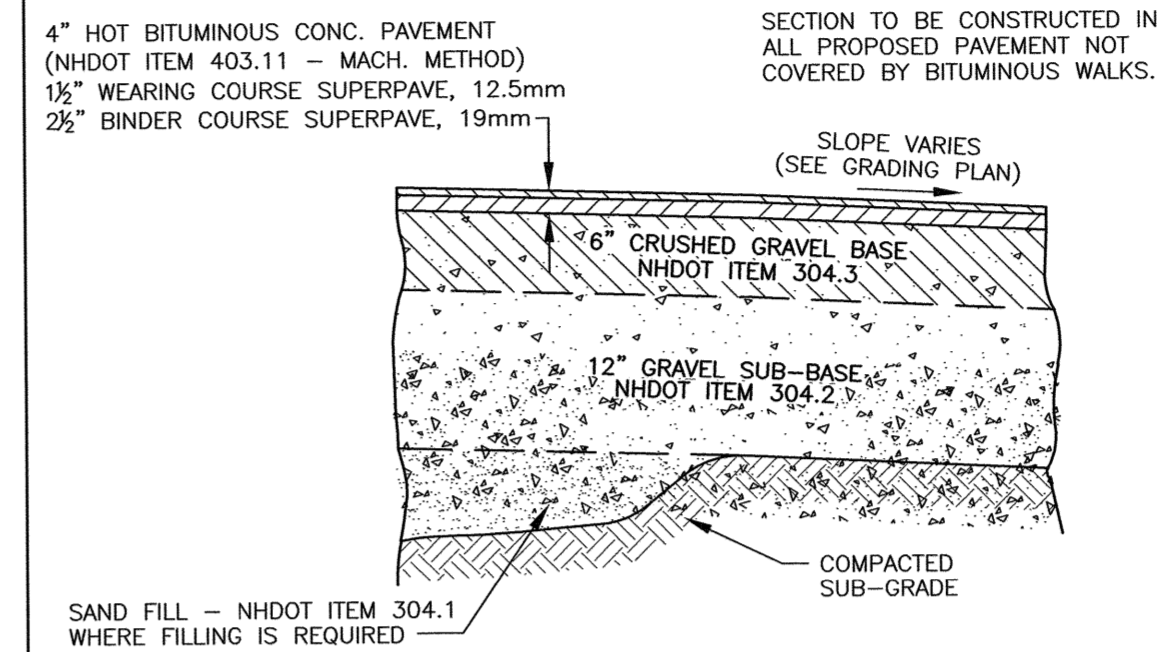
- NOTES:
1. ALL MATERIAL TO MEET FILTREXX SPECIFICATIONS.
 2. FILTREXX SYSTEM SHALL BE INSTALLED BY A CERTIFIED FILTREXX INSTALLER.
 3. THE CONTRACTOR SHALL MAINTAIN THE COMPOST FILTRATION SYSTEM IN A FUNCTIONAL CONDITION AT ALL TIMES. IT WILL BE ROUTINELY INSPECTED AND REPAIRED WHEN REQUIRED.
 4. SILTSOXX DEPICTED IS FOR MINIMUM SLOPES, GREATER SLOPES MAY REQUIRE ADDITIONAL PLACEMENTS.
 5. THE COMPOST FILTER MATERIAL WILL BE DISPERSED ON SITE WHEN NO LONGER REQUIRED, AS DETERMINED BY THE ENGINEER.

A **C3** FILTREXX® SILTSOXX™ FILTRATION SYSTEM NTS

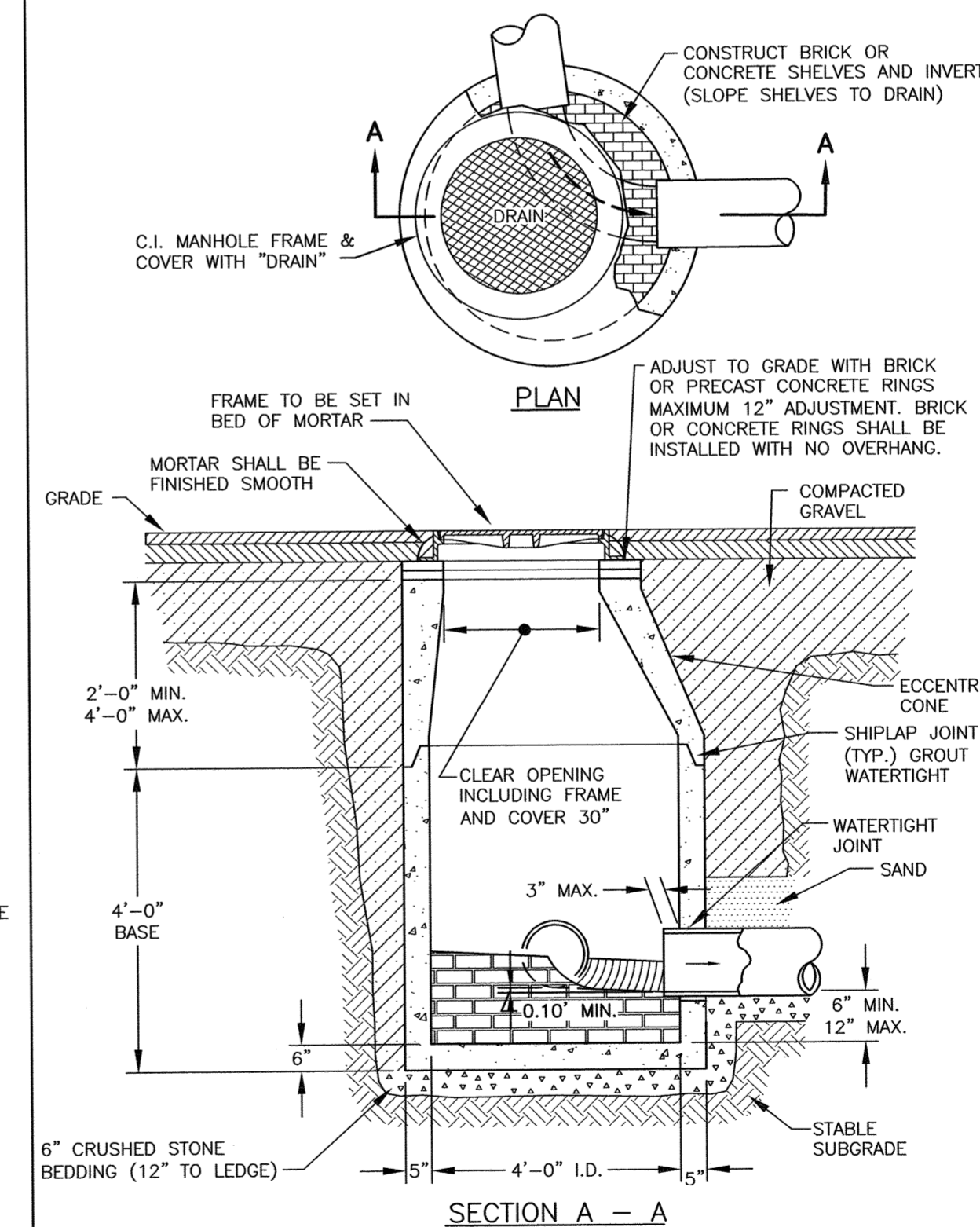


- 1) INLET BASKETS SHALL BE INSTALLED IMMEDIATELY AFTER CATCH BASIN CONSTRUCTION IS COMPLETE AND SHALL REMAIN IN PLACE AND BE MAINTAINED UNTIL PAVEMENT BINDER COURSE IS COMPLETE.
- 2) FILTER FABRIC SHALL BE PUSHED DOWN AND FORMED TO THE SHAPE OF THE BASKET. THE SHEET OF FABRIC SHALL BE LARGE ENOUGH TO BE SUPPORTED BY THE BASKET FRAME WHEN HOLDING SEDIMENT AND, SHALL EXTEND AT LEAST 6" PAST THE FRAME. THE INLET GRATE SHALL BE PLACED OVER THE BASKET/FRAME AND WILL SERVE AS THE FABRIC ANCHOR.
- 3) THE FILTER FABRIC SHALL BE A GEOTEXTILE FABRIC; POLYESTER, POLYPROPYLENE, STABILIZED NYLON, POLYETHYLENE, OR POLYVINYLIDENE CHLORIDE MEETING THE FOLLOWING SPECIFICATIONS:
 - TENSILE STRENGTH: 45 LB. MIN. IN ANY PRINCIPAL DIRECTION (ASTM D1682)
 - MULLEN BURST STRENGTH: MIN. 60 psi (ASTM D774)
- 4) THE FABRIC SHALL HAVE AN OPENING NO GREATER THAN A NUMBER 20 U.S. STANDARD SIEVE AND A MINIMUM PERMEABILITY OF 120 gpm/s.f. (MULTIPLY THE PERMITTIVITY IN SEC.-1 FROM ASTM 54491-85 USING THE CONVERSION FACTOR OF 74.)
- 5) THE INLET BASKET SHALL BE INSPECTED WITHIN 24 HOURS AFTER EACH RAINFALL OR DAILY DURING EXTENDED PERIODS OF PRECIPITATION. REPAIRS SHALL BE MADE IMMEDIATELY, AS NECESSARY, TO PREVENT PARTICLES FROM REACHING THE DRAINAGE SYSTEM AND/OR CAUSING SURFACE FLOODING.
- 6) SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT, OR MORE OFTEN IF THE FABRIC BECOMES CLOGGED.

B **C3** CATCH BASIN INLET BASKET NTS



C **C3** FULL DEPTH PAVEMENT SECTION NTS



- NOTES:
1. CONCRETE SHALL BE 4,000 P.S.I. AFTER 28 DAYS.
 2. CIRCUMFERENTIAL REINFORCEMENT SHALL BE 0.12 SQ. IN. PER LINEAR FT. IN ALL SECTIONS AND SHALL BE PLACED IN THE CENTER THIRD OF THE WALL.
 3. THE TONGUE OR THE GROOVE OF THE JOINT SHALL CONTAIN ONE LINE OF CIRCUMFERENTIAL REINFORCEMENT EQUAL TO 0.12 SQ. IN. PER LINEAR FT..
 4. EACH CASTING TO HAVE LIFTING HOLES CAST IN.
 5. STRUCTURE TO BE DESIGNED FOR H2O LOADING.

D **C3** DRAIN MANHOLE DETAIL NTS

NOTES:

- 1) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.
- 2) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.
- 3) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL, VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008)".

No.	DATE	DESCRIPTION	BY	CHK.
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-	-	-	-	-
1	7/17/23	ADD DETAILS	OS	JC
0	5/2/23	ISSUED FOR COMMENT	OS	JC

NOT FOR CONSTRUCTION

AMBIT ENGINEERING, INC.
A DIVISION OF HALEY WARD, INC.

200 Griffin Road, Unit 3
Portsmouth, NH 03801
603.430.9282

PROJECT: **BUILDING EXPANSION PLAN**
PORTSMOUTH AUTO BODY CENTER
700 PEVERLY HILL ROAD, PORTSMOUTH, NH

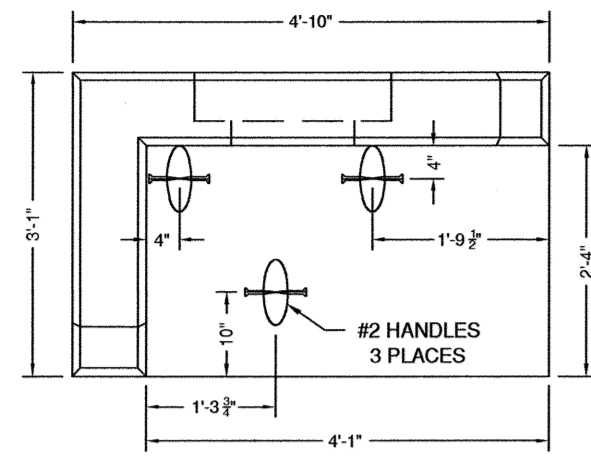
TITLE: **EROSION CONTROL NOTES & DETAILS**

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CHECKED BY: JC	
PROJECT No: 5010265-3576	FIELD BOOK & PAGE: FB 389 PG 18
DRAWING No:	
SHEET 6	D1

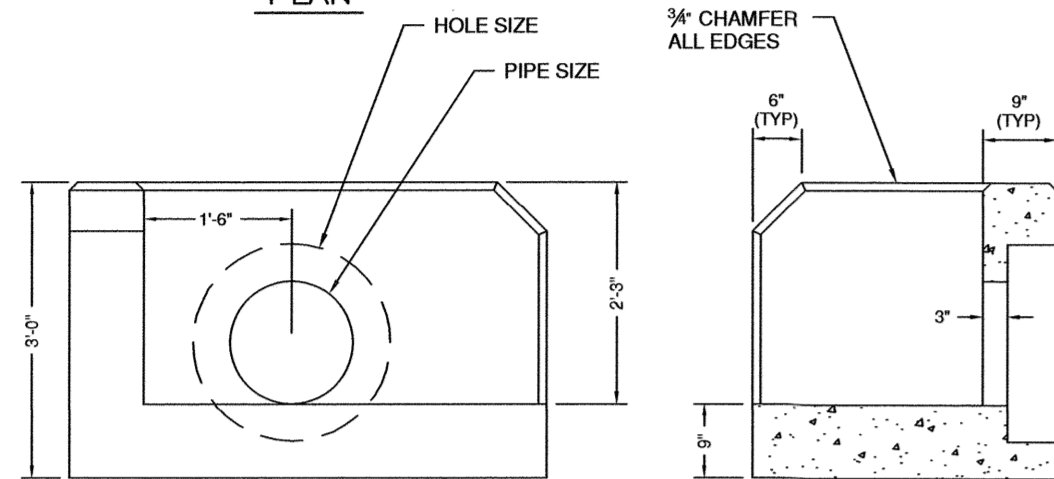
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Pipe Size	Hole Size	Weight
8"	12"	3,383#
12"	20"	3,262#
15"	24"	3,173#
18"	27"	3,090#

SHOWN AS LEFT STYLE HEADWALL
- ALSO AVAILABLE AS RIGHT

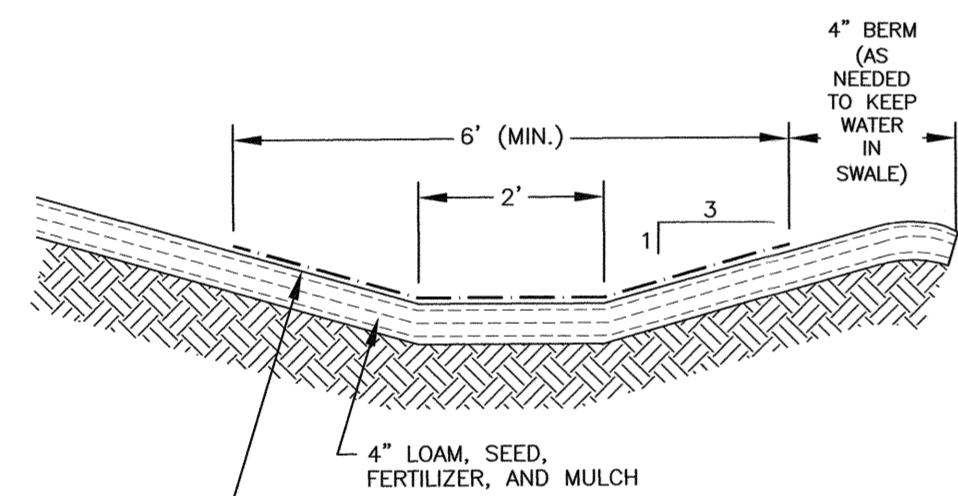


PLAN



ELEVATION

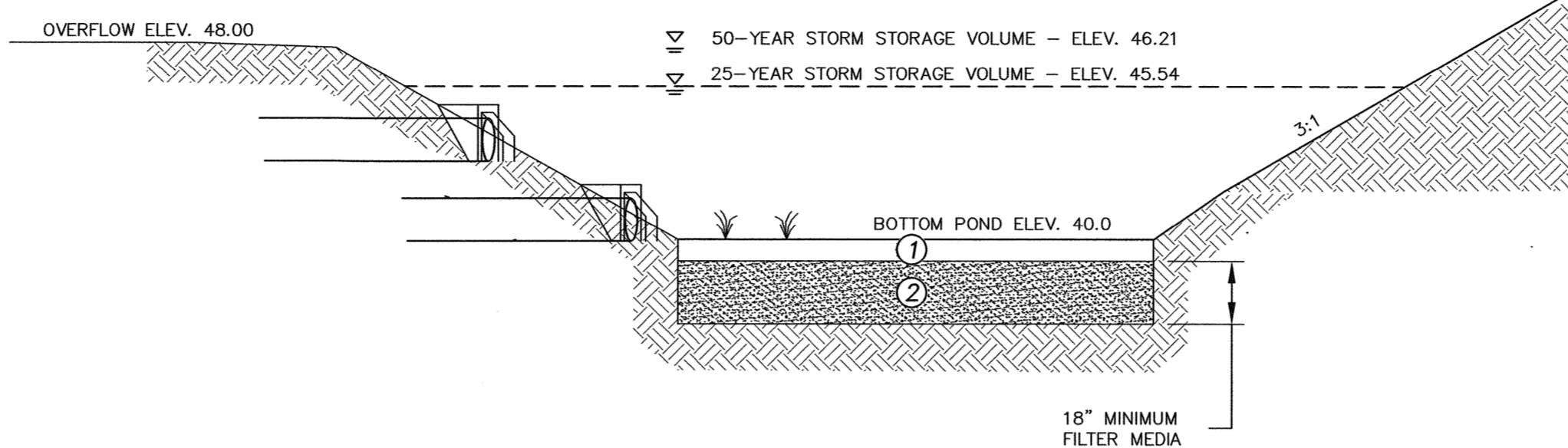
E HEADWALL DETAIL
C3 NTS



CROSS SECTION

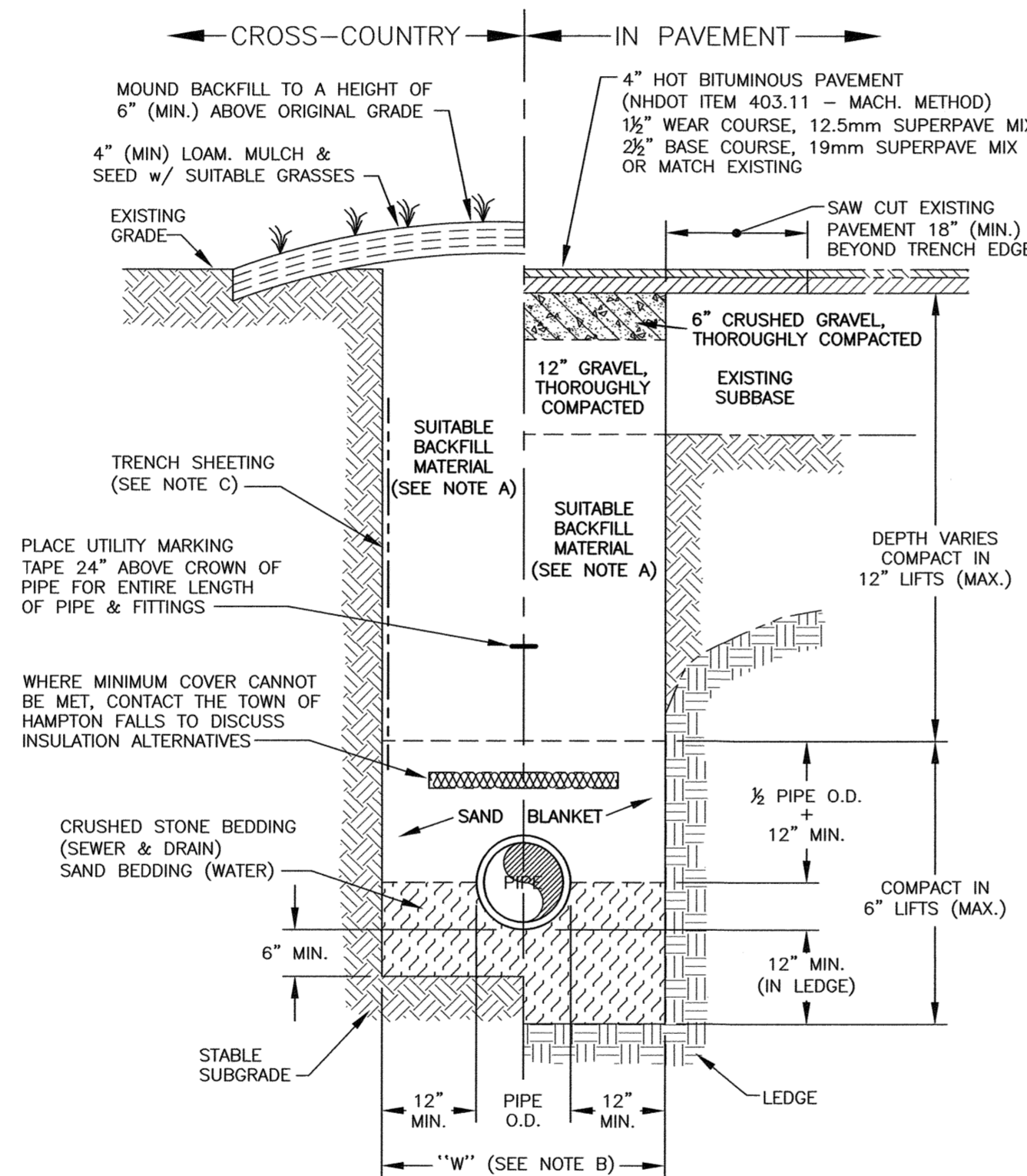
*VEGETATED SWALE TO BE SEEDED WITH TICKLESEED/ROUGH BENTGRASS (AGROSTIS SCABRA), VIRGINIA WILD RYE (ELYMUS VIRGINIUS) AND LITTLE BLUESTEM (SCHIZACHYRIUM SCOPARIUM) SPREAD THROUGHOUT.

F VEGETATED SWALE
C3 NTS



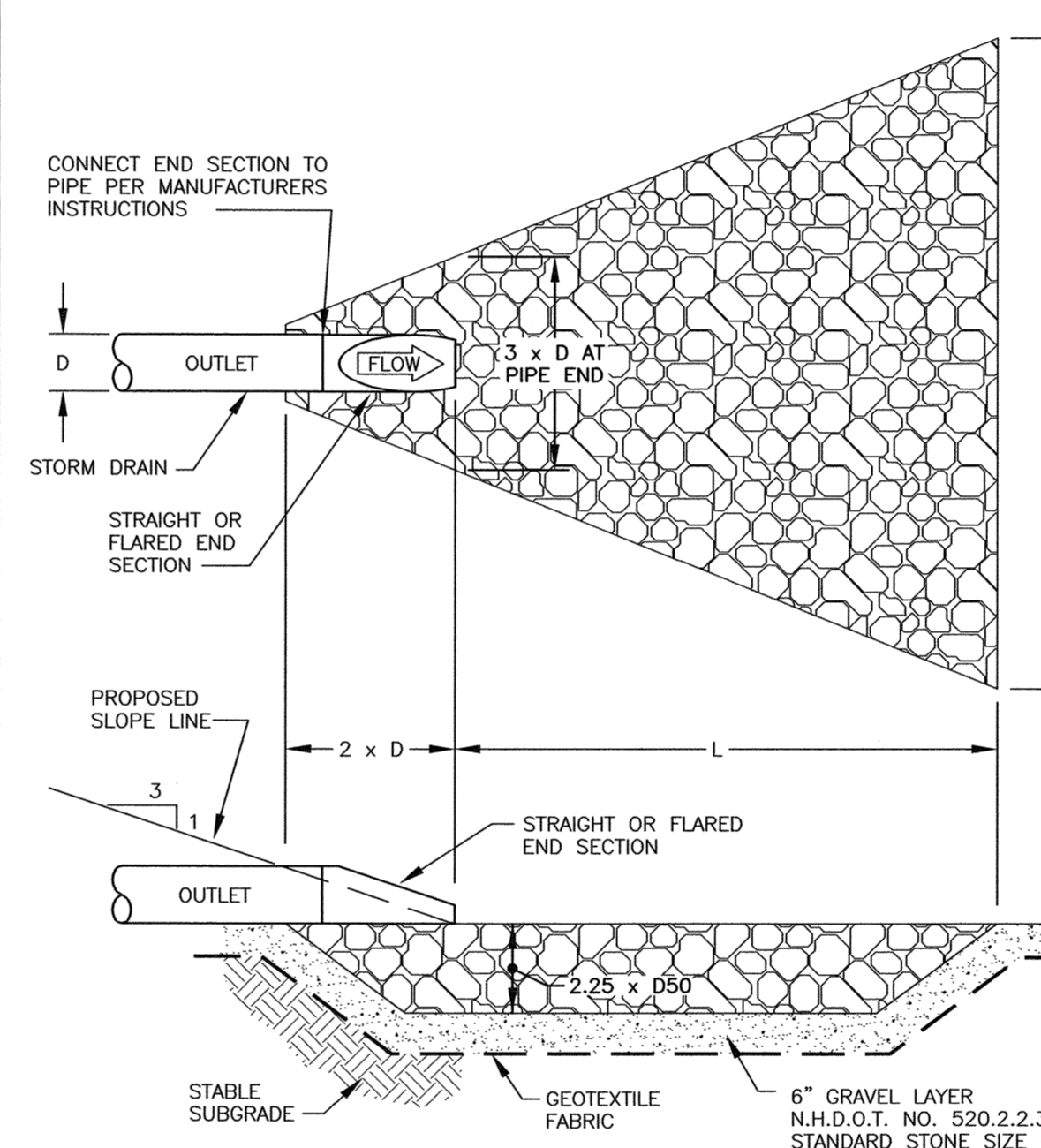
G DETENTION POND DETAILS
C3 NTS

FILTER MEDIA	
① MULCH/GROWING MEDIUM: GRASS SEED MIX A WITH LOAM	
② SOIL FILTER LAYER: USE UNHSC BIORETENTION SOIL SPECIFICATIONS DATED FEBRUARY, 2017. 20% - 30% MULCH BY VOLUME, MIXED THOROUGHLY WITH LOAMY, COARSE SAND (70% - 80% BY VOLUME) MEETING THE FOLLOWING GRADATION;	
SIEVE NO.	% BY WEIGHT, PASSING
4	100
10	95
40	40 - 15
200	10 - 20
<200	0 - 5



H TYPICAL PIPE TRENCH
C3 NTS

TRENCH NOTES:
A) TRENCH BACKFILL: - IN PAVED AREAS, SUITABLE MATERIAL FOR TRENCH BACKFILL SHALL BE THE NATURAL MATERIAL EXCAVATED DURING CONSTRUCTION, BUT SHALL EXCLUDE DEBRIS, PIECES OF PAVEMENT, ORGANIC MATTER, TOP SOIL, ALL WET OR SOFT MUCK, PEAT OR CLAY, ALL EXCAVATED LEDGE MATERIAL, AND ALL ROCKS OVER SIX INCHES IN LARGEST DIMENSION, OR ANY MATERIALS DEEMED TO BE UNACCEPTABLE BY THE ENGINEER.
B) "W" = MAXIMUM ALLOWABLE TRENCH WIDTH TO A PLANE 12 INCHES ABOVE THE PIPE. FOR PIPES 15 INCHES NOMINAL DIAMETER OR LESS, W SHALL BE NO MORE THAN 36 INCHES. FOR PIPES GREATER THAN 15 INCHES NOMINAL DIAMETER, W SHALL BE 24 INCHES PLUS PIPE O.D..
C) TRENCH SHEETING: IF REQUIRED, WHERE SHEETING IS PLACED ALONGSIDE THE PIPE AND EXTENDS BELOW MID-DIAMETER, IT SHALL BE CUT OFF AND LEFT IN PLACE TO AN ELEVATION NOT LESS THAN 1 FOOT ABOVE THE TOP OF THE PIPE. WHERE SHEETING IS ORDERED BY THE ENGINEER TO BE LEFT IN PLACE, IT SHALL BE CUT OFF AT LEAST 3 FEET BELOW FINISHED GRADE, BUT NOT LESS THAN 1 FOOT ABOVE THE TOP OF THE PIPE.
D) MINIMUM PIPE COVER FOR UTILITY MAINS (UNLESS GOVERNED BY OTHER CODES): 3' MINIMUM FOR STORMWATER DRAINS 5' MINIMUM FOR WATER MAINS
E) ALL PAVEMENT CUTS SHALL BE REPAIRED BY THE INFRARED HEAT METHOD.

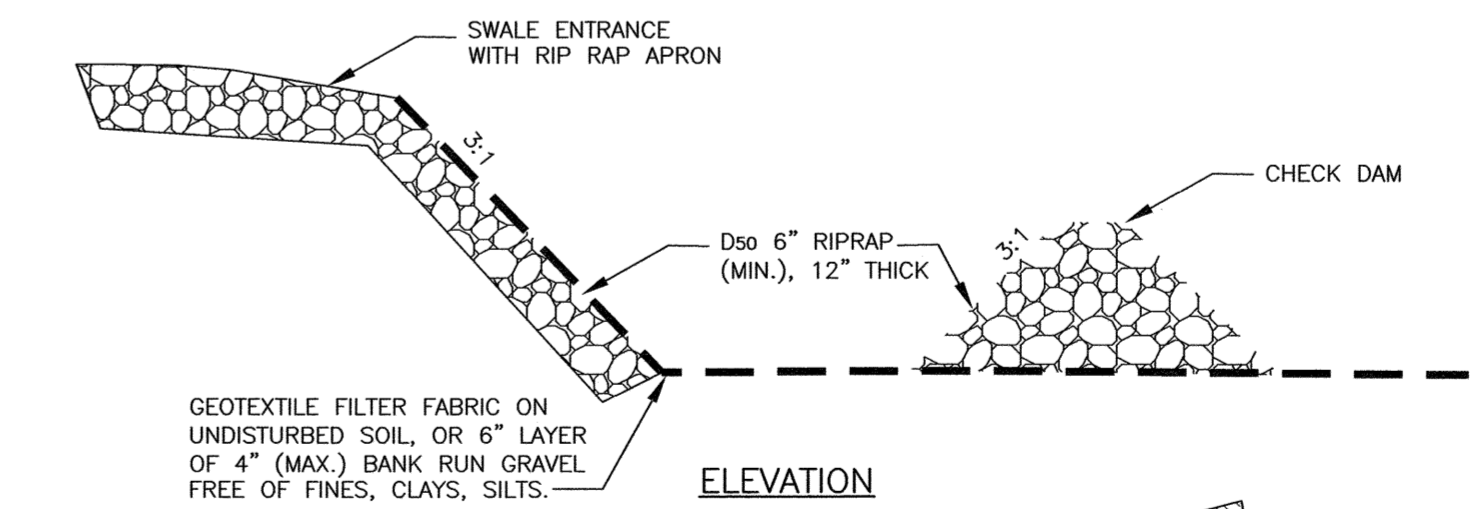


I CULVERT OUTLET PROTECTION
C3 NTS

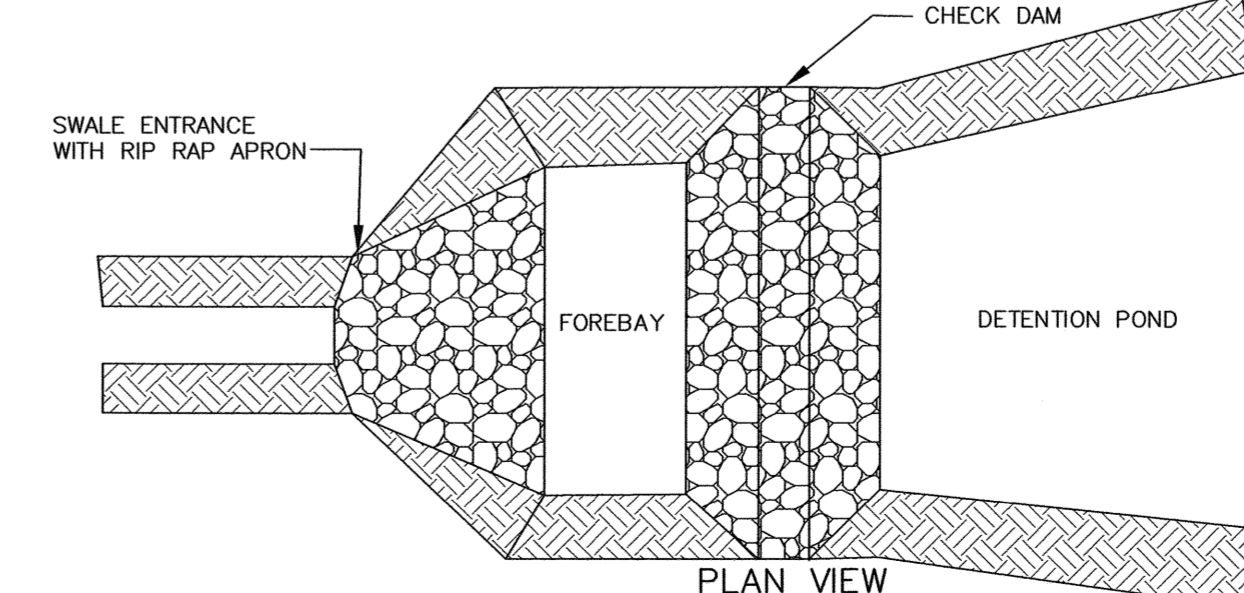
LENGTH TABLE			
D	L	W	D50
12"	14'	17'	3"
15"	16'	20'	4"
18"	20'	25'	6"
24"	30'	36'	8"

NOTES
1) USE #50 AS NOTED IN TABLE UNLESS SPECIFIED OTHERWISE ON PLANS.
2) UNDERLAY RIP-RAP WITH 6" OF SIZE #7 STONE FILL (N.H.D.O.T. NO. 520.2.2.3) & MIRAFI 700X OR APPROVED EQUAL GEOTEXTILE FABRIC.
3) USE WIDTHS NOTED IN TABLE OR CONFORM TO NATURAL OR PROPOSED SWALE TOPOGRAPHY.

NHDOT NO. 520.2.2.3 STANDARD STONE SIZE 67	
SIEVE SIZE	PERCENTAGE BY WEIGHT, PASSING
1" (25.0mm)	100
3/4" (19.0mm)	90 - 100
3/8" (9.5mm)	20 - 25
No. 4 (4.75mm)	0 - 10
No. 8 (2.36mm)	0 - 5



J SEDIMENT FOREBAY DETAIL
C3 NTS



NOTES:
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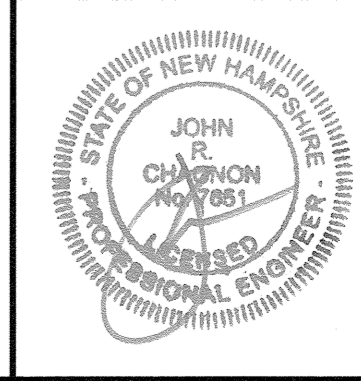
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200 Griffin Road, Unit 3
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PROJECT
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PORTSMOUTH AUTO BODY CENTER
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TITLE
DETAILS

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PROJECT No. 5010265-3576	FIELD BOOK & PAGE FB 389 PG 18
DRAWING No. SHEET 7	
D2	



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