

AMBIT ENGINEERING, INC. CIVIL ENGINEERS AND LAND SURVEYORS 200 Griffin Road, Unit 3, Portsmouth, NH 03801 Phone (603) 430-9282 Fax 436-2315

17 July 2018

Ms. Juliet Walker, Chair City of Portsmouth Technical Advisory Committee 1 Junkins Avenue Portsmouth, NH 03801

RE: Site Plan Approval for 140 Court Street; Portsmouth Housing Authority

Dear Ms. Walker and TAC Members:

We hereby submit, on behalf of the Portsmouth Housing Authority, this **Response to Comments** for consideration at your July 31 TAC Committee Meeting. The response is based on the comments from the July 3 TAC Committee meeting shown below with responses in **bold text**:

- 1. The label "Bench (TYP)" needs to be revised to say "Existing Bench to Remain". Site plans updated to indicate benches to remain.
- 2. There needs to be some additional bike parking outside. Perhaps a ½ Zagster with some added spaces for resident bikes. The Landscape Plans show a smaller (1/2) Zagster rack along Court Street with an additional bicycle rack added to the plan in the south end of the (central) park. The ordinance requires one bicycle space per 5 dwelling units; 33 would be required. We have 30 inside and 10 outside not including the Zagster rack.
- 3. Door swings need to be displayed on the plans; especially Basement Plan. Door swings are shown on the Basement Plan Sheet C4.
- 4. Basement Plan should identify uses in all rooms. Uses are shown on the Basement Plan Sheet C4.
- 5. Comments about the proposed property line with 152 Court Street with a suggestion we adjust the angle and extend the area a couple of feet. The property line has been adjusted as requested.
- 6. Can we design a more inviting entrance from Court Street? Plans updated.
- 7. The Community Space should not be labelled as Open Space. Ambit revised plans.
- 8. The drainage design/report will need further review and study. Ambit attended a meeting with Planning and DPW to facilitate a possible solution; which has been shown on the revised plans.
- 9. A Code Study should be provided for the roof deck. CJ provided narrative included in this submission.

We look forward to continuing the Site Review process at the July 31 TAC Meeting.

Sincerely,

John Chagnon, PE; Ambit Engineering, Inc.

CC (via email): Portsmouth Housing Authority, John Bosen, Peter Roche, CJ Architects

J:\JOBS2UN2700's\JN 2790's\JN 2790\2017 Site Planning\Applications\Portsmouth Site Plan\TAC Response to Comments Letter 7-17-18.doc



July 12, 2018

Carl Roediger, Deputy Fire Chief Portsmouth Fire Department 170 Court Street Portsmouth, NH 03801

Mr. Roediger,

In response to your inquiry during the Technical Advisory (TAC) meeting on July 3, 2018, we are providing the following analysis showing building code compliance as it relates to the 4th floor deck being proposed on the north side of the building at the 140 Court Street Development project.

IBC (2009):

The building will be a fully sprinklered building and complies with IBC 2009 section 1021.1 with 2 exits from each of the building's stories.

The proposed 4th floor deck is 584 square feet. For residential use R-2, the occupant load factor is 200 gross square feet per person, resulting in an occupant load of 3. (584 square feet / 200 square feet = 2.92.)

Per section 1015.1, Table 1501.1, spaces with one exit are limited to 10 occupants for residential occupancy, so the 4th floor deck would be allowed 1 exit.

If the 4th floor deck is interpreted to be Assembly A-3 (worst-case), the occupant load factor would be 15 net square feet per person, resulting in an occupant load of 39. (584 square feet / 15 square feet = 38.9.)

Per section 1015.1, Table 1501.1, spaces with one exit are limited to 49 occupants for assembly occupancy, so the 4th floor deck would be allowed 1 exit.

Both interpretations of IBC would allow for the 4th floor deck to have one exit.

NFPA 101 (2015):

Chapter 30/31 *New and Existing Apartment Buildings,* Section 30.2.4 *Number of Means of Egress* does not comment on the number of means of egress from spaces other than dwelling units.



Chapter 12/13 New and Existing Assembly Occupancies, Section 12.2.4.5 Number of Means of Egress states that balconies and mezzanines having an occupant load not exceeding 50 shall be permitted to be served by a single means of egress, and such means of egress shall be permitted to lead to the floor below.

Both interpretations of NFPA 101 would allow for the 4th floor deck to have one exit.

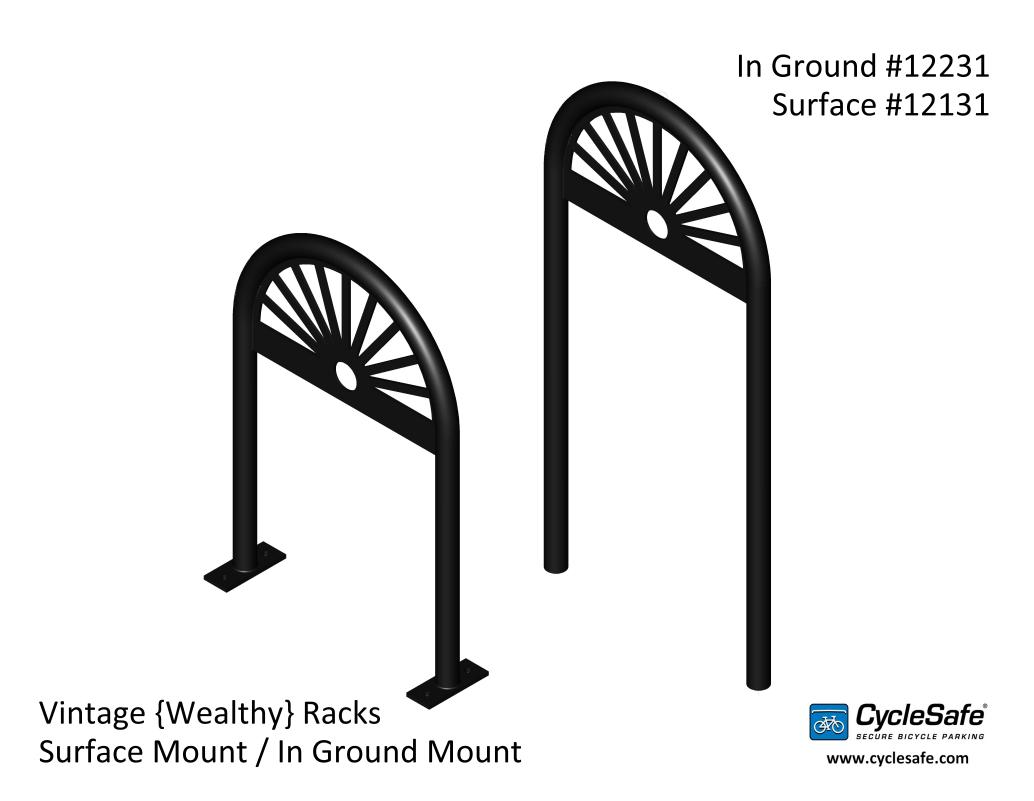
The common decks located at the first, second, third, and fourth floors on the south side of the building also comply with the above code sections.

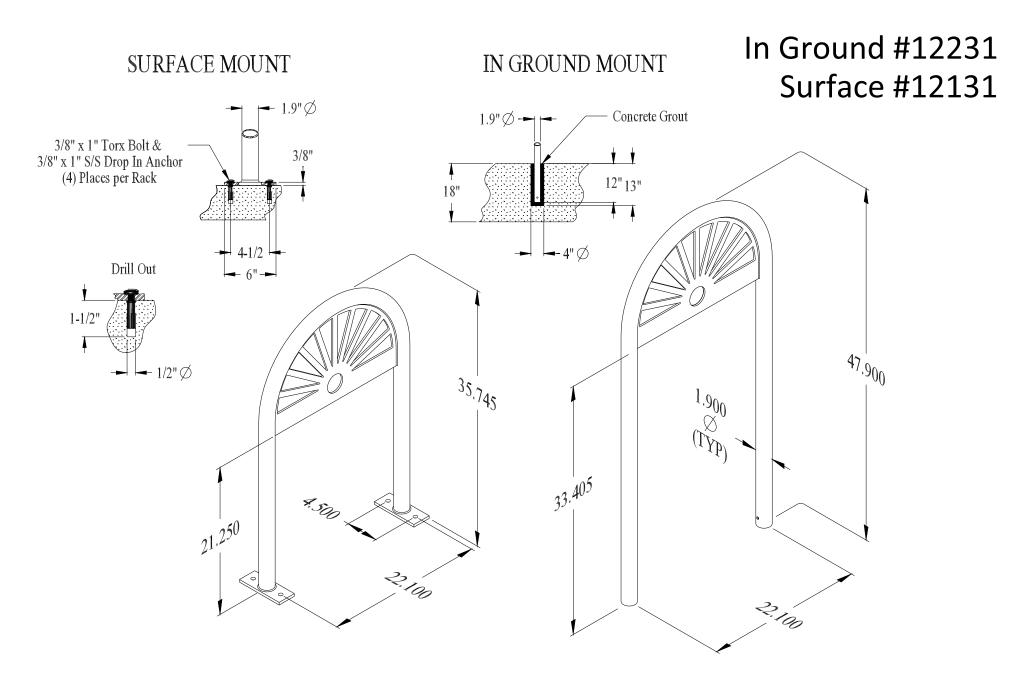
Please let us know if you have any questions.

Thank you,

Carla Goodknight – AIA

Cc: Robert Marsilia, Chief Building Inspector City of Portsmouth





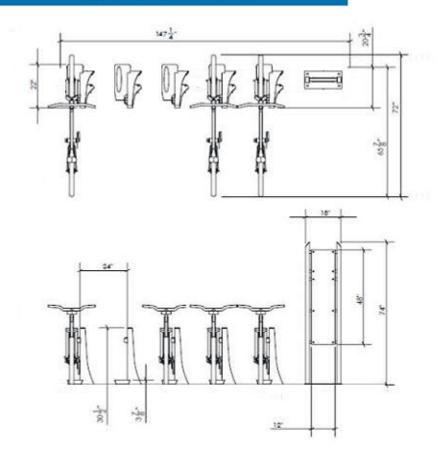
Vintage {Wealthy} Racks Surface Mount / In Ground Mount {Dims}



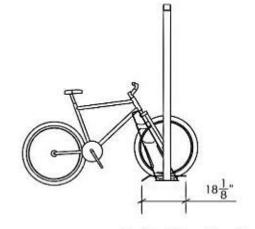
www.cyclesafe.com



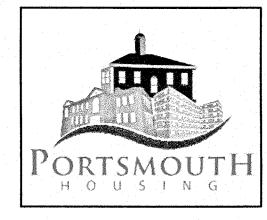
Zagster K1 Station- 5 bike







Confidential and Proprietary



OWNERS:

PORTSMOUTH HOUSING AUTHORITY 245 MIDDLE STREET PORTSMOUTH, NH 03801 TEL. (603) 436-4310

ED PAC, LLC 242 CENTRAL AVENUE DOVER, NH 03820

CIVIL ENGINEER & LAND SURVEYOR:

AMBIT ENGINEERING, INC. 200 GRIFFIN ROAD, UNIT 3 PORTSMOUTH, N.H. 03801 Tel. (603) 430–9282 Fax (603) 436-2315

ARCHITECT:

CJ ARCHITECTS 233 VAUGHN STREET PORTSMOUTH NH, 03801 TEL.(603) 431–2808

PORTSMOUTH APPROVAL CONDITIONS NOTE:

PORTSMOUTH SITE PLAN REVIEW REGULATIONS.

CHAIRMAN

ALL CONDITIONS ON THIS PLAN SET SHALL REMAIN IN EFFECT IN PERPETUITY PURSUANT TO THE REQUIREMENTS OF THE CITY OF

APPROVED BY THE PORTSMOUTH PLANNING BOARD

DATE

WORKFORCE HOUSING DEVELOPMENT **140 COURT STREET** PORTSMOUTH, NEW HAMPSHIRE PERMIT LIST: NHDES SEWER DISCHARGE PERMIT: TO BE SUBMITTED G2+1 LLC SITE PERMIT PLANS 70 NEW ROAD

LANDSCAPE ARCHITECT:

SALISBURY, NH 03268 TEL./FAX. (603) 648-6434

GEOTECHNICAL:

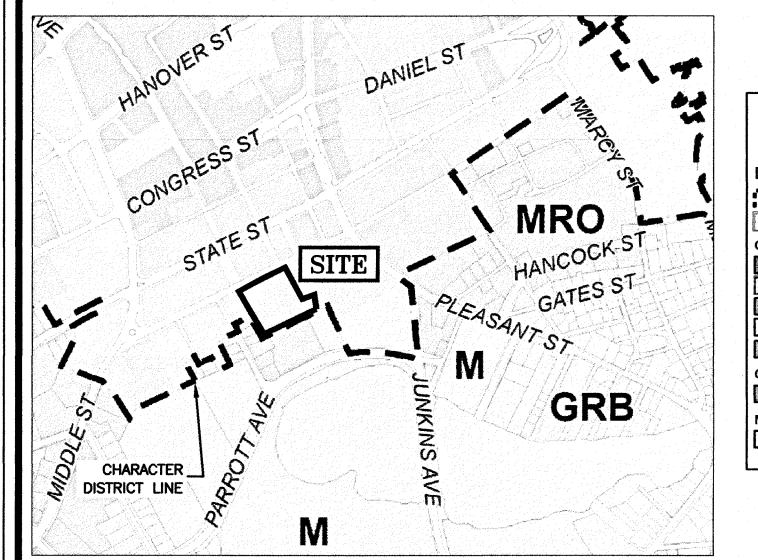
JOHN TURNER CONSULTING 19 DOVER STREET DOVER, NH 03820 (603) 749-1841

ARCHAEOLOGICAL:

INDEPENDENT ARCHAEOLOGICAL 801 ISLINGTON STREET #31 PORTSMOUTH NH 03801 (603) 430–2970

ATTORNEY:

BOSEN & ASSOCIATES 266 MIDDLE STREET PORTSMOUTH NH 03801 (603) 427-5500



Character Districts and Civic Districts Downtown Overlay District **Character Districts** CD5 Character District 5 CD4 Character District 4 -325 CD4-L2 Character District 4-L2 **Civic District** Civic District

Map 10.5A21A

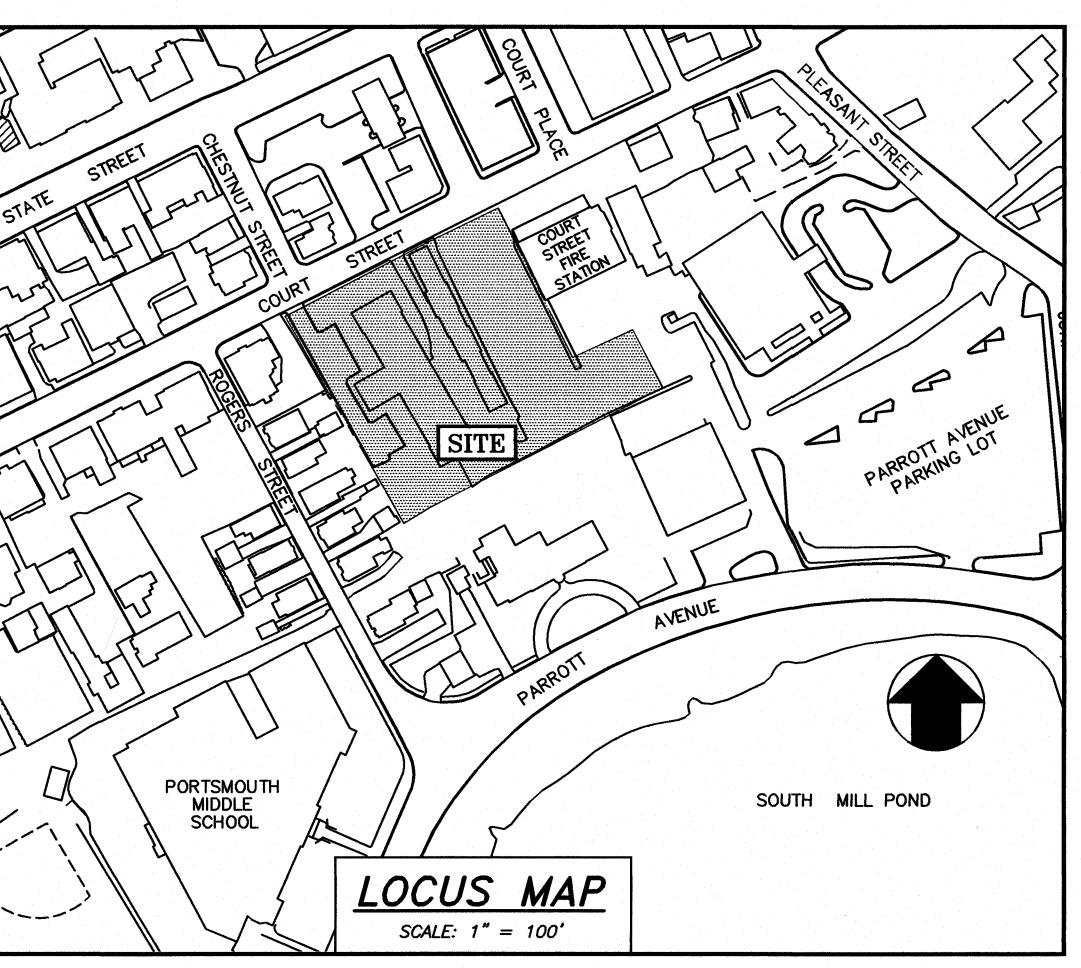
CD4-W Character District 4-W CD4-L1 Character District 4-L1 **Municipal District** Municipal District

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. —	BUUNDART PLAN
	LOT LINE RELOCATION PL
C1	EXISTING CONDITIONS PL
C2	DEMOLITION PLAN
C3	SITE LAYOUT PLAN
C4	PARKING AND OPEN SPA
C5	UTILITY PLAN
C6	GRADING & EROSION CO
C7	OFF-SITE IMPROVEMENTS
A 1.0-4.0	LANDSCAPE PLANS
LT1	LIGHTING PLAN
D1	EROSION CONTROL NOTE
D2-D4	DETAILS
7.0	FLOOR PLANS
8.0-8.5	ELEVATIONS





PLAN _AN

ACE PLAN

ONTROL PLAN S PLAN

ES & DETAILS

UTILITY CONTACTS

ELECTRIC: EVERSOURCE 1700 LAFAYETTE ROAD PORTSMOUTH, N.H. 03801 Tel. (603) 436-7708, Ext. 555.5678 ATTN: MICHAEL BUSBY, P.E. (MANAGER)

SEWER & WATER: PORTSMOUTH DEPARTMENT OF PUBLIC WORKS 680 PEVERLY HILL ROAD

PORTSMOUTH, N.H. 03801

Tel. (603) 427-1530

ATTN: JIM TOW

NATURAL GAS: UNITIL 325 WEST ROAD PORTSMOUTH, N.H. 03801 Tel. (603) 294–5144 ATTN: DAVE BEAULIEU

CABLE: COMCAST 155 COMMERCE WAY PORTSMOUTH, N.H. 03 Tel. (603) 679-5695 ATTN: MIKE COLLINS

COMMUNICATIONS: FAIRPOINT COMMUNICATIONS JOE CONSIDINE 1575 GREENLAND ROAD GREENLAND, N.H. 03840 Tel. (603) 427-5525



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PROPERTY LINE SETBACK SEWER PIPE SEWER LATERAL GAS LINE STORM DRAIN VATER LINE ATER SERVICE INDERGROUND ELECTRIC OVERHEAD ELECTRIC/WIRES FOUNDATION DRAIN EDGE OF PAVEMENT (EP) CONTOUR

SPOT ELEVATION

UTILITY POLE WALL MOUNTED EXTERIOR LIGHTS TRANSFORMER ON CONCRETE PAD

ELECTRIC HANDHOLD

SHUT OFFS (WATER/GAS)

GATE VALVE HYDRANT

CATCH BASIN

SEWER MANHOLE

DRAIN MANHOLE

TELEPHONE MANHOLE

PARKING SPACE COUNT

PARKING METER

LANDSCAPED AREA

TO BE DETERMINED CAST IRON PIPE COPPER PIPE DUCTILE IRON PIPE POLYVINYL CHLORIDE PIPE REINFORCED CONCRETE PIPE ASBESTOS CEMENT PIPE VITRIFIED CLAY PIPE EDGE OF PAVEMENT ELEVATION FINISHED FLOOR INVERT SLOPE FT/FT TEMPORARY BENCH MARK TYPICAL

SITE PERMIT PLANS PORTSMOUTH HOUSING AUTHORITY WORKFORCE HOUSING DEVELOPMENT 140 COURT STREET PORTSMOUTH, N.H.



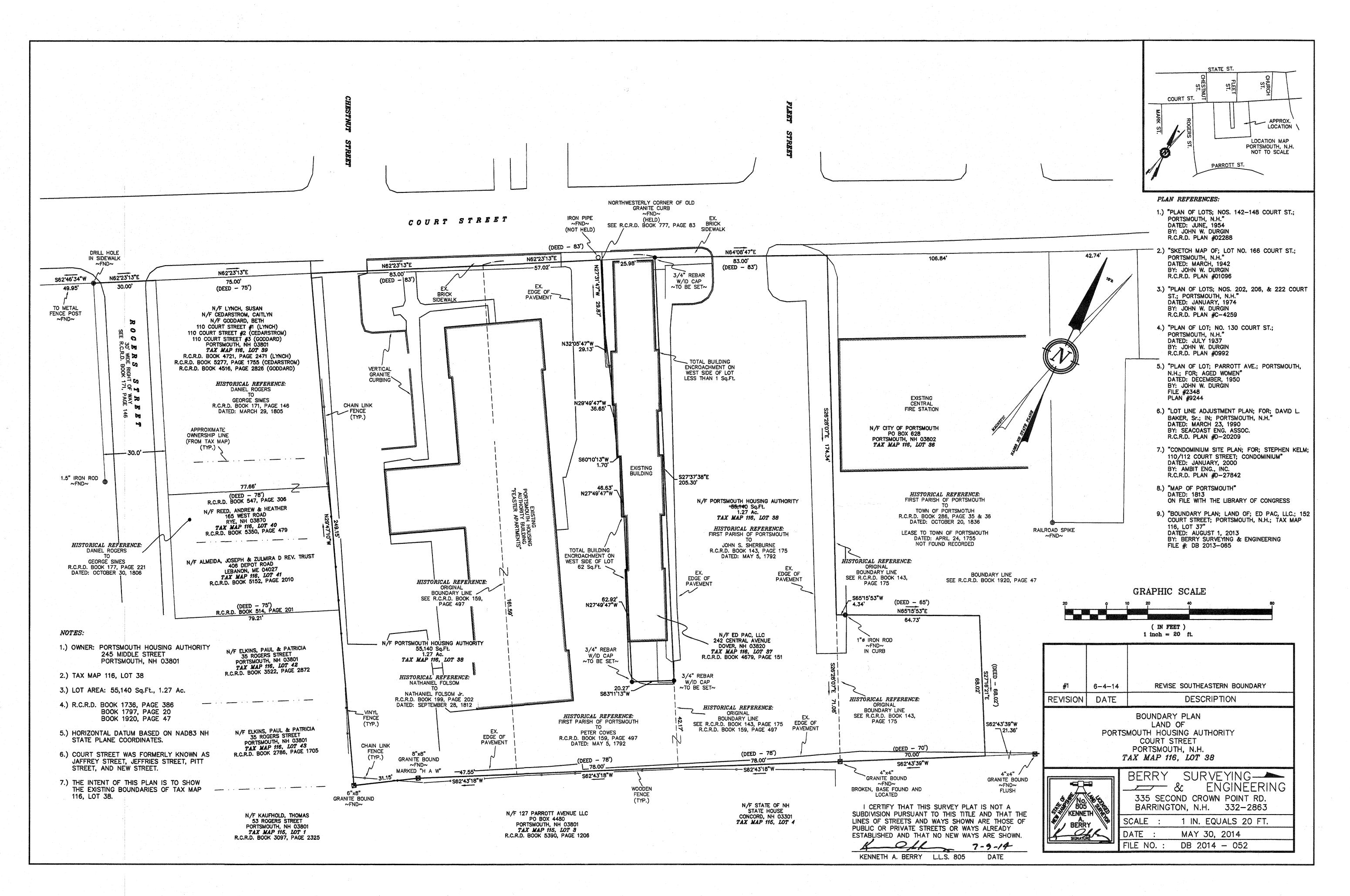
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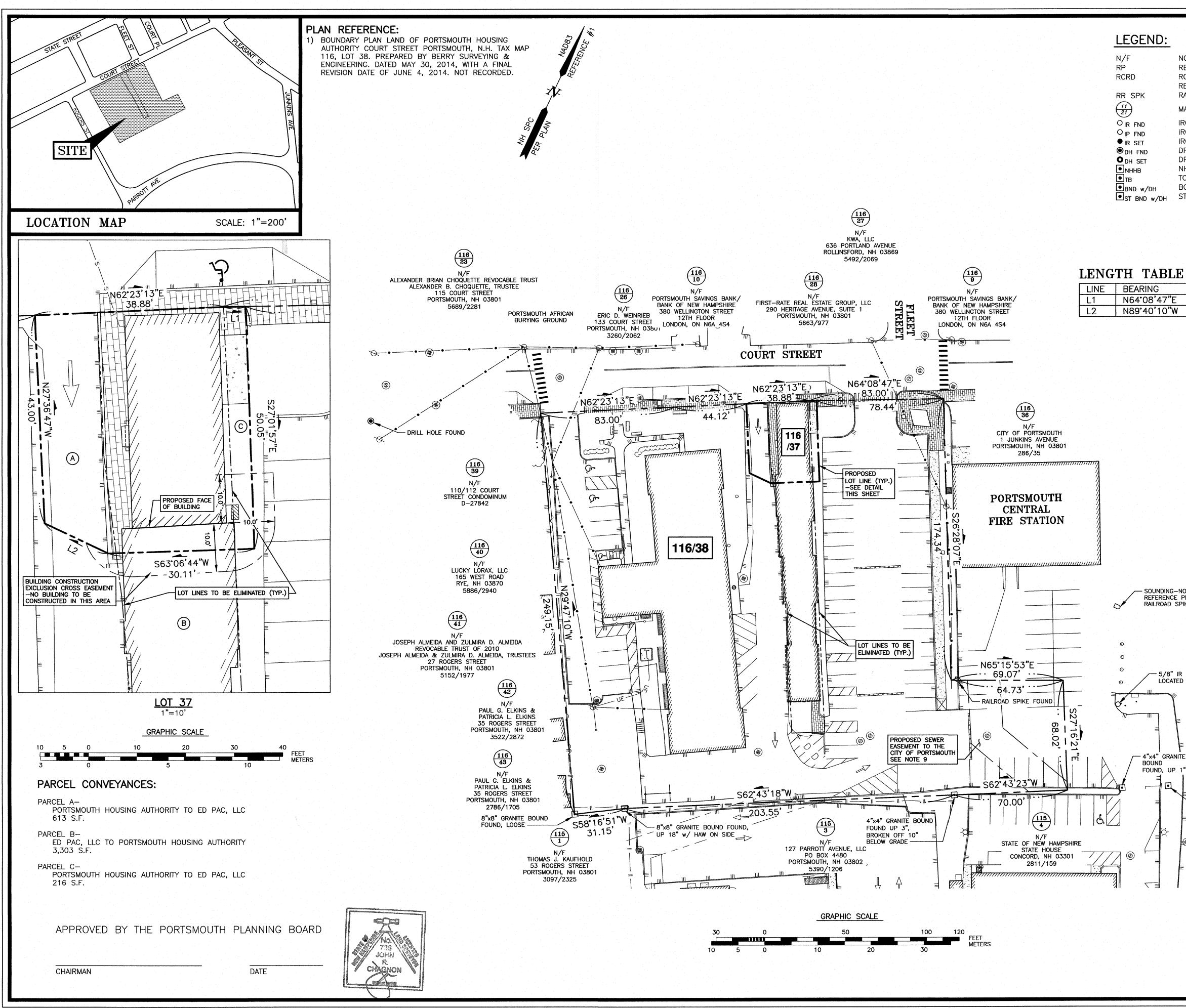
AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors 200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114 Tel (603) 430-9282 Fax (603) 436-2315

PLAN SET SUBMITTAL DATE: 17 JULY 2018

TYP

2790





NOW OR FORMERLY RECORD OF PROBATE ROCKINGHAM COUNTY REGISTRY OF DEEDS RAILROAD SPIKE MAP 11/LOT 21 IRON ROD FOUND IRON PIPE FOUND IRON ROD SET DRILL HOLE FOUND DRILL HOLE SET NHDOT BOUND FOUND TOWN BOUND BOUND WITH DRILL HOLE STONE BOUND WITH DRILL HOLE

· .	DISTANCE
ŀ7"Ε	4.56'
0"W	14.52'



AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors

200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114 Tel (603) 430-9282 Fax (603) 436-2315

NOTES: 1) PARCELS ARE SHOWN ON THE CITY OF PORTSMOUTH ÁSSESSOR'S MAP 116 AS LOT 38 AND LOT 37.

2) OWNERS OF RECORD:

116/38 PORTSMOUTH HOUSING AUTHORITY

245 MIDDLE STREET PORTSMOUTH, NH 03801

R.C.R.D BK 1736, PG 386, BK 1797 PG 20, AND BK 1920, PG 47

<u>116/37</u> ED PAC, LLC

242 CENTRAL AVENUE DOVER, NH 03820

BK 4679, PG 151

3) PARCEL 116/38 AND 116/37 ARE NOT IN A SPECIAL FLOOD HAZARD AREA AS SHOWN ON FIRM PANEL 3301SC0259E. EFFECTIVE 5/17/2005

4) LOT AREAS:

LOT 11/38 EXISTING: 59,976 (S.F.) 1.3769 ACRES PROPOSED: 62,450 (S.F.) 1.4337 ACRES

LOT 11/37 EXISTING: 4,587 (S.F.) 0.1053 ACRES PROPOSED: 2,113 (S.F.) 0.0485 ACRES

5) PARCELS ARE LOCATED IN CHARACTER DISTRICT 4 (ČD4).

6) THE PURPOSE OF THIS PLAN IS TO SHOW THE RÉLOCATION OF LOT LINES BETWEEN TAX MAP 116 LOTS 38 AND 37.

7) EXISTING BOUNDARY LINES FROM PLAN REFERENCE 1.

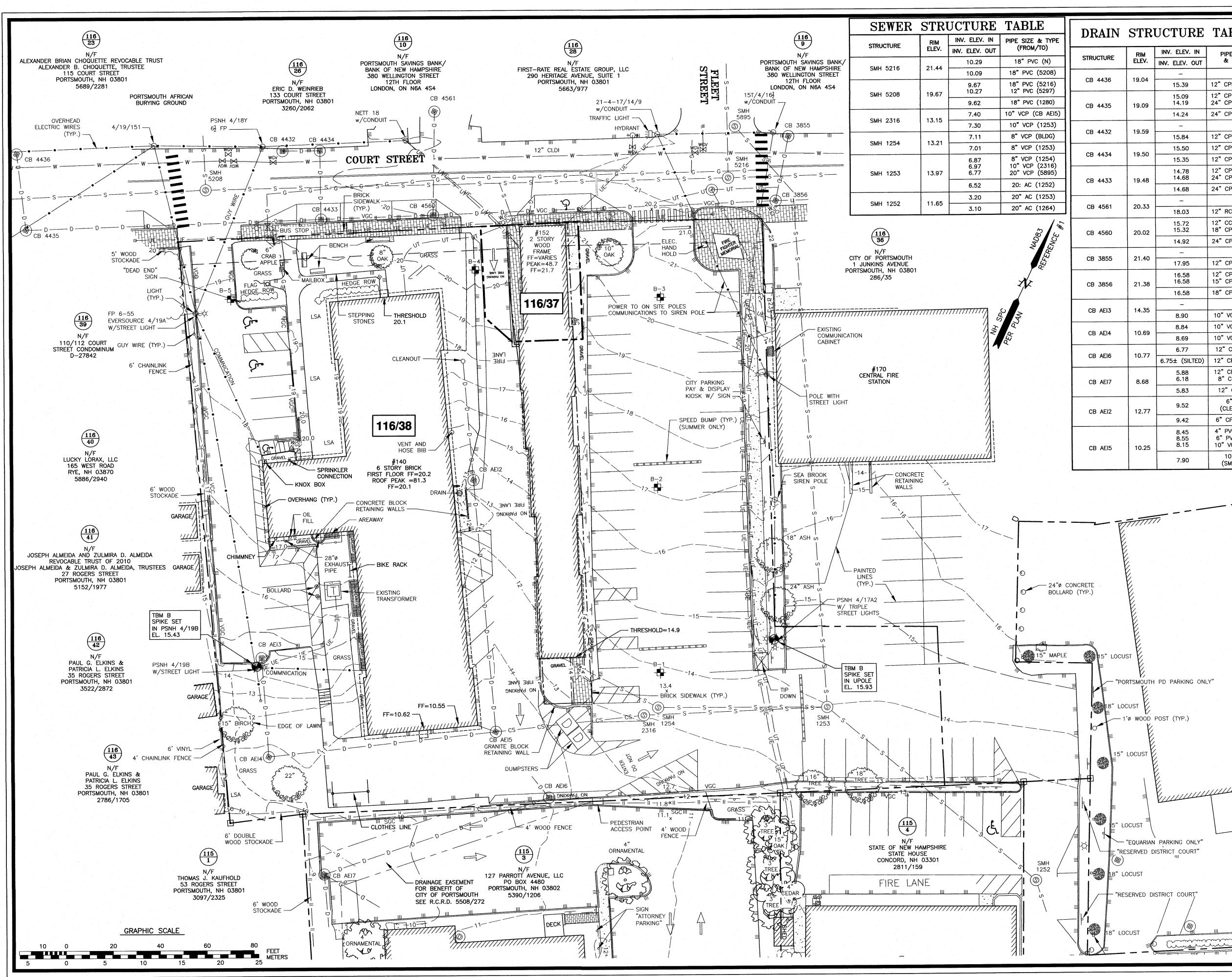
8) PERMANENT MONUMENTS ON LOT 37 TO BE SET IN ACCORDANCE WITH CITY OF PORTSMOUTH STANDARDS AFTER SITE DEVELOPMENT.

9) PROPOSED 20 FT WIDE SEWER EASEMENT TO BE CONVEYED TO THE CITY OF PORTSMOUTH. LOCATION OF SEWER LINE RUNNING NORTHERLY TO COURT STREET IS APPROXIMATE. EASEMENT IS TO BE 20 FEET WIDE, 10 FEET EITHER SIDE OF THE CENTERLINE OF THE EXISTING SEWER PIPE, WETHER THE LOCATION IS PRECISELY AS SHOWN HEREON OR NOT.

NING-NOTED ON ENCE PLAN AS AD SPIKE FOUND			
	5	REVISE LOT LINES	7/9/18
	4	ADD SEWER EASEMENT	7/3/18
		LOT LAYOUTS	6/18/18
8" IR BENT UP 6"	2	ISSUED TO TAC	5/8/18
CATED AT BASE	1	ISSUED FOR APPROVAL	4/25/18
CITIZENS BANK	0	ISSUED FOR COMMENT	3/5/17
	NO.	DESCRIPTION	DATE
		REVISIONS	
UP 1"		TAX MAP 116 - LOTS	
4"x4" GRANITE BOUND FOUND, FLUSH			AUTHORITY AUTHORITY REET
4"x4" GRANITE BOUND FOUND, FLUSH		FOR PORTSMOUTH HOUSING OWNERS PORTSMOUTH HOUSING 245 MIDDLE STR	AUTHORITY AUTHORITY REET 03801 C ENUE

FB_321 PG_19

2790



STRUCTURE TABLE				
RIM ELEV.	INV. ELEV. IN INV. ELEV. OUT	PIPE SIZE & TYPE		
		-		
19.04	15.39	12" CPP (4435)		
19.09	15.09 14.19	12" CPP (4436) 24" CPP (4433)		
	14.24	24" CPP (5364)		
10.50		-		
19.59	15.84	12" CPP (4434)		
10.50	15.50	12" CPP (4432)		
19.50	15.35	12" CPP (4433)		
19.48	14.78 14.68	12" CPP (4434) 24" CPP (4560)		
	14.68	24" CPP (4435)		
00.77				
20.33	18.03	12" RCP (4560)		
20.02	15.72 15.32	12" CCP (4561) 18" CPP (3856)		
	14.92	24" CPP (4433)		
01.40				
21.40	17.95	12" CPP (3856)		
21.38	16.58 16.58	12" CPP(3855) 15" CPP(4445)		
	16.58	18" CPP (4560)		
14 75	-	_		
14.35	8.90	10" VCB (AEI4)		
10.69	8.84	10" VCB (AEI3)		
10.09	8.69	10" VCP (AEI5)		
10.77	6.77	12" CPP (NW)		
10.77	6.75± (SILTED)	12" CPP (AEI7)		
8.68	5.88 6.18	12" CPP (AEI6) 8" CPP (SE)		
	5.83	12" CPP (S)		
12.77	9.52	6" PVC (CLEANOUT)		
	9.42	6" CPP (AEI5)		
10.25	8.45 8.55 8.15	4" PVC (BLDG) 6" PVC (AEI2) 10" VCP (AEI4)		
	7.90	10" VCP (SMH 2316)		



AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors 200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114

NOTES: 1) PARCELS ARE SHOWN ON THE CITY OF PORTSMOUTH ASSESSOR'S MAP 116 AS LOT 38 AND LOT 37.

Tel (603) 430-9282

Fax (603) 436-2315

2) OWNERS OF RECORD:

BK 4679, PG 151

116/38 PORTSMOUTH HOUSING AUTHORITY 245 MIDDLE STREET PORTSMOUTH, NH 03801 R.C.R.D BK 1736, PG 386, BK 1797 PG 20 AND BK 1920, PG 47 116/37 ED PAC. LLC 242 CENTRAL AVENUE DOVER, NH 03820

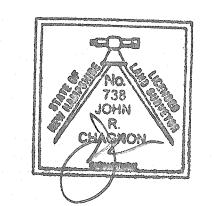
3) PARCEL 116/38 AND 116/37 ARE NOT IN A SPECIAL FLOOD HAZARD AREA AS SHOWN ON FIRM PANEL 3301SC0259E. EFFECTIVE 5/17/2005

4) EXISTING LOT AREA: 11/38: 59,976 (S.F.) 1.3769 ACRES 11/37: 4,587 (S.F.) 0.1053 ACRES

PARCELS ARE LOCATED IN CHARACTER DISTRICT 4 (CD4) 6) THE PURPOSE OF THIS PLAN IS TO SHOW THE EXISTING CONDITIONS ON THE LOTS.

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

ISSUED FOR APPROVAL 6/18/18 3/5/18 ISSUED FOR COMMENT DESCRIPTION DATE REVISIONS



SCALE: 1'=20'

EXISTING CONDITIONS

PLAN

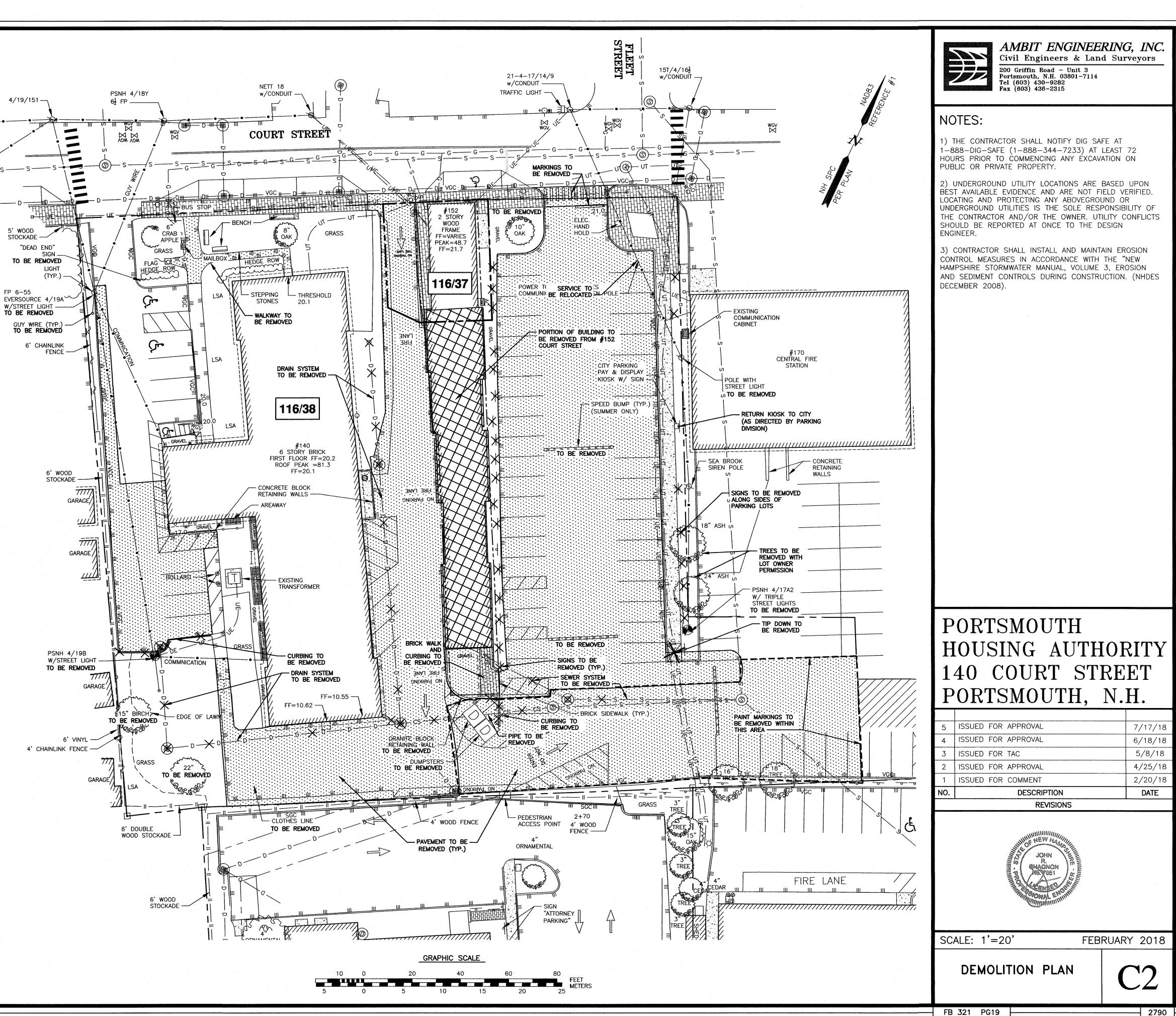
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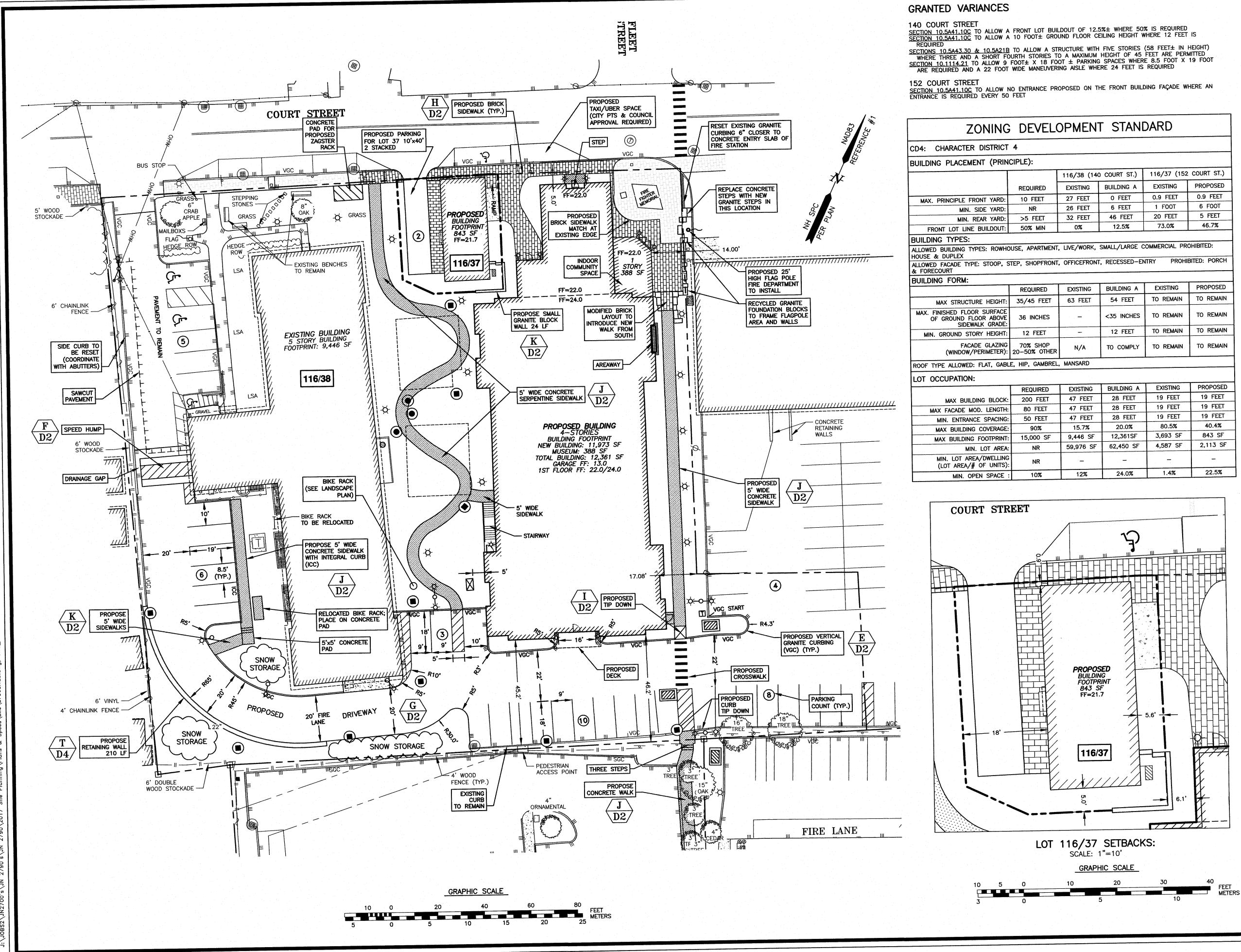
MARCH 2018

FB 321 PG 19

DEMOLITION NOTES

- A) THE LOCATIONS OF UNDERGROUND UTILITIES ARE APPROXIMATE AND THE LOCATIONS ARE NOT GUARANTEED BY THE OWNER OR THE DESIGNER. IT IS THE CONTRACTORS' RESPONSIBILITY TO LOCATE UTILITIES AND ANTICIPATE CONFLICTS. CONTRACTOR SHALL REPAIR EXISTING UTILITIES DAMAGED BY THEIR WORK AND RELOCATE EXISTING UTILITIES THAT ARE REQUIRED TO BE RELOCATED PRIOR TO COMMENCING ANY WORK IN THE IMPACTED AREA OF THE PROJECT.
- B) ALL MATERIALS SCHEDULED TO BE REMOVED SHALL BECOME THE PROPERTY OF THE CONTRACTORS UNLESS OTHERWISE SPECIFIED. THE CONTRACTOR SHALL DISPOSE OF ALL MATERIALS OFF-SITE IN ACCORDANCE WITH ALL FEDERAL, STATE, AND LOCAL REGULATIONS, ORDINANCES AND CODES. THE CONTRACTOR SHALL COORDINATE REMOVAL, RELOCATION, DISPOSAL, OR SALVAGE OF UTILITIES WITH THE OWNER AND APPROPRIATE UTILITY COMPANY.
- C) ANY EXISTING WORK OR PROPERTY DAMAGED OR DISRUPTED BY CONSTRUCTION/ DEMOLITION ACTIVITIES SHALL BE REPLACED OR REPAIRED TO THE ORIGINAL EXISTING CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE OWNER.
- D) THE CONTRACTOR SHALL VERIFY LOCATION OF ALL EXISTING UTILITIES AND CALL DIG SAFE AT LEAST 72 HOURS PRIOR TO THE COMMENCEMENT OF ANY DEMOLITION/CONSTRUCTION ACTIVITIES.
- E) SAWCUT AND REMOVE PAVEMENT ONE FOOT OFF PROPOSED EDGE OF PAVEMENT OR EXISTING CURB LINE IN AREAS WHERE PAVEMENT TO BE REMOVED ABUTS EXISTING PAVEMENT OR CONCRETE TO REMAIN.
- F) IT IS THE CONTRACTOR'S RESPONSIBILITY TO FAMILIARIZE THEMSELVES WITH THE CONDITIONS OF ALL THE PERMIT APPROVALS.
- G) THE CONTRACTOR SHALL OBTAIN AND PAY FOR ADDITIONAL CONSTRUCTION PERMITS, NOTICES AND FEES NECESSARY TO COMPLETE THE WORK AND ARRANGE FOR AND PAY FOR ANY INSPECTIONS AND APPROVALS FROM THE AUTHORITIES HAVING JURISDICTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY ADDITIONAL AND OFF-SITE DISPOSAL OF MATERIALS REQUIRED TO COMPLETE THE WORK.
- H) THE CONTRACTOR SHALL REMOVE AND DISPOSE OF ALL EXISTING STRUCTURES, CONCRETE, UTILITIES, VEGETATION, PAVEMENT, AND CONTAMINATED SOIL WITHIN THE WORK LIMITS SHOWN UNLESS SPECIFICALLY IDENTIFIED TO REMAIN. ANY EXISTING DOMESTIC , IRRIGATION SERVICE WELLS IN THE PROJECT AREA IDENTIFIED DURING THE CONSTRUCTION AND NOT CALLED OUT ON THE PLANS SHALL BE BROUGHT TO THE ATTENTION OF THE OWNER AND ENGINEER FOR PROPER CAPPING / RE-USE. ANY EXISTING MONITORING WELLS IN THE PROJECT AREA IDENTIFIED DURING THE CONSTRUCTION AND NOT CALLED OUT ON THE PLANS SHALL BE BROUGHT TO THE ATTENTION OF THE OWNER AND ENGINEER TO COORDINATE MONITORING WELL REMOVAL AND/OR RELOCATION WITH NHDES AND OTHER AUTHORITY WITH JURISDICTION PRIOR TO CONSTRUCTION.
- I) ALL WORK WITHIN THE CITY OF PORTSMOUTH RIGHT OF WAY SHALL BE COORDINATED WITH THE CITY OF PORTSMOUTH DEPARTMENT OF PUBLIC WORKS (DPW).
- J) REMOVE TREES AND BRUSH AS REQUIRED FOR COMPLETION OF WORK. CONTRACTOR SHALL GRUB AND REMOVE ALL SLUMPS WITHIN LIMITS OF WORK AND DISPOSE OF OFF-SITE IN ACCORDANCE WITH FEDERAL, STATE, AND LOCAL LAWS AND REGULATIONS.
- K) CONTRACTOR SHALL PROTECT ALL PROPERTY MONUMENTATION THROUGHOUT DEMOLITION AND CONSTRUCTION OPERATIONS. SHOULD ANY MONUMENTATION BE DISTURBED, THE CONTRACTOR SHALL EMPLOY A NH LICENSED LAND SURVEYOR TO REPLACE THEM.
- L) PROVIDE INLET PROTECTION BARRIERS AT ALL CATCH BASINS WITHIN CONSTRUCTION LIMITS AND MAINTAIN FOR THE DURATION OF THE PROJECT. INLET PROTECTION BARRIERS SHALL BE HIGH FLOW SILT SACK BY ACF ENVIRONMENTAL OR APPROVED EQUAL. INSPECT BARRIERS WEEKLY AND AFTER EACH RAIN OF 0.25 INCHES OR GREATER. CONTRACTOR SHALL COMPLETE A MAINTENANCE INSPECTION REPORT AFTER EACH INSPECTION. SEDIMENT DEPOSITS SHALL BE REMOVED AFTER EACH STORM EVENT OR MORE OFTEN IF WARRANTED OR FABRIC BECOMES CLOGGED. EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF ANY CLEARING OR DEMOLITION ACTIVITIES.
- M) THE CONTRACTOR SHALL PAY ALL COSTS NECESSARY FOR TEMPORARY PARTITIONING, BARRICADING, FENCING, SECURITY AND SAFELY DEVICES REQUIRED FOR THE MAINTENANCE OF A CLEAN AND SAFE CONSTRUCTION SITE.
- N) ANY CONTAMINATED MATERIAL REMOVED DURING THE COURSE OF THE WORK WILL REQUIRE HANDLING IN ACCORDANCE WITH NHDES REGULATIONS. CONTRACTOR SHALL HAVE A HEALTH AND SAFETY PLAN IN PLACE, AND COMPLY WITH ALL APPLICABLE PERMITS, APPROVALS, AUTHORIZATIONS, AND REGULATIONS





OT OCCUPATION:				1	
	REQUIRED	EXISTING	BUILDING A	EXISTING	PROPOSED
MAX BUILDING BLOCK:	200 FEET	47 FEET	28 FEET	19 FEET	19 FEET
MAX FACADE MOD. LENGTH:	80 FEET	47 FEET	28 FEET	19 FEET	19 FEET
MIN. ENTRANCE SPACING:	50 FEET	47 FEET	28 FEET	19 FEET	19 FEET
MAX BUILDING COVERAGE:	90%	15.7%	20.0%	80.5%	40.4%
MAX BUILDING FOOTPRINT:	15,000 SF	9,446 SF	12,361SF	3,693 SF	843 SF
MIN. LOT AREA:	NR	59,976 SF	62,450 SF	4,587 SF	2,113 SF
MIN. LOT AREA/DWELLING (LOT AREA/# OF UNITS):	NR	—	—	-	-
MIN. OPEN SPACE :	10%	12%	24.0%	1.4%	22.5%

STANDARD				
OURT ST.)	116/37 (152	2 COURT ST.)		
UILDING A	EXISTING	PROPOSED		
0 FEET	0.9 FEET	0.9 FEET		
6 FEET	1 FOOT	6 FOOT		
46 FEET	20 FEET	5 FEET		
12.5%	73.0%	46.7%		

BUILDING A	EXISTING	PROPOSED
54 FEET	TO REMAIN	TO REMAIN
<35 INCHES	to remain	TO REMAIN
12 FEET	to remain	TO REMAIN
TO COMPLY	to remain	TO REMAIN



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NOTES: 1) PARCELS ARE SHOWN ON THE CITY OF PORTSMOUTH ASSESSOR'S MAP 116 AS LOT 38 AND LOT 37.

2) OWNERS OF RECORD:

116/38 PORTSMOUTH HOUSING AUTHORITY 245 MIDDLE STREET

> PORTSMOUTH, NH 03801 R.C.R.D BK 1736, PG 386, BK 1797 PG 20 AND BK 1920, PG 47

116/37

- ED PAC, LLC 242 CENTRAL AVENUE
- DOVER, NH 03820 BK 4679, PG 151

3) PARCELS 116/38 AND 116/37 ARE NOT IN A SPECIAL FLOOD HAZARD AREA AS SHOWN ON FIRM PANEL 3301SC0259E. EFFECTIVE 5/17/2005

4) LOT AREAS: <u>LOT 11/38</u> EXISTING: 59,976 (S.F.) 1.3769 ACRES PROPOSED: 62,450 (S.F.) 1.4337 ACRES

> LOT 11/37 EXISTING: 4,587 (S.F.) 0.1053 ACRES PROPOSED: 2,113 (S.F.) 0.0485 ACRES

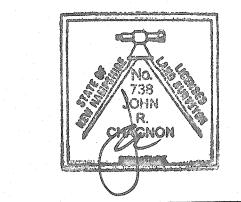
5) PARCELS ARE LOCATED IN CHARACTER DISTRICT 4 (CD4)

- 6) THE PURPOSE OF THIS PLAN IS TO SHOW THE SITE LAYOUT FOR THE PROJECT.
- 7) SEE BASEMENT PLAN (C4) FOR TRASH ENCLOSURE AREA. PICK UP SCHEDULE WILL BE AS NEEDED TO MAINTAIN CAPACITY.

8) SITE ELEMENTS SHOWN IN FRONT (NORTH) OF 140 COURT (EXISTING APARMENT BUILDING) TO REMAIN.

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

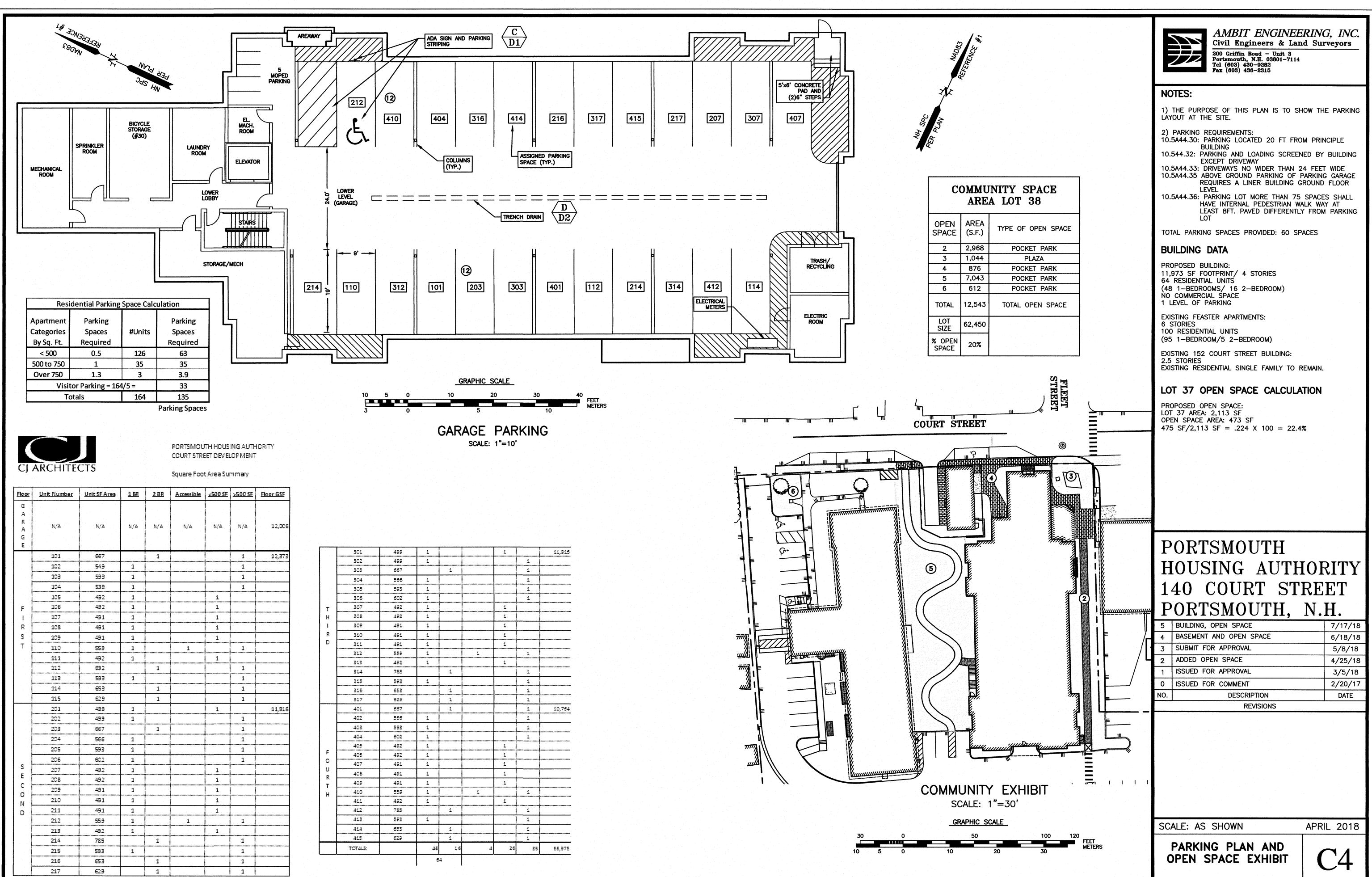
4	116/37 LOT LINE & PARKING, ZAGSTER	7/17/18	
3	PARKING SPACE NOTE, RADIUS, NOTE 8	7/3/18	
2	ISSUED FOR APPROVAL	6/18/18	
1	ISSUED FOR COMMENT	5/8/18	
0	ISSUED FOR COMMENT	4/25/18	
NO.	DESCRIPTION	DATE	
REVISIONS			



APRIL 2018 SCALE: 1'=20' SITE LAYOUT C3 PLAN

FB 321 PG19

2790



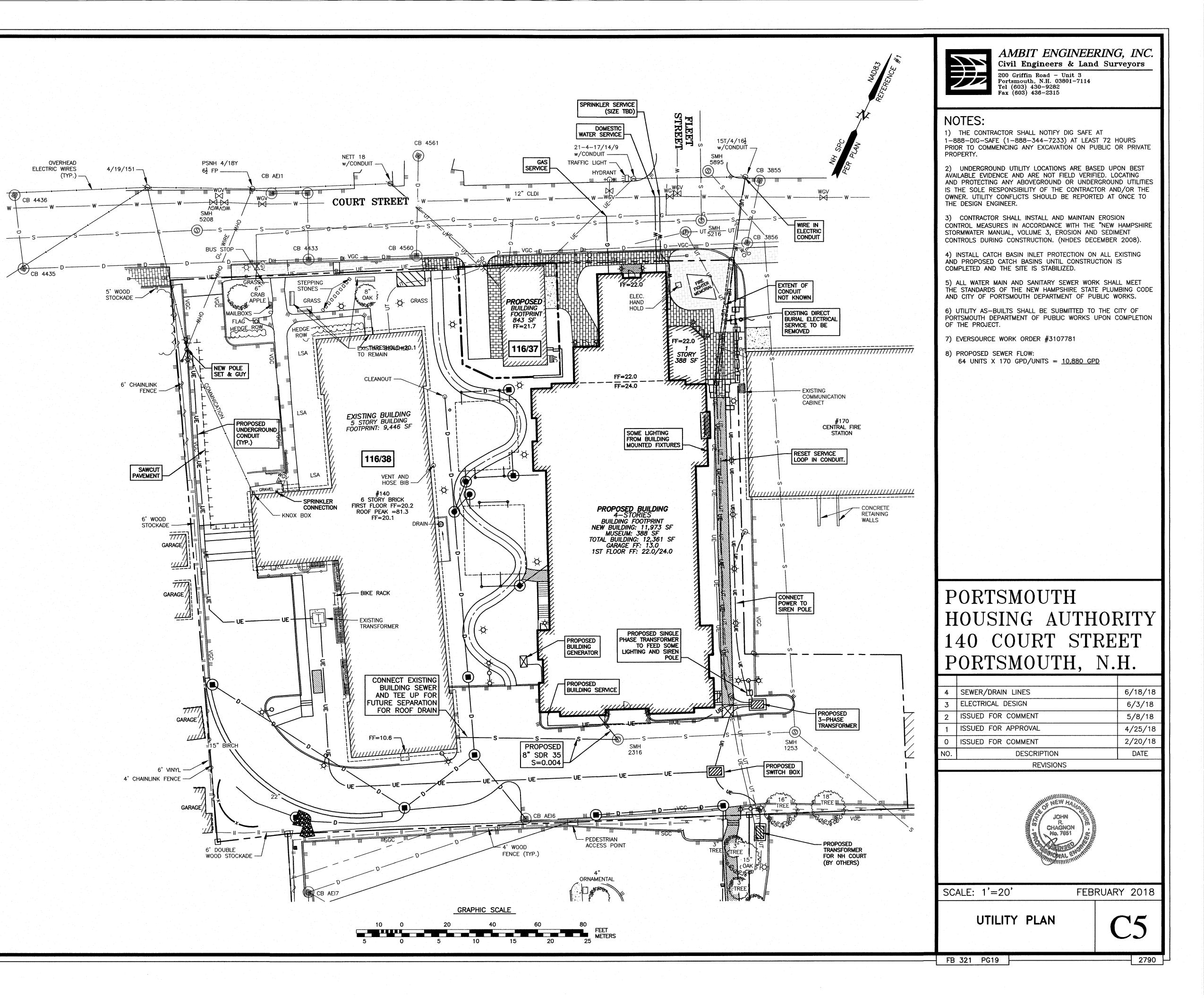
FB 321 PG19

2790

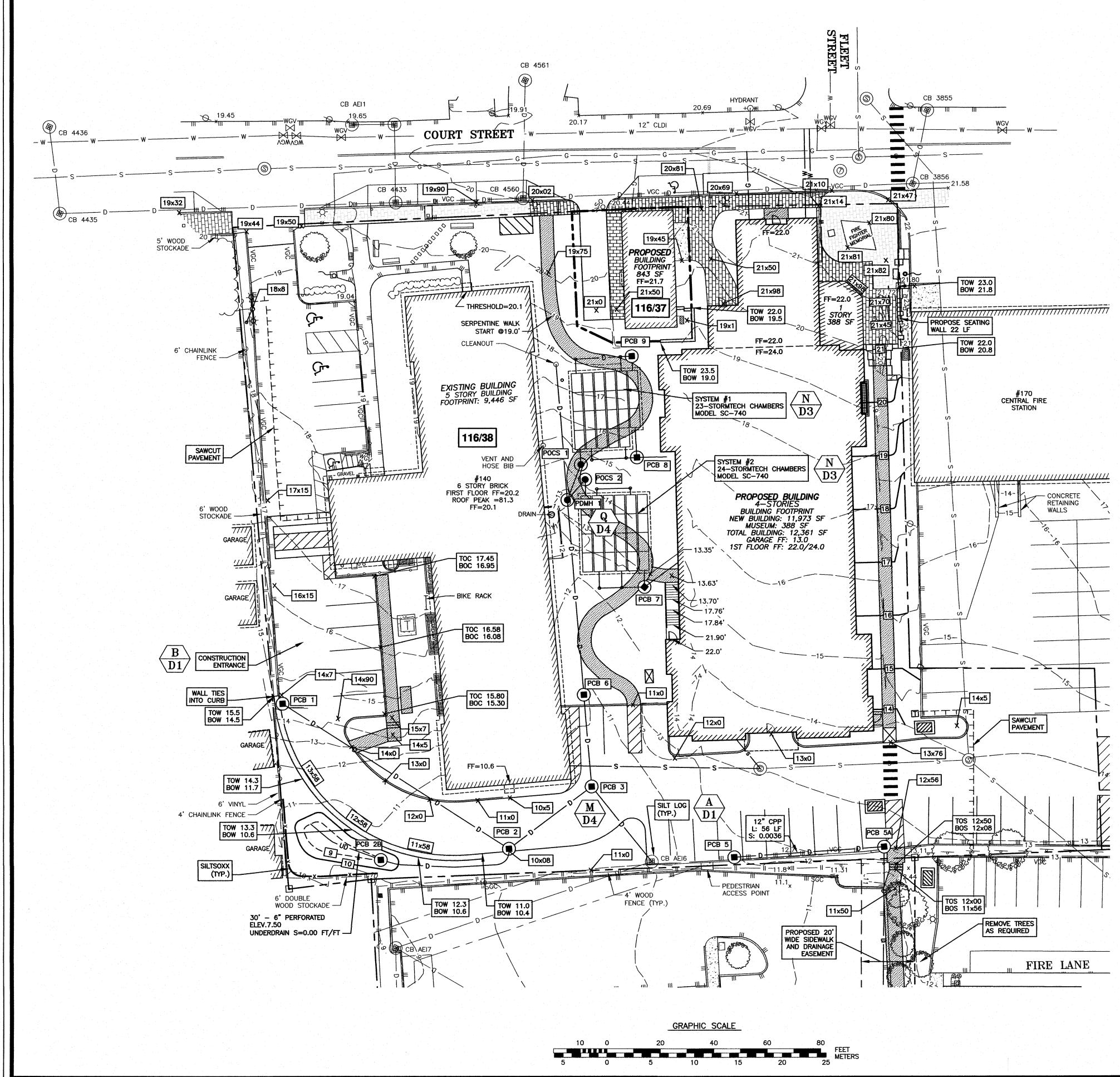
UTILITY NOTES:

- 1) SEE EXISTING CONDITIONS PLAN FOR BENCHMARK INFORMATION.
- 2) COORDINATE ALL UTILITY WORK WITH APPROPRIATE UTILITY.
- 3) SEE GRADING AND DRAINAGE PLAN FOR PROPOSED GRADING AND EROSION CONTROL MEASURES.
- 4) ALL WATER MAIN INSTALLATIONS SHALL BE CLASS 52, POLYWRAPPED, CEMENT LINED DUCTILE IRON PIPE.
- 5) ALL WATERMAIN INSTALLATIONS SHALL BE PRESSURE TESTED AND CHLORINATED AFTER CONSTRUCTION AND BEFORE ACTIVATING THE SYSTEM. CONTRACTOR SHALL COORDINATE WITH THE CITY OF PORTSMOUTH.
- 6) ALL SEWER PIPE SHALL BE PVC SDR 35 UNLESS OTHERWISE STATED.
- 7) ALL WORK WITHIN CITY R.O.W. SHALL BE COORDINATED WITH CITY OF PORTSMOUTH
- 8) CONTRACTOR SHALL MAINTAIN UTILITY SERVICES TO ABUTTING PROPERTIES THROUGHOUT CONSTRUCTION.
- 9) ANY CONNECTION TO EXISTING WATERMAIN SHALL BE CONSTRUCTED BY THE CITY OF PORTSMOUTH.
- 10) EXISTING UTILITIES TO BE REMOVED SHALL BE CAPPED AT THE MAIN AND MEET THE DEPARTMENT OF PUBLIC WORKS STANDARDS FOR CAPPING OF WATER AND SEWER SERVICES.
- 11) ALL ELECTRICAL MATERIAL WORKMANSHIP SHALL CONFORM TO THE NATIONAL ELECTRIC CODE, LATEST EDITION, AND ALL APPLICABLE STATE AND LOCAL CODES.
- 12) THE EXACT LOCATION OF NEW UTILITY SERVICES AND CONNECTIONS SHALL BE COORDINATED WITH BUILDING DRAWINGS AND UTILITY COMPANIES.
- 13) ADJUST ALL MANHOLES, CATCH BASINS, CURB BOXES, ETC. WITHIN LIMITS OF WORK TO FINISH GRADE.
- 14) ALL UNDERGROUND CONDUITS SHALL HAVE NYLON PULL ROPES TO FACILITATE PULLING CABLES.
- 15) THE CONTRACTOR SHALL OBTAIN, PAY FOR, AND COMPLY WITH ALL REQUIRED PERMITS, ARRANGE FOR ALL INSPECTIONS, AND SUBMIT COPIES OF ACCEPTANCE CERTIFICATED TO THE OWNER PRIOR TO THE COMPLETION OF PROJECT.
- 16) THE CONTRACTOR SHALL PROVIDE AND INSTALL ALL MANHOLES, BOXES, FITTINGS, CONNECTORS, COVER PLATES AND OTHER MISCELLANEOUS ITEMS NOT NECESSARILY DETAILED IN THESE DRAWING TO RENDER INSTALLATION OF UTILITIES COMPLETE AND OPERATIONAL.
- 17) CONTRACTOR SHALL PROVIDE EXCAVATION, BEDDING, BACKFILL AND COMPACTION FOR NATURAL GAS SERVICES.
- 18) A 10-FOOT MINIMUM EDGE TO EDGE HORIZONTAL SEPARATION SHALL BE PROVIDED BETWEEN ALL WATER AND SANITARY SEWER LINES. AN 18-INCH MINIMUM OUTSIDE TO OUTSIDE VERTICAL SEPARATION SHALL BE PROVIDED AT ALL WATER/SANITARY SEWER CROSSINGS WATER ABOVE SEWER.
- 19) SAWCUT AND REMOVE PAVEMENT AND CONSTRUCT PAVEMENT TRENCH PATCH FOR ALL PROPOSED UTILITIES LOCATED IN EXISTING PAVEMENT AREAS TO REMAIN.
- 20) GATE VALVES, FITTINGS, ETC. SHALL MEET THE REQUIREMENTS OF THE CITY OF PORTSMOUTH.
- 21) COORDINATE TESTING OF SEWER CONSTRUCTION WITH THE CITY OF PORTSMOUTH.
- 22) ALL SEWER PIPES WITH LESS THAN 6' COVER SHALL BE INSULATED.
- 23) CONTRACTOR SHALL COORDINATE ALL ELECTRIC WORK INCLUDING BUT NOT LIMITED TO: CONDUIT CONSTRUCTION, MANHOLE CONSTRUCTION, UTILITY POLE CONSTRUCTION, OVERHEAD WIRE RELOCATION, AND TRANSFORMER CONSTRUCTION WITH POWER COMPANY.
- 24) CONTRACTOR SHALL PHASE UTILITY CONSTRUCTION, PARTICULARLY WATER MAIN AND GAS MAIN CONSTRUCTION AS TO MAINTAIN CONTINUOUS SERVICE TO ABUTTING PROPERTIES. CONTRACTOR SHALL COORDINATE TEMPORARY SERVICES TO ABUTTERS WITH UTILITY COMPANY AND AFFECTED ABUTTER.
- 25) SITE LIGHTING SPECIFICATIONS, CONDUIT LAYOUT AND CIRCUITRY FOR PROPOSED SITE LIGHTING AND SIGN ILLUMINATION SHALL BE PROVIDED BY THE PROJECT ELECTRICAL ENGINEER IN COORDINATION WITH THE SITE CIVIL ENGINEER.
- 26) CONTRACTOR SHALL CONSTRUCT ALL UTILITIES AND DRAINS TO WITHIN 10' OF THE FOUNDATION WALLS AND CONNECT THESE TO SERVICE STUBS FROM THE BUILDING.
- 27) THE CONTRACTOR SHALL INSTALL THE SEWER LINE AND MANHOLE IN CONSULTATION AND COORDINATION WITH DEPARTMENT OF PUBLIC WORKS.

PROPOSED SEWER CONNECTION				
STRUCTURE RIM		INV. ELEV. IN	PIPE SIZE & TYPE	
SIRUCIORE	ELEV.	INV. ELEV. OUT	(FROM/TO)	
SMH 2316 (EXISTING)	12.75	7.40 7.40	8" SDR35 (BLDG) 10" SDR35 (PSMH 1)	
		7.30	10" VCP (1253)	
BUILDING			-	
DOILDING		7.45	8" SDR35 (2316)	



is2\JN2700's\JN 2790's\JN 2790\2017 Site Planning\Plans & Specs\Site\2790SITE3.dwg,



PROPOSED STORM DRAIN TABLE

PCB 1 RIM EL. 14.7 INV. OUT 9.70 PCB 1 - PCB 2 12" HDPE (SMOOTH) L = 95', S = 0.0271 ft./ft.PCB 2 RIM EL. 10.00 INV. IN 7.13 INV. IN 7.13 (6" UD) INV. OUT 7.03 PCB 2 - PCB 3 12" HDPE (SMOOTH) L = 34', S = 0.0041 ft./ftPCB 2B (BEE-HIVE GRATE) RIM EL. 9.50

INV. IN 7.50 OUT 7.39 PCB 2B - PCB 2 6" UNDERDRAIN L = 53', S = 0.005 ft./ft.

PCB 3 RIM EL.10.4 INV. IN 6.89 INV. IN 6.89 INV. OUT 6.89

CB AEI6 EXIST. RIM EL. 10.77 INV. IN 6.77 (NEW) INV. OUT 6.77

PCB 3 - CB 4 12" HDPE (SMOOTH) L = 31', S = 0.0039 ft./ft.

PCB 5 RIM EL. 12.39 INV. OUT 8.06 PCB 5-PCB 5A

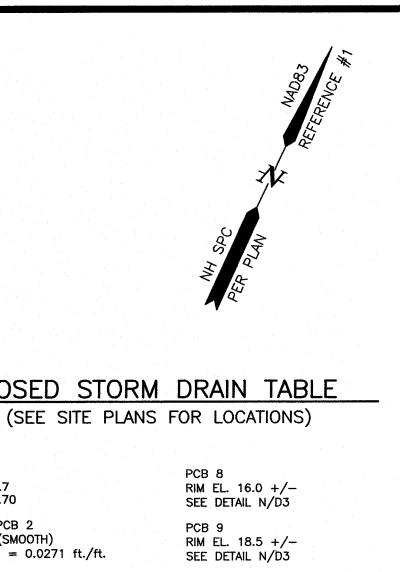
12" CPP L=56', S=0.0036 ft./ft.

PCB 5A RIM EL. 12.50 INV. IN 7.86 INV. OUT 7.76

PCB 5A-PCB 5B 12" CPP L=180', S=0.0039 ft./ft.

PCB 6 RIM EL. 11.6 INV. IN 7.04 INV. OUT 7.04

PCB 7 RIM EL. 13.0 +/-SEE DETAIL N/D3



PDMH 1 RIM EL. 13.0 +/-INV. IN 7.38 INV. IN 7.38 INV. OUT 7.38 POCS 1 RIM EL. 15.0 +/-INV. OUT 11.40

SEE DETAIL N/D3 POCS 2 RIM EL. 14.0 +/-INV. OUT 7.40 SEE DETAIL N/D3

POCS 1 - PDMH 1 12" HDPE (SMOOTH) $L = 14^{\circ}$, S = 0.005 ft./ft.

POCS 2 - PDMH 1 12" HDPE (SMOOTH) L = 5', S = 0.004 ft./ft.

PDMH 1 - PCB 6 12" HDPE (SMOOTH) L = 68', S = 0.005 ft./ft.

PCB 6 - PCB 3 12" HDPE (SMOOTH) L = 30', S = 0.005 ft./ft.



AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors

200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114 Tel (603) 430-9282 Fax (603) 436-2315

NOTES:

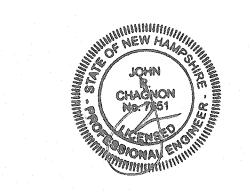
1) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.

2) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.

3) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL, VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008).

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

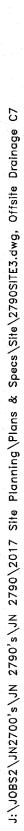
3	ISSUED FOR APPROVAL	7/17/18				
2	ADDED DESIGN	6/18/18				
1	ISSUED FOR APPROVAL	4/25/18				
0	ISSUED FOR COMMENT	2/20/18				
NO.	DESCRIPTION	DATE				
	REVISIONS					

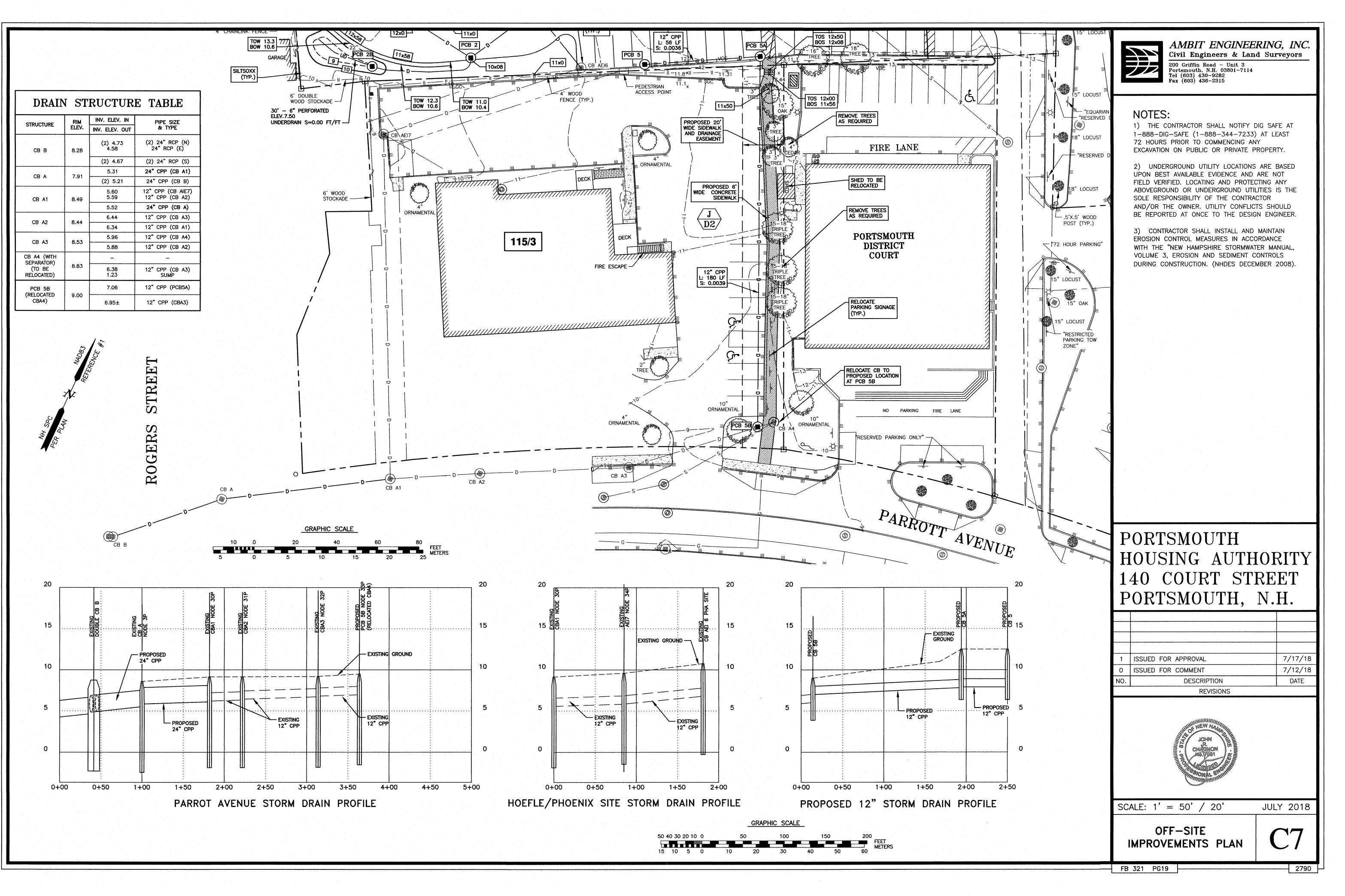


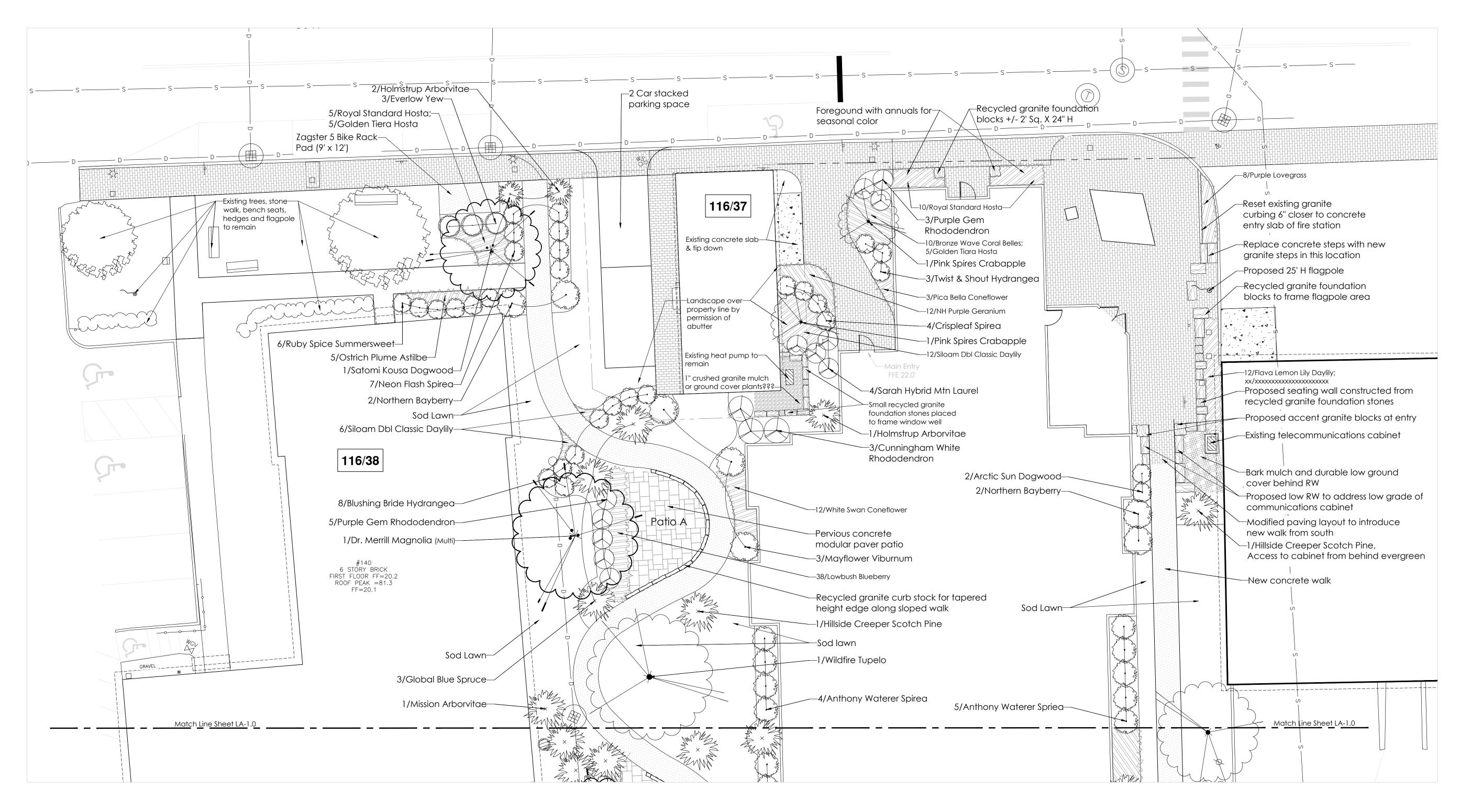
SCALE: 1'=20' FEBRUARY 2018 DRAINAGE, GRADING AND EROSION CONTROL C6PLAN

2790

FB 321 PG19







gg2+1 LLC Landscape Architecture Site Planning Graphics

> 70 New Road Salisbury, NH 03268 tel/fax: 603.648.6434 web: www.g2plus1.com

Project Name:

Workforce Housing Development 140 Court Street Portsmouth, New Hampshire 03801

Applicant/Owner of Record:

Portsmouth Housing Authority 245 Middle Street

Portsmouth, NH 03801

Ed Pac, LLC 242 Central Avenue Dover, NH 03820

For City Approval

registration:

revisions:

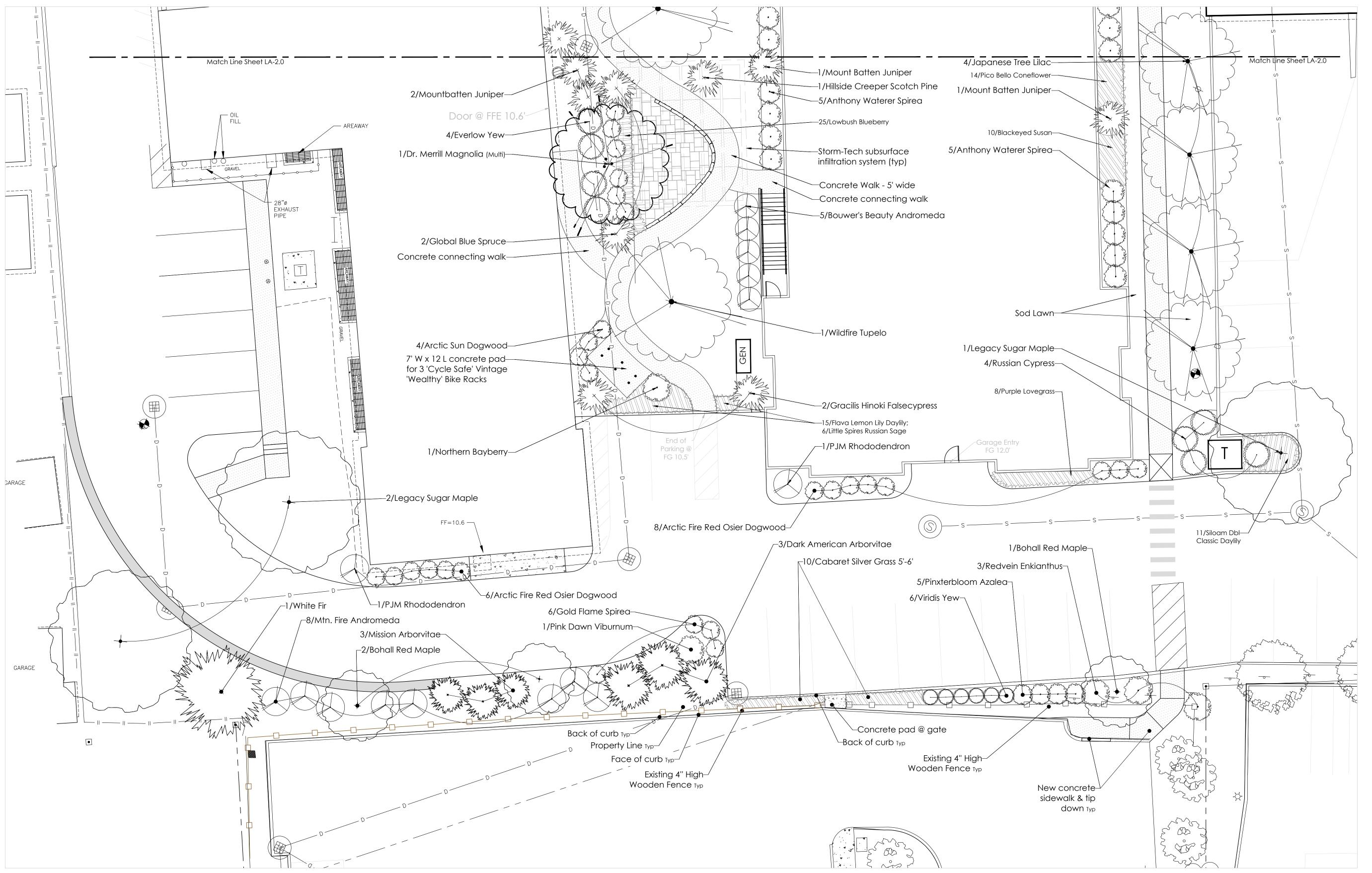
no.	date	issued
1	7/17/18	Revised per TAC hearing & project
2		coordination
3		
4		
5		
6		
7		
8		
9		

project number:	1306.0
scale:	1'' = 10'
drawn by:	dhg
date:	6/18/2018

sheet title/number:

Landscape Plan







70 New Road Salisbury, NH 03268 tel/fax: 603.648.6434 web: www.g2plus1.com

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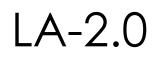
registration:

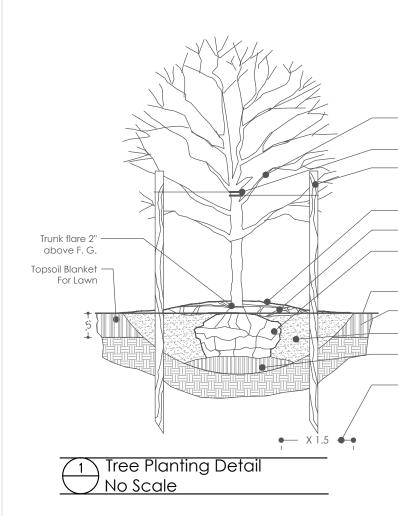
revisions:							
no.	date	issued					
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project number:	1306.0
scale:	1'' = 10'
drawn by:	dhg
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sheet title/number:

Landscape Plan





NOTE: For all trees the trunk flare and top of rootball shall be 2" above established finish grade of planting bed or individual planting hole.

Prune out dead/damaged branches Preserve normal plant shape and form with pruning. Use adjustable tree ties for anchoring tree to stakes Stake with three 2" x 2" wooden stakes placed @120°. Drive stakes in at an angle and bring to plumb when securing tree ties. Do not pierce rootball.

Form earth saucer a minimum of 2" deep x 3'-0" diameter. - 3" depth pine bark mulch and do not place within 2" of trunk.

Remove burlap & rope from top of rootball with tree placed at proper grade. Cut & remove wire basket. No plants with synthetic burlap or with loose/broken rootballs will be accepted.

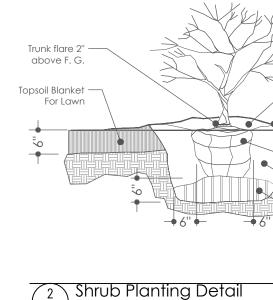
Finish grade of lawn or planting bed. Topsoil blanket for adjoining lawn.

Planting soil mix as specified.

Set rootball on 9" tamped mound of planting mix. Scarify sides of plant pit. Compact to 92% density. - Form planting pit width @ 1.5 times the ball diameter to each side or a minimum of 2' minimum width on

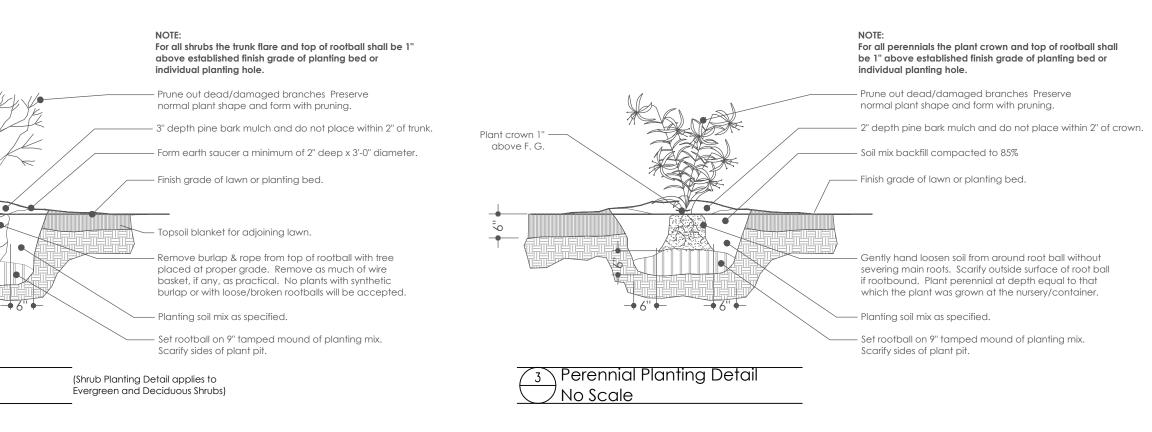
each side. Construct in a 'saucer' shape as shown.

Tree Planting Detail applies to Evergreen and Deciduous Trees. Evergreen trees shall not be staked. Tamp backfill soil around rootball firmly to minimize rootball shift. Tree to be set plumb, after settlement. All nursery tags, tape, and similar materials shall be removed.



Typical Planting Details

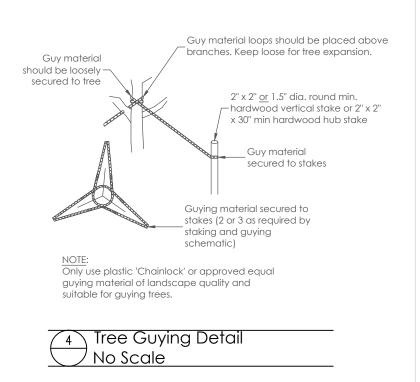
							NEFS 7 Neon Flash Spirea	Spirea japonica 'neon flash'	1 2'	3' 3 gal.	CTN Compact facer
Plan	it Schedule					6/18/2018	BAY 5 Northern Bayberry	Myrica pensylvanica	4 3' 2 6-8'	6-8' 3'-3-1/2' ht.	B&B shade tolerant aromatic, Withstands poor soils
									2 00	0-0 J -J-1/2 III.	
	Street Landscape					REV: 7/17/18	Decorative Grasses				
Portsmout	h, New Hampshire							-			
				Habit of Growth			DCGR-4 16 Purple Lovegrass	Eragrostis spectabilis	4 18-24"		2 gal. 18"-24", S, Aug/Oct, bronze-red seed heads
Sym C	Qty Common Name	Botanical Name	Zone	Height Spread		Notes	DCGR-9 10 Cabaret Silver Grass	Miscanthus sinensis 'cabaret'	4 5-6'	36" 2 gal	CTN 5-6', S, Aug/Oct, wide white/greenstripped foliage, White plumes
	Deciduous Trees										
LSM	3 Legacy Sugar Maple	Acer saccharinum 'legacy'	2	50-60' 35-40	' 2-1/2-3" cal. B&B	hardy, vigorous	Perennials/Seasonal Color				
	4 Bowhall Columnar Maple	Acer rubrum 'bowhall'		40-50' 10-15		Columnar form	S - Sun; S/Sh - Sun/Shade; S/PSh - Sun and Part Shad	de; PSh - Part Shade; PSh/Sh - Part Shade/Shade			
TUP	2 Wildfire Tupelo	Nyssa sylvatica 'wildfire'		30-40' 20-30		Brilliant red leaves in sprint to glossy green, pyramidal	Sym Qty Common Name	Botanical Name	Zone Height	f Growth Spread Type	Features Size Ht., Exposure, Bloom Period, Color
						5	GC.A-3 27 Daylily	Hemerocallis flava - 'Lemon Lily'	Zone neight	1 yr. potted	2 qt 36", S/PSh, June/July, Lemon Yellow
Small	Accent Flowering Trees						GC.A-9 28 Daylily	Hemerocallis flava 'Siloam Dbl. Classic'		1 yr. potted	2 qt 18". S/PSh. June. Double Soft Salmon Pink
T			_	20 251 25 20			GC.C-1 17 Purple Coneflower	Echinacea purpurea 'Pica bella'		1 yr. potted	2 qt 24"-29",S/PSh, July/Sept, Deep Pink
DMM	2 Dr. Merrill Magnolia - MULTI	Magnolia loebneri 'merrill'		20-25' 25-30 20-30' 15-25		Large 3-4" flowers before leaves, Specimen	GC.C-3 12 White Coneflower	Echinacea purpurea 'White Swan'		1 yr. potted	2 qt 18"-24",S/PSh, June/Sept, White
JTL PSC	4 Japanese Tree Lilac2 Pink Spires Crabapple	Syringa reticulata Malus 'pink spires'		20-30 15-25 20-25' 12-15		tough, full sun	GC.D-1 4 Little Spire Russian Sage	Perovskia atriplicifolia 'little spire'	4	1 yr. potted	2 qt 18"-24", S, July/Sept, Medium Violet
KD	1 Satomi Kousa Dogwood	Cornus kousa 'satomi'		15-20' 10-15		Reddish purple fall foliage, exfoliating bark	GC.G-2 10 Coral Belles	Heuchera 'Bronze Wave'	4	1 yr. potted	1 gal. 18", S/PSh, Sept/Oct, Bronze-Purple foliage, tan flowers
				15 20 10-15			GC.H-5 15 Hosta	Hosta 'Royal Standard'		1 yr. potted	1 gal. 24-28", S/Sh, Aug/Sept, White flower, Rich Grn leaf
Even v	an Trace O Assert From						GC.H-7 10 Hosta	Hosta 'golden tiara'	3	1 yr. potted	1 gal. 10", S/PSh, July/Aug, dark purple
_	een Trees & Accent Ever			-			GC.I 63 Lowbush Blueberry	Vaccinium angustifolium		1 yr. potted	2 qt 12", S, May, Violet-Blue
CNCF	1 White Fir	Abies concolor		30-50' 15-20		Soft blue green foliage	GC.L-3 5 Astilbe	Astilbe 'ostrich plume'		1 yr. potted	2 qt 24-30", PSh/Sh, June, Dark Foliage w/ Salmon Pink
DRK	3 Dark American Arborvitae	Thuja occidentalis 'nigra'		10-30' 10-12	······································	columnar, wide base, shade tolerant	GC.X-3 12 Bloody Cransbill	Geranium sanguineum 'NH Purple'		1 yr. potted	2 qt 9"-12", S/PSh, May/Sept, Magenta Pink
GHFC	2 Gracilis Hinoki Falsecypress	Chamaecyparis obtusa 'gracilis'		15-20' 6-8'		- · · ·	GC.ZZ 10 Black Eyed Susan	Rudbeckia fulgida 'Goldsturm'		1 yr. potted	1 gal. 24-36", S/Psh, Jul/Aug, golden yellow-black center
MSA	5 Mission Arborvitae	Thuja occidentalis 'techney'	3 4		6'-7' ht. B&B 6' ht. B&B						
MTB VRY	4 Mountbatten Juniper6 Viridis Yew	Juniperus chinensis 'mountbatten' Taxus media 'viridis'		15' 6' 10-15' 12-24'			0 SF Seasonal Annual Beds	Mixed selection by Landscape Maintenar	nce Contracto	or, Directed by Owner	
HLMS	2 Holmstrup Arborvitae	Thuja occidentalis 'holmstrup'	4			Very upright narrow form, great vertical accent columnar, shade tolerant	. /a				
TILIVIS			2	10 5-4	5-4 III. DQD		Lawns/Seeding				
	vergreen Ground Cover		-				0 SF Soded Fine Lawn	Fine Grade, fertilize, seed and Hydromulch (Kentu	ucky Bluegrass	and Creeping Red Fescue B	end)
					1011 2411 1 000						
ELY	4 Ever-Low Yew3 Hillside Creeper Scotch Pine	Taxus media 'ever-low'	4			Hardy, shade tolerant	Notes:				
HSCP RSCP	4 Russian Cypress	Pinus sylvestris 'hillside creeper' Microbiata decussata	2			Sun and shade, arborvitae like foliage	1.) All planting beds shall be mulched with	a minimum of 3" of shredded pine bark mulch			
	5 Global Blue Spruce	Picea pungens 'glauca globosa'	2			Compact, flat topped rounded form	2.) All sod and/or seeded lawn areas to have	ve minimum 6" topsoil blanket.			
	3 Ever-Low Yew	Taxus media 'ever-low'			18"-24" spd. B&B		3.) All native grass seeded areas to have m	ninimum 4" topsoil blanket.			
				1.5 4 0	10 21 5pa. Dab			AAN, American Standard for Nursery Stock, AN		6.	
Accent	t/Flowering Evergreen Sh	rube						rs around building shall receive a minimum 18	jii		
Accent			_					the very sandy/granular sub-grade material			
BBA	5 Brouwer's Beauty Andromeda	Pieris 'brouwer's beauty'	5		2'-3' ht. B&B		expected on this site. Topsoil shall me	et requirements as called out in specifications			
CNW MFA	3 Cunningham White Rhododendror8 Mountain Fire Andromeda	n Rhododendron cat. 'cunningham white' Pieris japonica 'mountain fire'	4			shade, hardy Upright form, Pendulous white flowers					
	4 Sarah Hybrid Mountain Laurel	Kalmia latifolia 'sarah'		9-12' 6-8' 3-1/2' 3-1/2'		Small Accent					
PJM	2 PJM Rhododendron	Rhododendron 'PJM'	4			full sun, hardy					
	8 Purple Gem Rhododendron	Rhododendron 'Purple gem'	4			full sun, hardy, low					
Decidu	ous Flowering Shrubs										
	8 Blushing Bride Hydrangea	Hudrangaa 'bluching bride'	4	3-4' 3-4'		Dentiel electre William file					
FLH-2 FLH-5	3 Twist & Shout Hydrangea	Hydrangea 'blushing bride' Hydrangea 'twist & shout'	4			Partial shade, White flowers continuous bloom to fall Partial shade, Lace cap multi color, continuous bloom to fall					
GFS	4 Gold Flame Spirea	Spirea x bumalda 'gold flame'	44			New foliage mottled with red/copper/orange					
	10 Crispleaf Spirea	Spirea x bulmalda 'crispa'	4			Compact facer, Serrated & twisted foliage					
MFV	3 Mayflower Viburnum	Viburnum carlesi	4			shade tolerant, wetland					
RVE	3 Redvein Enkianthus	Enkianthus campanulatus				partial shade					
	19 Anthony Waterer Spirea	Spirea	3			Reddish purple new foliage, pink flowers					
PNKV	1 Pink Dawn Viburnum	Viburnum bodnantense 'pink dawn'	3		4'-5' ht. B&B						
	14 Arctic Fire Red Osier Dogwood	Cornus sericea 'arctic fire'	3			Sun/Shade, Bright red stems for winter interest					
PXA	4 Pinxterbloom Azalea	Azalea periclymenoides (nudiflorum)	3	5-6' 4-5'		Spring blooming densely branched, dry sandy soil					
ARSD	6 Arctic Sun Dogwood	Cornus sanguinea 'arctic sun'	4		4'-5' ht. B&B	Brilliant yellow stems					
RSSMS	6 Ruby Spice Summersweet	Clethra alnifolia 'ruby spice'	3	4-5' 4-5'	5 gal. CTN	Fragrant and compact, dense plant					



Planting Notes

- 2. This project shall comply with the City of Portsmouth, NH Construction Standards and Details.
- protect the site from erosion
- 4. Erosion Control shall be in place prior to construction.
- plan shall govern.
- All new plant material shall conform to the minimum guidelines established for nursery stock published by the American Association of Nurserymen, Inc. In addition all new plant material for the project shall be of specimen quality. 6.
- 7. All new plants to be balled and burlapped or container grown, unless otherwise noted on the plant list. All plants shall be legibly tagged with the proper botanical name.
- 9. Any proposed substitutions of plant species shall be made with plants of equivalent overall form, height, branching habit, flower leat, color, truit and culture, and only after written approval of the Landscape Architect.
- 10. Contractor shall locate and verify all existing utility lines prior to planting and shall report any conflicts to the Landscape Architect.
- 12. New shrubs and ground cover shall bear the same relationship to grade as it bore to previous grade at nursery. Trees shall be set 2" higher than previous grade. No tress shall be planted before ačceptancė of rough grading.
- 13. Planting Soil Mix shall consist of: 3 parts sandy loam topsoil, 1.0 part 1/4" minus composted pine bark mulch and .5 parts of composted cow manure.
- 15. Landscape (weed) fabric is not allowed.
- All existing trees to remain shall be properly protected during construction. Protection techniques shall be reviewed and approved by the Landscape Architect.
- Prune trees and large shrubs in accordance to guidelines established for nursery stock published by the American Association of Nurserymen, Inc.
- 18. All disturbed areas will be dressed with 6" of topsoil and planted as noted on the plans or seeded except plant beds. Plant beds shall be prepared to a depth of 12" with 75% loam and 25% of ¼" minus composted bark mulch compost.
- 19. All alterations to these drawings made in the field during construction shall be recorded by the contractor on "as-built drawings.
- 20. There shall be a full one (1) year replacement guarantee for all trees and shrubs after final acceptance of initial planting.





N. T. S.

- Design is based on drawings by Ambit Engineering, Inc., dated June 18, 2018 and may require adjustment due to actual field conditions.
- 3. The contractor shall follow best management practices during construction and shall take all means necessary to stabilize and
- 5. If discrepancies exist between the number of plants drawn on the planting plan and the number of plants in the plant list, the planting
- 8. The contractor shall supply all new plant material in quantities sufficient to complete the planting shown on the drawings.
- 11. Stake the location of all proposed plantings for approval by Landscape Architect prior to the commencement of planting.

14. All plant beds to receive two inches (3") of bark mulch. Bark mulch shall be one year old, well composted, shredded native bark not longer than 4" in length and ½" in width, free of woodchips and sawdust. Mulch for terns and herbaceous perennial shall be no longer than 1" in length. Trees in lawn areas shall be mulched in a 6' diameter minimum saucer. Color of mulch shall be dark brown. Red, orange/red or black colored mulch is not acceptable.

70 New Road Salisbury, NH 03268 tel/fax: 603.648.6434 web: www.g2plus1.com

Project Name:

Workforce Housing Development 140 Court Street Portsmouth, New Hampshire 03801

Applicant/Owner of Record:

Portsmouth Housing Authority

245 Middle Street Portsmouth, NH 03801

Ed Pac, LLC 242 Central Avenue Dover, NH 03820

For City Approval

registration:

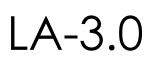
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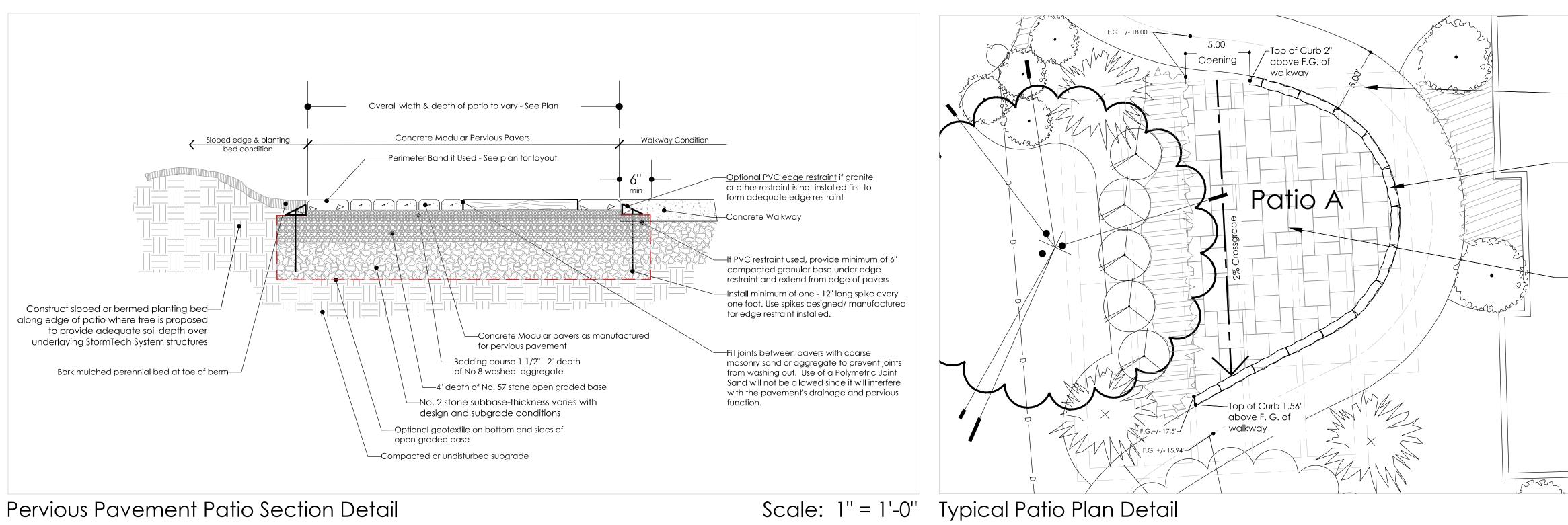
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1	7/17/18	Revised per TAC hearing & project
2		coordination
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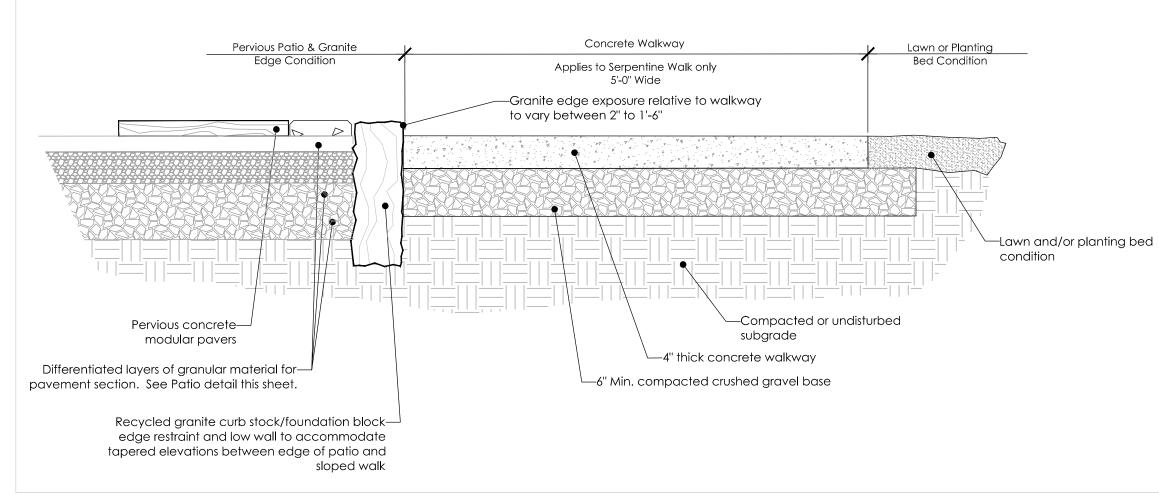
project number:	1306.0
scale:	1'' = 10'
drawn by:	dhg
date:	6/18/2018

sheet title/number:



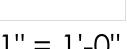






Stabilized Crushed Granite Walk Section Detail

Scale: 1" = 1'-0"



Landscape Architecture Site Planning Graphi

70 New Road Salisbury, NH 03268 tel/fax: 603.648.6434 web: www.g2plus1.com

Project Name:

Workforce Housing Development 140 Court Street Portsmouth, New Hampshire 03801

Applicant/Owner of Record:

Portsmouth Housing Authority

245 Middle Street Portsmouth, NH 03801

Ed Pac, LLC 242 Central Avenue Dover, NH 03820

Scale: 1" = 5'-0"

For City Approval

registration:

revisions:							
no.	date	issued					
1	7/17/18	Revised per TAC hearing & project					
2		coordination					
3							
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6							
7							
8							
9							

project number: 1306.0 1'' = 10' scale: dhg drawn by: 6/18/2018 date:

sheet title/number:

Construction Details

LA-4.0

g2+1 LLC copyright 2001

-Recycled granite curb stock/foundation blocks. > Set in compacted 3/4" crushed gravel base @ minimum of 12" depth. > Curb stock shall have minimum of 12" bury relative to walkway.

-Serpentine concrete walk centerline

Walkway width is 5'-0"

> Stone unit widths and depths may vary. Top of stone edge to mirror 4% average slope of walk. > Stone edge acts as low edge between 4% average slope of walkway and 2% cross grade of patio

-Concrete modular paver patio constructed from pervious pavers. Paver style is <u>Blu 60 MM SLAB</u> in slate finish as manufactured by Techo-Bloc, 5255, Albert-Millichamp, St-Hubert, QC J3Y 8Z8

> Patio A area is approximately 284 SF.

> Paver pattern is an Ashlar paver pattern as

illustrated. Actual pattern governed by paver style used.

> Paver color TBD

> See section detail this sheet for paver installation.

LUMINAIRE SCHEDULE										
SYMBOL	LABEL	QTY.	MANUFACTURER	CATALOG NUMBER	DESCRIPTION	LAMP	NUMBER LAMPS	LUMENS PER LAMP	LIGHT LOSS FACTOR	WATTAGE
¢	Α	14	AURORALIGHT	LBD 350 C11 GTR NL 12 32 300K	CONICAL 11" STACKED COPPER SHADES WITH NO LOUVERS AND CYLI NDRICAL 32" COPPER STEM WITH BRASS BASE; HT 3'	LED	1	395	0.9	12.42
•-≯	В	3	AURORALIGHT	LML 350 C11 GRL 30 P	CONICAL 11" STACKED COPPER SHADES WITH LOUVERS, PAINTED WHITE UNDERSIDE AND FROSTED GLASS LENS, HT 10'	LED	1	400	0.9	18.012
\$ 0 \$	С	4	AURORALIGHT	LML 350 C11 GRL 30 P	CONICAL 11" STACKED COPPER SHADES WITH LOUVERS, PAINTED WHITE UNDERSIDE AND FROSTED GLASS LENS, HT 10'	LED	2	800	0.9	36.024
-ở-	D	9	AURORALIGHT	LML 350 C11 GRL 30 P	CONICAL 11" STACKED COPPER SHADES WITH LOUVERS, PAINTED WHITE UNDERSIDE AND FROSTED GLASS LENS, ARM LENGTH 1'	LED	1	400	0.9	18.012

5' WOOD

STOCKADE

0.3

0:

•.0

¢.0

6' WOOD

STOCKADE -

ō,

0.0

GARAGE

7777 GARAGE

6' VINYL -

4' CHAINLINK FENCE -

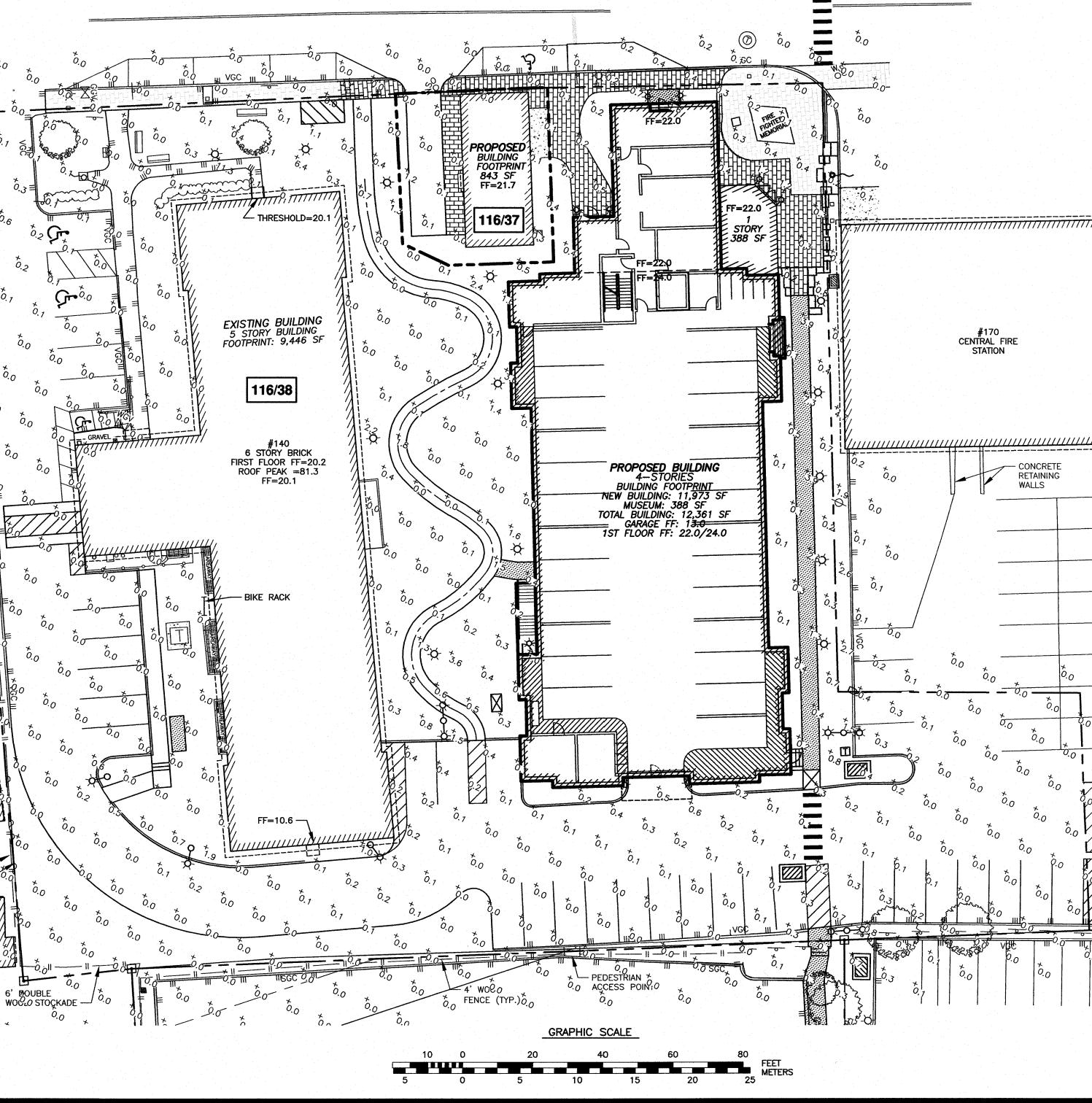
0,7

0.0

6' CHAINLINK FENCE —

COURT STREET

•••





*

#170 CENTRAL FIRE

STATION

- CONCRETE

RETAINING

WALLS

AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors

200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114 Tel (603) 430-9282 Fax (603) 436-2315

NOTES:

1) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.

2) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.

3) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL, VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008).

4) POLE MOUNTED LIGHTS SHALL HAVE A MAXIMUM FIXTURE OF HEIGHT OF 20 FEET.

5) ALL LIGHTING SHALL BE SHIELDED TO MINIMIZE LIGHT TRESPASS AND DIRECT GLARE BEYOND THE PROPERTY.

6) ALL LIGHTS SHALL BE DARK SKY COMPLIANT AND DIRECTED DOWNWARD.

7) LIGHTING PLAN PREPARED USING AGI32 SOFTWARE. LIGHTING DESIGN BASED ON .IES FILES THAT WERE LAB-TESTED OR COMPUTER GENERATED. ACTUAL RESULTS MAY VARY DEPENDING ON FIELD CONDITIONS, AREA GEOMETRY OR CHANGES IN ELECTRICAL SUPPLY VOLTAGE.

8) LIGHTS SHALL COMPLY WITH ALL LOCAL, STATE, AND FEDERAL REGULATIONS.

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

0	ISSUED FOR COMMENT	4/25/18
NO.	DESCRIPTION	DATE
	REVISIONS	

SCALE: 1'=20'

FB 321 PG19

FEBRUARY 2018

LT1

2790

LIGHTING PLAN

EROSION CONTROL NOTES

CONSTRUCTION SEQUENCE

DO NOT BEGIN CONSTRUCTION UNTIL ALL LOCAL, STATE AND FEDERAL PERMITS HAVE BEEN APPLIED FOR AND RECEIVED.

IF REQUIRED THE CONTRACTOR SHALL OBTAIN AN NPDES PHASE II STORMWATER PERMIT AND SUBMIT A NOTICE OF INTENT (N.O.I) BEFORE BEGINNING CONSTRUCTION AND SHALL HAVE ON SITE A STORMWATER POLLUTION PREVENTION PLAN (S.W.P.P.P.) AVAILABLE FOR INSPECTION BY THE PERMITTING AUTHORITY DURING THE CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR CARRYING OUT THE S.W.P.P.P. AND INSPECTING AND MAINTAINING ALL BMP'S CALLED FOR BY THE PLAN. THE CONTRACTOR SHALL SUBMIT A NOTICE OF TERMINATION (N.O.T.) FORM TO THE REGIONAL EPA OFFICE WITHIN 30 DAYS OF FINAL STABILIZATION OF THE ENTIRE SITE OR TURNING OVER CONTROL OF THE SITE TO ANOTHER OPERATOR.

INSTALL PERIMETER CONTROLS, i.e., SILTSOXX AND CATCH BASIN PROTECTION AROUND THE LIMITS OF DISTURBANCE BEFORE ANY EARTH MOVING OPERATIONS. THE USE OF HAYBALES IS NOT ALLOWED.

CONSTRUCT STABILIZED CONSTRUCTION ENTRANCE.

CUT AND GRUB ALL TREES, SHRUBS, SAPLINGS, BRUSH, VINES AND REMOVE OTHER DEBRIS AND RUBBISH AS REQUIRED. DEMOLISH BUILDINGS AND FENCES AS NEEDED.

LAYOUT AND INSTALL ALL BURIED UTILITIES AND SERVICES UP TO 10' OF THE PROPOSED BUILDING FOUNDATIONS. CAP AND MARK TERMINATIONS OR LOG SWING TIES.

CONSTRUCT BUILDINGS. CONNECT UTILITIES.

BASIN INLET PROTECTION.

PLACE BINDER LAYER OF PAVEMENT, THEN RAISE CATCH BASIN FRAMES TO FINAL GRADE. REINSTALL

PLANT LANDSCAPING IN AREAS OUT OF WAY OF BUILDING CONSTRUCTION. PREPARE AND STABILIZE FINAL SITE GRADING BY ADDING TOPSOIL, SEED, MULCH AND FERTILIZER.

AFTER BUILDINGS ARE COMPLETED, FINISH ALL REMAINING LANDSCAPED WORK.

CONSTRUCT ASPHALT WEARING COURSE.

REMOVE TRAPPED SEDIMENTS FROM COLLECTION DEVICES AS APPROPRIATE, AND THEN REMOVE TEMPORARY EROSION CONTROL MEASURES UPON COMPLETION OF FINAL STABILIZATION OF THE SITE.

GENERAL CONSTRUCTION NOTES

THE EROSION CONTROL PROCEDURES SHALL CONFORM TO SECTION 645 OF THE "STANDARD SPECIFICATION FOR ROAD AND BRIDGE CONSTRUCTION" OF THE NHDOT, AND "STORM WATER MANAGEMENT AND EROSION AND SEDIMENT CONTROL HANDBOOK FOR URBAN AND DEVELOPING AREAS IN NEW HAMPSHIRE". THE PROJECT IS TO BE MANAGED IN A MANNER THAT MEETS THE REQUIREMENTS AND INTENT OF RSA 430:53 AND CHAPTER AGR 3800 RELATIVE TO INVASIVE SPECIES.

DURING CONSTRUCTION AND THEREAFTER, EROSION CONTROL MEASURES ARE TO BE IMPLEMENTED AS NOTED. THE SMALLEST PRACTICAL AREA OF LAND SHOULD BE EXPOSED AT ANY ONE TIME DURING DEVELOPMENT. NO DISTURBED AREA SHALL BE LEFT UNSTABILIZED FOR MORE THAN 45 DAYS.

ANY DISTURBED AREAS WHICH ARE TO BE LEFT TEMPORARILY, AND WHICH WILL BE REGRADED LATER DURING CONSTRUCTION SHALL BE MACHINE HAY MULCHED AND SEEDED WITH RYE GRASS TO PREVENT EROSION.

DUST CONTROL: IF TEMPORARY STABILIZATION PRACTICES, SUCH AS TEMPORARY VEGETATION AND MULCHING, DO NOT ADEQUATELY REDUCE DUST GENERATION, APPLICATION OF WATER OR CALCIUM CHLORIDE SHALL BE APPLIED IN ACCORDANCE WITH BEST MANAGEMENT PRACTICES.

SILT FENCES AND SILTSOXX SHALL BE PERIODICALLY INSPECTED DURING THE LIFE OF THE PROJECT AND AFTER EACH STORM. ALL DAMAGED SILT FENCES AND SILTSOXX SHALL BE REPAIRED. SEDIMENT DEPOSITS SHALL PERIODICALLY BE REMOVED AND DISPOSED IN A SECURED LOCATION.

AVOID THE USE OF FUTURE OPEN SPACES (LOAM AND SEED AREAS) WHEREVER POSSIBLE DURING CONSTRUCTION. CONSTRUCTION TRAFFIC SHALL USE THE ROADBEDS OF FUTURE ACCESS DRIVES AND PARKING AREAS.

ADDITIONAL TOPSOIL REQUIRED FOR THE ESTABLISHMENT OF VEGETATION SHALL BE STOCKPILED IN AMOUNTS NECESSARY TO COMPLETE FINISHED GRADING OF ALL EXPOSED AREAS -- CONSTRUCT SILT FENCE OR SILTSOXX AROUND TOPSOIL STOCKPILE.

AREAS TO BE FILLED SHALL BE CLEARED, GRUBBED AND STRIPPED OF TOPSOIL TO REMOVE TREES, VEGETATION, ROOTS OR OTHER OBJECTIONABLE MATERIAL. STUMPS SHALL BE DISPOSED OF IN AN APPROVED FACILITY.

ALL FILLS SHALL BE PLACED AND COMPACTED TO REDUCE EROSION, SLIPPAGE, SETTLEMENT, SUBSIDENCE OR OTHER RELATED PROBLEMS.

ALL NON-STRUCTURAL, SITE-FILL SHALL BE PLACED AND COMPACTED TO 90% MODIFIED PROCTOR DENSITY IN LAYERS NOT EXCEEDING 18 INCHES IN THICKNESS UNLESS OTHERWISE NOTED.

FROZEN MATERIAL OR SOFT, MUCKY OR HIGHLY COMPRESSIBLE MATERIAL, TRASH, WOODY DEBRIS, LEAVES, BRUSH OR ANY DELETERIOUS MATTER SHALL NOT BE INCORPORATED INTO FILLS.

FILL MATERIAL SHALL NOT BE PLACED ON FROZEN FOUNDATION SUBGRADE.

DURING CONSTRUCTION AND UNTIL ALL DEVELOPED AREAS ARE FULLY STABILIZED, ALL EROSION CONTROL MEASURES SHALL BE INSPECTED WEEKLY AND AFTER EACH ONE HALF INCH OF RAINFALL.

THE CONTRACTOR SHALL MODIFY OR ADD EROSION CONTROL MEASURES AS NECESSARY TO ACCOMMODATE PROJECT CONSTRUCTION.

ALL ROADWAYS AND PARKING AREAS SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.

AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:

- BASE COURSE GRAVELS HAVE BEEN INSTALLED ON AREAS TO BE PAVED - A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED

- A MINIMUM OF 3 INCHES OF NON-EROSIVE MATERIAL SUCH AS STONE OR RIPRAP HAS BEEN INSTALLED
- EROSION CONTROL BLANKETS HAVE BEEN INSTALLED

VEGETATIVE PRACTICE

FOR PERMANENT MEASURES AND PLANTINGS:

LIMESTONE SHALL BE THOROUGHLY INCORPORATED INTO THE LOAM LAYER AT A RATE OF 2 TONS PER ACRE.

FERTILIZER SHALL BE SPREAD ON THE TOP LAYER OF LOAM AND WORKED INTO THE SURFACE. FERTILIZER APPLICATION RATE SHALL BE 500 POUNDS PER ACRE OF 10-20-20 FERTILIZER.

SEED SHALL BE SOWN AT THE RATES SHOWN IN THE TABLE BELOW. IMMEDIATELY BEFORE SEEDING. THE SOIL SHALL BE LIGHTLY RAKED. ONE HALF THE SEED SHALL BE SOWN IN ONE DIRECTION AND THE OTHER HALF AT RIGHT ANGLES TO THE ORIGINAL DIRECTION. IT SHALL BE LIGHTLY RAKED INTO THE SOIL TO A DEPTH NOT OVER 1/4 INCH AND ROLLED WITH A HAND ROLLER WEIGHING NOT OVER 100 POUNDS PER LINEAR FOOT OF WIDTH. HAY MULCH SHALL BE APPLIED IMMEDIATELY AFTER SEEDING AT A RATE OF 1.5 TO 2 TONS PER ACRE, AND SHALL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE EROSION AND SEDIMENT CONTROL HANDBOOK.

THE SURFACE SHALL BE WATERED AND KEPT MOIST WITH A FINE SPRAY AS REQUIRED, WITHOUT WASHING AWAY THE SOIL, UNTIL THE GRASS IS WELL ESTABLISHED. ANY AREAS WHICH ARE NOT SATISFACTORILY COVERED SHALL BE RESEEDED, AND ALL NOXIOUS WEEDS REMOVED.

A GRASS SEED MIXTURE CONTAINING THE FOLLOWING SEED REQUIREMENTS SHALL BE:

GENERAL COVER PROPORTION SEEDING RATE

- CREEPING RED FESCUE 50% 100 LBS/ACRE KENTUCKY BLUEGRASS 50%
- SLOPE SEED (USED ON ALL SLOPES GREATER THAN OR EQUAL TO 3:1)
- CREEPING RED FESCUE 42% TALL FESCUE 42% 48 LBS/ACRE BIRDSFOOT TREFOIL 16%

IN NO CASE SHALL THE WEED CONTENT EXCEED ONE PERCENT BY WEIGHT. ALL SEED SHALL COMPLY WITH APPLICABLE STATE AND FEDERAL SEED LAWS.

FOR TEMPORARY PROTECTION OF DISTURBED AREAS: MULCHING AND SEEDING SHALL BE APPLIED AT THE FOLLOWING RATES: PERENNIAL RYE: 0.7 LBS/1,000 S.F.

MULCH: 1.5 TONS/ACRE

MAINTENANCE AND PROTECTION THE CONTRACTOR SHALL MAINTAIN ALL LOAM & SEED AREAS UNTIL FINAL ACCEPTANCE AT THE COMPLETION OF THE CONTRACT. MAINTENANCE SHALL INCLUDE WATERING, WEEDING, REMOVAL OF STONES AND OTHER FOREIGN OBJECTS OVER 1/2 INCHES IN DIAMETER WHICH MAY APPEAR AND THE FIRST TWO (2) CUTTINGS OF GRASS NO CLOSER THEN TEN (10) DAYS APART. THE FIRST CUTTING SHALL BE ACCOMPLISHED WHEN THE GRASS IS FROM 2 1/2 TO 3 INCHES HIGH. ALL BARE AND DEAD SPOTS WHICH BECOME APPARENT SHALL BE PROPERLY PREPARED, LIMED AND FERTILIZED, AND RESEEDED BY THE CONTRACTOR AT HIS EXPENSE AS MANY TIMES AS NECESSARY TO SECURE GOOD GROWTH. THE ENTIRE AREA SHALL BE MAINTAINED, WATERED AND CUT UNTIL ACCEPTANCE OF THE LAWN BY THE OWNER'S REPRESENTATIVE.

THE CONTRACTOR SHALL TAKE WHATEVER MEASURES ARE NECESSARY TO PROTECT THE GRASS WHILE IT IS DEVELOPING.

TO BE ACCEPTABLE, SEEDED AREAS SHALL CONSIST OF A UNIFORM STAND OF AT LEAST 90 PERCENT ESTABLISHED PERMANENT GRASS SPECIES, WITH UNIFORM COUNT OF AT LEAST 100 PLANTS PER SQUARE FOOT.

SEEDED AREAS WILL BE FERTILIZED AND RESEEDED AS NECESSARY TO INSURE VEGETATIVE ESTABLISHMENT.

THE SWALES WILL BE CHECKED WEEKLY AND REPAIRED WHEN NECESSARY UNTIL ADEQUATE VEGETATION IS ESTABLISHED.

THE SILT FENCE OR SILTSOXX BARRIER SHALL BE CHECKED AFTER EACH RAINFALL AND AT LEAST DAILY DURING PROLONGED RAINFALL.

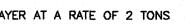
SILT FENCING AND SILTSOXX SHALL BE REMOVED ONCE VEGETATION IS ESTABLISHED, AND DISTURBED AREAS RESULTING FROM SILT FENCE AND SILTSOXX REMOVAL SHALL BE PERMANENTLY SEEDED.

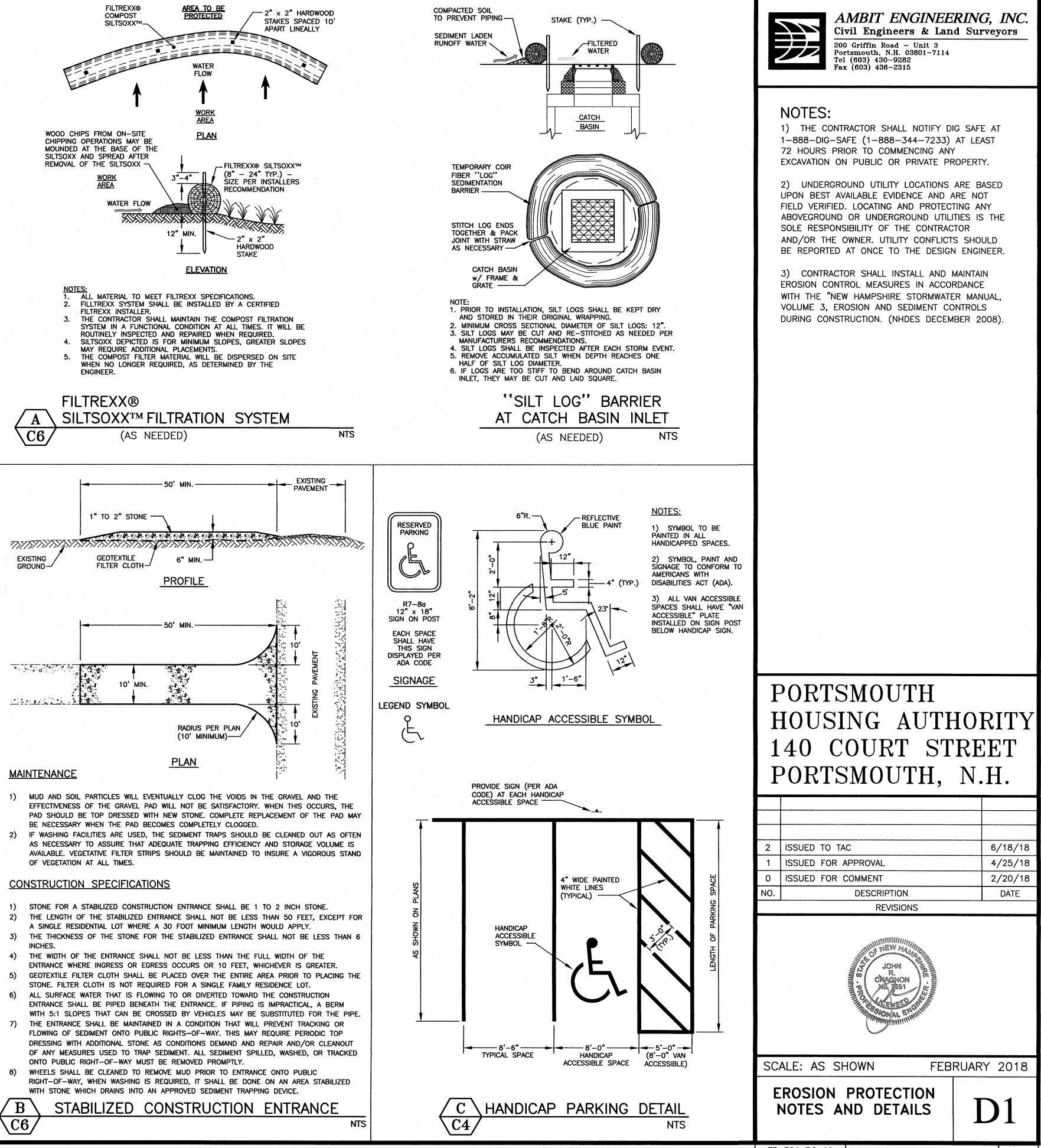
WINTER NOTES

ALL PROPOSED VEGETATED AREAS WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHALL BE STABILIZED BY SEEDING AND INSTALLING EROSION CONTROL BLANKETS ON SLOPES GREATER THAN 3:1. AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE. SECURED WITH ANCHORED NETTING. ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.

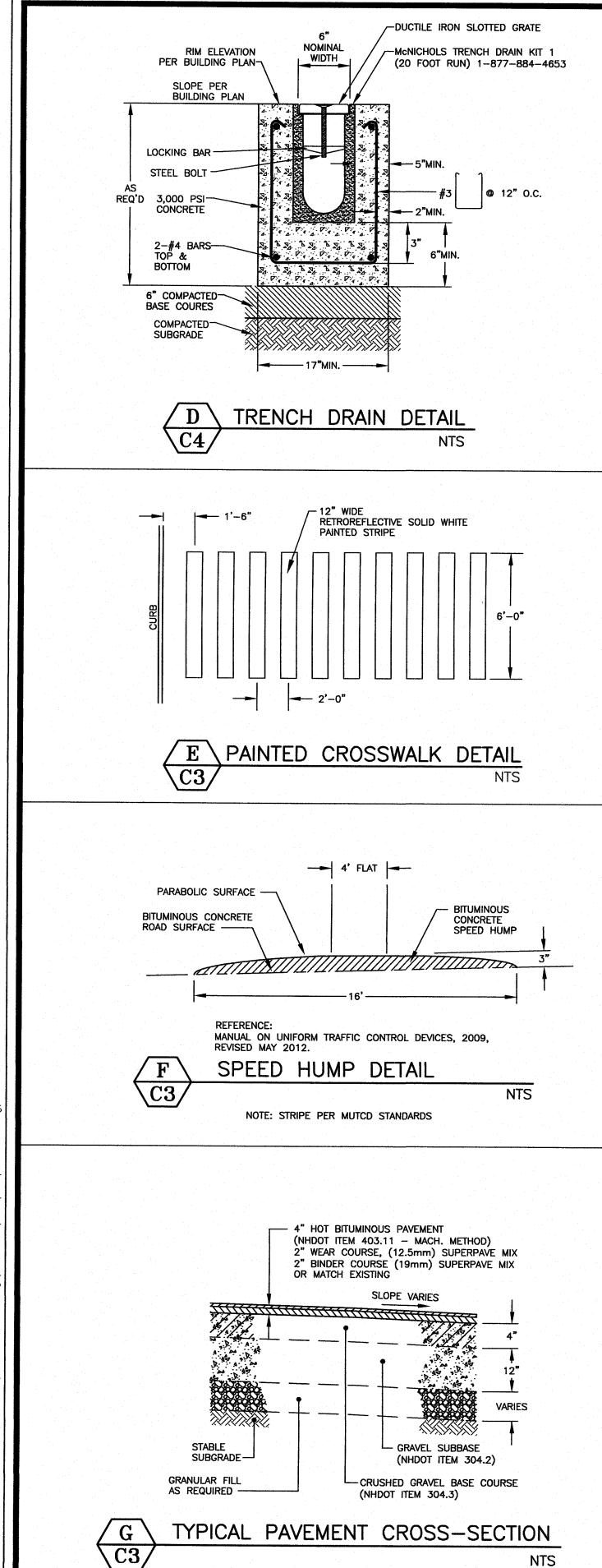
ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85% VEGETATIVE GROWTH BY OCTOBER 15TH, OR WHICH ARE DISTURBED AFTER OCTOBER 15TH, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.

AFTER NOVEMBER 15TH. INCOMPLETE ROAD OR PARKING SURFACES. WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3 INCHES OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.





FB 321 PG 19



CAST IRON WARNING PLATE OR EQUAL. INSTALL IN ACCORDANCE WITH MANUFACTURER'S **RECOMMENDATIONS & ADA** FEDERAL GUIDELINES.

 $\overline{C3}$

BRICK PAVEMENT NOTES

SCOPE OF WORK:

CONSTRUCTION NOTE:

EXISTING GRANITE CURB

MISSING CURB SHALL BE

MATCHING EXISTING CURB

3' IN LENGTH WILL BE

ALLOWED.

REPLACED WITH NEW CURB

SIZE. NO CURB LESS THAN

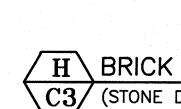
DISTURBED BY CONSTRUCTION

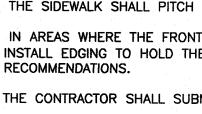
SHALL BE REUSED AND ANY

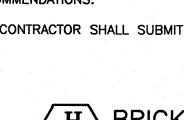
SIDEWALK AS DIRECTED IN THE FIELD BY THE ENGINEER. 2) REVEAL SHALL BE 5" (COORDINATE WITH PORTSMOUTH DPW).

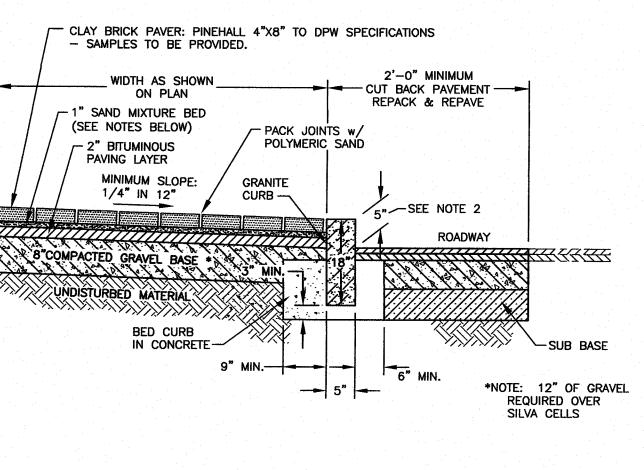
METHODS OF CONSTRUCTION:

- BE OF A STANDARD SIZE (2.25" X 4 X 8").
- DISPOSED OF OFF-SITE AT THE CONTRACTOR'S OWN EXPENSE.
- WITH 1 PART PORTLAND CEMENT.
- G) THE SIDEWALK SHALL PITCH TOWARDS THE STREET AS SHOWN ON THE GRADING PLAN.









1) THE WORK SHALL CONSIST OF CONSTRUCTING/RECONSTRUCTING THE SUB-BASE AND CONSTRUCTING A NEW BRICK

A) ALL LABOR AND MATERIALS SHALL CONFORM TO THE STATE OF NEW HAMPSHIRE STANDARD SPECIFICATIONS FOR ROAD AND BRIDGE CONSTRUCTION, SECTION 608, AND CITY OF PORTSMOUTH SPECIFICATIONS FOR NEW BRICK SIDEWALK, SECTION 6.

B) ALL BRICKS SHALL CONFORM TO THE REQUIREMENTS OF ASTM STANDARD SPECIFICATIONS FOR BUILDING BRICKS: CLASS SX, TYPE 1, APPLICATION PX. THE BRICKS SHALL BE NO. 1, WIRE CUT TYPE FOR PAVING, WITH A COMPRESSIVE STRENGTH OF NOT LESS THAN 6,000 POUNDS PER SQUARE INCH. THE BRICKS SHALL NOT BE CORED OR HAVE FROGS AND SHALL

C) EXCAVATION FOR SIDEWALKS SHALL BE AT A DEPTH OF 10 INCHES BELOW FINISH GRADE. IN AREAS NOT BUTTING CURBING OR BUILDINGS, THE EXCAVATION SHALL BE 6 INCHES WIDER THAN THE FINISHED SIDEWALK WIDTH. AT ALL DRIVE CROSSINGS, THE DEPTH OF EXCAVATION SHALL BE INCREASED ACCORDINGLY. THE CONTRACTOR SHALL PROVIDE NEAT AND SQUARE CUTTING OF EXISTING ASPHALT ROAD SURFACE AS NEEDED. ALL UNSUITABLE MATERIAL SHALL BE REMOVED AND

D) THE BASE MATERIAL SHALL CONSIST OF A MIXTURE OF STONES OR ROCK FRAGMENTS AND PARTICLES WITH 100% PASSING THE 3 INCH SIEVE, 95% TO 100% PASSING THE 2 INCH SIEVE, 55% TO 85% PASSING THE 1 INCH SIEVE, AND 27% TO 52% PASSING THE NO. 4 SIEVE. AT LEAST 50% OF THE MATERIALS RETAINED ON THE 1 INCH SIEVE SHALL HAVE A FRACTURED FACE. THE BASE MATERIAL SHALL BE THOROUGHLY COMPACTED TO THE DEPTH SPECIFIED OR DIRECTED. IN THE WAY OF ALL DRIVE CROSSINGS THE BASE WILL BE INCREASED TO A COMPACTED DEPTH OF 12 INCHES. GRAVEL REQUIREMENTS FOR RECONSTRUCTION WILL BE AS DIRECTED, BASED ON SITE CONDITIONS. THE WORK INCLUDES BACKING UP ANY AND ALL CURB BEING INSTALLED BY OTHERS ON BOTH SIDES.

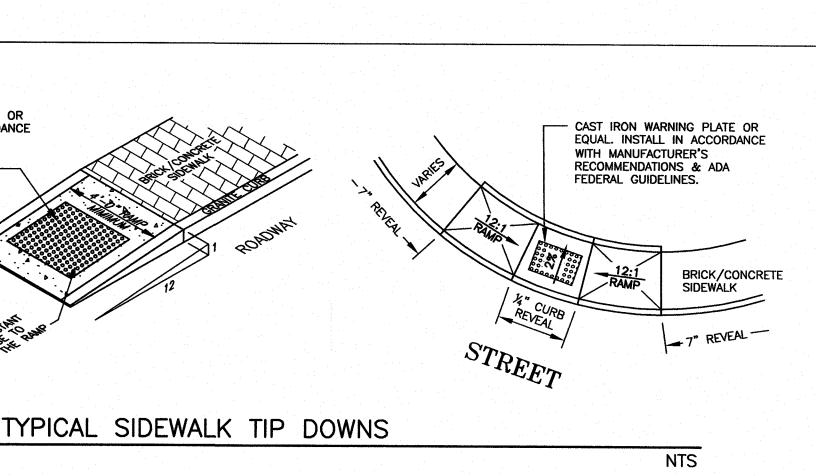
E) THE CLAY BRICK PAVERS SHALL BE LAID IN A 1 INCH BED OF A SAND MIXTURE COMPRISED OF: 3 PARTS SAND MIXED

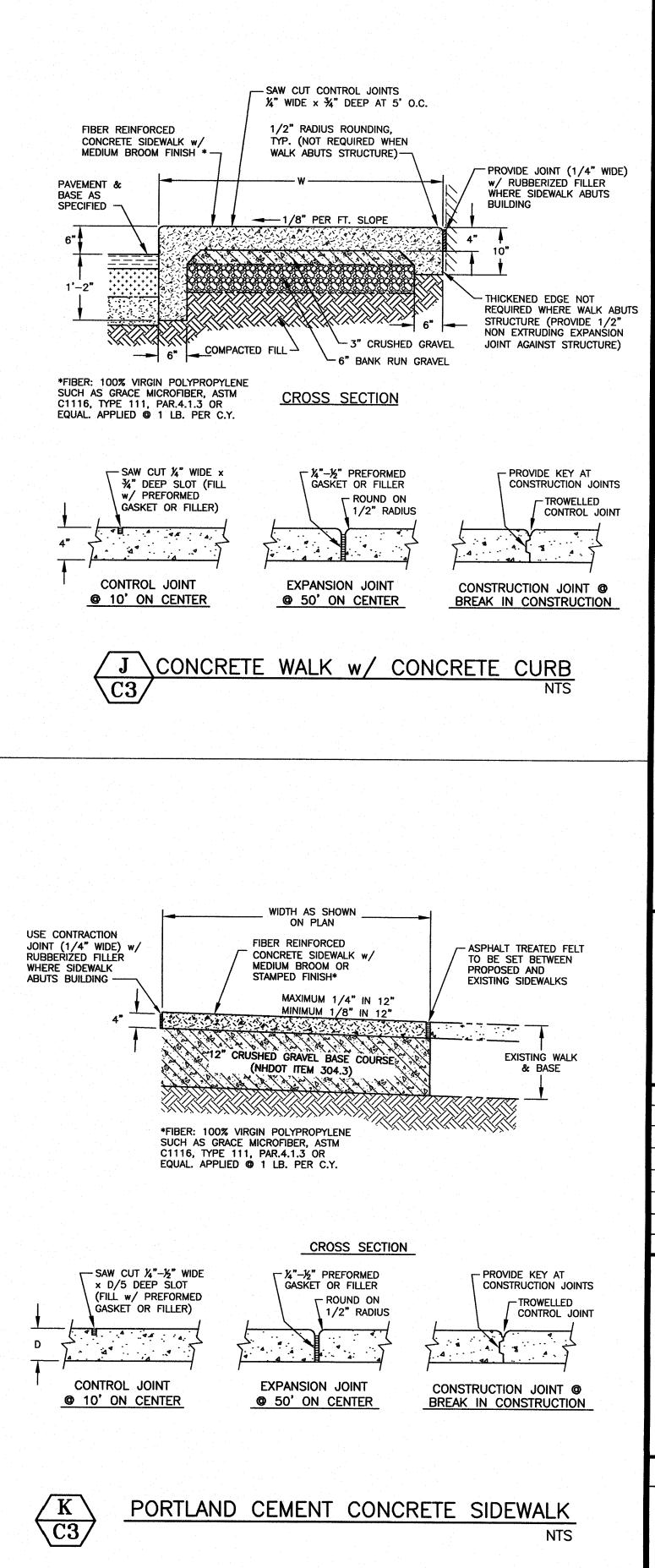
F) THE CONTRACTOR SHALL LAY THE BRICKS SO THAT APPROXIMATELY 5.2 BRICKS SHALL COVER ONE SQUARE FOOT.

H) IN AREAS WHERE THE FRONT OF THE BRICK SIDEWALK IS NOT ADJACENT TO GRANITE CURBING, THE CONTRACTOR SHALL INSTALL EDGING TO HOLD THE BRICKS IN PLACE. SUCH EDGING SHALL BE INSTALLED PER THE MANUFACTURER'S

I) THE CONTRACTOR SHALL SUBMIT A SAMPLE OF THE BRICKS FOR APPROVAL BY THE CITY BEFORE BRICKS ARE INSTALLED.

BRICK SIDEWALK w/ VERTICAL GRANITE CURB (STONE DUST BEDDING OVER BITUMINOUS PAVING) NTS







AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors 200 Griffin Road - Unit 3 Portsmouth, N.H. 03801-7114

Tel (603) 430-9282 Fax (603) 436-2315

NOTES:

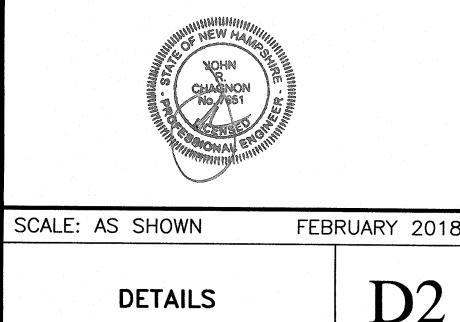
1) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.

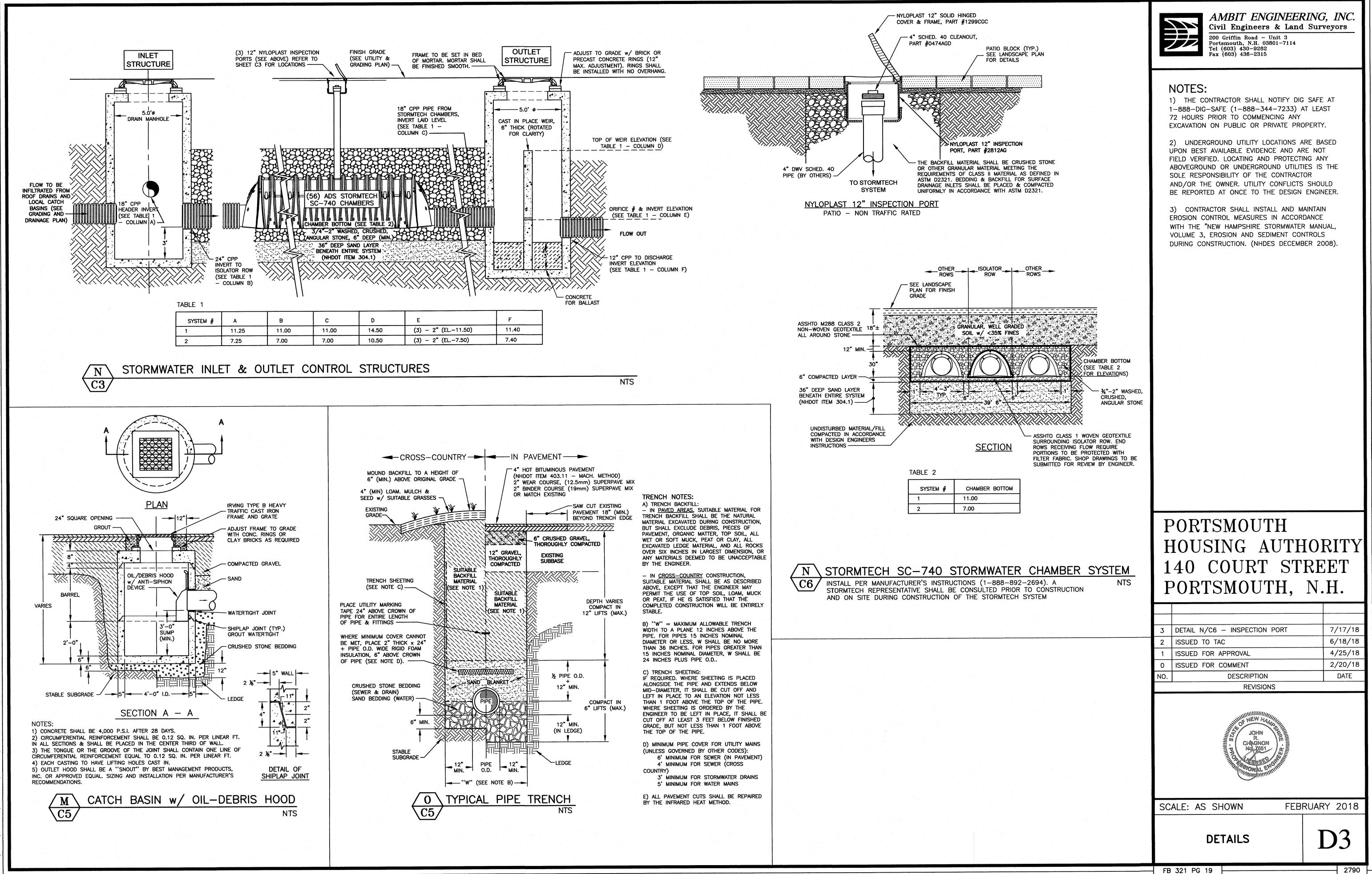
2) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.

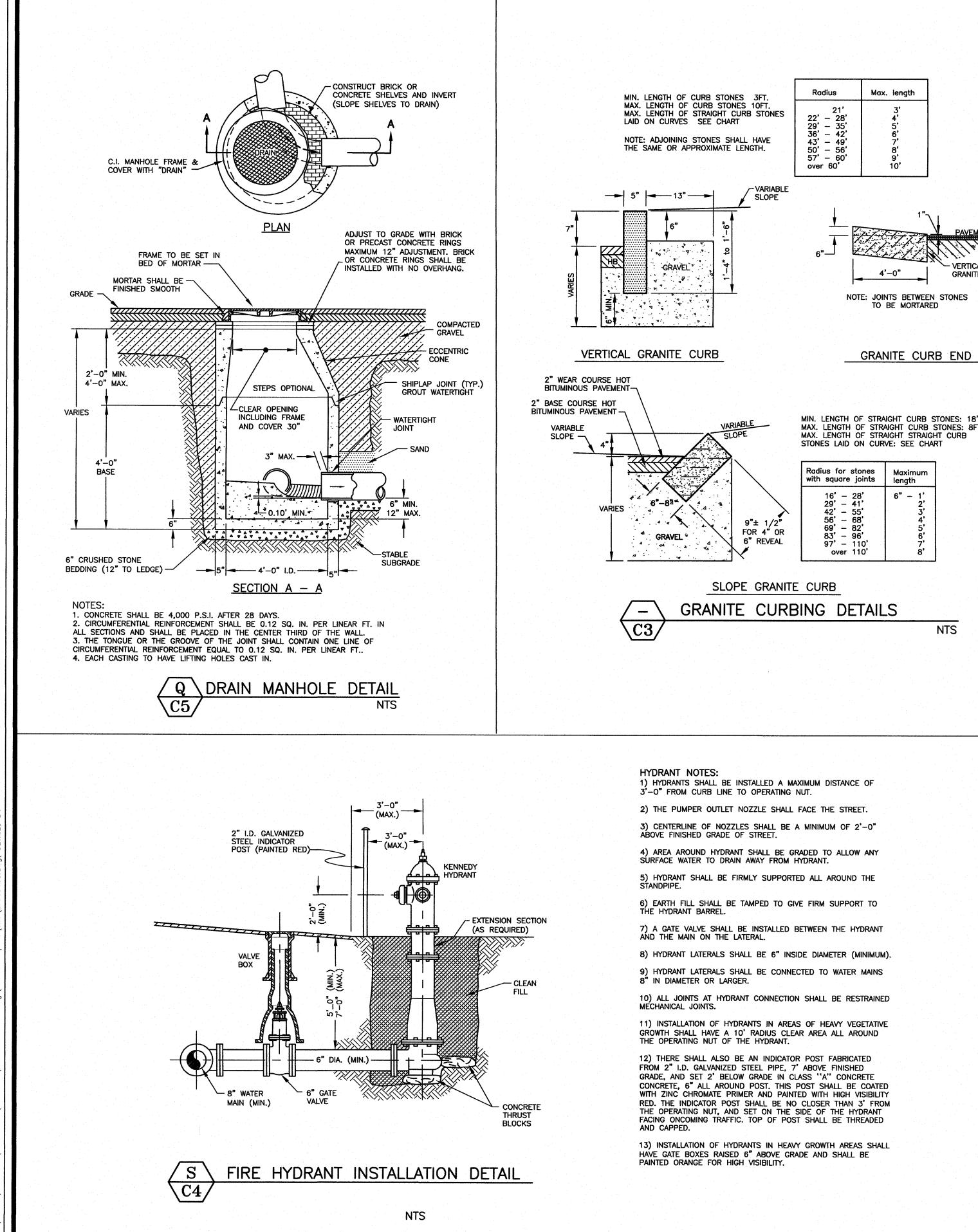
3) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL. VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008).

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

2	ISSUED TO TAC	6/18/18
1	ISSUED FOR APPROVAL	4/25/18
0	ISSUED FOR COMMENT	2/20/18
NO.	DESCRIPTION	DATE
	REVISIONS	
	· · · · · · · · · · · · · · · · · · ·	



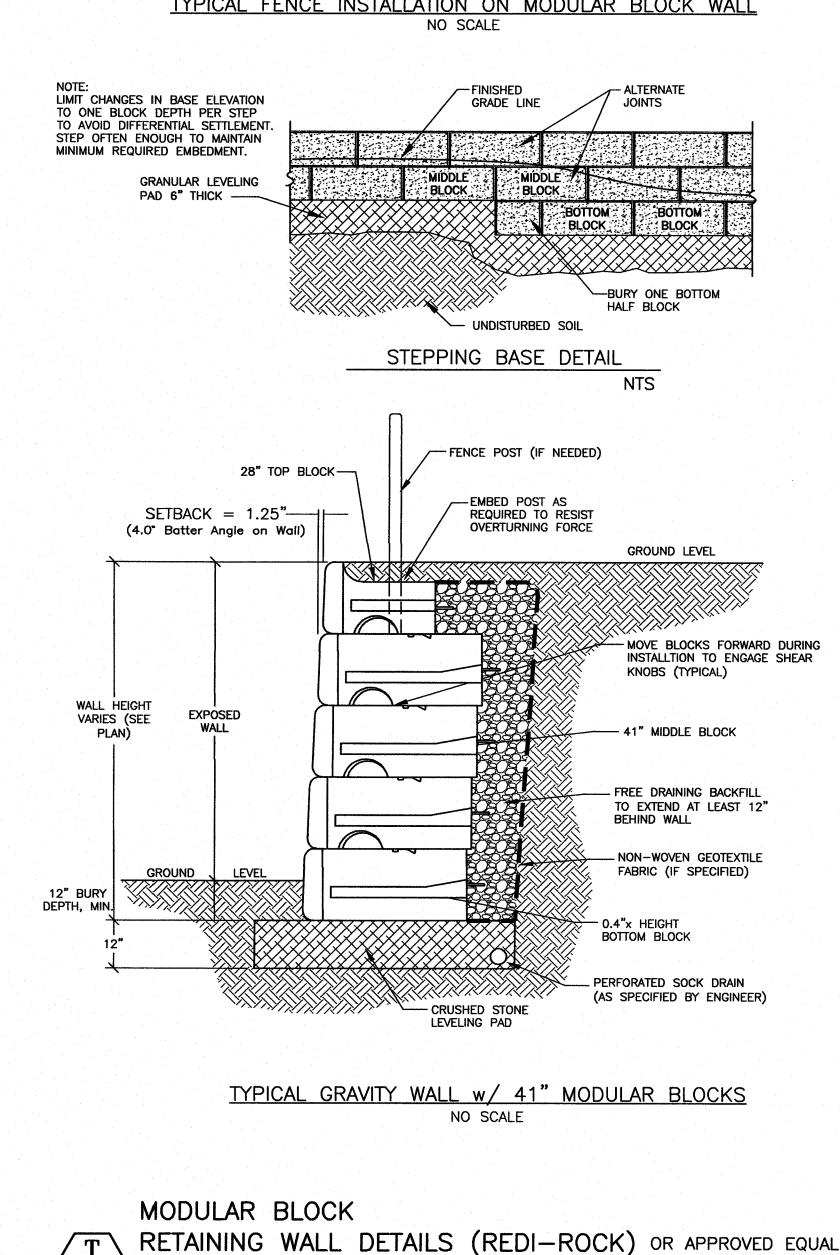




MIN. LENGTH OF STRAIGHT CURB STONES: 18" MAX. LENGTH OF STRAIGHT CURB STONES: 8FT. MAX. LENGTH OF STRAIGHT STRAIGHT CURB STONES LAID ON CURVE: SEE CHART

- VERTICAL

GRANITE CURB

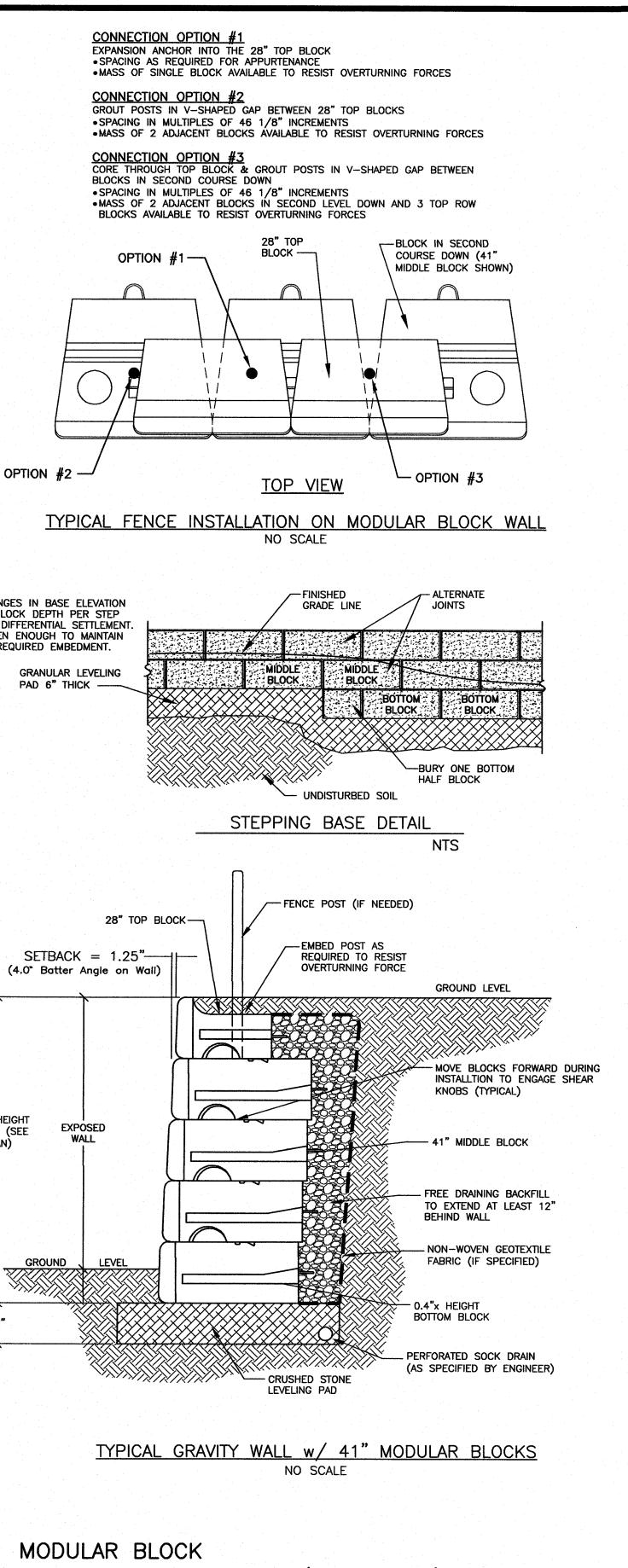


NOTE: STAMPED DESIGN DRAWINGS SHALL BE SUBMITTED

TO THE CITY OF PORTSMOUTH FOR APPROVAL PRIOR TO

 $\sqrt{C3}$

CONSTRUCTION.



NTS

AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors 200 Griffin Road - Unit 3

Portsmouth, N.H. 03801-7114 Tel (603) 430-9282 Fax (603) 436-2315

NOTES:

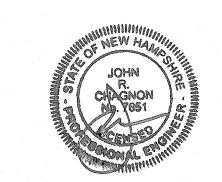
1) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.

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PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.

	and a second	
2	ISSUED TO TAC	6/18/18
1	ISSUED FOR APPROVAL	4/25/18
0	ISSUED FOR COMMENT	2/20/18
NO.	DESCRIPTION	DATE
REVISIONS		



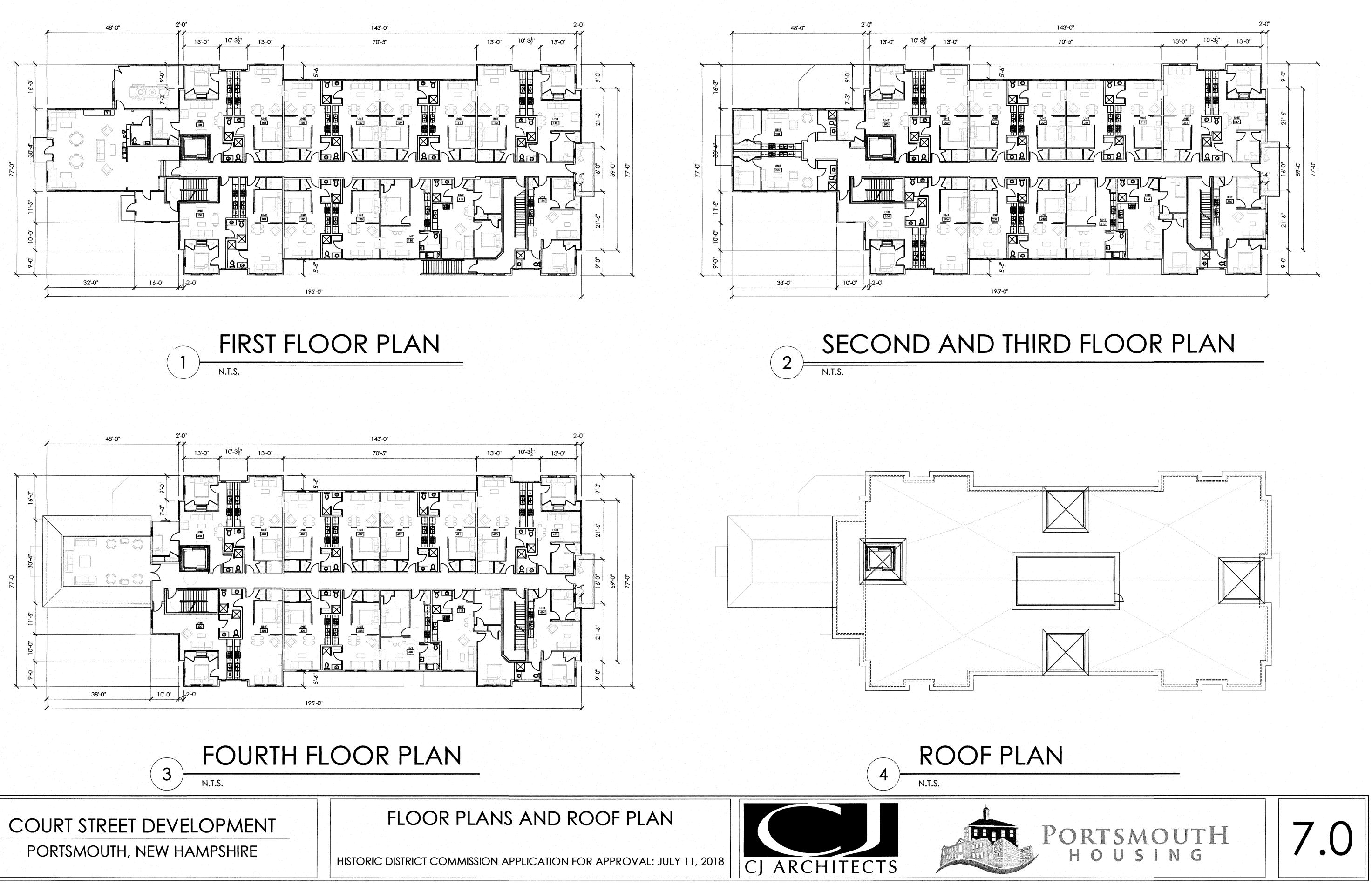
SCALE: AS SHOWN

DETAILS

FEBRUARY 2018

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2790





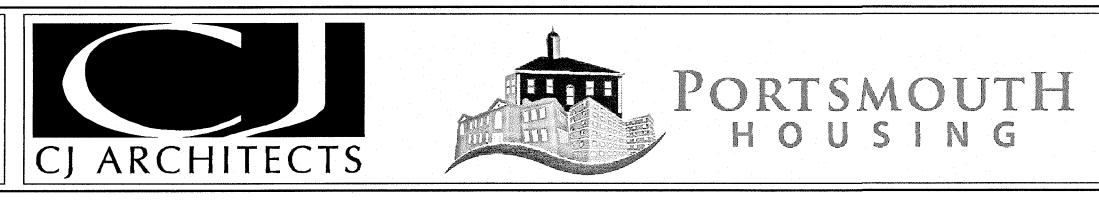
COURT STREET DEVELOPMENT

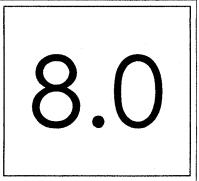
PORTSMOUTH, NEW HAMPSHIRE

HISTORIC DISTRICT COMMISSION APPLICATION FOR APPROVAL: JULY 11, 2018

NORTH ELEVATION

NORTH ELEVATION





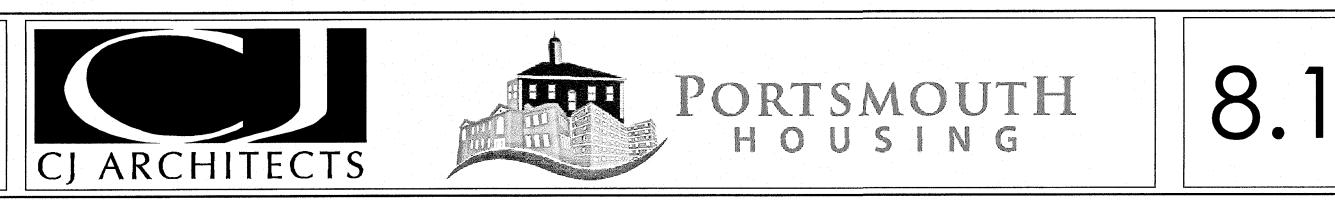


HISTORIC DISTRICT COMMISSION APPLICATION FOR APPROVAL: JULY 11, 2018



1 PARTIAL EAST ELEVATION

EAST ELEVATION



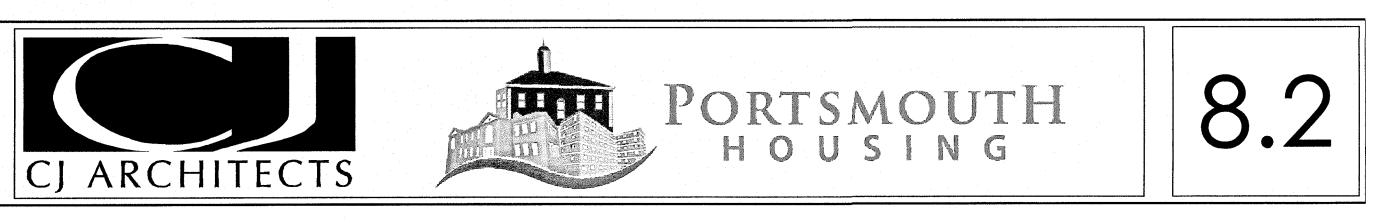


COURT STREET DEVELOPMENT

PORTSMOUTH, NEW HAMPSHIRE

HISTORIC DISTRICT COMMISSION APPLICATION FOR APPROVAL: JULY 11, 2018

EAST ELEVATION

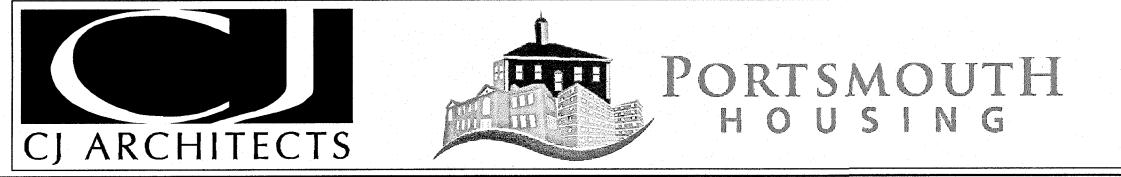




COURT STREET DEVELOPMENT PORTSMOUTH, NEW HAMPSHIRE

HISTORIC DISTRICT COMMISSION APPLICATION FOR APPROVAL: JULY 11, 2018

SOUTH ELEVATION







PORTSMOUTH, NEW HAMPSHIRE

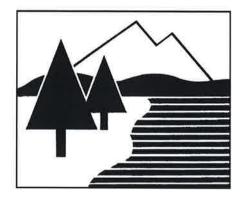
HISTORIC DISTRICT COMMISSION APPLICATION FOR APPROVAL: JULY 11, 2018



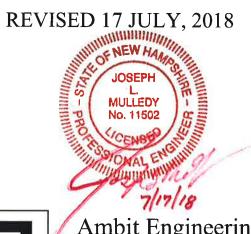




DRAINAGE ANALYSIS SITE REDEVELOPMENT **140 COURT STREET** PORTSMOUTH HOUSING AUTHORITY PORTSMOUTH, NH



18 JUNE, 2018





Ambit Engineering, Inc.

Civil Engineers and Land Surveyors 200 Griffin Road, Unit 3 Portsmouth, NH 03801 Phone: 603.430.9282; Fax: 603.436.2315 E-mail: jlm@ambitengineering.com (Ambit Job Number 2790)

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Executive Summary	
Introduction / Project Description	2
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APPE	NDIX
A.	Vicinity (Tax) Map
B.	Tables, Charts, Etc.
C.	HydroCAD Drainage Analysis Calculations
D.	Soil Survey Information
E.	FEMA FIRM Map
F.	Inspection & Maintenance Plan

ATTACHMENTS

Existing Drainage Plan - W1

Proposed Drainage Plan - W2

EXECUTIVE SUMMARY

The hydrologic modeling utilized for this analysis uses the "Extreme Precipitation" values for rainfall from The Northeast Regional Climate Center (Cornell University).

This drainage analysis examines the pre-development (existing) and post-development (proposed) stormwater drainage patterns for the proposed construction of a new 11,973 square foot building and associated site improvements at 140 Court Street in Portsmouth, NH. The site is shown on the City of Portsmouth Assessor's Tax Map 116 as Lots 38 and 37. The project proposes to relocate the lot lines between the two lots. Portsmouth Housing Authority will retain Lot 38 to support the proposed redevelopment. The total proposed size of new lot 38 is 62,500 square-feet. The total proposed size of new lot 37 is 2,113 square-feet.

The new and renovated buildings will be serviced by public water and sewer. The development has the potential to increase stormwater runoff to adjacent properties, and therefore must be designed in a manner to prevent that occurrence. This will be done primarily by capturing stormwater runoff and routing it through appropriate stormwater facilities, designed to ensure that there will be no increase in peak runoff from the site as a result of this project. A significant portion of the site currently drains to a combined sewer system. The project will need to separate the flow and remove the stormwater from the City sewer system. End of pipe treatment is provided in the existing drainage network.

SITE REDEVELOPMENT

140 COURT STREET

PORTSMOUTH HOUSING AUTHORITY

PORTSMOUTH, NH

INTRODUCTION / PROJECT DESCRIPTION

This drainage report is designed to assist the owner, planning board, contractor, regulatory reviewer, and others in understanding the impact of the proposed development project on local surface water runoff and quality. The project site is shown on the City of Portsmouth, NH Assessor's Tax Map 116 as Lots 38 and 37.

Bounding the site to the north and west are single and multi-family residential properties. Bounding the site to the east is the Portsmouth Fire Department. Bounding the site to the south are the Rockingham County Family Court and the Portsmouth District Court. The property is located in the Character District (CD4). A vicinity map is included in the Appendix to this report.

The proposed development will construct a new residential building, new parking area, and other associated improvements such as a utilities and landscaping.

This report includes information about the existing site and the proposed development necessary to analyze stormwater runoff and to design any required mitigation. The report includes maps of pre-development and post-development watersheds, sub-catchment areas and calculations of runoff. The report will provide a narrative of the stormwater runoff and describe numerically and graphically the surface water runoff patterns for this site. Proposed stormwater management and treatment structures and methods will also be described, as well as erosion and sediment control practices. To fully understand the proposed site development the reader should also review a complete site plan set in addition to this report.

METHODOLOGY

This report uses the US Soil Conservation Service (SCS) Method for estimating stormwater runoff. The SCS method is published in The National Engineering Handbook (NEH), Section 4 "Hydrology" and includes the Technical Release No. 20, (TR-20) "Computer Program for Project Formulation Hydrology", and Technical Release No. 55 (TR-55) "Urban Hydrology for Small Watersheds" methods. This report uses the HydroCAD version 10.0 program, written by

HydroCAD Software Solutions LLC, Chocorua, N.H., to apply these methods for the calculation of runoff and for pond modeling.

Time of Concentration (Tc) is calculated by entering measured flow path data such as flow path type, length, slope and surface characteristics into the HydroCAD program. For the purposes of this report, a minimum time of concentration of 5 minutes is used.

The storm events used for the calculations in this report are the 10-year and 50-year (24-hour) storms. Watershed basin boundaries have been delineated using topographic maps prepared by Ambit Engineering and field observations to confirm.

SITE SPECIFIC INFORMATION

Based on the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS), Soil Survey of Rockingham County, New Hampshire, and confirmed by field exploration conducted by Ambit Engineering, Inc., the site is made up of one soil type:

799 – Urban land – Canton Complex (3-15% slopes), well drained with a typical depth to restrictive feature of more than 80 inches. This soil has a Hydrologic Soil Group (HSG) classification of A, with a Low runoff class.

The physical characteristics of the site consist of (3-15%) grades that generally slope from the north to the south. Elevations on the site range from 10 to 20 feet above sea level. The existing site is developed and includes 3 existing buildings with paved parking. Vegetation around the developed portion of the lot consists of established grasses, shrubs and trees.

According to the Federal Emergency Management Agency (FEMA) Flood Insurance Rate Map (FIRM) number 33015C0259E (effective date May 17, 2005), the project site is located in Zone X and is determined to be outside of the 0.2% annual chance floodplain. A copy of the FIRM map is included in the Appendix.

PRE-DEVELOPMENT DRAINAGE

The majority of the existing site drains via overland flow from the front of the lots along Court Street at the north towards the rear of the site to the south. Runoff is collected in a series of catch basins that enter a closed drainage system and then enter the combined sewer system. There is no existing stormwater detention or treatment on the site. There are portions to the rear of the site that flow to an existing catch basin that flow off site to a closed drainage system to the Mill Pond.

In the pre-development condition, the site has been analyzed as eleven subcatchments (ES1, ES1a, ES2, ES2a, ES3, ES4, ES4a, ES5, ES6, ES7 and ES8) based on localized topography and discharge location. Subcatchment ES1 is the western most paved parking and driveway entrance

DRAINAGE ANALYSIS

to the site and flows overland directly to a catch basin located at the end of the driveway. Subcatchment ES2 is the rooftop runoff of the western most building and flows by pipe to a catch basin located at the southeastern corner of this building. Subcatchment ES1a is a small strip of land between an existing curb and the property line to the west. Subcatchment ES2a is a small depressed area within the center driveway between the two existing buildings which flows to a yard drain and into the closed drainage system for the site. Subcatchment ES3 is a combination of grass and paved area in the northeast corner of the western most building and flows to a catch basin within the center driveway which then enters the closed drainage system for the site. Subcatchment ES4 is a grassed yard to the southwest of the western most building and flows to a catch basin within the center driveway which then enters the closed drainage system for the site. Subcatchment ES4a is a small strip of land between an existing curb and the property line to the sothwest. Subcatchment ES5 is the eastern most portion of the paved parking to the south and west of the Central Fire Station which flows to a catch basin along the southern boundary of the site which then leaves the site to a private closed drainage system to the south. Subcatchments ES6, ES7 and ES8 flow along the frontage with Court Street which flows off site to the existing closed drainage system in Court Street. The final outflow from ES8 is Discharge Point 2 (DP2).

Watershed Basin ID	Basin Area (SF)	Tc (MIN)	CN	10-Year Runoff (CFS)	50-Year Runoff (CFS)	Design Point
ES1	8,698	2.8	87	0.80	1.32	DP1
ES1a	667	5.0	61	0.02	0.05	DP5
ES2	32,053	2.5	97	3.49	5.35	DP1
ES2a	196	5.0	98	0.02	0.03	DP1
ES3	2,371	5.0	68	0.11	0.24	DP1
ES4	2,604	5.0	61	0.08	0.21	DP1
ES4a	491	5.0	61	0.02	0.04	DP4
ES5	33,193	5.0	96	3.58	5.52	DP3
ES6	2,738	5.0	98	0.30	0.46	DP2
ES7	1,263	5.0	98	0.14	0.21	DP2
ES8	4,051	5.0	98	0.44	0.68	DP2

Additionally, eight off site subcatchments and associated closed drainage nodes are included in the model. These represent the off site drainage through 127 Parrot Avenue and along Parrot

Avenue to a point at the southwest corner of Rogers Road. This system was duplicated from a drainage analysis provided by Altus Engineering, Inc. dated July 16, 2012. This system was analyzed for existing and potential flooding as well as for development of a mitigation plan.

POST-DEVELOPMENT DRAINAGE

The proposed development has been designed to match the pre-development drainage patterns to the greatest extent feasible. In the post-development condition, the site has been analyzed as fourteen separate watersheds (PS1, PS1a, PS2, PS4, PS4a PS5, PS5a, PS5aa, PS5aaa, PS5b, PS5bb, PS6, PS7 and PS8 based on localized topography and discharge locations. Basins PS1a and PS4a are small relatively inconsequential areas that drain offsite. PS1 (driveway), PS2 (Existing Rooftop) and PS4 (driveway) are similar in size and area as in the existing condition and discharge to Discharge Point 3 (DP3). Basins PS5a (New Rooftop), PS5aa, PS5aaa (Both Landscaped Areas) all flow to Infiltration System # 1. This system consists of 23 StormTech Chambers (SC-740). Basins PS5b (New Rooftop) and PS5bb (Landscaped Area) flow to Infiltration System # 2. This system consists of 24 StormTech Chambers (SC-740). Outflows from System #1 and System #2 enter a combined system and discharge together with outflows from PS1, PS3 and PS4 to Discharge Point 3 (DP3). Basin PS5 is primarily runoff from the existing Fire Station and parking to the rear of the Fire Station. Basin PS5 flow to Discharge Point 1 (Combined Sewer). Flow from PS6, PS7 and PS8 all flow to a closed drainage system in Court Street and are quantified together at Discharge Point 2 (DP2).

Watershed Basin ID	Basin Area (SF)	Tc (MIN)	CN	10-Year Runoff (CFS)	50- Year Runoff (CFS)	Design Point
PS1	10,582	5.0	80	0.79	1.43	DP3
PS1a	667	5.0	61	0.02	0.05	DP5
PS2	10,300	5.0	98	1.13	1.73	DP3
PS4	7,681	5.0	71	0.41	0.84	DP3
PS4a	1,231	5.0	61	0.04	0.10	DP4
PS5	31,135	5.0	92	3.17	5.02	DP1A
PS5a	6,560	5.0	98	0.72	1.10	DP133
PS5aa	4,139	5.0	60	0.12	0.32	DP3
PS5aaa	1,478	5.0	50	0.02	0.07	DP3
PS5b	5,413	5.0	98	0.59	0.91	DP3
PS5bb	2,809	5.0	47	0.02	0.10	DP3

Table 2: Post-Development Watershed Basin Summary	Table 2: Post-Developm	nent Watershed	Basin Summarv
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PS6	2,751	5.0	98	0.30	0.46	DP2
PS7	1,263	5.0	98	0.14	0.21	DP2
PS8	4,051	5.0	98	0.44	0.68	DP2

Since the existing conditions at the site are predominantly impervious surface, and no treatment or dedicated infiltration systems currently exist for the site, providing the proposed treatment by means of the two StormTech Stormwater Chamber and infiltration systems represents a vast improvement on the water quality of the runoff.

Additionally, eight off site subcatchments and associated closed drainage nodes are included in the model. These represent the off site drainage through 127 Parrott Avenue and along Parrott Avenue to a point at the southwest corner of Rogers Road. This system was modelled from a drainage analysis provided by Altus Engineering, Inc. dated July 16, 2012. This system was analyzed for existing and potential flooding as well as for development of a mitigation plan.

The removal of flow from the combined sewer system created a new point discharge to a new catch basin (CB #5) located along the southern boundary of the site. This catch basin will outlet through a corridor presently used as a drainage swale and then to the closed drainage system within Parrot Avenue. Two pipe segment of the closed drainage system along Parrott Avenue will be upgraded from 12" to 24" pipe to accommodate the additional flow while improving the existing system hydraulics.

Table 3 shows a summary of the comparison between pre-developed flows and post-developed flows for the design point.

	Q10 (CFS)	Q50	(CFS)	
Design Point	Pre	Post	Pre	Post	Description
DP 1	4.9	0	7.7	0	Combined Sewer
DP1A	0.00	2.6	0.0	4.3	CB # 5 Southern Boundary of Site
DP2	1.0	1.0	1.5	1.5	Court Street Storm Drain
DP3	3.1	2.5	4.8	4.3	Storm Drain through 127 Parrot Ave
DP4	0.0	0.0	0.0	0.0	Western Property Line
DP5	0.0	0.0	0.1	0.1	Southwest Corner of Property

Table 3: Pre-Development to Post-Development Comparison

Note that the increase in run-off at Design Point 1A (DP1A) represents the removal of stormwater from the City sewer system. Improvements in downstream piping will accommodate the increase.

EROSION AND SEDIMENT CONTROL PRACTICES

The erosion potential for this site as it exists is low due to the existing vegetation and the built-up nature of the surrounding sites. During construction, the major potential for erosion is wind and stormwater runoff. The contractor will be required to inspect and maintain all necessary erosion control measures, as well as installing any additional measures as required. All erosion control practices shall conform to "The Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire." Some examples of erosion and sediment control measures to be utilized for this project during construction may include:

- Silt Soxx (or approved alternative) located at the toe of disturbed slopes
- Stabilized construction entrance at access point to the site
- Temporary mulching and seeding for disturbed areas
- Spraying water over disturbed areas to minimize wind erosion

After construction, permanent stabilization will be accomplished by permanent seeding, landscaping and surfacing the access drives and parking areas with either compacted gravel or asphalt paving.

CONCLUSION

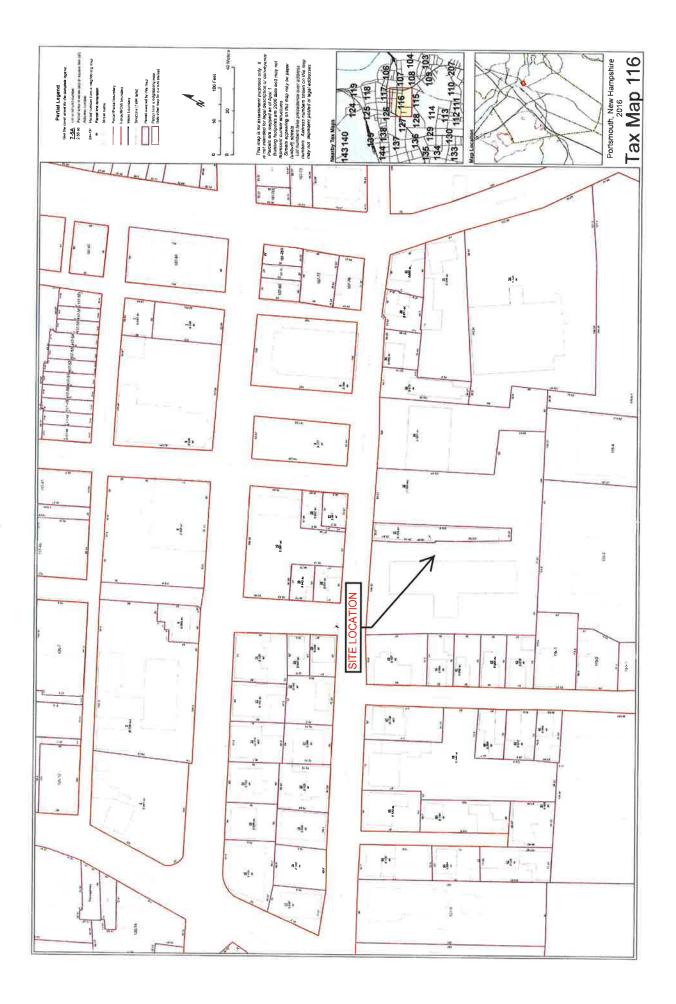
The proposed development has been designed to discharge less runoff than the pre-development runoff for the rain fall events that were analyzed. With the design of two Stormwater infiltration systems to slow the release of storm water, the post-development runoff rates are reduced to be below the pre-development runoff rates and will provide treatment. There is a new discharge due to the removal of stormwater from the combined sewer system. This point is located at the southern boundary of the site and discharges to the existing closed drainage system along Parrott Avenue. Off site improvements are being proposed to ensure that the closed drainage system along Parrott Ave. can handle the additional flow. These improvements include increasing the pipe size from 12" to 24" for the pipe segment across Rogers Road which is then directed to an existing swirl separation technology system before discharge to the Mill Pond. Erosion and sediment control practices will be implemented for both the temporary condition during construction and for final stabilization after construction. Therefore, there are no negative impacts to downstream receptors or adjacent properties anticipated as a result of this project. There is also no negative impact to the City of Portsmouth storm drainage system, rather a significant improvement to the Portsmouth sewer system.

REFERENCES

- 1. City of Portsmouth, NH. Site Plan Review Regulations amended December 18, 2014.
- 2. Comprehensive Environmental Inc. and New Hampshire Department of Environmental Services. *New Hampshire Stormwater Manual (Volumes 1, 2 and 3)*, December 2008 (Revision 1.0).
- Minnick, E.L. and H.T. Marshall. Stormwater Management and Erosion and Sediment Control Handbook for Urban and Developing Areas in New Hampshire, prepared by Rockingham County Conservation District, prepared for New Hampshire Department of Environmental Services, in cooperation with USDA Soil Conservation Service, August 1992.
- 4. HydroCAD Software Solution, LLC. *HydroCAD Stormwater Modeling System Version* 10.0 copyright 2013.

APPENDIX A VICINITY (TAX) MAP

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APPENDIX B

TABLES, CHARTS, ETC.

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Extreme Precipitation Tables Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing State Location Longitude Latitude	Yes New Hampshire 70.758 degrees West 43.074 degrees North
Elevation	0 feet
Date/Time	Fri, 08 Jun 2018 09:51:05 -0400

Extreme Precipitation Estimates

	1yr	2yr	5yr	10yr	25yr	50yr	100yr	200yr	500yr
10day	4.55	5.33	6.70	7.98	10.05	11.97	14.27	17.01	
7day	3.94	4.68	5.94	7.11	9.03	10.81	11.39 12.96	10.60 12.55 200yr 9.38 12.06 13.76 15.55	10.22 13.47 16.14 500yr 11.92 15.52 17.68 19.78 21.48
4day	3.22	3.94	5.04	6.09	7.81	9.43		13.76	17.68
2day	2.81	3.43	4.40	5.32	6.83	8.25	9.98	12.06	15.52
1day	2.35	2.84	3.60	4.31	5.46	6.54	7.83	9.38	11.92
	1yr	2yr	5yr	10yr	25yr	50yr	100yr	200yr	500yr
48hr	2.92	3.57	4.58	5.53	7.10	8.58	10.38	12.55	16.14
24hr	2.66	3.21	4.07	4.86	6.17	7.39	8.85		13.47
12hr	2.03	2.49	3.14	3.75	4.74	5.66	6.77	8.08	10.22
6hr	1.56	1.94	1.89 2.43	2.23 2.89	3.63	4.33	5.16	6.14	7.71
r 3hr	8 1.21	8 1.52		3 2.23	1.53 2.14 2.78 3.63	1.79 2.53 3.29 4.33	2.98 3.91	200yr 2.44 3.52 4.62 6.14	500yr 3.01 4.39 5.78 7.71
1hr 2hr	70 0.98	0.88 1.18	1.08 1.47	1.25 1.73	53 2.1	79 2.5	99 2.9	44 3.5	01 4.3
巪	1yr 0.70			10yr 1.:	25yr 1.:	50yr 1.	100yr 2.09	br 2.4)yr 3.(
	<u>1</u>	2yr	5yr	10	25		100	200	500
120min	1.04	1.30	1.61	1.89	2.34	2.76	3.26	3.84	4.78
60min	0.81	1.02	1.25	1.45	1.78	2.08	2.42	2.83	3.49
30min	0.65	0.81	0.98	1.12	1.34	1.54	1.77	2.05	2.49
15min 30min 60min	0.50	0.62	0.73	0.82	0.97	1.10	1.25	1.43	1.72
10min	0.40	0.50	0.58	0.65	0.76	0.86	0.97	1.10	1.32
Smin	0.26	0.32	0.37	0.41			0.60		0.80
	1yr	2yr	Syr	10yr	25yr 0.48	50yr 0.54	100yr	200yr 0.68	500yr 0.80

Lower Confidence Limits

imin	-	5min 10min	15min	15min 30min	60min	60min 120min		1hr	2hr	3hr	6hr	1hr 2hr 3hr 6hr 12hr 24hr 48hr	24hr	48hr		1day	2day	1day 2day 4day 7day		10day	
0.23	-	0.23 0.36	0.44	0.59	0.72	0.88	1yr	0.63	0.63 0.86 0.93 1.33	0.93	1.33	1.69 2.24	2.24	2.49	1yr	1.98	2.39	2.87	3.19	3.90	1yr
0.31	1	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.82	0.86 1.16 1.37 1.82 2.34 3.06 3.45	3.06	3.45	2yr	2.71	3.32	3.82	4.55	5.09	2yr
0.3	5	0.35 0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.12 2.73	2.73	3.78	4.19	5yr	3.35	4.03	4.72	5.53	6.24	5yr
0.3	6	10yr 0.39 0.59	0.73	1.03	1.33	1.60	10yr	1.14	1.56	1.80	2.39	1.14 1.56 1.80 2.39 3.05 4.37 4.85	4.37		10yr	3.87	4.67	10yr 3.87 4.67 5.43 6.41	6.41	7.19	10yr

Extreme Precipitation Tables: 43.074°N, 70.758°W

25yr 0.444 0.67 0.83 1. 50yr 0.48 0.73 0.91 1. 100yr 0.54 0.81 1.01 1. 200yr 0.59 0.89 1.13 1.	1.19		UTWINT I UTWING UTWING UTWICT UTWINT UTWIC	Thr	Zhr .	3hr 6	Shr 1	2hr 2	1hr 2hr 3hr 6hr 12hr 24hr 48hr	Shr		1day	2day	1day 2day 4day 7day 10day	7day	10day	
0.91 1.01 1.13	, ,	1.56 1.90	0 25yr		1.35 1.86 2.10 2.75 3.53 4.73 5.88	2.102	.75 3	1.53 4	1.73	-	25yr 4.19 5.65	4.19	5.65	6.64 7.78		8.67	25yr
1.01 1.13	1.31	1.76 2.17	7 50yr	1.52	1.52 2.12 2.35 3.06 3.92 5.35 6.78	2.35 3	.06 3	.92 5	.35		50yr 4.73 6.52	4.73		7.71	9.03	9.03 10.00	50yr
1.13	1.46	2.01 2.47		. 1.73	100yr 1.73 2.41 2.62 3.40 4.33 6.02 7.82	2.62 3	.40 4	1.33 6	5.02	7.82	100yr 5.32 7.52	5.32	7.52	8.95	10.49	8.95 10.49 11.55 100yr	100yr
-	1.63	2.27 2.81	31 200yr	. 1.96	2.75 2	2.93 3	.77 4	4.77 6	5.75	0.02	:00yr	5.97	8.68	10.38	12.20	1.96 2.75 2.93 3.77 4.77 6.75 9.02 2.00yr 5.97 8.68 10.38 12.20 13.35 200yr	200yr
500yr 0.68 1.02 1.31 1.90 2.71	1.90	2.71 3.36		• 2.33	3.28 3	3.41 4	.30 5	.43 7	7.86 1	0.89	00yr	6.95	10.47	12.63	14.92	500yr 2.33 3.28 3.41 4.30 5.43 7.86 10.89 500yr 6.95 10.47 12.63 14.92 16.17 500yr	500yr

Upper Confidence Limits

bher commence runns	5)	Inna																			
	5min	10min	15min	30min	60min	5min 10min 15min 30min 60min 120min		1hr	1hr 2hr 3hr		6hr	6hr 12hr 24hr		48hi		1 day	2day	4day	7day	10day	
1yr	0.28	0.44	0.54	0.72	0.89	1.08	1yr	0.77	0.77 1.06 1.26		1.74	2.20	2.98	3.17	1yr	2.64	3.05	3.58	4.37	5.04	1yr
2yr	0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	0.92 1.24 1.48		1.96	2.52	3.42	3.71	2yr	3.03	3.56	4.09	4.84	5.63	2yr
5yr	0.40	0.62	0.77	1.05	1.34	1.62	5yr	1.15	1.15 1.59 1.89 2.54	89	2.54	3.25	4.34	4.97	5yr	3.84	4.78	4.78 5.38 6.38	6.38	7.16	Syr
10yr	10yr 0.47	0.72	0.89	1.25	1.61	1.98	10yr	1.39	1.39 1.93 2.28	_	3.11	3.96	5.34	6.21	10yr	4.72	5.97	6.83	7.85	8.76	10yr
25yr	25yr 0.58	0.88	1.09	1.56	2.05	2.57	25yr	1.77	1.77 2.52 2.96 4.08	.96		5.16 7.76	7.76	8.36	25yr	6.87	8.04	9.17	10.35	11.42	25yr
50yr	0.67	1.02	1.27	1.83	2.47	3.13	50yr	2.13	2.13 3.06 3.60	3.60	5.01	6.34	9.71	10.48	50yr	8.59		10.08 11.48 12.74	12.74	13.98	50yr
100yr	100yr 0.79	1.20	1.50	1.50 2.16 2.97	2.97	3.82	100yr 2.56 3.73 4.38	2.56	3.73 4	1.38	6.17	7.79	7.79 12.15 13.14	13.14	100yr 10.75 12.63 14.36 15.72	10.75	12.63	14.36	15.72	17.11	100yr
200yr 0.93	0.93	1.39	1.77	2.56	3.57	4.66	200yr	3.08	4.56 5	5.35	7.60	9.57	15.23	16.48	:00yr 3.08 4.56 5.35 7.60 9.57 15.23 16.48 200yr 13.48 15.85 18.00 19.38	13.48	15.85	18.00	19.38	20.94	200yr
500yr	1.15	1.71	2.20	3.20	4.55	6.06	500yr	3.93	5.92 6	5.94	10.05	12.62	500yr 3.93 5.92 6.94 10.05 12.62 20.58 22.27	22.27	500yr 18.21 21.41 24.26 25.55 27.37	18.21	21.41	24.26	25.55		500yr



SCS METHODS

Technical Release - 55 Urban Hydrology for Small Watersheds

TR-55 presents simplified procedures to calculate storm runoff volume, peak rate of discharge, partial hydrographs and storage volumes for water control structures. The procedures are applicable to small watersheds, especially urbanizing watersheds with time of concentration between 0.1 hours and 10.0 hours. TR-55 is an approximation of the more detailed TR-20 method and does not have TR-20's capability to flood route. The user should examine the sensitivity of the analysis being conducted to ensure that the degree of error is tolerable. TR-55 contains two methods, the Tabular Hydrograph method and the Graphical Peak Discharge method. The accuracy of both methods is comparable; they differ only in their output. Both methods are based on open and unconfined flow over land and in channels.

The TR-55 Tabular Method can develop partial composite flood hydrographs at any point in a watershed by dividing the watershed into homogeneous subareas. By doing this, the method can estimate runoff from a larger nonhomogeneous watershed. The method is especially applicable for estimating the effects of land use change in a portion of a watershed. It can also be used to estimate the effects of proposed structures. The TR-55 Graphical Peak Discharge method calculates peak discharge using an assumed unit hydrograph and a thorough, but rapid, evaluation of the soils, slope, and surface cover characteristics of the watershed. This method is recommended for use in the design of all erosion and sediment control measures and simple stormwater management practices. When more detail and accuracy are required or when an accurate simulation of natural conditions is required, one of the other appropriate methods should be used. The TR-55 Graphical Peak Discharge method is the method that is discussed in this manual.

SCS TR-55 Graphical Peak Discharge Method

The peak discharge equation used in this method is:

$$q_p = q_u A_m Q F_p$$

where:

 q_p is the peak discharge in cubic feet per second (cfs).

 q_{ij} is the unit peak discharge in cubic feet per second per square mile per inch of runoff (csm/in).

 A_m is the drainage area in square miles.

Q is the runoff from the watershed in inches.

 F_p is a pond and swamp adjustment factor that can be applied for ponds or swamps that are spread throughout the watershed and not in the time of concentration flow path.

Technical Release-20 Computer Program for Project Formulation Hydrology

The TR-20 computer program assists the engineer in hydrologic evaluation of flood events for use in analysis of water resource projects. The program is a single event model which computes direct runoff resulting from any natural or synthetic rainstorm. It develops flood hydrographs from runoff and routes the flow through stream channels and reservoirs. It combines the routed hydrograph with those from tributaries and computes the peak discharges, their times of occurrence and the water surface elevations at any desired cross section or structure. The program provides for the analysis of up to nine different rainstorm distributions over a watershed under various combinations of land treatment. The analysis can be performed on as many as 200 reaches and 99 structures in any one continuous run. The procedure should probably not be used for subarea drainage areas less than 5 acres nor more than 20 square miles.

Input Data Required

The following information is required to use TR-20:

Drainage Area - The drainage area of each subwatershed in square miles.

Runoff Curve Number - A factor that relates mass rainfall to mass runoff. It is based on soil characteristics, cover type, and land treatment. Tables 6-4.1 - 6-4.3 provides runoff curve numbers for urban areas and agricultural areas.

Time of Concentration - The time which would be required for the surface runoff from the hydraulically most remote part of the drainage area to reach the point being evaluated. A more detailed discussion of time of concentration is found later in this chapter.

Reach Length - The length of the stream or valley in feet selected for generally constant hydraulic characteristics for use in the study. A watershed may have several reaches in the flow path.

Cross Section Information - This information consists of either surveyed valley and channel sections with appropriate Manning's "n" values or "x" and "m" discharge coefficient values obtained from nomographs in the TR-20 documentation for the valley and channel reach.

Rainfall Data - The average depth, in inches, of rainfall occurring over a watershed or subwatershed for a given design frequency and duration storm event.

Structural Data - Information on any culverts, bridges, or reservoirs in the watershed that includes elevations, discharges, and storage behind the structures.

Output Data

The type and amount of output can be controlled by options within the program. In general the output data will provide estimates of peak flow, hydrographs, peak times, runoff volumes, and water surface elevations at any location within the watershed.

Runoff Curve Number (RCN)

The runoff curve number is a factor that relates mass rainfall to mass runoff. It is based on soil characteristics, cover type, hydrologic condition, and land treatment. Tables 6-4.1 through 6-4.3 provide runoff curve numbers for urban areas, cultivated agricultural areas, and other agricultural areas for various hydrologic conditions

Cover type relates to the kind of cover found on the soil such as vegetation, bare soil, and impervious surfaces such as parking areas, roofs, streets, and roads.

Hydrologic condition indicates the effects of cover type and treatment on infiltration and runoff rates. It is generally estimated from the density of plant and crop residue on the area. Good hydrologic condition indicates that the soil usually has low runoff potential for that specific hydrologic soil group, cover type and treatment. Some factors to consider in estimating the effect of cover on infiltration and runoff are: canopy or density of leaves, amount of year-round cover, amount of grass or close-seeded legumes in a rotation, percent of residue cover, and the degree of surface roughness.

Treatment is a cover type modifier used to describe the management of cultivated agricultural lands. It includes mechanical practices such as contouring and terracing, and management practices, such as crop rotations and reduced or no tillage.

Use for the design of temporary measures during grading and construction. Impervious area percent for urban areas under development vary considerably. The user will determine the percent impervious. Then using the newly graded area RCM and Table 6-4, the composite RCM can be computed for any degree of development. CURVE NUMBERS FOR HYDROLOGIC SOIL GROUP For land uses with impervious areas, curve numbers are computed assuming that 100% of runoff from impervious areas is directly connected to the drainage system. Pervious areas (lawn) are considered to be equivalent to lawns in good condition and the impervious areas have an RCN of 98. 82 28 98 86585 52 8 8828283 26 Δ 223 98 98 89 92 87 92 \$5 8 د 85822 5 362 8 6 8 8 8 88 õ 8 た て み ぬ む ä 69 49 M 86 8228 85 2 22223 < 4 Average percent² împervious area² むえ ŝ 12 23 33 Lawns, open spaces, parks, golf courses, cemeteries, etc. good condition; grass cover on 75% or more of the area fair condition; grass cover on 50% to 75% of the area poor condition; grass cover on 50% or less of the area FULLY DEVELOPED URBAN AREAS¹ (Vegetation Established) DEVELOPING URBAN AREAS³ (No vegetation Established) Cover type and hydrologic condition Paved parking lots, roofs, driveways, etc. Row houses, town houses, and residential with lot sizes 1/8 acre or less COVER DESCRIPTION Streets and roads; paved with curbs and storm sewers Commercial and business areas Industrial districts Includes paved streets. paved with open ditches Average Lot size Newly graded area 1/4 acre 1/3 acre 1/2 acre acre 2 acre Resideritial gravel ູ m

(Average Watershed Condition)

RUNOFF CURVE NUMBIERS

6-4.1

TABLE

Source: USDA Soil Conservation Service

70	COVER DESCRIPTION	Hydrologic _k	CURVE NUP	CURVE NUMBERS FOR HYDROLOGIC SOIL	DROLOGIC	SOIL GROUP
er type and h AGRICULTURAL	cover type and hydrologic condition <u>TED AGRICULTURAL LAND</u>	condition ⁴	•	•	υ	-
800	Bare soil Crop residue cover (CR) CR	poor	287	8 8 8 8 8	90 88	328
	Straight row (SR) SR & CR SR & CR SR & CR Contoured (C) C & CR C & CR Contoured & Terraces (C&T) C&T & CR C&T & CR	9000 9000 9000 9000 9000 9000 9000	69235383882	52325555555555555555555555555555555555	88888888888888	28888888888888888888888888888888888888
	4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	9000 9000 9000 9000 9000 9000 9000 900	&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&&	************	************	88 28 28 28 28 28 28 28 28 28 28 28 28 2
ເຮັ ¹ ເດ ຮູ ຮູ		good good good good	<u>ኇቘ</u> ዿ ጜ ፚዸ	F56866	85 83 78 80 78 80 78	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
일 관 원 명 분	For conservation tillage poor hydrologic condition, 5 to 20 pe 750 #/acre row crops or 300#/acre small grain). For conservation tillage good hydrologic condition, more than (greater than 750 #/acre row crops or 300 #/acre small grain). Close-drilled or broadcast.	ion, 5 to 20 percent of the surface is covered with residue (less than on, more than 20 percent of the surface is covered with residue small grain).	f the surface is o ant of the surface	overed with is covered	residue (les with residue	(less than idue

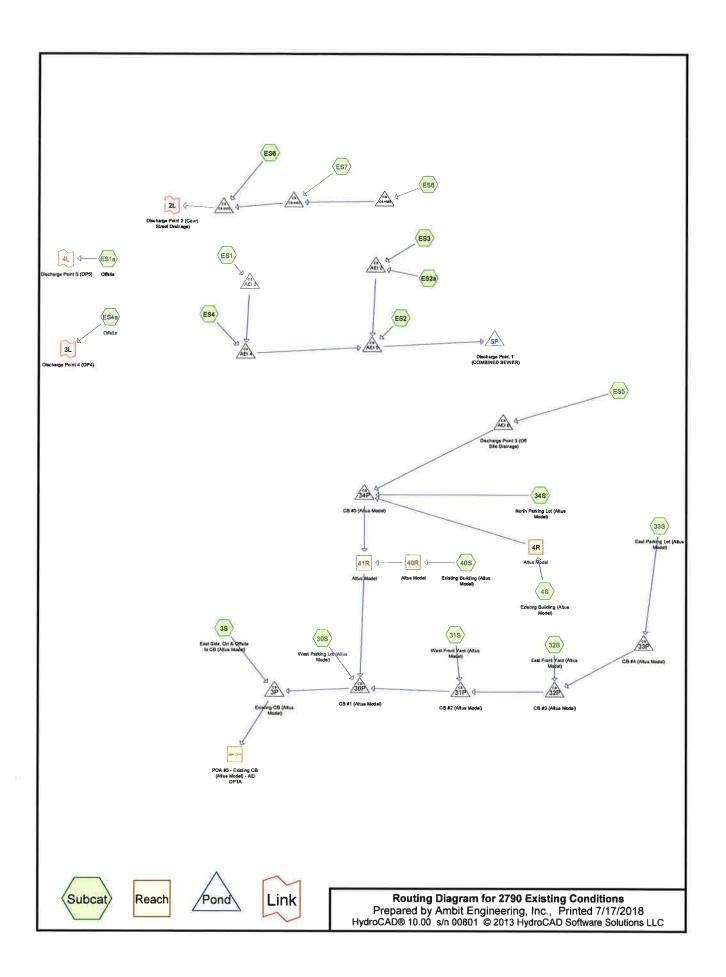
Source: USDA Soil Conservation Service

TABLE 6-4.3 -- RUNOFF CURVE NUMBERS (Average Watershed Condition)

		CURVE NUMBERS FOR HYDROLOGIC SOIL GROUP	FOIL HYDR	ologic so	IL GROUP
Cover type and hydrologic condition	Hydrouogac condition ⁶	*	æ	IJ	٩
NON-CULTIVATED AGRICULTURAL LAND					
Pasture, grassland, or range - continuous forage			Ŗ	2	ŝ
	pour fair	83	29	8 R	20 77
	DCOD	ŝ	61	2	58
Meadow - continuous grass, protected from grazing and generally mowed for hay	ł	30	58	7	82
Woods-urass combination (orchard or tree farm)	1000	22	ĸ	87	Rc
	fair	54 M	; ? 8	122	388
		ł	2	!	2
Brush ~ brush-weed-grass mixture with brush the major element	poor	48 75	67 54	2	8
	good	22	8 8 9	2 S	:2
Noods	poor. fair	45 36	% 9	κ	in c
	Boord	30	5	22	4
Farmsteads - buildings, lanes, driveways, and surrounding lots	••••	59	74	82	88
6. Pour hydrologic condition has less than 50 percent ground cover density. Fair hydrologic condition has between 50 and 75 percent ground cover density. Good hydrologic condition has more than 75 percent ground cover density.	cent ground cover density. 5 percent ground cover density. cent ground cover density.			a	

Source: USDA Soil Conservation Service

APPENDIX C HYDROCAD DRAINAGE ANALYSIS CALCULATIONS



2790 Existing Conditions Prepared by Ambit Engineering, Inc. HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Printed 7/17/2018 Page 2

_	Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
	1	4R	8.38	7.28	110.0	0.0100	0.012	8.0	0.0	0.0
	2	40R	6.82	6.62	10.0	0.0200	0.012	8.0	0.0	0.0
	3	41R	6.45	6.21	81.0	0.0030	0.012	12.0	0.0	0.0
	4	3P	5.76	5.21	55.0	0.0100	0.012	12.0	0.0	0.0
	5	30P	6.11	5.86	82.0	0.0030	0.013	12.0	0.0	0.0
	6	31P	6.33	6.21	40.0	0.0030	0.012	12.0	0.0	0.0
	7	32P	6.71	6.43	92.0	0.0030	0.012	12.0	0.0	0.0
	ô	33P	6.96	0.01	50.0	0.0030	0.012	12.0	0.0	0.0
	9	34P	5.83	5.58	85.0	0.0029	0.013	12.0	0.0	0.0
	10	AEI 2	9.42	8.55	102.8	0.0085	0.010	6.0	0.0	0.0
	11	AEI 3	8.90	8.84	37.5	0.0016	0.013	10.0	0.0	0.0
	12	AEI 4	8.69	8.15	92.4	0.0058	0.013	10.0	0.0	0.0
	13	AEI 5	7.90	7.40	58.5	0.0085	0.013	10.0	0.0	0.0
	14	AEI 6	6.77	5.88	96.0	0.0093	0.013	12.0	0.0	0.0
	15	CB 4433	14.38	13.99	121.0	0.0032	0.013	24.0	0.0	0.0
	16	CB 4435	13.99	15.41	100.0	-0.0142	0.013	24.0	0.0	0.0
	17	CB 4560	14.92	14,38	42,8	0.0126	0.013	24.0	Û .Ū	0 .0

Pipe Listing (selected nodes)

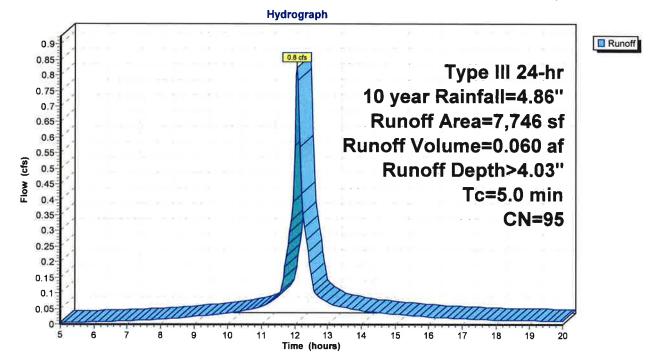
Summary for Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)

Runoff = 0.8 cfs @ 12.07 hrs, Volume= 0.060 af, Depth> 4.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN E	Description						
*		7,746	95							
-		7,746	1	100.00% Pervious Area						
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	5.0					Direct Entry,				

Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)



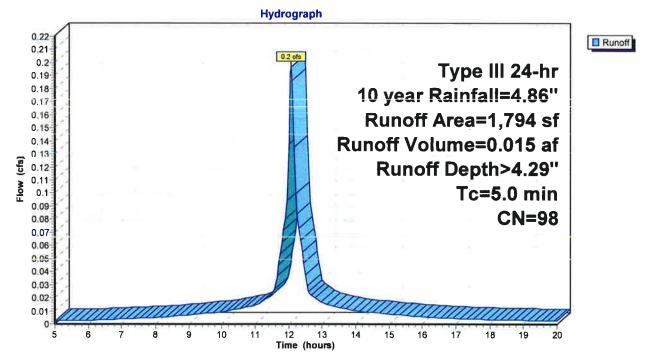
Summary for Subcatchment 4S: Existing Building (Altus Model)

Runoff = 0.2 cfs @ 12.07 hrs, Volume= 0.015 af, Depth> 4.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Are	a (sf)	CN [Description						
*		1,794	98							
		1,794	100.00% Impervious Area							
	Tc I in)	_ength (f ee t)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	5.0					Direct Entry,				

Subcatchment 4S: Existing Building (Altus Model)

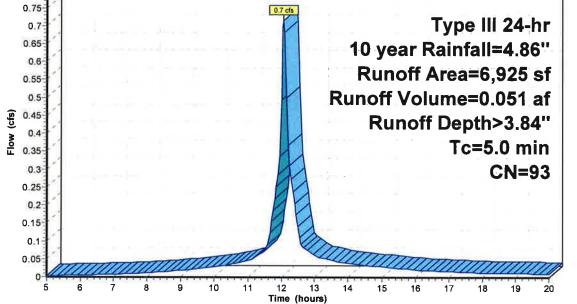


Summary for Subcatchment 30S: West Parking Lot (Altus Model)

Runoff = 0.7 cfs @ 12.07 hrs, Volume= 0.051 af, Depth> 3.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Area (sf)	CN I	Description				
*	6,925	93					
-	6,925		100.00% Pe	ervious Are	а		
To (min)		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description		
5.0)				Direct Entry,		
		Sul	bcatchme		•	Lot (Altus Model)	
	1			нуаго	graph		1 ⁷
	8						🛄 Runoff
0.7 0	7			0.7	cfs	Type III 24-hr	



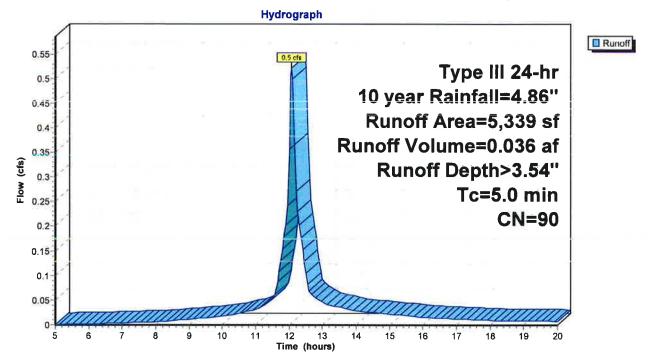
Summary for Subcatchment 31S: West Front Yard (Altus Model)

Runoff = 0.5 cfs @ 12.07 hrs, Volume= 0.036 af, Depth> 3.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

<i>F</i>	Area (sf)	CN E	Description			
*	5,339	90				
	5,339	a				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment 31S: West Front Yard (Altus Model)



Summary for Subcatchment 32S: East Front Yard (Altus Model)

Runoff = 0.8 cfs @ 12.07 hrs, Volume= 0.053 af, Depth> 3.74"

11

10

12

Time (hours)

14

13

15

16

17

18

19

20

0.25 0.2 0.15 0.1 0.05

5

6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Area (sf)	CN I	Description							
*	7,376	92								
	7,376		100.00% Pe	ervious Are	a					
(mi		Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
5	.0				Direct Entry,					
	Subcatchment 32S: East Front Yard (Altus Model)									
				Hydro	graph					
low (cfs)	0.8 0.75 0.7 0.65 0.6 0.55 0.5 0.45 0.4 0.35 0.3			0.8	Type III 24-hr 10 year Rainfall=4.86" Runoff Area=7,376 sf Runoff Volume=0.053 af Runoff Depth>3.74" Tc=5.0 min CN=92	Runoff				

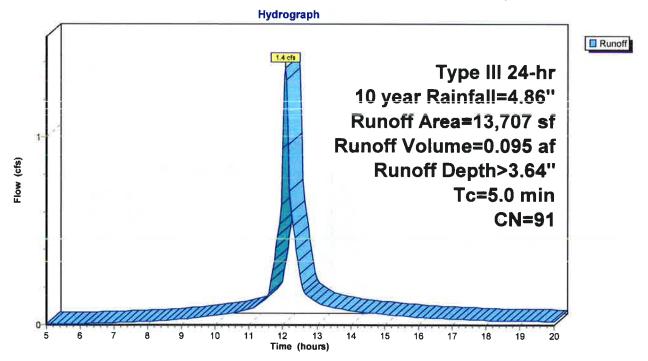
Summary for Subcatchment 33S: East Parking Lot (Altus Model)

Runoff = 1.4 cfs @ 12.07 hrs, Volume= 0.095 af, Depth> 3.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN E	Description			
*		13,707	91				
		13,707	1	00.00% P	ervious Are	28	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	5.0					Direct Entry,	

Subcatchment 33S: East Parking Lot (Altus Model)



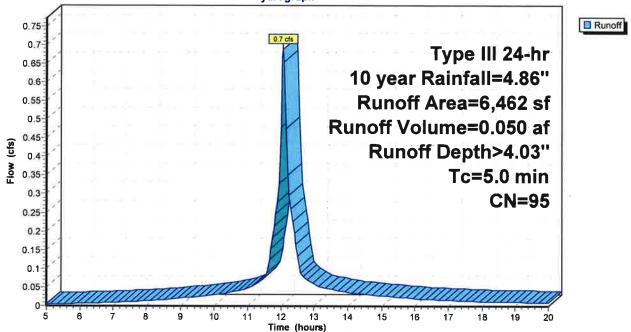
Summary for Subcatchment 34S: North Parking Lot (Altus Model)

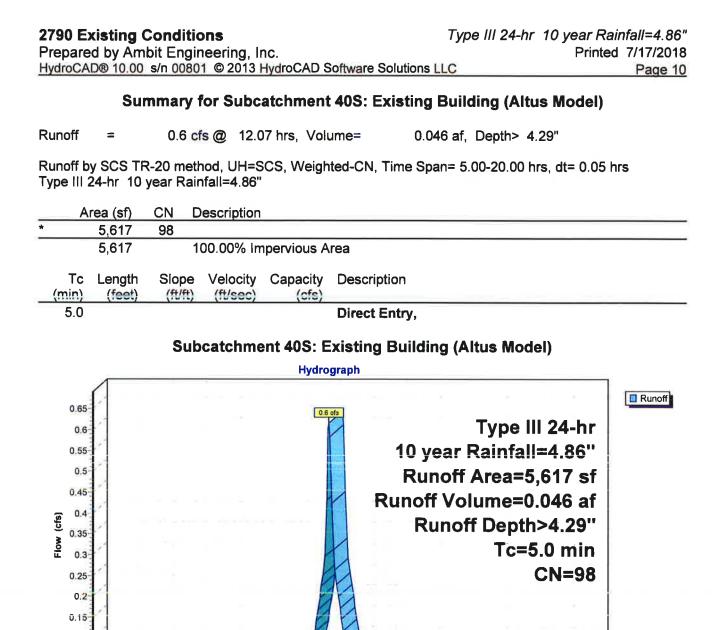
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Runoff 0.7 cfs @ 12.07 hrs, Volume= 0.050 af, Depth> 4.03" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN	Description	ĥ					
*		6,462	95							
	6,462 100.00% Pervious Area									
(Tc min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
	5.0					Direct Entry,				
Subcatchment 34S: North Parking Lot (Altus Model)										
Hydrograph										





Time (hours)

0.1 0.05

2790 Existing Conditions	Type III 24-hr	10 year Rainfall=4.86"
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HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LL	.C	Page 11

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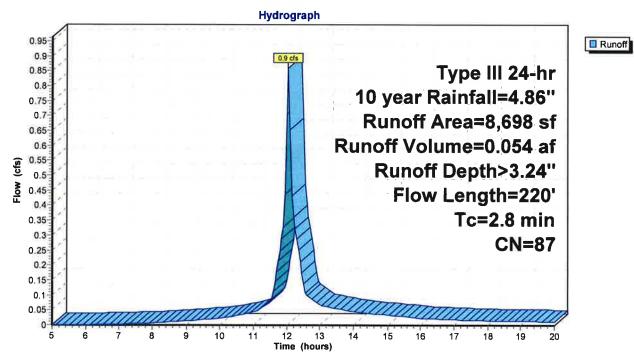
Summary for Subcatchment ES1:

Runoff 0.9 cfs @ 12.05 hrs, Volume= 0.054 af, Depth> 3.24" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN [Description							
		5,487	98 F	Paved park	ing, HSG B	3					
*		658	98 L	Jnconnecte	ed pavemer	nt, sidewalk, HSG B					
		2,553				ood, HSG B					
		8,698	87 V	Veighted A	verage						
		2,553		29.35% Pervious Area							
		6,145	7	70.65% Impervious Area							
		658		10.71% Unconnected							
	Тс	Length	Slope	Velocity	Capacity	Description					
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
17	2.1	84	0.0089	0.66		Shallow Concentrated Flow,					
						Short Grass Pasture Kv= 7.0 fps					
	0.7	136	0.0239	3.14		Shallow Concentrated Flow,					
-						Paved Kv= 20.3 fps					
	2.8	220	Total								

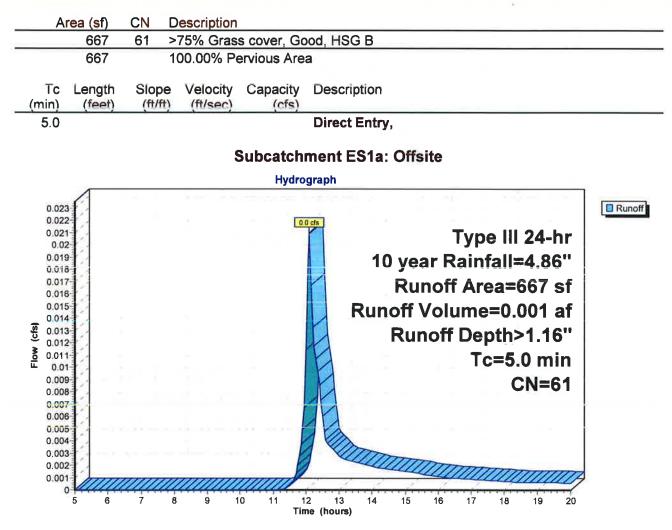
Subcatchment ES1:



Summary for Subcatchment ES1a: Offsite

Runoff = 0.0 cfs @ 12.09 hrs, Volume= 0.001 af, Depth> 1.16"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"



2790 Existing Conditions

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Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018 C Page 13

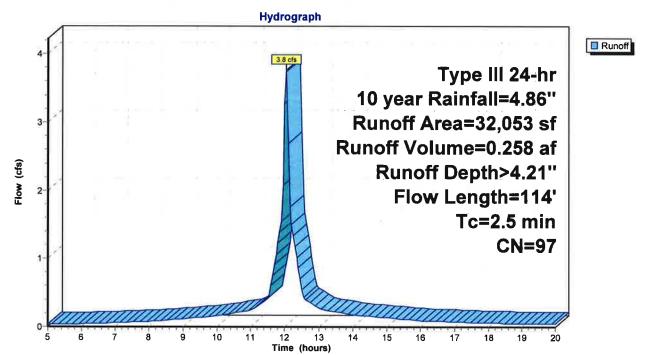
Summary for Subcatchment ES2:

Runoff = 3.8 cfs @ 12.04 hrs, Volume= 0.258 af, Depth> 4.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Area (sf)	CN	Description					
	10,300	98	Roofs, HSC	GВ				
	3,910	98	Roofs, HSC	ЭB				
	641	61	>75% Gras	s cover, Go	ood, HSG B			
*	480	98	Unconnecte	ed pavemei	nt,sidewalks, HSG	В		
	9,865	98	Paved park	king, HSG E	}			
*	6,857	98	Gravel surf	ace, HSG E	3			
	32,053	97	Weighted A	verage				
	641 2.00% Pervious Area							
	31,412		98.00% Im	oervious Ar	ea			
	480		1.53% Unc	onnected				
	Tc Length	Slope	e Velocity	Capacity	Description			
(m	in) (feet)	(ft/ft) (ft/sec)	(cfs)				
C).8 35	0.0071	1 0.74		Sheet Flow,			
					Smooth surfaces	n= 0.011	P2= 3.21"	
1	.7 79	0.0050	0.75		Sheet Flow,			
-					Smooth surfaces	n= 0.011	P2= 3.21"	
2	2.5 114	Total						

Subcatchment ES2:



			1 © 2013 I		Software Solution	ons LLC		- milea	Page 14
			Sum	nmary for	Subcatchn	nent ES2a:			
Runoff	=	0.0 c	fs @ 12.0	0 hrs, Volu	ume=	0.002 af, De	epth> 4.29"		
Runoff b	V SCS TI	R-20 met	hod. UH=S	CS. Weiah	ted-CN, Time	Span= 5 00-	20.00 hrs. dt=	: 0 05 hr	
			nfall=4.86"				20.00 1.00, 41	0.00 11	-
А	rea (sf)	CN E	escription						
	102			ing, HSG B					
	94				nt, sidewalk, ⊢	ISG B			
	196 196		Veighted A	verage pervious A	rea				
	94		7.96% Un						
Тс	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	Description				
0.1	27	0.0740	5.52			ncentrated F	low,		
					Paved Kv=	20.3 fps			
				Subca	tchment ES	32a:			
				Hydro	graph				
									Runoff
0.02	1.12			0.0	cfs	_			
0.02	4						ype III 24-		
0.02	1			-	10) year Ra	infall=4.8	6"	
0.0	1					Runoff /	Area=196	sf	
0.01	1			-	Run	off Volur	ne=0.002	af	
(s) 0.01	1					Runoff [)epth>4.2	9"	
0.01 (cts)	1 34						Length=2		
_	1	2		k	1		e=0.0740		
0.0 0.00	1 22			·		Siop			20
0.00	12			E	12		Tc=0.1 m		
0.00				P	A		CN=	98	
0.00					Tim	1	12	11	
0.00	VIIII	////////				11111111		1111	

2790 Existing Conditions Prepared by Ambit Engineering, Inc.

12 13 Time (hours)

Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018

2790 Existing Conditions	Type III 24-hr 10 year Rainfall=4.86"
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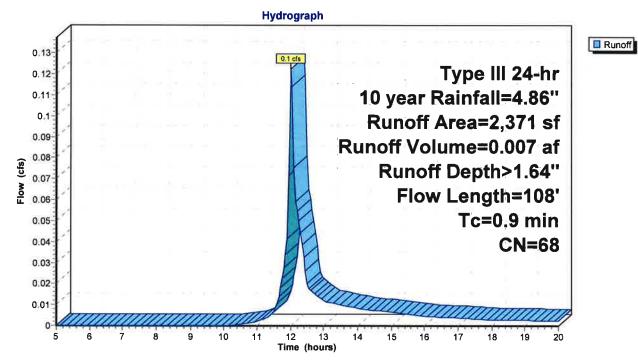
Summary for Subcatchment ES3:

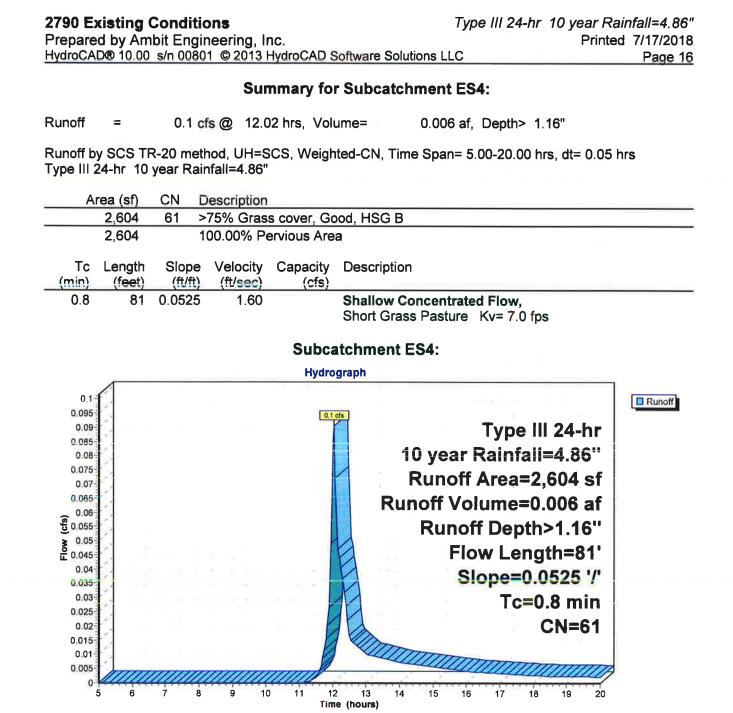
Runoff = 0.1 cfs @ 12.02 hrs, Volume= 0.007 af, Depth> 1.64"

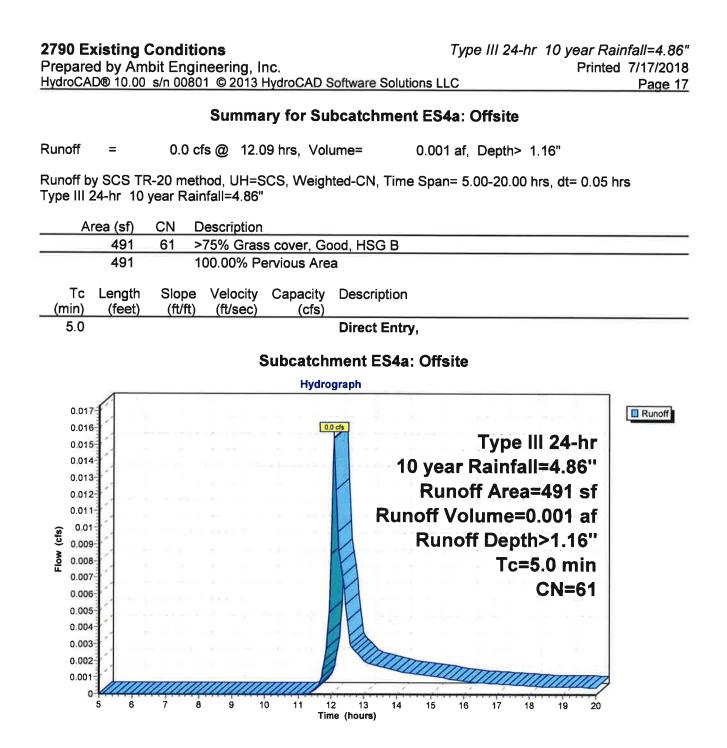
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN [Description						
*		414	98 (98 Gravel surface, HSG B						
*		33	98 l	Jnconnecte	ed pavemer	nt, sidewalk, HSG B				
-		1,924	61 >							
		2,371	68 V							
		1,924	81.15% Pervious Area							
		447	1	8.85% Imp	pervious Ar	ea				
		33	7	.38% Unc	onnected					
	Тc	Length	Slope	Velocity	Capacity	Description				
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.2	58	0.0819	5.81		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	0.7	50	0.0300	1.21		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.9	108	Total							

Subcatchment ES3:







Summary for Subcatchment ES5:

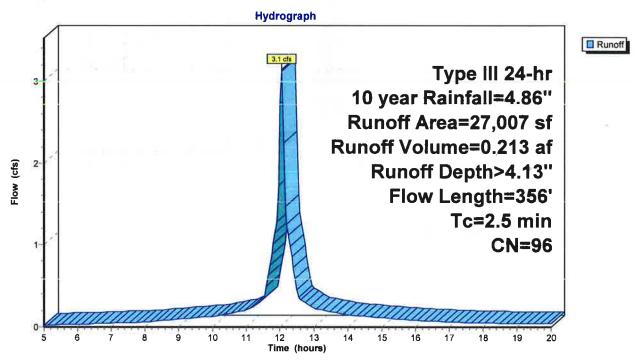
Runoff = 3.1 cfs @ 12.04 hrs, Volume= 0.213 af, Depth> 4.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Area (sf)	CN I	Description					
	23,335	98	98 Paved parking, HSG B					
*	1,456	98	Jnconnecte	ed pavemer	nt, sidewalk, HSG B			
	1,658	61 3	>75% Gras	s cover, Go	bod, HSG B			
*	558	98 0	Gravel surf	ace, HSG E	3			
	27,007	96	Neighted A	verage				
	1,658		6.14% Pervious Area					
	25,349	9	93.86% Imp	pervious Ar	ea			
	1,456		5.74% Unc					
т	c Length	Slope	Velocity	Capacity	Description			
(mir	n) (feet)	(ft/ft)	(ft/sec)	(cfs)				
1.	3 56	0.0050	0.70		Sheet Flow,			
					Smooth surfaces n= 0.011 P2= 3.21"			
1.	2 300	0.0417	4.15		Shallow Concentrated Flow,			
					Paved Kv= 20.3 fps			
2	5 256	Tatal						

2.5 356 Total

Subcatchment ES5:



2790 Existing ConditionsType III 24-hr 10 year Rainfall=4.86"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 19

Summary for Subcatchment ES6:

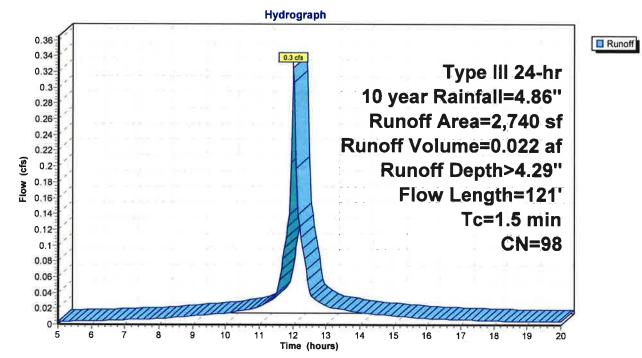
Runoff = 0.3 cfs @ 12.02 hrs, Volume= 0.022 af, Depth> 4.29"

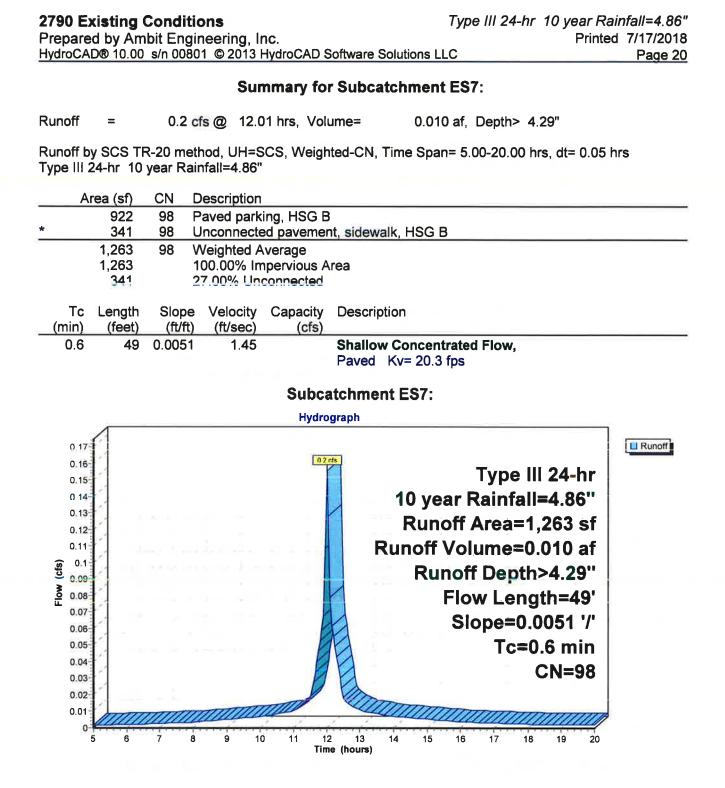
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN	Description			
		2,330	98				
- *		410	98	Jnconnecte	ed pavemer	nt, sidewalk, HSG B	
		2,740	98				
		2,740		100.00% Impervious Area			
		410		14.96% Un	connected		
	Тс	Length	Slope		Capacity	Description	
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	0.6	26	0.0096	0.69		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.9	95	0.0078	1.79		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	15	121	Total				

1.5 121 Total

Subcatchment ES6:





2790 Existing Conditions	Type III 24-hr 10 year Rainfall=4.86"
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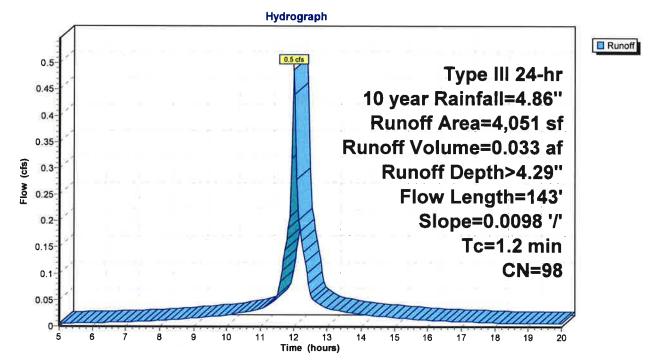
Summary for Subcatchment ES8:

Runoff = 0.5 cfs @ 12.02 hrs, Volume= 0.033 af, Depth> 4.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN (Description		
		2,607	98 F	Paved park	ing, HSG B	3
1		1,444	98 l	Jnconnecte	ed pavemer	nt,sidewalk, HSG B
		4,051	98 \	Neighted A	verage	
		4,051		100.00% Im	npervious A	vrea
		1,444	3	85.65% Un	connected	
	Тс	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.2	143	0.0098	2.01		Shallow Concentrated Flow, Paved Kv= 20.3 fps

Subcatchment ES8:



Summary for Reach 4R: Altus Model

 Inflow Area =
 0.041 ac,100.00% Impervious, Inflow Depth > 4.29" for 10 year event

 Inflow =
 0.2 cfs @ 12.07 hrs, Volume=
 0.015 af

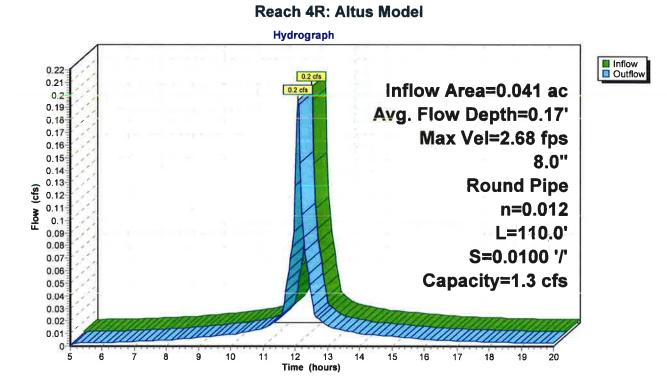
 Outflow =
 0.2 cfs @ 12.08 hrs, Volume=
 0.015 af, Atten= 1%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 2.68 fps, Min. Travel Time= 0.7 min Avg. Velocity = 1.02 fps, Avg. Travel Time= 1.8 min

Peak Storage= 8 cf @ 12.08 hrs Average Depth at Peak Storage= 0.17' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.3 cfs

8.0" Round Pipe n= 0.012 Length= 110.0' Slope= 0.0100 '/' Inlet Invert= 8.38', Outlet Invert= 7.28'





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Summary for Reach 40R: Altus Model

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth > 4.29" for 10 year event

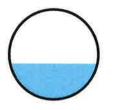
 Inflow =
 0.6 cfs @ 12.07 hrs, Volume=
 0.046 af

 Outflow =
 0.6 cfs @ 12.07 hrs, Volume=
 0.046 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 4.74 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.84 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 12.07 hrs Average Depth at Peak Storage= 0.27' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.9 cfs

8.0" Round Pipe n= 0.012 Length= 10.0' Slope= 0.0200 '/' Inlet Invert= 6.82', Outlet Invert= 6.62'



Hydrograph Inflow Outflow 0.65 Inflow Area=0.129 ac 0.6 ct 0.6 Avg. Flow Depth=0.27' 0.55 Max Vel=4.74 fps 0.5 8.0" 0.45 **Round Pipe** 0.4 Flow (cfs) 0.35 n=0.012 0.3 L=10.0' 0.25 S=0.0200 '/' 0.2 Capacity=1.9 cfs 0.15 0.1 0.05 0 10 12 16 17 18 11 13 14 15 19 20 Time (hours)

Reach 40R: Altus Model

Summary for Reach 41R: Altus Model

 Inflow Area =
 0.938 ac, 80.14% Impervious, Inflow Depth > 4.14" for 10 year event

 Inflow =
 4.6 cfs @
 12.05 hrs, Volume=
 0.324 af

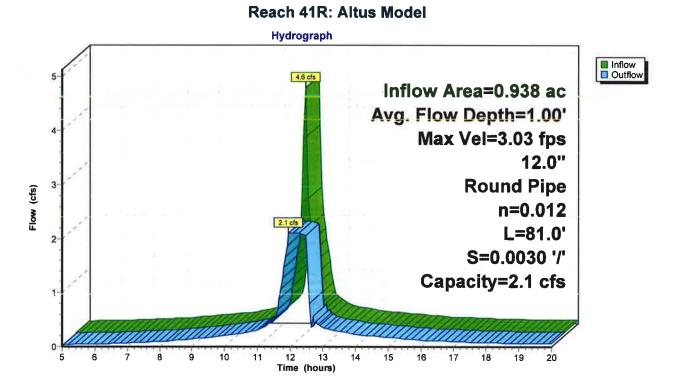
 Outflow =
 2.1 cfs @
 11.95 hrs, Volume=
 0.324 af, Atten= 54%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 3.03 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.56 fps, Avg. Travel Time= 0.9 min

Peak Storage= 64 cf @ 11.95 hrs Average Depth at Peak Storage= 1.00' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.1 cfs

12.0" Round Pipe n= 0.012 Length= 81.0' Slope= 0.0030 '/' Inlet Invert= 6.45', Outlet Invert= 6.21'



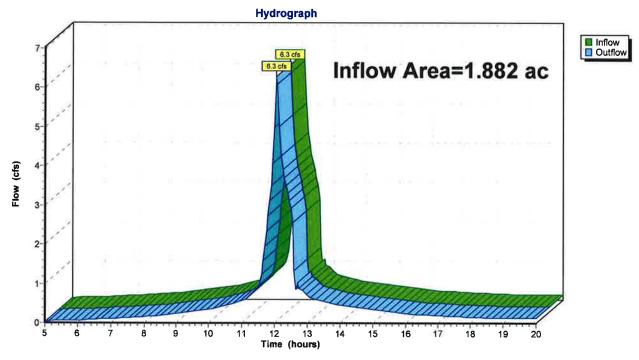


Summary for Reach 300R / DP1A: POA #3 - Existing CB (Altus Model) - AEI DP1A

Inflow Area =	1.882 ac, 39.96% Impervious,	Inflow Depth > 3.94" for 10 year event
Inflow =	6.3 cfs @ 12.07 hrs, Volume	e= 0.619 af
Outflow =	6.3 cfs @ 12.07 hrs, Volume	e= 0.619 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Reach 300R / DP1A: POA #3 - Existing CB (Altus Model) - AEI DP1A



Summary for Pond 3P: Existing CB (Altus Model)

 Inflow Area =
 1.882 ac, 39.96% Impervious, Inflow Depth > 3.94" for 10 year event

 Inflow =
 6.3 cfs @ 12.07 hrs, Volume=
 0.619 af

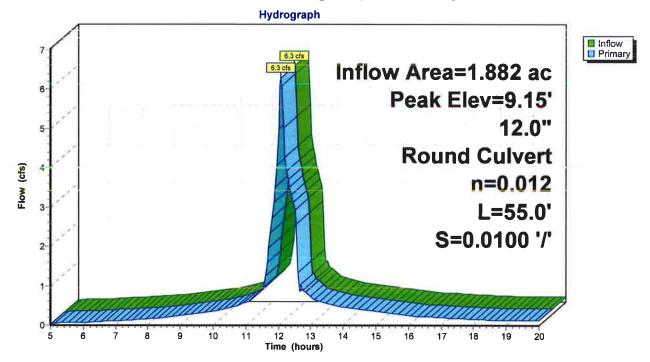
 Outflow =
 6.3 cfs @ 12.07 hrs, Volume=
 0.619 af, Atten= 0%, Lag= 0.0 min

 Primary =
 6.3 cfs @ 12.07 hrs, Volume=
 0.619 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 9.15' @ 12.07 hrs Flood Elev= 8.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	5.76'	12.0" Round Culvert L= 55.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.76' / 5.21' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=6.1 cfs @ 12.07 hrs HW=9.02' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 6.1 cfs @ 7.81 fps)

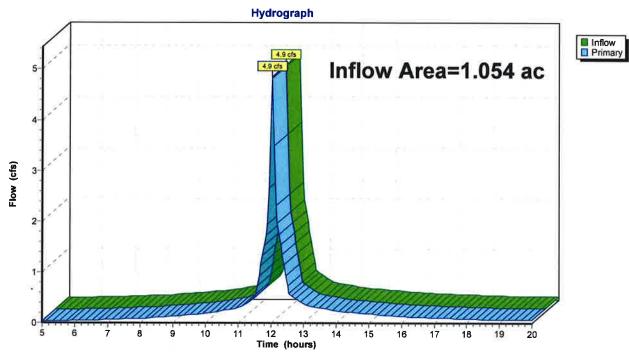


Pond 3P: Existing CB (Altus Model)

Summary for Pond 5P: Discharge Point 1 (COMBINED SEWER)

Inflow Are	a =	1.054 ac, 83.18% Impervious, Inflow Depth > 3.72" for 10 year event	
Inflow	=	4.9 cfs @ 12.04 hrs, Volume= 0.327 af	
Primary	=	4.9 cfs @ 12.04 hrs, Volume= 0.327 af, Atten= 0%, Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 5P: Discharge Point 1 (COMBINED SEWER)

Summary for Pond 30P: CB #1 (Altus Model)

 Inflow Area =
 1.704 ac, 44.13% Impervious, Inflow Depth > 3.94" for 10 year event

 Inflow =
 5.5 cfs @ 12.07 hrs, Volume=
 0.559 af

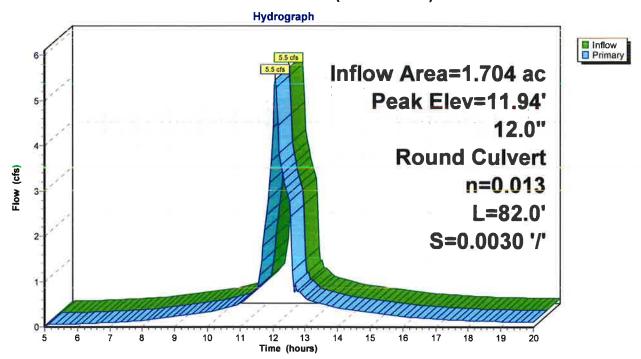
 Outflow =
 5.5 cfs @ 12.07 hrs, Volume=
 0.559 af, Atten= 0%, Lag= 0.0 min

 Primary =
 5.5 cfs @ 12.07 hrs, Volume=
 0.559 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 11.94' @ 12.10 hrs Flood Elev= 9.15'

Device	Routing	Invert	Outlet Devices
#1	Primary	6 11'	12.0" Round Culvert L= 82.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.11' / 5.86' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=4.8 cfs @ 12.07 hrs HW=11.42' TW=9.02' (Dynamic Tailwater) -1=Culvert (Outlet Controls 4.8 cfs @ 6.16 fps)



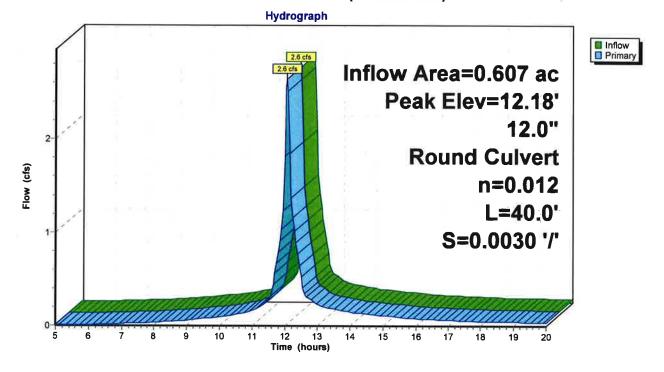
Pond 30P: CB #1 (Altus Model)

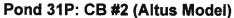
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Summary for Pond 31P: CB #2 (Altus Model)

Inflow A			00% Impervious, Inflow Depth > 3.64" for 10 year event			
Inflow	=	2.6 cfs @ 1	2.07 hrs, Volume= 0.184 af			
Outflow	=	2.6 cfs @ 1	2.07 hrs, Volume= 0.184 af, Atten= 0%, Lag= 0.0 min			
Primary	=	2.6 cfs @ 1	2.07 hrs, Volume= 0.184 af			
Peak Ele	Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 12.18' @ 12.15 hrs Flood Elev= 9.15'					
Device	Routing	Invert	Outlet Devices			
#1	Primary	6.33'	12.0" Round Culvert L= 40.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.33' / 6.21' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf			

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=10.59' TW=11.43' (Dynamic Tailwater) **1=Culvert** (Controls 0.0 cfs)





Type III 24-hr 10 year Rainfall=4.86" 2790 Existing Conditions Prepared by Ambit Engineering, Inc. Printed 7/17/2018 HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Summary for Pond 32P: CB #3 (Altus Model)

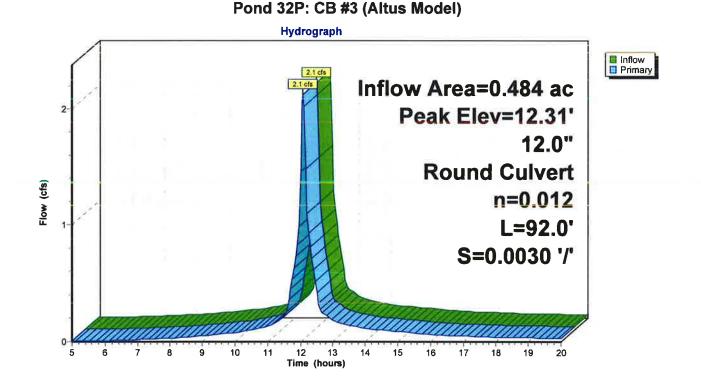
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Inflow Area = 0.484 ac, 0.00% Impervious, Inflow Depth > 3.67" for 10 year event Inflow 2.1 cfs @ 12.07 hrs, Volume= 0.148 af = Outflow 2.1 cfs @ 12.07 hrs, Volume= 0.148 af, Atten= 0%, Lag= 0.0 min = 2.1 cfs @ 12.07 hrs, Volume= 0.148 af Primary Ξ

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 12.31' @ 12.19 hrs Flood Elev= 9.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	6 71'	12.0'' Round Culvert L= 92.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.71' / 6.43' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=9.67' TW=10.59' (Dynamic Tailwater) 1=Cuivert (Controls 0.0 cfs)



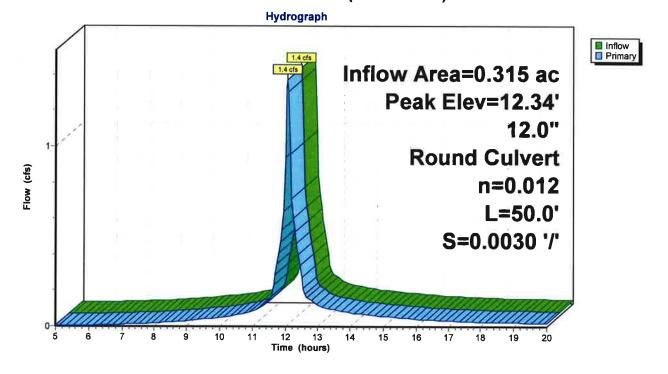
2790 Existing Conditions Type III 24-hr 10 year Rainfall=4.86" Prepared by Ambit Engineering, Inc. Printed 7/17/2018 HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Summary for Pond 33P: CB #4 (Altus Model)

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Inflow Area = 0.315 ac. 0.00% Impervious, Inflow Depth > 3.64" for 10 year event Inflow 1.4 cfs @ 12.07 hrs, Volume= = 0.095 af Outflow 1.4 cfs @ 12.07 hrs, Volume= = 0.095 af, Atten= 0%, Lag= 0.0 min Primary 1.4 cfs @ 12.07 hrs, Volume= = 0.095 af Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 12.34' @ 12.24 hrs Flood Elev= 9.50' Device Routing Invert Outlet Devices #1 Primary 6.96' 12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.96' / 6.81' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=8.81' TW=9.67' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs)



Pond 33P: CB #4 (Altus Model)

Summary for Pond 34P: CB #5 (Altus Model)

 Inflow Area =
 0.810 ac, 76.97% Impervious, Inflow Depth > 4.12" for 10 year event

 Inflow =
 4.0 cfs @ 12.05 hrs, Volume=
 0.278 af

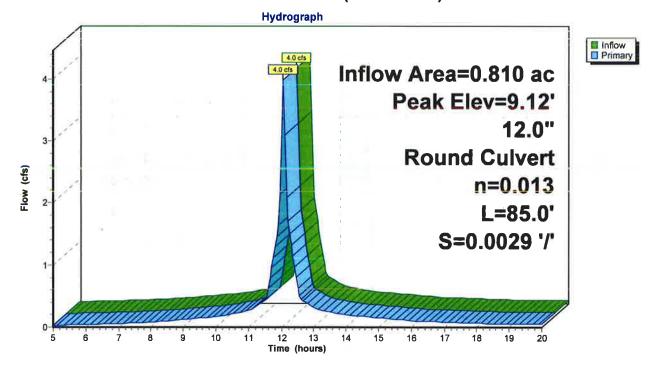
 Outflow =
 4.0 cfs @ 12.05 hrs, Volume=
 0.278 af, Atten= 0%, Lag= 0.0 min

 Primary =
 4.0 cfs @ 12.05 hrs, Volume=
 0.278 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 9.12' @ 12.05 hrs Flood Elev= 8.68'

Device	Routing	Invert	Outlet Devices
#1	Primary	5.83'	12.0" Round Culvert L= 85.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.83' / 5.58' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.9 cfs @ 12.05 hrs HW=9.07' TW=7.45' (Dynamic Tailwater) 1=Culvert (Outlet Controls 3.9 cfs @ 5.01 fps)



Pond 34P: CB #5 (Altus Model)

2790 Existing Conditions	Type III 24-hr	10 year Rainfall=4.86"
Prepared by Ambit Engineering, Inc.		Printed 7/17/2018
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Summary for Pond AEI 2:

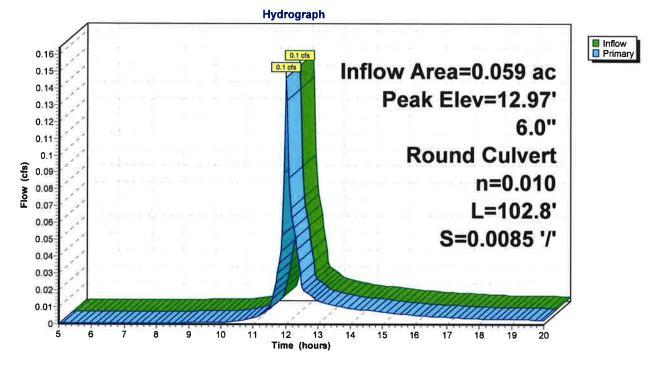
Inflow Area =	0.059 ac, 25.05% Impervious, Inflow Depth > 1	.84" for 10 year event
Inflow =	0.1 cfs @ 12.02 hrs, Volume= 0.009 a	f
Outflow =	0.1 cfs @ 12.02 hrs, Volume= 0.009 a	f, Atten= 0%, Lag= 0.0 min
Primary =	0.1 cfs @ 12.02 hrs, Volume= 0.009 a	f

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 12.97' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	9.42'	6.0" Round Culvert L= 102.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 9.42' / 8.55' S= 0.0085 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf

Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=10.49' TW=12.17' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs)

Pond AEI 2:



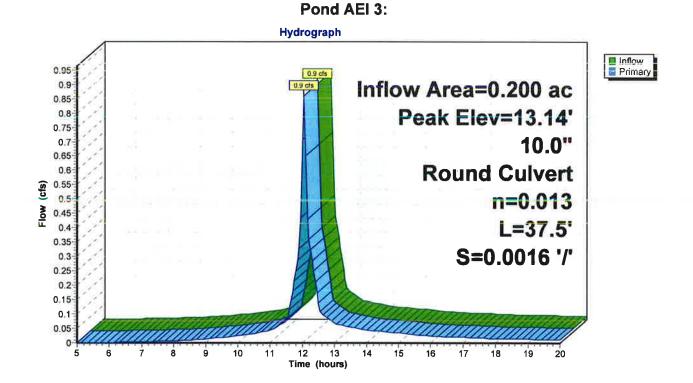
Summary for Pond AEI 3:

Inflow Area =	0.200 ac, 70.65% Impervious, Inflow D	epth > 3.24" for 10 year event
Inflow =	0.9 cfs @ 12.05 hrs, Volume=	0.054 af
Outflow =	0.9 cfs @ 12.05 hrs, Volume=	0.054 af, Atten= 0%, Lag= 0.0 min
Primary =	0.9 cfs @ 12.05 hrs, Volume=	0.054 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 13.14' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	8.90'	10.0" Round Cuivert L= 37.5' CPP, square edge headwall. Ke= 0.500 Inlet / Outlet Invert= 8.90' / 8.84' S= 0.0016 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=9.90' TW=11.87' (Dynamic Tailwater)



2790 Existing Conditions	Type III 24-hr 10 year Rainfall=4.86"
Prepared by Ambit Engineering, Inc.	Printed 7/17/2018
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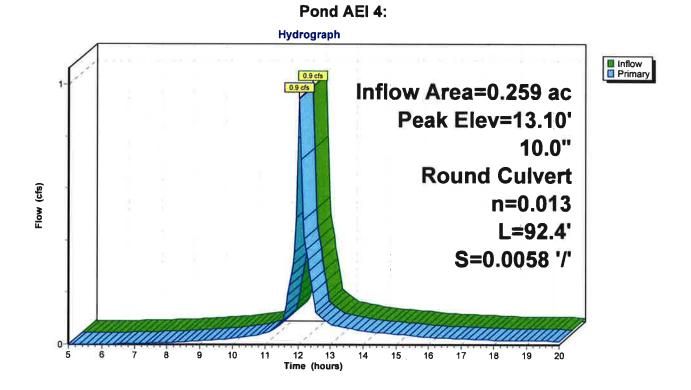
Summary for Pond AEI 4:

Inflow Area =	0.259 ac, 54.37% Impervious, Inflo	w Depth > 2.76" for 10 year event
Inflow =	0.9 cfs @ 12.04 hrs, Volume=	0.060 af
Outflow =	0.9 cfs @ 12.04 hrs, Volume=	0.060 af, Atten= 0%, Lag= 0.0 min
Primary =	0.9 cfs @ 12.04 hrs, Volume=	0.060 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 13.10' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	8.69'	10.0" Round Culvert L= 92.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 8.69' / 8.15' S= 0.0058 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=11.80' TW=12.78' (Dynamic Tailwater)



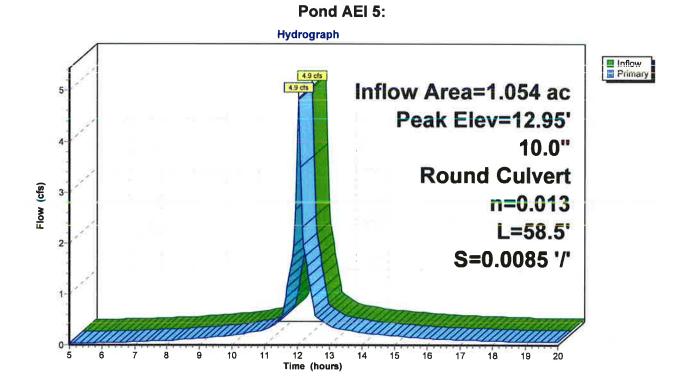
Summary for Pond AEI 5:

Inflow Area =	1.054 ac, 83.18% Impervious, Inflow Depth > 3.72" for 10 year event	
Inflow =	4.9 cfs @ 12.04 hrs, Volume= 0.327 af	
Outflow =	4.9 cfs @ 12.04 hrs, Volume= 0.327 af, Atten= 0%, Lag= 0.0 min	
Primary =	4.9 cfs @ 12.04 hrs, Volume= 0.327 af	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 12.95' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	7.90'	10.0" Round Cuivert L= 58.5' CPP. square edge headwall. Ke= 0.500 Inlet / Outlet Invert= 7.90' / 7.40' S= 0.0085 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf	

Primary OutFlow Max=4.7 cfs @ 12.04 hrs HW=12.69' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 4.7 cfs @ 8.65 fps)



2790 Existing ConditionsType III 24-hr 10 year Rainfall=4.86"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 37

Summary for Pond AEI 6: Discharge Point 3 (Off Site Drainage)

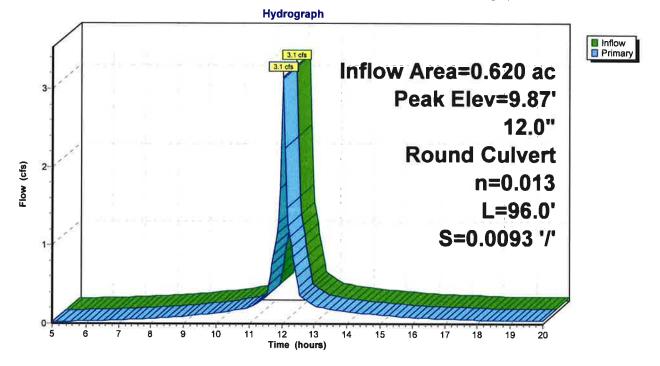
Inflow Area =	0.620 ac, 93.86% Impervious,	Inflow Depth > 4.13" for 10 year event
Inflow =		
Outflow =	3.1 cfs @ 12.04 hrs, Volum	e= 0.213 af, Atten= 0%, Lag= 0.0 min
Primary =	3.1 cfs @ 12.04 hrs, Volume	e= 0.213 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 9.87' @ 12.07 hrs Flood Elev= 10.77'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.77'	12.0" Round Culvert L= 96.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.77' / 5.88' S= 0.0093 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.1 cfs @ 12.04 hrs HW=9.50' TW=9.02' (Dynamic Tailwater) **1=Culvert** (Outlet Controls 2.1 cfs @ 2.62 fps)





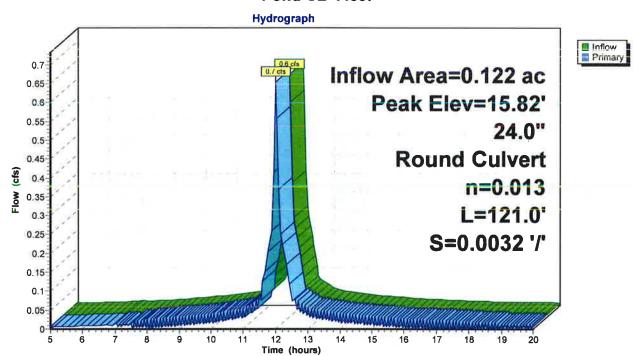
Summary for Pond CB 4433:

Inflow Area =	0.122 ac,100.00% Impervious,	Inflow Depth > 4.29" for 10 year event
Inflow =	0.6 cfs @ 12.01 hrs, Volume	e= 0.044 af
Outflow =	0.7 cfs @ 12.01 hrs, Volume	e= 0.044 af, Atten= 0%, Lag= 0.0 min
Primary =	0.7 cfs @ 12.01 hrs, Volume	e= 0.044 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.82' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.38'	24.0" Round Cuivert L= 121.0' CPP. square edge headwall. Ke= 0.500 Inlet / Outlet Invert= 14.38' / 13.99' S= 0.0032 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
			-

Primary OutFlow Max=0.0 cfs @ 12.01 hrs HW=15.75' TW=15.80' (Dynamic Tailwater)



Pond CB 4433:

2790 Existing Conditions Tyl	pe III 24-hr 10 year Rainfall=4.86"
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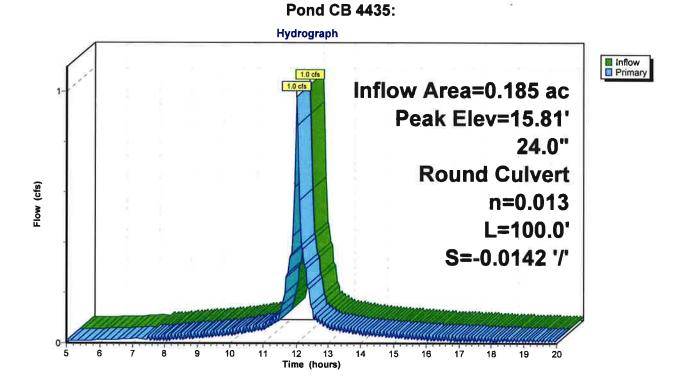
Summary for Pond CB 4435:

Inflow Area	=	0.185 ac,10	0.00% Impervious	, Inflow Depth >	4.29" for	10 year event
Inflow	=	1.0 cfs @	12.01 hrs, Volum	ne= 0.066	af	
Outflow	=	1.0 cfs @	12.01 hrs, Volum	ie= 0.066	af, Atten=	0%, Lag= 0.0 min
Primary	= '	1.0 cfs @	12.01 hrs, Volum	ne= 0.066 a	af	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.81' @ 12.01 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		24.0" Round Culvert L= 100.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 13.99' / 15.41' S= -0.0142 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.9 cfs @ 12.01 hrs HW=15.80' TW=0.00' (Dynamic Tailwater) -1=Culvert (Inlet Controls 0.9 cfs @ 2.14 fps)



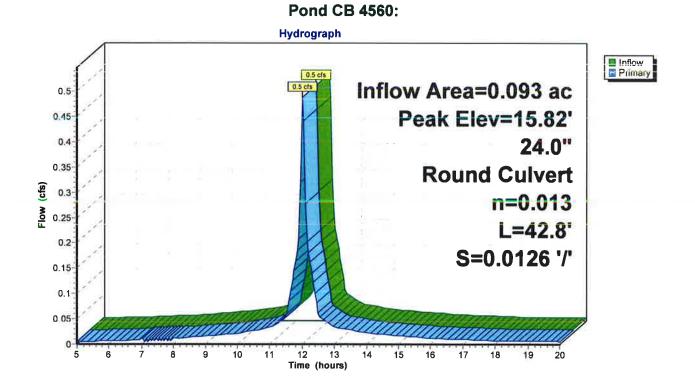
Summary for Pond CB 4560:

Inflow Area =	0.093 ac,100.00% Impervious, Inflow Depth > 4.29" for 10 year event
Inflow =	0.5 cfs @ 12.02 hrs, Volume= 0.033 af
Outflow =	0.5 cfs @ 12.02 hrs, Volume= 0.033 af, Atten= 0%, Lag= 0.0 min
Primary =	0.5 cfs @ 12.02 hrs, Volume= 0.033 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.82' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.92'	24.0" Round Cuivert L= 42.8' CPP. square edge headwall. Ke= 0.500 Inlet / Outlet Invert= 14.92' / 14.38' S= 0.0126 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

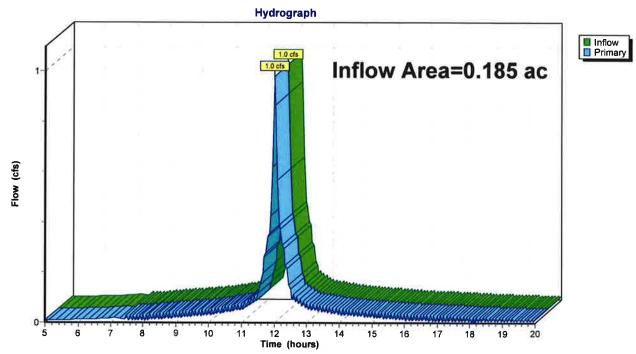
Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=15.71' TW=15.76' (Dynamic Tailwater)



Summary for Link 2L: Discharge Point 2 (Court Street Drainage)

Inflow Are	a =	0.185 ac,100.00% Impervious, Inflow Depth > 4.29" for 10 ye	ear event
	=	1.0 cfs @ 12.01 hrs, Volume= 0.066 af	
Primary	=	1.0 cfs @ 12.01 hrs, Volume= 0.066 af, Atten= 0%, I	_ag= 0 .0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

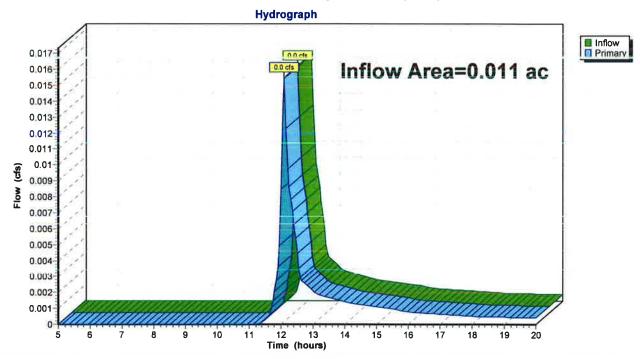


Link 2L: Discharge Point 2 (Court Street Drainage)

Summary for Link 3L: Discharge Point 4 (DP4)

Inflow Area =	0.011 ac, 0.00% Impervious, Inflow Depth > 1.16" for 10 year event	
Inflow =	0.0 cfs @ 12.09 hrs, Volume= 0.001 af	
Primary =	0.0 cfs @ 12.09 hrs, Volume= 0.001 af, Atten= 0%, Lag= 0.0 min	

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



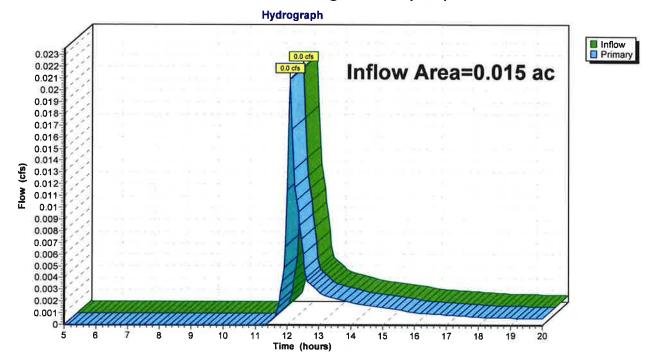
Link 3L: Discharge Point 4 (DP4)

Summary for Link 4L: Discharge Point 5 (DP5)

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Inflow Are	a =	0.015 ac,	0.00% Impervious,	Inflow Depth > 1	.16" for 10 year event
Inflow	=	0.0 cfs @	12.09 hrs, Volum	e= 0.001 at	f
Primary	=	0.0 cfs @	12.09 hrs, Volum	e= 0.001 at	f, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link 4L: Discharge Point 5 (DP5)

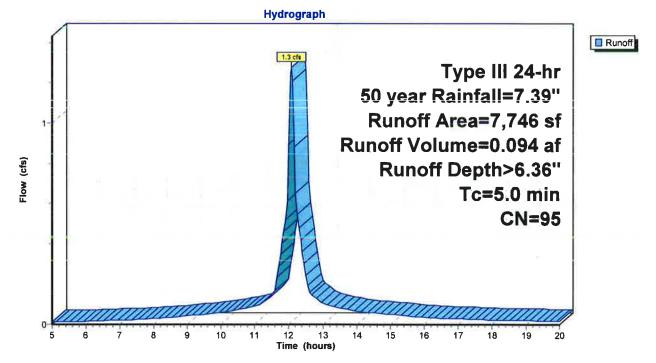
Summary for Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)

Runoff = 1.3 cfs @ 12.07 hrs, Volume= 0.094 af, Depth> 6.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN I	Description			
*		7,746	95				
· · · · ·		7,746		100.00% P	ervious Are	a	
(n	Tc nin)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
	5.0					Direct Entry,	

Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)



Summary for Subcatchment 4S: Existing Building (Altus Model)

Runoff = 0.3 cfs @ 12.07 hrs, Volume= 0.023 af, Depth> 6.59"

Time (hours)

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN	Description			
*		1,794	98				
		1,794		100.00% Im	npervious A	s Area	
	Tc (min)	Length (feet)	Slop (ft/ft		Capacity (cfs)		
	5.0					Direct Entry,	
			S	ubcatchm	ent 4S: E	Existing Building (Altus Model)	
		/				drograph	
	0.32	(i)			0.	0.3.cfs	f
	0.3	Server 1				Type III 24-hr	
	0.28	1				50 year Rainfall=7.39"	
	0.24	1				Runoff Area=1,794 sf	
	0.22	1				A set of the set of th	
	0.2	ř. –				Runoff Volume=0.023 af	
	0.18	Č -				Runoff Depth>6.59"	
	(S) 0.18 0.16					Tc=5.0 min	
	0.14 0.12					CN=98	
	0.12	2				C14-30	
	0.08	1			P		
	0.06	-1			P		
	0.04	×,					
	0.02	Inn	//////	mmm			
	0-	5 6	7	8 9 10) 11 1	12 13 14 15 16 17 18 19 20	

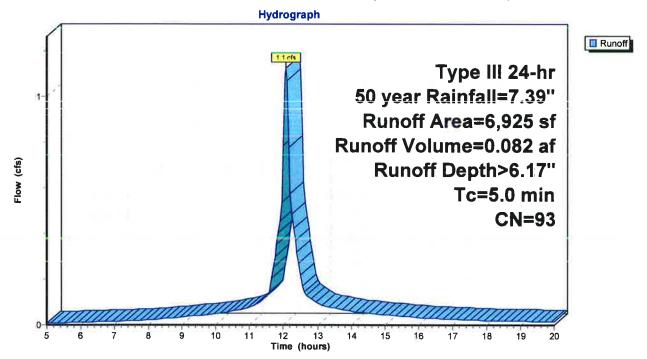
Summary for Subcatchment 30S: West Parking Lot (Altus Model)

Runoff = 1.1 cfs @ 12.07 hrs, Volume= 0.082 af, Depth> 6.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

2	A	rea (sf)	CN E	Description		
*		6,925	93			
		6,925		100.00% Pe	ervious Are	28
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
8	5.0	(ieet)	(1010)	(10900)	(018)	Direct Entry,

Subcatchment 30S: West Parking Lot (Altus Model)



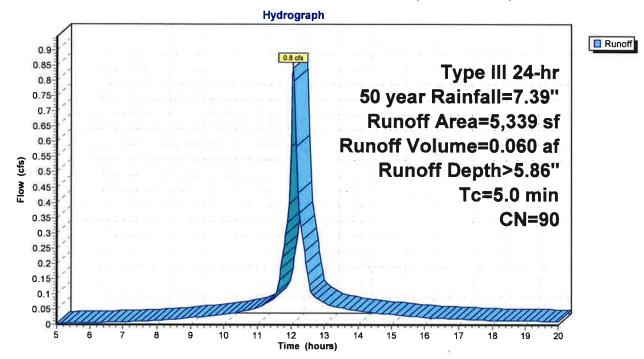
Summary for Subcatchment 31S: West Front Yard (Altus Model)

Runoff = 0.8 cfs @ 12.07 hrs, Volume= 0.060 af, Depth> 5.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	Α	rea (sf)	CN I	Description			
*		5,339	90				
		5,339		100.00% P	ervious Are	2	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
	5.0					Direct Entry,	

Subcatchment 31S: West Front Yard (Altus Model)



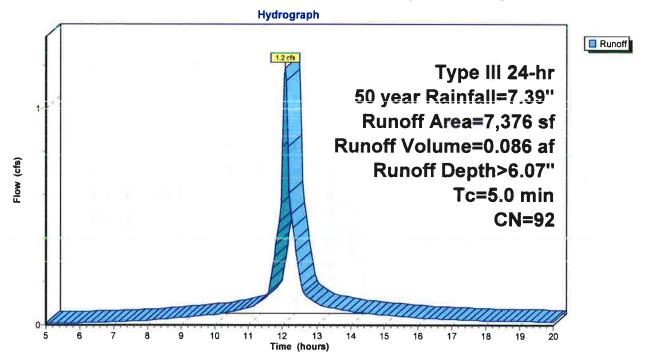
Summary for Subcatchment 32S: East Front Yard (Altus Model)

Runoff = 1.2 cfs @ 12.07 hrs, Volume= 0.086 af, Depth> 6.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

/	Area (sf)	CN I	Description			
*	7,376	92				
	7,376	100.00% Pervious Area				
Tc (min)	9	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment 32S: East Front Yard (Altus Model)



Summary for Subcatchment 33S: East Parking Lot (Altus Model)

Runoff = 2.2 cfs @ 12.07 hrs, Volume= 0.156 af, Depth> 5.97"

6

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

Area (sf)	CN Description			
* 13,707	91			
13,707	100.00% P	ervious Area		
Tc Length (min) (feet)	Slope Velocity (ft/ft) (ft/sec)	Capacity [(cfs)	Description	
5.0		0	Direct Entry,	
	Subcatchm	ent 33S: Ea	st Parking Lot (Altus Model)	
		Hydrogra	aph	
Flow (cfs)		2.2 cfs	Type III 24-hr 50 year Rainfall=7.39" Runoff Area=13,707 sf Runoff Volume=0.156 af Runoff Depth>5.97" Tc=5.0 min CN=91	Runoff

14

15

16

18

19

10

11

12

Time (hours)

13

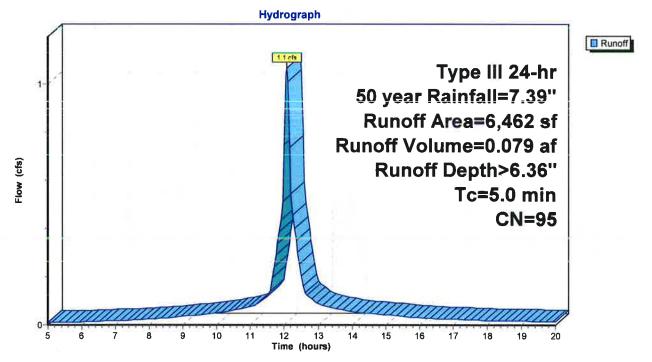
Summary for Subcatchment 34S: North Parking Lot (Altus Model)

Runoff = 1.1 cfs @ 12.07 hrs, Volume= 0.079 af, Depth> 6.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

A	rea (sf)	CN I	Description			
*	6,462	95				
	6,462		100.00% P	ervious Are	a	
Tc (min)	Length (feet)	Siope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment 34S: North Parking Lot (Altus Model)



Summary for Subcatchment 40S: Existing Building (Altus Model)

Runoff = 0.9 cfs @ 12.07 hrs, Volume= 0.071 af, Depth> 6.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

Α	rea (sf)	CN	Description								
*	5,617	98									
	5,617		100.00% In	npervious A	геа						
Tc (min)	Length (feet)	Slop (ft/ft		Capacity (cfs)	Descrip	otion					
5.0					Direct	Entry,					
		с.	. h a a fa h m					4 8 4	1		
		31	bcatchme		-	Bulla	ing (Ai	tus M	ioaei)		
	1			Hydro	graph						
Flow (cfs)				0.8		Ru Runo	/ear F inoff / ff Vol	Rainf Area ume Dep	e III 24 all=7.3 =5,617 =0.071 oth>6.9 =5.0 n CN=	39" 'sf af 59" nin	Runoff
0- <mark>1</mark> 5	6 6	7 8	9 10	11 12 Tim	13 e (hours)	14 1	5 16	17	18 19	20	

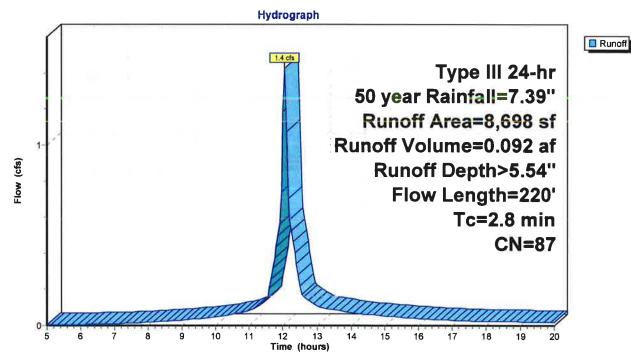
Summary for Subcatchment ES1:

Runoff = 1.4 cfs @ 12.05 hrs, Volume= 0.092 af, Depth> 5.54"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	Α	rea (sf)	CN [Description					
		5,487	98 F	aved park	ing, HSG B	3			
*		658	98 l	Inconnecte	ed pavemer	nt, sidewalk, HSG B			
		2,553	61 >	75% Gras	s cover, Go	bod, HSG B			
1		8,698 87 Weighted Average							
		2,553 29 35% Pervious Area							
		6,145	7	0.65% Imp	pervious Are	ea			
		658	1	0.71% Un	connected				
	Тс	Length	Slope	Velocity	Capacity	Description			
~	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	2.1	84	0.0089	0.66		Shallow Concentrated Flow,			
						Short Grass Pasture Kv= 7.0 fps			
	0.7	136	0.0239	3.14		Shallow Concentrated Flow,			
						Paved Kv= 20.3 fps			
	2.8	220	Total						

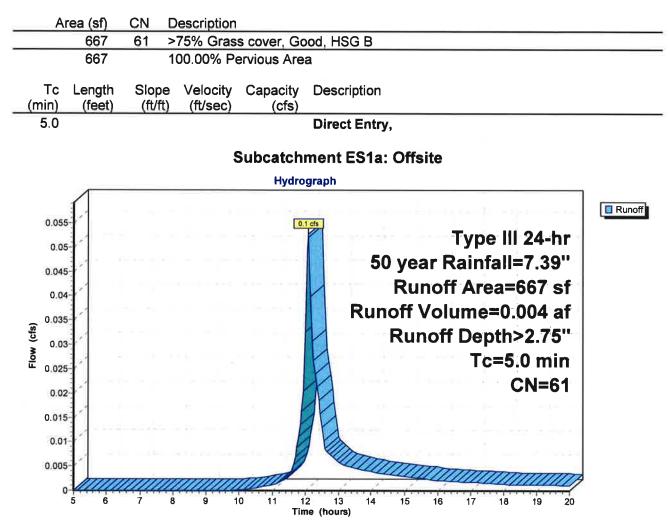
Subcatchment ES1:



Summary for Subcatchment ES1a: Offsite

Runoff = 0.1 cfs @ 12.08 hrs, Volume= 0.004 af, Depth> 2.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"



Summary for Subcatchment ES2:

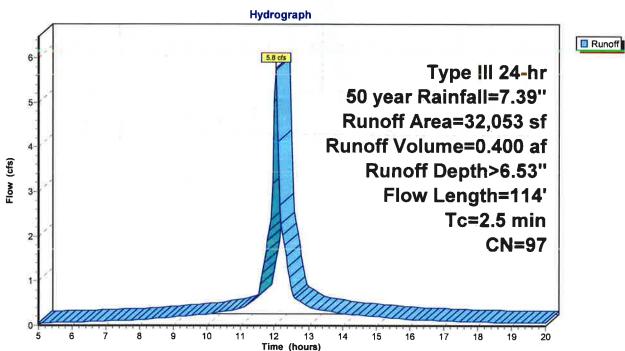
Runoff = 5.8 cfs @ 12.04 hrs, Volume= 0.400 af, Depth> 6.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

~	A	rea (sf)	CN I	Description						
		10,300	98	Roofs, HSC	ЭB					
		3,910	98 I	Roofs, HSC	ЭB					
		641	61 3	>75% Gras	s cover, Go	ood, HSG B				
*		480	98 (Jnconnecte	ed pavemer	nt,sidewalks, HSG	B			
		9.865	98 I	aved parking. HSG B						
*		6,857	98 (Gravel surf	ace, HSG E	3				
		32,053	97 \	Neighted A	verage			_		
		641	1	2.00% Perv	vious Ārea					
		31,412	9	98.00% Imp	pervious Ar	ea				
		480		1.53% Unc	onnected					
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
-	0.8	35	0.0071	0.74	(0.0/	Sheet Flow,				
						Smooth surfaces	n= 0.011	P2= 3.21"		
	1.7	79	0.0050	0.75		Sheet Flow,				
						Smooth surfaces	n= 0.011	P2= 3.21"		
		444								

2.5 114 Total

Subcatchment ES2:



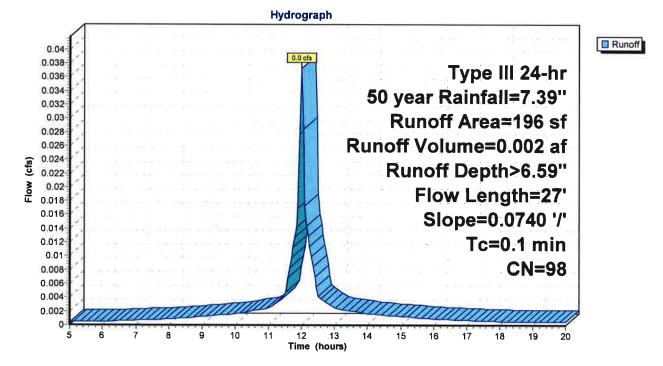
Summary for Subcatchment ES2a:

Runoff = 0.0 cfs @ 12.00 hrs, Volume= 0.002 af, Depth> 6.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

-	Α.	rea (sf)	CN [Description						
		102	98 F	8 Paved parking, HSG B						
*		94	98 L	Unconnected pavement, sidewalk, HSG B						
		196	98 V	Veighted A	verage		_			
		196	1	100.00% Impervious Area						
		94	4	47.96% Unconnected						
	Тс	Length	Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.1	27	0.0740	5.52		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
					• •					





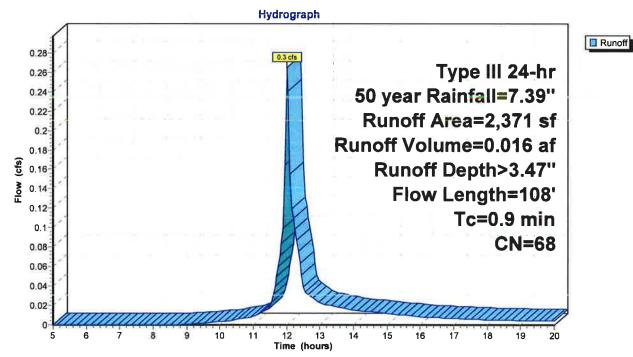
Summary for Subcatchment ES3:

Runoff = 0.3 cfs @ 12.02 hrs, Volume= 0.016 af, Depth> 3.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN [Description							
*		414	98 (B Gravel surface, HSG B							
*		33	98 l	Inconnecte	ed pavemer	nt, sidewalk, HSG B					
		1,924	61 >	75% Gras	s cover, Go	bod, HSG B					
		2,371	68 \	Veighted A	verage						
		1 924	8	81 15% Pervious Area							
		447	1	18.85% Impervious Area							
		33	7	7.38% Unconnected							
	Тс	Length	Slope		Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	0.2	58	0.0819	5.81		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
	0.7	50	0.0300	1.21		Shallow Concentrated Flow,					
_						Short Grass Pasture Kv= 7.0 fps					
-	0.9	108	Total								

Subcatchment ES3:



Summary for Subcatchment ES4:

Runoff = 0.2 cfs @ 12.02 hrs, Volume= 0.014 af, Depth> 2.76"

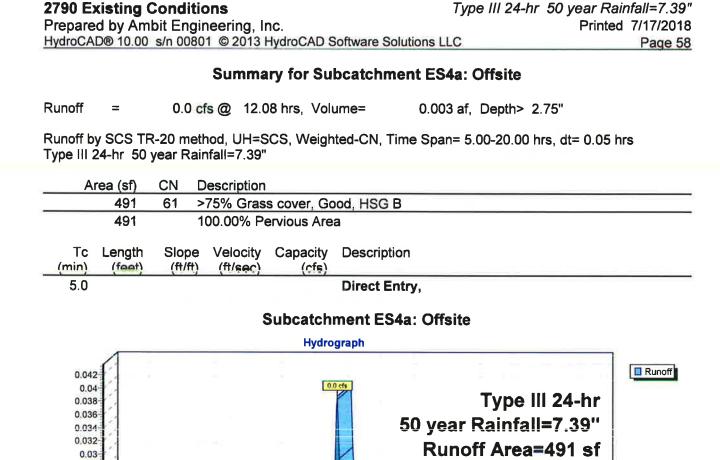
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN [Description							
	2,604 61 >75% Grass cover, Good, HSG B										
		2,604		100.00% Pervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description					
	0.8	81	0.0525	1.60		Shallow Concentrated Flow, Short Grass Pasture Kv= 7.0 fps					
Subsetshment FS4											

Subcatchment ES4:

Hydrograph Runoff 0.25 0.24-0.2 cfs 0.23 Type III 24-hr 0.22-0.21 50 year Rainfall=7.39" 0.2 0.19 Runoff Area=2,604 sf 0.18 0.17 Runoff Volume=0.014 af 0.16 Runoff Depth>2.76" 0.13 Flow 0.12 Flow Length=81' 0.11 0.1 Slope=0.0525 '/' 0.09 0.08 Tc=0.8 min 0.07 0.06 **CN=61** 0.05 0.04 0.03-0.02 0.01 10 11 12 13 14 15 16 17 18 19 20 Time (hours)



Runoff Volume=0.003 af

Runoff Depth>2.75"

Tc=5.0 min

18

CN=61

19

20

0.028

0.026

0.022

0.018

0.016 0.014 0.012 0.01 0.008 0.006 0.004 0.002 0 5

6

7

8

9

10

11

12

Time (hours)

13

14

15

16

17

(S) 0.024-

0.022

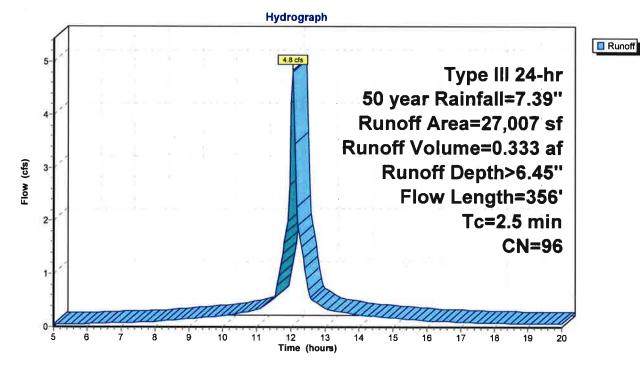
Summary for Subcatchment ES5:

Runoff = 4.8 cfs @ 12.04 hrs, Volume= 0.333 af, Depth> 6.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	A	rea (sf)	CN I	Description						
\ <u></u>		23,335	98	Paved park	ing, HSG E	3				
*		1,456	98 l	Jnconnecte	ed paveme	nt, sidewalk, HSG B				
		1,658				bod, HSG B				
*		558	98 (Gravel surf	ace, HSG E	3				
		27,007	96 \	6 Weighted Average						
		1,658	e	6.14% Pervious Area						
		25,349	9	93.86% Impervious Area						
		1,456	ŧ	5.74% Unc	onnected					
	Τ.		0	N	•					
	Tc	Length	Slope		Capacity	Description				
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	1.3	56	0.0050	0.70		Sheet Flow,				
						Smooth surfaces n= 0.011 P2= 3.21"				
	1.2	300	0.0417	4.15		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	2.5	356	Total							

Subcatchment ES5:



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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 60

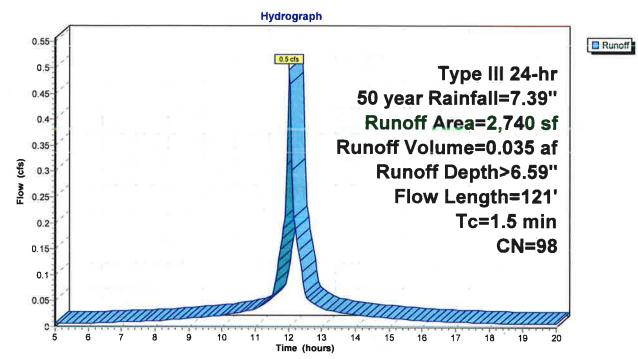
Summary for Subcatchment ES6:

Runoff = 0.5 cfs @ 12.02 hrs, Volume= 0.035 af, Depth> 6.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	Α	rea (sf)	CN [Description						
		2,330	98 F	aved park	ing, HSG B					
4		410	98 l	Inconnecte	ed pavemer	nt, sidewalk, HSG B				
		2,740	98 V	98 Weighted Average						
		2,740								
		410	1	4 96% Un	connected					
	Тс	Length	Slope	Velocity	Capacity	Description				
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	0.6	26	0.0096	0.69		Shallow Concentrated Flow,				
						Short Grass Pasture Kv= 7.0 fps				
	0.9	95	0.0078	1.79		Shallow Concentrated Flow,				
						Paved Kv= 20.3 fps				
	1.5	121	Total							

Subcatchment ES6:



Prepare	xisting d by Am D® 10.00	bit Engi	ineering, I	nc. HydroCAD \$	Type III 24-hr 50 year R Printe Software Solutions LLC	ainfall=7.39' d 7/17/2018 Page 61
			Su	nmary fo	r Subcatchment ES7:	
Runoff	=	0.2 c	cfs @ 12.0	01 hrs, Vol	ume= 0.016 af, Depth> 6.59"	
					nted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05	hrs
		-	infall=7.39"			
A	rea (sf)		Description			
	922 341			ing, HSG E	3 nt, sidewalk, HSG B	
	1,263		Neighted A		In, sidewalk, HOO D	
	1,263		100.00% In	npervious A	Area	
	341	2	27.00% Un	connected		
Тс	Length	Slope	Velocity	Capacity	Description	
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
0.6	49	0.0051	1.45		Shallow Concentrated Flow,	
					Paved Kv= 20.3 fps	
				Subca	atchment ES7:	
				Hydro	ograph	
0.26			1.00		· · · · · · · · · · · · · · · · · · ·	🔲 Runoff
0.24	1			0.2	cfs	Kunoir
1	2				Type III 24-hr	
0.22	2				50 year Rainfall=7.39"	
0.2	1			e de la composition de la comp	Runoff Area=1,263 sf	
0,18	54				Runoff Volume=0.016 af	
0.16						
(sj) 0.14 Mol 0.12	Č,				Runoff Depth>6.59"	
6 0.12-					Flow Length=49'	
0.1	1			Ľ	Slope=0.0051 '/'	
0.08	1				Tc=0.6 min	
0.06	1			E	CN=98	
0.04	2			D	CIN=98	
	-1			- and	man	
0.02			mmm	1110		
0		7 8	9 10	D 11 1:	2 13 14 15 16 17 18 19 20	

Prepare	d by Am	Conditions bit Engineerin s/n 00801 © 20		<i>Type III 24-hr 50 year R</i> Printe Software Solutions LLC	ainfall=7.39" ed 7/17/2018 Page 62			
			Summary fo	r Subcatchment ES8:				
Runoff	=	0.7 cfs @	12.02 hrs, Vol	ume= 0.051 af, Depth> 6.59"				
	Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"							
A	rea (sf)	CN Descrip						
*	2,607 1,444		parking, HSG E	3 nt,sidewalk, HSG B				
N	4,051	98 Weight	ed Average					
	4,051 1,444		% Impervious A	Area				
Tc (min)	Length (feet)	Slope Velo (ft/ft) (ft/s		Description				
1.2	143		.01	Shallow Concentrated Flow,				
				Paved Kv= 20.3 fps				
			Subca	atchment ES8:				
			Hydro	ograph				
0.8					Runoff			
0.75	1 G C		.0.7	Type III 24-hr				
0.7- 0.65-	100			50 year Rainfall=7.39"				
0.6-	1.24			Runoff Area=4,051 sf				
0.55				Runoff Volume=0.051 af				
0.5 S 0.45				Runoff Depth>6.59"				
(Sj) 0.45 MO				Flow Length=143'				
ш _{0.35} - 0.3-	1.1			Slope=0.0098 '/'				
0.25	1.21		E	Tc=1.2 min				
0.2			E	CN=98				
0.15 0.1	2		D					
0.05	Imm	mmmm	mm					
0	5 6	7 8 9		2 13 14 15 16 17 18 19 20 ne (hours)				

2790 Existing ConditionsType III 24-hr 50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 63

Summary for Reach 4R: Altus Model

 Inflow Area =
 0.041 ac,100.00% Impervious, Inflow Depth > 6.59" for 50 year event

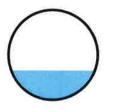
 Inflow =
 0.3 cfs @ 12.07 hrs, Volume=
 0.023 af

 Outflow =
 0.3 cfs @ 12.08 hrs, Volume=
 0.023 af, Atten= 1%, Lag= 0.7 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 3.02 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.17 fps, Avg. Travel Time= 1.6 min

Peak Storage= 11 cf @ 12.08 hrs Average Depth at Peak Storage= 0.22' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.3 cfs

8.0" Round Pipe n= 0.012 Length= 110.0' Slope= 0.0100 '/' Inlet Invert= 8.38', Outlet Invert= 7.28'



Hydrograph Inflow Outflow 0.3 cf 0.32 Inflow Area=0.041 ac 0.3 cfs 0.3 Avg. Flow Depth=0.22' 0.28 0.26 Max Vel=3.02 fps 0.24 8.0" 0,22 0.2 **Round Pipe** (cfs) 0.18 n=0.012 Flow 0.16 0.14 L=110.0' 0.12 S=0.0100 '/' 0.1 0.08 Capacity=1.3 cfs 0.06 0.04 0.02 0 10 11 12 13 14 15 16 17 18 19 20 Time (hours)

Reach 4R: Altus Model

Summary for Reach 40R: Altus Model

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth > 6.59" for 50 year event

 Inflow =
 0.9 cfs @ 12.07 hrs, Volume=
 0.071 af

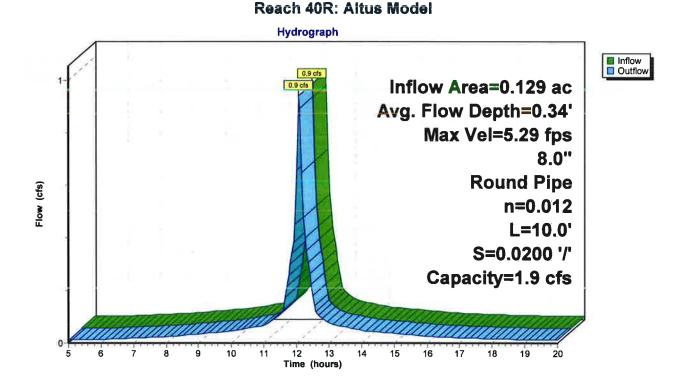
 Outflow =
 0.9 cfs @ 12.07 hrs, Volume=
 0.071 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 5.29 fps, Min. Travel Time= 0.0 min Avg. Velocity = 2.10 fps, Avg. Travel Time= 0.1 min

Peak Storage= 2 cf @ 12.07 hrs Average Depth at Peak Storage= 0.34' Bank-Full Depth= 0.67' Flow Area= 0.3 sf. Capacity= 1.9 cfs

8.0" Round Pipe n= 0.012 Length= 10.0' Slope= 0.0200 '/' Inlet Invert= 6.82', Outlet Invert= 6.62'





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Summary for Reach 41R: Altus Model

 Inflow Area =
 0.938 ac, 80.14% Impervious, Inflow Depth > 6.46" for 50 year event

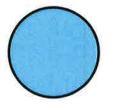
 Inflow =
 7.1 cfs @ 12.05 hrs, Volume=
 0.505 af

 Outflow =
 2.3 cfs @ 11.81 hrs, Volume=
 0.505 af, Atten= 68%, Lag= 0.0 min

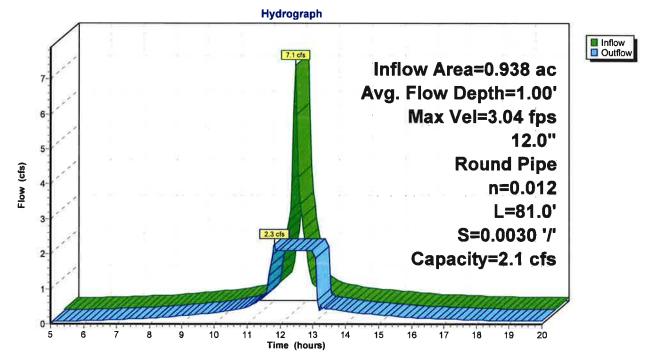
Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Max. Velocity= 3.04 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.78 fps, Avg. Travel Time= 0.8 min

Peak Storage= 64 cf @ 11.85 hrs Average Depth at Peak Storage= 1.00' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.1 cfs

12.0" Round Pipe n= 0.012 Length= 81.0' Slope= 0.0030 '/' Inlet Invert= 6.45', Outlet Invert= 6.21'



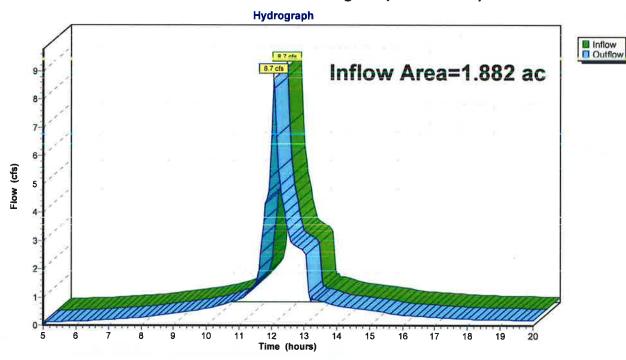
Reach 41R: Altus Model



Summary for Reach 300R / DP1A: POA #3 - Existing CB (Altus Model) - AEI DP1A

Inflow Area =	1.882 ac, 39.96% Impervious, Inflow Depth > 6.27" for 50 year event
Inflow =	8.7 cfs @ 12.07 hrs, Volume= 0.983 af
Outflow =	8.7 cfs @ 12.07 hrs, Volume= 0.983 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Reach 300R / DP1A: POA #3 - Existing CB (Altus Model) - AEI DP1A

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Summary for Pond 3P: Existing CB (Altus Model)

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Inflow A Inflow Outflow Primary	= =	8.7 cfs @ 1 8.7 cfs @ 1	96% Impervious, Inflow Depth > 6.27" for 50 year event 2.07 hrs, Volume= 0.983 af 2.07 hrs, Volume= 0.983 af, Atten= 0%, Lag= 0.0 min 2.07 hrs, Volume= 0.983 af
Routing Peak Ele	by Dyn-Sto	-	Time Span= 5.00-20.00 hrs, dt= 0.05 hrs
Device	Routing	Invert	Outlet Devices
#1	Primary	5.76'	12.0" Round Culvert L= 55.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.76' / 5.21' S= 0.0100 '/' Cc= 0.900

n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=8.5 cfs @ 12.07 hrs HW=11.60' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 8.5 cfs @ 10.80 fps)

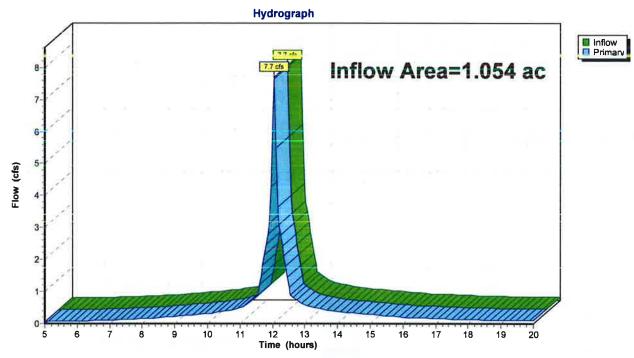
Hydrograph Inflow
Primary 8.7 Inflow Area=1.882 ac 8.7 cf 9 Peak Elev=11.88' 8 12.0" 7 **Round Culvert** 6 Flow (cfs) n=0.012 5 L=55.0' 4 S=0.0100 '/' 3 2 ö 6 Ŕ 10 11 12 13 14 15 16 17 18 19 20 Time (hours)

Pond 3P: Existing CB (Altus Model)

Summary for Pond 5P: Discharge Point 1 (COMBINED SEWER)

Inflow Area =	=	1.054 ac, 8	3.18% Impervious	Inflow Depth >	5.97"	for 50 year event
Inflow =		7.7 cfs @	12.04 hrs, Volun	ne= 0.524	l af	-
Primary =		7.7 cfs @	12.04 hrs, Volun	ne= 0.524	l af, Att	en= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Pond 5P: Discharge Point 1 (COMBINED SEWER)

 2790 Existing Conditions
 Type III 2

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Summary for Pond 30P: CB #1 (Altus Model)

 Inflow Area =
 1.704 ac, 44.13% Impervious, Inflow Depth > 6.26" for 50 year event

 Inflow =
 7.4 cfs @ 12.07 hrs, Volume=
 0.889 af

 Outflow =
 7.4 cfs @ 12.07 hrs, Volume=
 0.889 af, Atten= 0%, Lag= 0.0 min

 Primary =
 7.4 cfs @ 12.07 hrs, Volume=
 0.889 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 16.97' @ 12.10 hrs Flood Elev= 9.15'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.11'	12.0" Round Culvert L= 82.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.11' / 5.86' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=6.4 cfs @ 12.07 hrs HW=15.86' TW=11.60' (Dynamic Tailwater) -1=Culvert (Outlet Controls 6.4 cfs @ 8.21 fps)

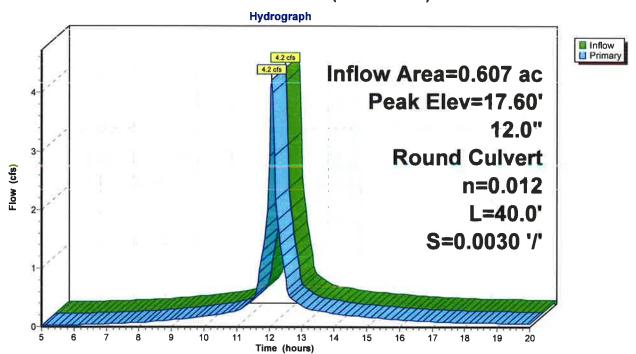
Hydrograph Inflow 8 Inflow Area=1.704 ac Peak Elev=16.97' 12.0" 6 Round Culvert 5 Flow (cfs) n=0.013 L=82.0' 3 S=0.0030 '/' 2 0 6 7 Å à 10 11 14 15 16 17 18 19 20 12 13 Time (hours)

Pond 30P: CB #1 (Altus Model)

Summary for Pond 31P: CB #2 (Altus Model)

Inflow Area = Inflow = Outflow = Primary =	4.2 cfs @ 1 4.2 cfs @ 1	00% Impervious, Inflow Depth > 5.98" for 50 year event 2.07 hrs, Volume= 0.302 af 2.07 hrs, Volume= 0.302 af, Atten= 0%, Lag= 0.0 min 2.07 hrs, Volume= 0.302 af
Routing by Dyn-Sto Peak Elev= 17.60' Flood Elev= 9.15'		Гіme Span= 5.00-20.00 hrs, dt= 0.05 hrs
Device Routing	invert	Outlet Devices
#1 Primary	6 33'	12.0" Round Culvert L= 40.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.33' / 6.21' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=14.30' TW=15.86' (Dynamic Tailwater)



Pond 31P: CB #2 (Altus Model)

2790 Existing ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 71

Summary for Pond 32P: CB #3 (Altus Model)

 Inflow Area =
 0.484 ac,
 0.00% Impervious,
 Inflow Depth > 6.00"
 for 50 year event

 Inflow =
 3.4 cfs @
 12.07 hrs,
 Volume=
 0.242 af

 Outflow =
 3.4 cfs @
 12.07 hrs,
 Volume=
 0.242 af

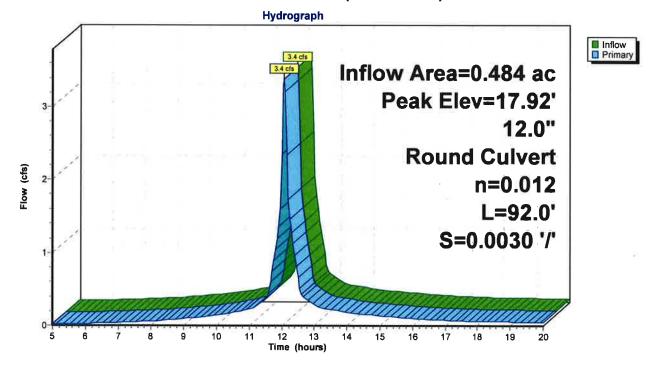
 Primary =
 3.4 cfs @
 12.07 hrs,
 Volume=
 0.242 af

 0.242 af
 0.242 af
 0.242 af
 0.242 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 17.92' @ 12.19 hrs Flood Elev= 9.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.71'	12.0" Round Culvert L= 92.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.71' / 6.43' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=12.70' TW=14.29' (Dynamic Tailwater)

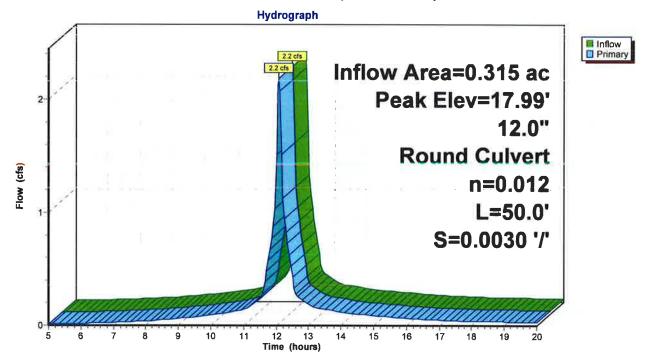


Pond 32P: CB #3 (Altus Model)

Summary for Pond 33P: CB #4 (Altus Model)

Inflow Area = 0.315 ac. 0.00% Impervious, Inflow Depth > 5.97" for 50 year event Inflow 2.2 cfs @ 12.07 hrs, Volume= 0.156 af = Outflow 2.2 cfs @ 12.07 hrs, Volume= = 0.156 af, Atten= 0%, Lag= 0.0 min 2.2 cfs @ 12.07 hrs, Volume= Primary Ξ 0.156 af Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 17.99' @ 12.24 hrs Flood Elev= 9.50' Device Routing Invert Outlet Devices #1 Primary 6 96' 12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.96' / 6.81' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.07 hrs HW=11.29' TW=12.70' (Dynamic Tailwater) 1=Culvert (Controls 0.0 cfs)



Pond 33P: CB #4 (Altus Model)

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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 SLLC Page 73

Summary for Pond 34P: CB #5 (Altus Model)

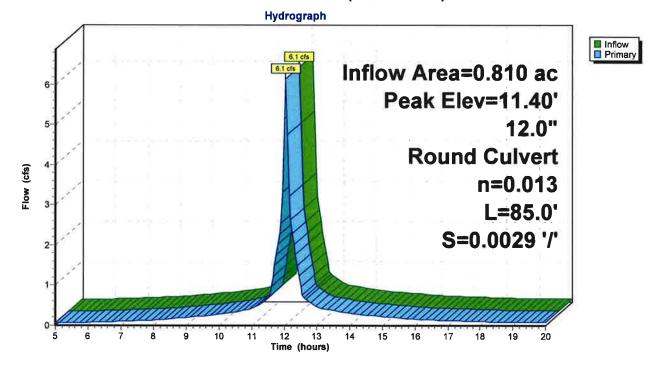
Inflow Area =	=	0.810 ac, 76	5.97% Impervious,	Inflow Depth > 6.	44" for 50 year event
Inflow =	:	6.1 cfs @	12.05 hrs, Volum	e= 0.434 at	f
Outflow =	:	6.1 cfs @	12.05 hrs, Volum	e= 0.434 at	f, Atten= 0%, Lag= 0.0 min
Primary =	:	6.1 cfs 🥘	12.05 hrs, Volum	e= 0.434 at	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 11.40' @ 12.05 hrs Flood Elev= 8.68'

Device	Routing	Invert	Outlet Devices
#1	Primary	5.83'	12.0" Round Culvert L= 85.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.83' / 5.58' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=6.1 cfs @ 12.05 hrs HW=11.30' TW=7.45' (Dynamic Tailwater) 1=Culvert (Outlet Controls 6.1 cfs @ 7.71 fps)

Pond 34P: CB #5 (Altus Model)



2790 Existing Conditions	Type III 24-hr 50 year Rainfall=7.39"
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Summary for Pond AEI 2:

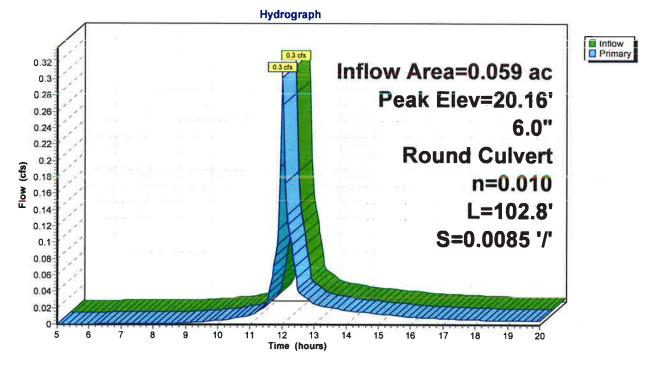
Inflow Area =	0.059 ac, 25.05% Impervious, Inflow Depth > 3.71" for 50 year event
Inflow =	0.3 cfs @ 12.01 hrs, Volume= 0.018 af
Outflow =	0.3 cfs @ 12.01 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min
Primary =	0.3 cfs @ 12.01 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 20.16' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices	
#1	Primary	9.42'	6.0" Round Culvert	
			L= 102.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 9.42' / 8.55' S= 0.0085 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 0.20 sf	

Primary OutFlow Max=0.0 cfs @ 12.01 hrs HW=13.67' TW=18.08' (Dynamic Tailwater)





2790 Existing ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00s/n 00801© 2013 HydroCAD Software Solutions LLCPage 75

Summary for Pond AEI 3:

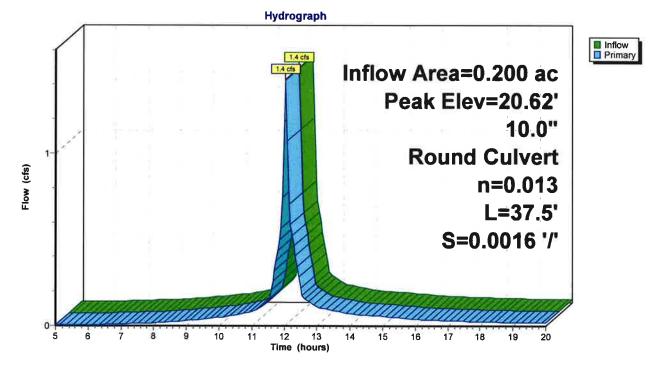
Inflow Area =	0.200 ac, 70.65% Impervious, Inflow	Depth > 5.54" for 50 year event
Inflow =	1.4 cfs @ 12.05 hrs, Volume=	0.092 af
Outflow =	1.4 cfs @ 12.05 hrs, Volume=	0.092 af, Atten= 0%, Lag= 0.0 min
Primary =	1.4 cfs @ 12.05 hrs, Volume=	0.092 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 20.62' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	8.90'	10.0" Round Culvert L= 37.5' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 8.90' / 8.84' S= 0.0016 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=12.54' TW=17.51' (Dynamic Tailwater)

Pond AEI 3:



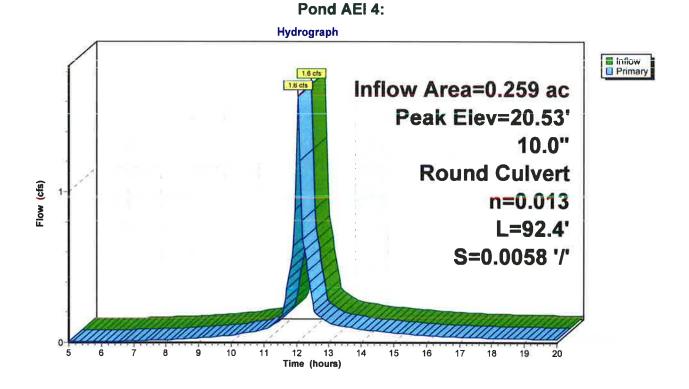
Summary for Pond AEI 4:

Inflow Area =	0.259 ac, 54.37% Impervious, Inflow Depth > 4.90" for 50 year event	
Inflow =	1.6 cfs @ 12.04 hrs, Volume= 0.106 af	
Outflow =	1.6 cfs @ 12.04 hrs, Volume= 0.106 af, Atten= 0%, Lag= 0.0 min	
Primary =	1.6 cfs @ 12.04 hrs, Volume= 0.106 af	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 20.53' @ 12.09 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	8.69'	10.0" Round Culvert L= 92.4' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 8.69' / 8.15' S= 0.0058 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=17.18' TW=19.53' (Dynamic Tailwater)



2790 Existing ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00s/n 00801© 2013 HydroCAD Software Solutions LLCPage 77

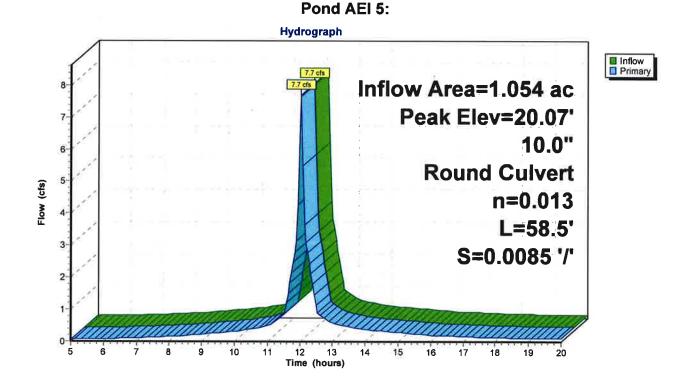
Summary for Pond AEI 5:

Inflow Area =	1.054 ac, 83.18% Impervious, Inflow De	epth > 5.97" for 50 year event
Inflow =	7.7 cfs @ 12.04 hrs, Volume=	0.524 af
Outflow =	7.7 cfs @ 12.04 hrs, Volume=	0.524 af, Atten= 0%, Lag= 0.0 min
Primary =	7.7 cfs @ 12.04 hrs, Volume=	0.524 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 20.07' @ 12.04 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.90'	10.0" Round Culvert L= 58.5' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.90' / 7.40' S= 0.0085 '/' Cc= 0.900 n= 0.013 Clay tile, Flow Area= 0.55 sf

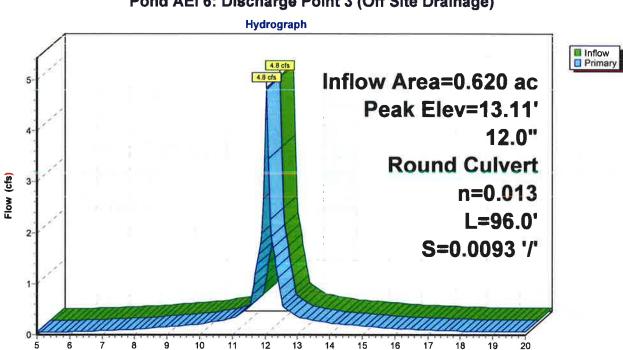
Primary OutFlow Max=7.5 cfs @ 12.04 hrs HW=19.41' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 7.5 cfs @ 13.68 fps)



Summary for Pond AEI 6: Discharge Point 3 (Off Site Drainage)

Inflow Area = 0.620 ac. 93.86% Impervious. Inflow Depth > 6.45" for 50 year event 0.333 af Inflow 4.8 cfs @ 12.04 hrs, Volume= = 4.8 cfs @ 12.04 hrs, Volume= Outflow = 0.333 af, Atten= 0%, Lag= 0.0 min 4.8 cfs @ 12.04 hrs, Volume= Primary = 0.333 af Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 13.11' @ 12.07 hrs Flood Elev= 10.77' Device Routing Invert Outlet Devices #1 Primary 6.77' 12.0" Round Culvert L= 96.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.77' / 5.88' S= 0.0093 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.3 cfs @ 12.04 hrs HW=12.43' TW=11.17' (Dynamic Tailwater) 1=Culvert (Outlet Controls 3.3 cfs @ 4.24 fps)



Time (hours)

Pond AEI 6: Discharge Point 3 (Off Site Drainage)

2790 Existing ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 79

Summary for Pond CB 4433:

Inflow Area =	0.122 ac,100.00% Impervious,	Inflow Depth > 6.59" for 50 year event
Inflow =	1.0 cfs @ 12.01 hrs, Volume	
Outflow =	1.0 cfs @ 12.01 hrs, Volume	e= 0.067 af, Atten= 0%, Lag= 0.0 min
Primary =	1.0 cfs @ 12.01 hrs, Volume	e= 0.067 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.92' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		24.0" Round Culvert L= 121.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.38' / 13.99' S= 0.0032 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.0 cfs @ 12.01 hrs HW=15.84' TW=15.90' (Dynamic Tailwater)

Hydrograph Inflow Primary Inflow Area=0.122 ac Peak Elev=15.92' 24.0" **Round Culvert** (cfs) n=0.013 Flow L=121.0' S=0.0032 '/' uuuuuuuuuuuuuuu 5 6 8 ģ 10 11 12 14 15 16 17 18 19 20 13 Time (hours)

Pond CB 4433:

2790 Existing Conditions	Type III 24-hr 50 year Rainfall=7.39"
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Summary for Pond CB 4435:

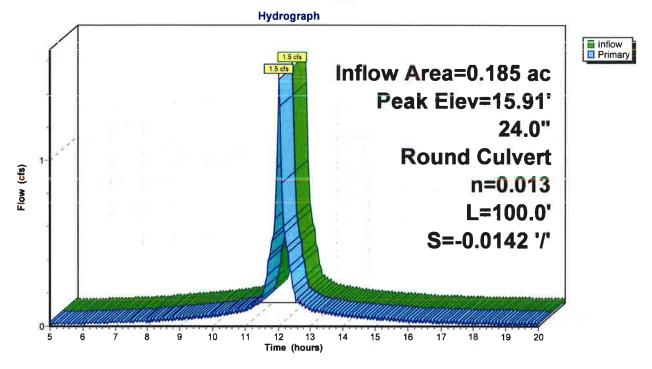
Inflow Area =	0.185 ac,100.00% Impervious, Inflow D	epth > 6.59" for 50 year event
Inflow =	1.5 cfs @ 12.01 hrs, Volume=	0.102 af
Outflow =	1.5 cfs @ 12.01 hrs, Volume=	0.102 af, Atten= 0%, Lag= 0.0 min
Primary =	1.5 cfs @ 12.01 hrs, Volume=	0.102 af

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.91' @ 12.01 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	15.41'	24.0" Round Culvert L= 100.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 13.99' / 15.41' S= -0.0142 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=1.4 cfs @ 12.01 hrs HW=15.90' TW=0.00' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.4 cfs @ 2.38 fps)

Pond CB 4435:



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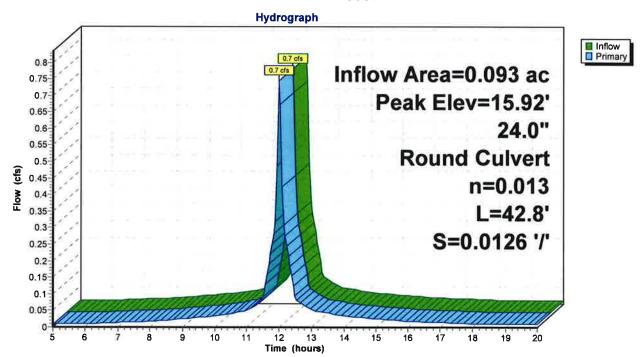
Summary for Pond CB 4560:

Inflow Area =	0.093 ac,100.00% Impervious, Infl	ow Depth > 6.59" for 50 year event	
Inflow =	0.7 cfs @ 12.02 hrs, Volume=	0.051 af	
Outflow =	0.7 cfs @ 12.02 hrs, Volume=	0.051 af, Atten= 0%, Lag= 0.0 min	I.
Primary =	0.7 cfs @ 12.02 hrs, Volume=	0.051 af	

Routing by Dyn-Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 15.92' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.92'	24.0" Round Culvert L= 42.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.92' / 14.38' S= 0.0126 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=15.79' TW=15.85' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs)

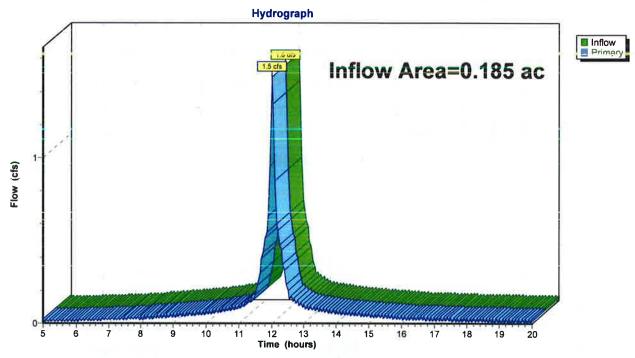


Pond CB 4560:

Summary for Link 2L: Discharge Point 2 (Court Street Drainage)

Inflow Are	a =	0.185 ac,10	0.00% Impervious,	Inflow Depth > 6.5	59" for 50 year event
Inflow	=	1.5 cfs @	12.01 hrs, Volume	e= 0.102 af	
Primary	=	1.5 cfs @	12.01 hrs, Volume	e= 0.102 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link 2L: Discharge Point 2 (Court Street Drainage)

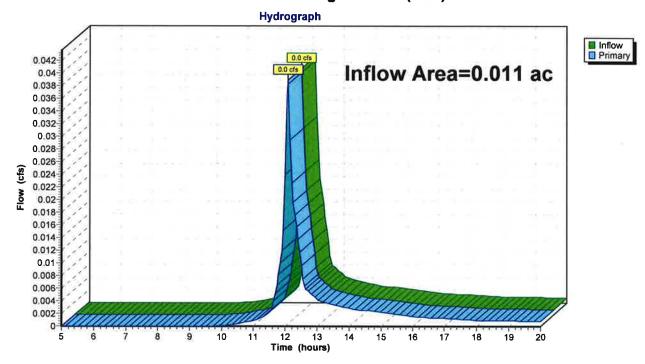
Summary for Link 3L: Discharge Point 4 (DP4)

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Inflow Area =	• 0.011 ac,	0.00% Impervious, Inflow	Depth > 2.75"	for 50 year event
Inflow =	0.0 cfs @	2 12.08 hrs, Volume=	0.003 af	
Primary =	0.0 cfs @	12.08 hrs, Volume=	0.003 af, Att	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



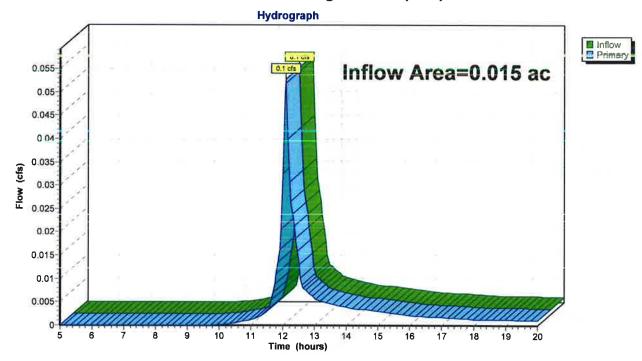
Link 3L: Discharge Point 4 (DP4)

2790 Existing Conditions	Type III 24-hr 50 year Rainfall=7.39"
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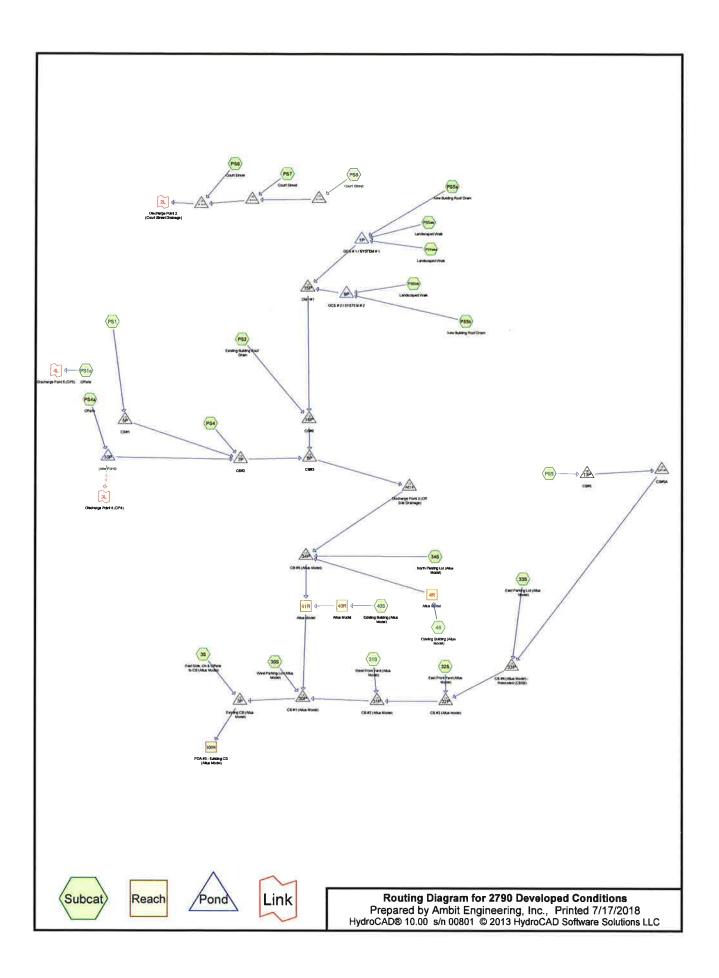
Summary for Link 4L: Discharge Point 5 (DP5)

Inflow Area =	0.015 ac,	0.00% Impervious, Inflo	w Depth > 2.75"	for 50 year event
Inflow =	0.1 cfs @	2 12.08 hrs, Volume=	0.004 af	-
Primary =	0.1 cfs @) 12.08 hrs, Volume=	0.004 af, Att	en= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs



Link 4L: Discharge Point 5 (DP5)



2790 Developed Conditions

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Line# Node In-Invert Out-Invert Length Slope Diam/Width n Height Inside-Fill Number (feet) (feet) (feet) (ft/ft) (inches) (inches) (inches) 1 4R 8.38 7.28 110.0 0.0100 0.012 8.0 0.0 0.0 2 40R 6.82 6.62 10.0 0.0200 0.012 8.0 Ū.Ū 0.0 3 41R 6.45 6.21 81.0 0.0030 0.012 12.0 0.0 0.0 4 **1P** 11.40 11.33 14.0 0.0050 0.013 12.0 0.0 0.0 5 3P 5.76 5.21 55.0 0.0100 0.012 24.0 0.0 0.0 6 5P 9.70 7.13 95.0 0.0271 0.013 12.0 0.0 0.0 7 7P 7.03 6.89 34.0 0.0041 0.013 12.0 0.0 0.0 8 82 6.89 6.11 31.0 0.0039 0.013 12.0 0.0 0.0 9 9P 7.40 7.38 5.0 0.0040 0.013 12.0 0.0 0.0 10 10P 7.39 7.13 53.0 0.0049 0.013 6.0 0.0 0.0 11 13P 8.06 7.86 50.0 0.0040 0.013 12.0 0.0 0.0 12 15P 7.38 7.04 68.0 12.0 0.0050 0.013 0.0 0.0 13 16P 7.04 6.89 30.0 0.0050 0.013 12.0 0.0 0.0 30P 6.11 14 5.86 82.0 0.0030 0.013 24.0 0.0 0.0 15 31P 6.33 6.21 40.0 0.0030 0.012 12.0 0.0 0.0 16 32P 6.71 6.43 92.0 0.0030 0.012 12.0 0.0 0.0 33P 6.96 50.0 17 6.81 0.0030 0.012 12.0 0.0 0.0 18 34P 5.83 5.58 85.0 0.0029 0.013 12.0 0.0 0.0 19 96.0 AEI 6 6.77 5.88 0.0093 0.013 12.0 0.0 0.0 20 CB 4433 14.38 13.99 121.0 0.0032 0.013 24.0 0.0 0.0 21 CB 4435 13.99 15.41 100.0 -0.0142 0.013 24.0 0.0 0.0 22 CB 4560 14.92 14.38 42.8 0.0126 0.013 24.0 0.0 0.0 23 DP1A 7.76 7.06 175.0 0.0040 0.013 12.0 0.0 0.0

Pipe Listing (selected nodes)

Summary for Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)

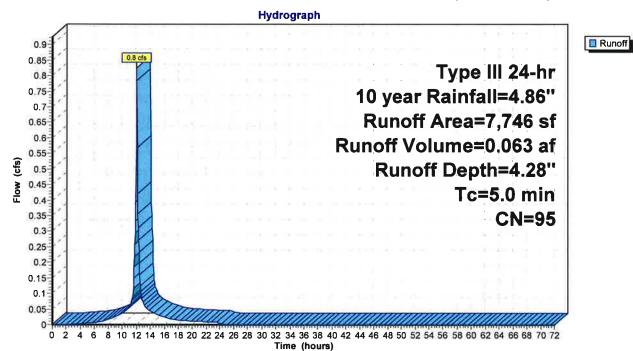
Page 3

Runoff 0.8 cfs @ 12.07 hrs, Volume= 0.063 af, Depth= 4.28" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Α	rea (sf)	CN I	Description		
*		7,746	95	a construction of the second s		
		7,746		100.00% P	ervious Are	a
	Тс	Length	Slope		Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	5.0					Direct Entry,

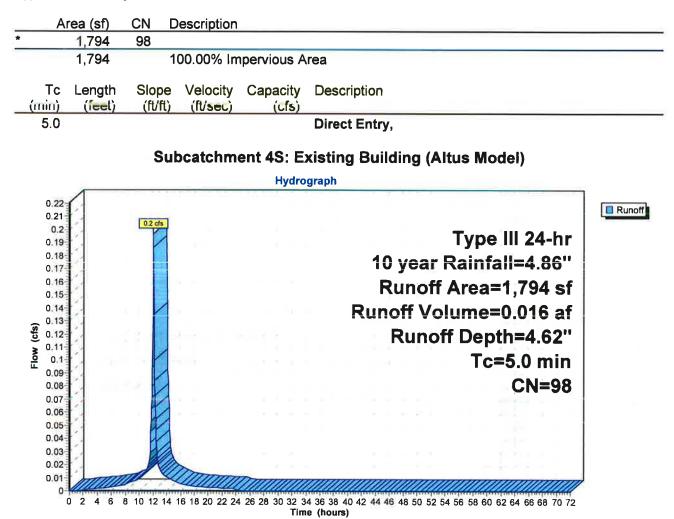
Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)



Summary for Subcatchment 4S: Existing Building (Altus Model)

Runoff = 0.2 cfs @ 12.07 hrs, Volume= 0.016 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"



Summary for Subcatchment 30S: West Parking Lot (Altus Model)

Page 5

Runoff 0.7 cfs @ 12.07 hrs, Volume= = 0.054 af, Depth= 4.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

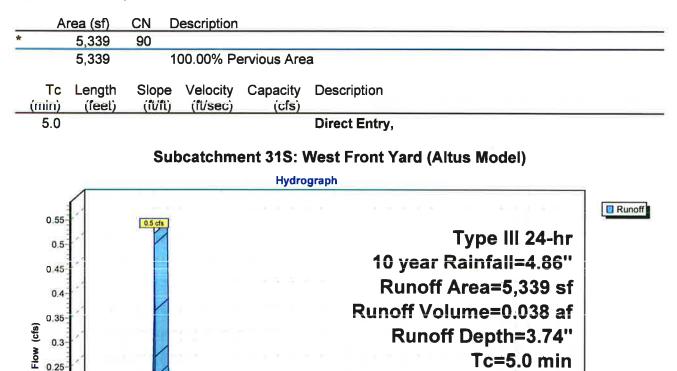
	93				
6,925	1	00.00% Pe	ervious Are	a	
Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
				Direct Entry,	
	Sub	catchme	ent 30S: V	Vest Parking Lot (Altus Model)	
			Hydro	graph	
1					🔲 Runoff
с ,с	0.7 cfs			T WA (1	
	-1				
	-			10 year Rainfall=4.86"	
1 1 1 1	1.			Runoff Area=6.925 sf	
đ.,					
1					
1				· · · · · · · · · · · · · · · · · · ·	
				Tc=5.0 min	
1				CN=93	
	12				
-					
mann		Umm	mmm		
		(feet) (ft/ft) Sub	(feet) (ft/ft) (ft/sec) Subcatchme	(feet) (ft/ft) (ft/sec) (cfs) Subcatchment 30S: V Hydro	(feet) (ft/ft) (ft/sec) (cfs) Direct Entry, Subcatchment 30S: West Parking Lot (Altus Model) Hydrograph Type III 24-hr 10 year Rainfall=4.86'' Runoff Area=6,925 sf Runoff Volume=0.054 af Runoff Depth=4.06'' Tc=5.0 min

Summary for Subcatchment 31S: West Front Yard (Altus Model)

Runoff = 0.5 cfs @ 12.07 hrs, Volume= 0.038 af, Depth= 3.74"

0.2 0.15 0.1 0.05

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"



0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

CN=90

0.056 af, Depth= 3.95"

Summary for Subcatchment 32S: East Front Yard (Altus Model)

Runoff 0.8 cfs @ 12.07 hrs, Volume= =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	7,376 7,376	<u>92</u>	00.00% Pe	ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0				i fan seren de fan	Direct Entry,	
		Su	bcatchm	ent 32S:	East Front Yard (Altus Model)	
					graph	
	(····					Runo
0.8		0.8 cfs			T	0
0.7-	1 55				Type III 24-hr	
0.65	1				10 year Rainfall=4.86"	
0.6	1	1			Runoff Area=7,376 sf	
0.55						
0.5	Č.				Runoff Volume=0.056 af	
0.45	0 0	. i			Runoff Depth=3.95"	
(cls) 0.45	0				Tc=5.0 min	
0.35					the second se	
0.3	(CN=92	
0.25	×				the second s	
0.2	×	R				
0.15	1				1 전 20 Min 2017년 2017년 - 12 Min 2017년 2017년 - 12 Min 2017년 2017년 2017년 2017년 2017년 2017년 2017년 2017년 2017년 2017	
0.05	1	K	The		5	
	ATTITA			11111111		

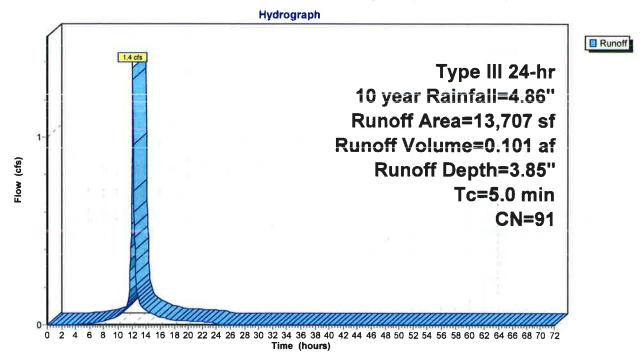
Summary for Subcatchment 33S: East Parking Lot (Altus Model)

Runoff = 1.4 cfs @ 12.07 hrs, Volume= 0.101 af, Depth= 3.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	rea (sf)	CN E	Description		
*	13,707	91			
	13,707	1	00.00% Pe	ervious Are	a
Тс	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(CfS)	
5.0					Direct Entry,

Subcatchment 33S: East Parking Lot (Altus Model)



2790 Developed Conditions	Type III 24-hr	10 year Rain	nfall=4.86"
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Summary for Subcatchment 34S: North Parking Lot (Altus Model)

Runoff = 0.7 cfs @ 12.07 hrs, Volume= 0.053 af, Depth= 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	6,462 6,462	<u>95</u> 1	00.00% P	ervious Are	a	
Tc nin)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	
5.0				i i	Direct Entry,	
		Sub	catchme	nt 34S: N	orth Parking Lot (Altus Model)	
				Hydro	graph	
0.75	f l	- Locks in				Rune
0.7-		0.7 cfs			Type III 24-hr	
0.65					10 year Rainfall=4.86"	
0.55	212.3				Runoff Area=6,462 sf	
0.5	. — ·			1 101 1	Runoff Volume=0.053 af	
0.45	1000				Runoff Depth=4.28"	
0.35					Tc=5.0 min	
0.3	Q				CN=95	
0.25	2					
0.15						
0.1	Ş		× · · · · ·			
0.05	mm		Imm	manna		

2790 Developed Conditions	Type III 24-hr	10 year Rainfall=4.86"
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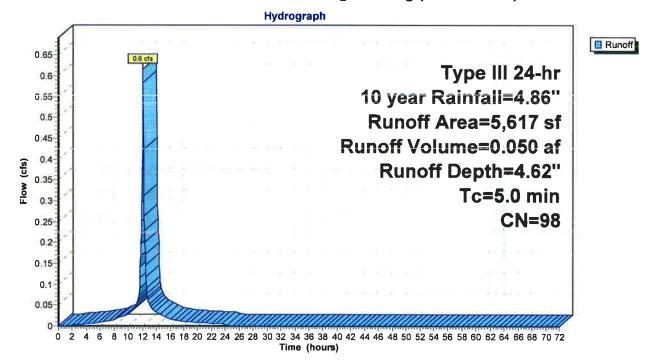
Summary for Subcatchment 40S: Existing Building (Altus Model)

Runoff = 0.6 cfs @ 12.07 hrs, Volume= 0.050 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

A	rea (sf)	CN E	Description			
*	5,617	98				
	5,617	1	00.00% Im	npervious A	Area	
Тс	Length	Slope	Velocity	Capacity	Description	
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(CfS)		
5.0			(1		Direct Entry,	
(min)		Slope (ft/ft)				

Subcatchment 40S: Existing Building (Altus Model)



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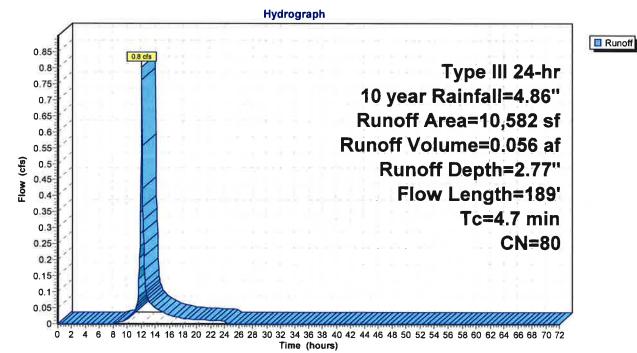
Summary for Subcatchment PS1:

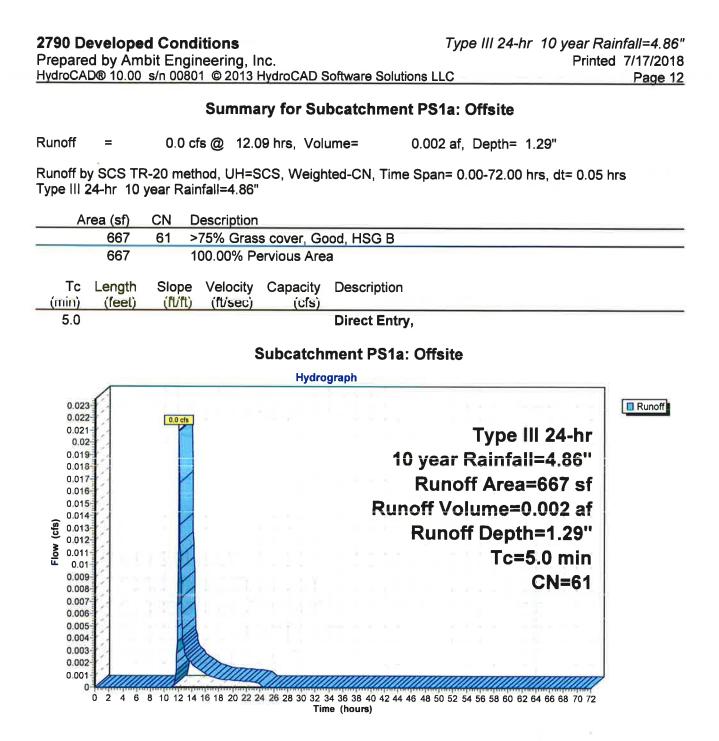
Runoff = 0.8 cfs @ 12.07 hrs, Volume= 0.056 af, Depth= 2.77"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN [Description									
		6,399	98 F	8 Paved parking, HSG A									
*		939	98 F	Paved sidewalks w/curbs & sewers, HSG A									
		3,244	39 >	>75% Grass cover, Good, HSG A									
		10,582	80 \										
		3,244	3	30.66% Pervious Area									
		7,338	6	69.34% Imp	pervious Ar	ea							
	Tc	Length	Slope	Velocity	Capacity	Description							
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)								
	3.9	32	0.0200	0.14		Sheet Flow,							
						Grass: Short n= 0.150 P2= 3.21"							
	0.8	157	0.0287	3.44		Shallow Concentrated Flow,							
						Paved Kv= 20.3 fps							
23	4.7	189	Total										

Subcatchment PS1:





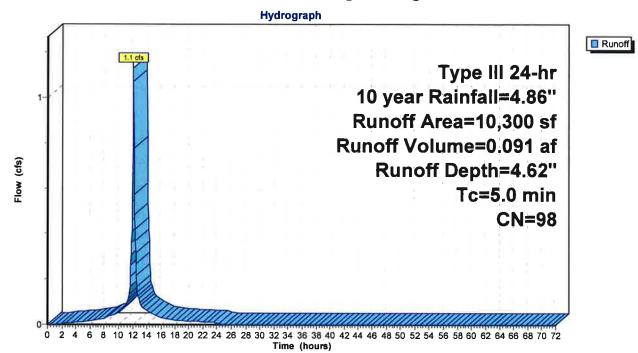
Summary for Subcatchment PS2: Existing Building Roof Drain

Runoff = 1.1 cfs @ 12.07 hrs, Volume= 0.091 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

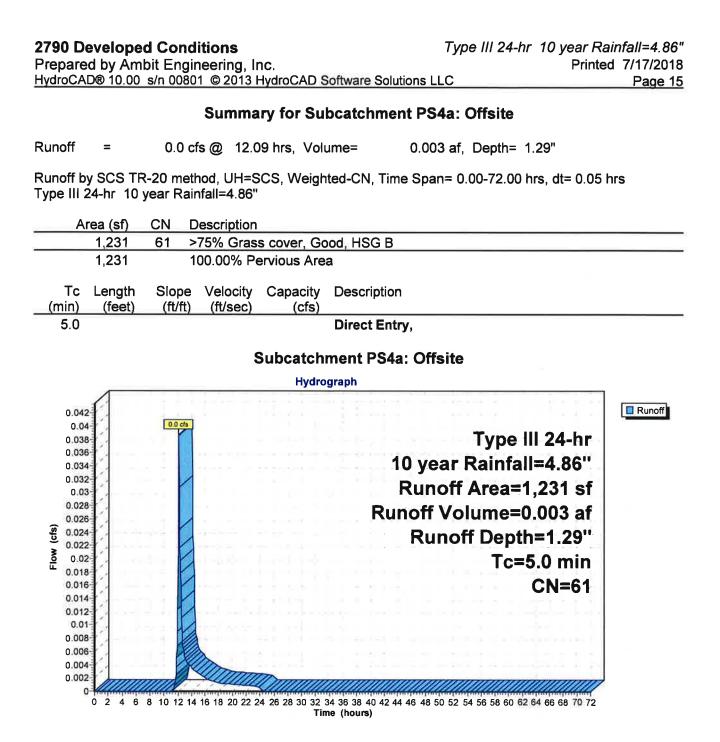
Α	rea (sf)	CN [Description		
	10,300	98 I	Roofs, HSG) A	
	10,300		00.00% Im	Area	
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Subcatchment PS2: Existing Building Roof Drain

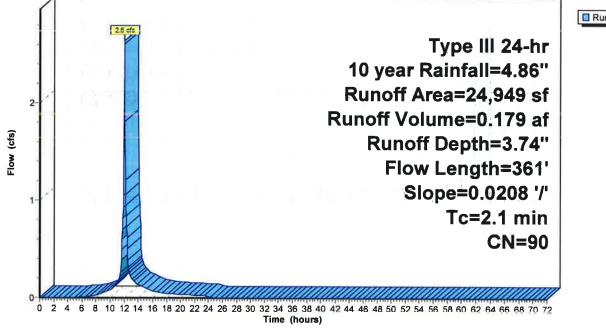


Prepare		bit Engi	neering, Ir		Software Sol		be III 24-hr	-	ainfall=4.86" ed 7/17/2018 Page 14
			Sur	nmary fo	r Subcato	hment PS	54 :		
Runoff	=	0.5 c	fs @ 12.0	2 hrs, Vol	ume=	0.030 af	, Depth= 2.	.01"	
			hod, UH=S nfall=4.86"	CS, Weigh	nted-CN, Tii	ne Span= 0	0.00-72.00 h	rs, dt= 0.05	hrs
ΑΑ	rea (sf)	CN D	escription						
	3,513 4,168				ood, HSG A & sewers, H				
·	7,681		Veighted A		a sewers, r	JU A			
	3,513	4	5.74% Per	vious Area					
	4,168	5	4.26% imp	pervious Ar	ea				
Tc	Length	Slope	Velocity	Capacity	Descriptio	n			
<u>(min)</u> 0.7	(feet) 114	(ft/ft) 0.0200	(ft/sec) 2.87	(cfs)	Shallow (Concentrate	ed Flow.		
						v= 20.3 fps	,		
				Subca	atchment	PS4:			
					atchment	PS4:			
0.5						PS4:			Runoff
0.48 0.46		0.5 uts				PS4:	Type II	l 24-hr	Runoff
0.48 0.46 0.44 0.42	the second s	0.5 uts			ograph		Type II Rainfall		Runoff
0.40 0.46 0.44 0.42 0.4 0.38		0.5 uts			ograph	10 year	Rainfall	=4.86"	Runoff
0.48 0.46 0.44 0.42 0.4 0.38 0.36 0.36		0.5 uts			ograph	10 year Runoff	Rainfall Area=7	=4.86'' ,681 sf	Runoff
0.48 0.46 0.44 0.42 0.4 0.38 0.36 0.34 0.32		0.5 uts			ograph	10 year Runoff inoff Vo	Rainfall Area=7 lume=0	=4.86" ,681 sf .030 af	Runoff
0.48 0.46 0.44 0.42 0.4 0.38 0.38 0.36 0.34 0.32 (\$\$)0.28		0.5 ds			ograph	10 year Runoff Inoff Vo Runo	Rainfall Area=7 lume=0 ff Depth	=4.86" ,681 sf .030 af =2.01"	Runoff
0.48 0.44 0.44 0.42 0.38 0.36 0.34 0.32 (\$2 0.33 0.28 0.28 0.28 0.24 0.22		0.5 ưs			ograph	10 year Runoff Inoff Vo Runof Flov	Rainfall Area=7 lume=0 ff Depth w Lengt	=4.86" ,681 sf .030 af =2.01" h=114'	Runoff
0.48 0.46 0.44 0.42 0.42 0.38 0.36 0.34 0.32 (sj) 0.28 0.28 0.28 0.26 0.24		0.5 uts			ograph	10 year Runoff Inoff Vo Runof Flov	Rainfall Area=7 lume=0 ff Depth w Lengt lope=0.0	=4.86" ,681 sf .030 af =2.01" h=114' 0200 '/'	Runoff
0.48 0.46 0.44 0.42 0.4 0.38 0.36 0.34 0.32 0.32 0.32 0.28 0.28 0.26 0.22 0.22 0.22 0.22		0.5 ds			ograph	10 year Runoff Inoff Vo Runof Flov	Rainfall Area=7 lume=0 ff Depth w Lengt lope=0.0 Tc=0	=4.86" ,681 sf .030 af =2.01" h=114' 0200 '/' 0.7 min	Runoff
0.48 0.46 0.44 0.38 0.36 0.34 0.32 0.32 0.32 0.28 0.26 0.22 0.22 0.22 0.22 0.22 0.22 0.24 0.16 0.14 0.14		0.5 uls			ograph	10 year Runoff Inoff Vo Runof Flov	Rainfall Area=7 lume=0 ff Depth w Lengt lope=0.0 Tc=0	=4.86" ,681 sf .030 af =2.01" h=114' 0200 '/'	Runoff
0.48 0.44 0.44 0.38 0.36 0.34 0.32 0.28 0.28 0.28 0.24 0.22 0.22 0.22 0.18 0.16 0.12 0.12		0.5 c/s			ograph	10 year Runoff Inoff Vo Runof Flov	Rainfall Area=7 lume=0 ff Depth w Lengt lope=0.0 Tc=0	=4.86" ,681 sf .030 af =2.01" h=114' 0200 '/' 0.7 min	Runoff

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)



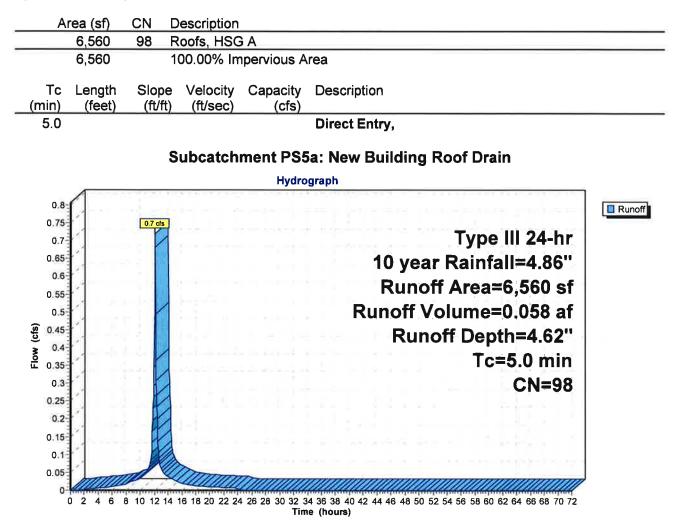
Prepare	d by Am	ed Cond	neering, I	nc. HydroCAD 9	Software S	דאָן Solutions LLC	be III 24-h	-	Rainfall=4.86" ed 7/17/2018
<u></u>		un obod				tchment PS	5 5:		Page 16
Runoff	=	2.6 c	fs @ 12.0	94 hrs, Vol	ume=	0.179 a f,	Depth= 3	3.74"	
Runoff by Type III 2	y SCS TI 24-hr 10	R-20 met year Raii	hod, UH=S nfall=4.86"	SCS, Weigh	nted-CN,	Time Span= 0	.00-72.00	hrs, dt= 0.05	i hrs
A	rea (sf)	CN E	Description						
	19,373		aved road	s w/curbs &	& sewers,	HSG A			
*	1,796				rbs & sew	vers, HSG A			
	388		Roofs, HSC						
	3,392			s cover, Go	000, HSG	A			
	24,949 3,392		Veighted A	werage vious Area					
	21,557			vious Area					
	21,007	0	0.4070 111		ca				
Тс	Length	Slope	Velocity		Descrip	tion			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
2.1	361	0.0208	2.93			/ Concentrate Kv= 20.3 fps	ed Flow,		
				Subca	atchmer	nt PS5:			
				Hydro	graph				
ſ									
		2.6 cfs							Runoff
								ll 24-hr	
						10 yoo-			
						10 year			
~	95 T T	100				Runoff A	rea=24	1949 ef	



Summary for Subcatchment PS5a: New Building Roof Drain

Runoff = 0.7 cfs @ 12.07 hrs, Volume= 0.058 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"



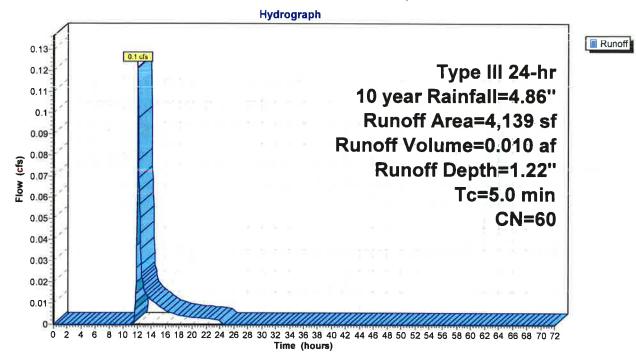
Summary for Subcatchment PS5aa: Landscaped Walk

Runoff = 0.1 cfs @ 12.09 hrs, Volume= 0.010 af, Depth= 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	Area (sf)	CN	Description					
	2,666	39	>75% Gras	75% Grass cover, Good, HSG A				
	852	98	Roofs, HSC					
*	621	98	Paved side	walks w/cu	rbs & sewers, HSG A			
	4,139 2,666 1,473	60	Weighted A 64.41% Pe 35.59% Imp	rvious Area				
To (min		Slope (ft/ft		Capacity (cfs)	Description			
5.0	כ				Direct Entry,			

Subcatchment PS5aa: Landscaped Walk



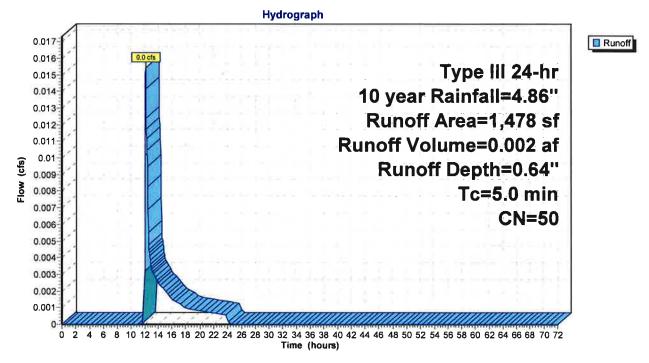
Summary for Subcatchment PS5aaa: Landscaped Walk

Runoff = 0.0 cfs @ 12.12 hrs, Volume= 0.002 af, Depth= 0.64"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

_	<u> </u>	rea (sf)	CN	Description			
		1,200	39	>75% Gras	75% Grass cover, Good, HSG A		
*		278	98	Paved side	walk w/curb	os & sewers, HSG A	
		1,478 1,200 278	50	Weighted A 81.19% Pei 18.81% Imp	rvious Area		
	Tc (min)	Length (feet)	Slop (ft/ff		Capacity (cfs)	Description	
	5.0					Direct Entry,	

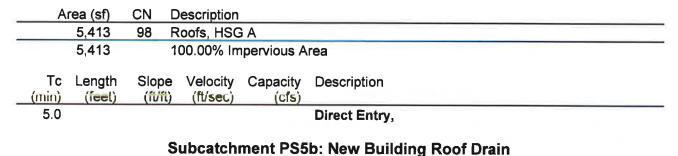
Subcatchment PS5aaa: Landscaped Walk



Summary for Subcatchment PS5b: New Building Roof Drain

Runoff = 0.6 cfs @ 12.07 hrs, Volume= 0.048 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"



Hydrograph 0.65 Runoff 0.6 cfs 0.6 Type III 24-hr 0.55 10 year Rainfall=4.86" 0.5 Runoff Area=5,413 sf 0.45 Runoff Volume=0.048 af 0.4 (cfs) Runoff Depth=4.62" 0.35 Flow Tc=5.0 min 0.3 0.25 **CN=98** 0.2 0.15 0.1 0.05 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

2790 Developed Conditions	Type III 24-hr	10 year Rain	fall=4.86"
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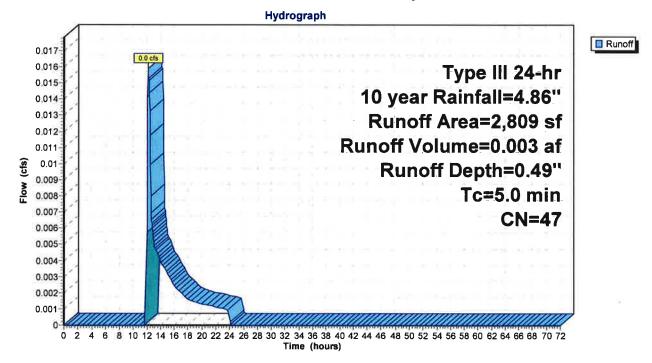
Summary for Subcatchment PS5bb: Landscaped Walk

Runoff = 0.0 cfs @ 12.16 hrs, Volume= 0.003 af, Depth= 0.49"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

_	A	rea (sf)	CN	Description	Description				
		2,409	39	>75% Gras	75% Grass cover, Good, HSG A				
*		400	98	Paved side	walk w/curb	bs & sewers, HSG A			
		2,809	47	Weighted Average					
		2,409		85.76% Pe	rvious Area				
		400		14.24% Imp	ea				
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description			
	5.0					Direct Entry,			

Subcatchment PS5bb: Landscaped Walk



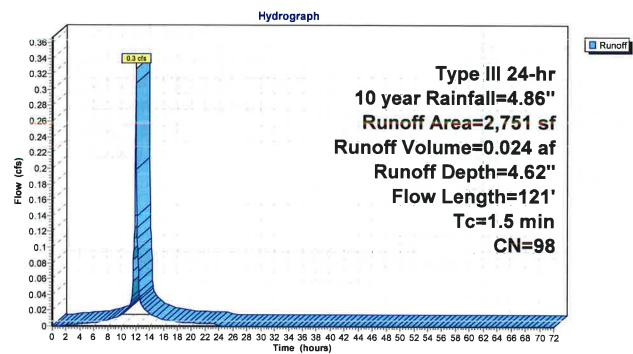
Summary for Subcatchment PS6: Court Street

Runoff = 0.3 cfs @ 12.02 hrs, Volume= 0.024 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN	Description			
		2,556	98	Paved park	ing, HSG B		
*		195	98	Unconnecte	ed pavemer	nt, sidewalk, HSG B	
		2,751	98	98 Weighted Average			
		2,751		100.00% In	npervious A	rea	
		195		7.09% Unconnected			
	Тс	Length	Slope	Velocity	Capacity	Description	
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	0.6	26	0.0096	0.69		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.9	95	0.0078	1.79		Shallow Concentrated Flow,	
-		_				Paved Kv= 20.3 fps	
	1.5	121	Total				

Subcatchment PS6: Court Street



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Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018 C Page 23

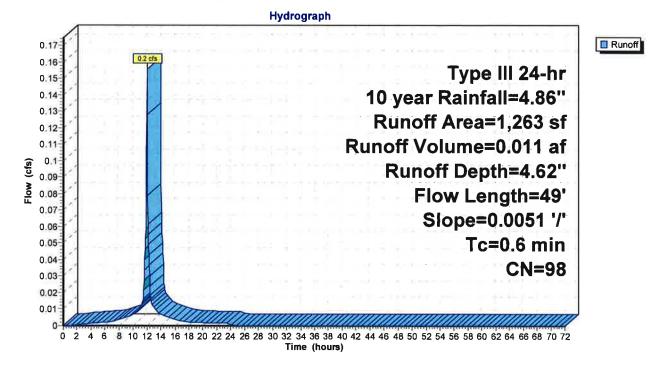
Summary for Subcatchment PS7: Court Street

Runoff = 0.2 cfs @ 12.01 hrs, Volume= 0.011 af, Depth= 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN	Description				
		922	98	Paved park	ing, HSG B	3		
*		341	98	Unconnecte	ed pavemer	nt, sidewalk, HSG B		
		1,263	98	Weighted A	Veighted Average			
		1,263		100.00% In	npervious A	Area		
		341		27.00% Unconnected				
	Tc (min)	Length	Slope		Capacity	Description		
-	(min)	(feet)	(ft/ft)		(cfs)			
	0.6	49	0.0051	1.45		Shallow Concentrated Flow, Paved Kv= 20.3 fps		

Subcatchment PS7: Court Street



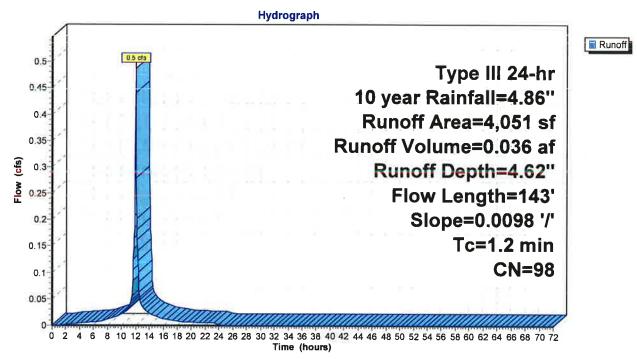
Summary for Subcatchment PS8: Court Street

Runoff = 0.5 cfs @ 12.02 hrs, Volume= 0.036 af.	Depth=	4.62"
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Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 10 year Rainfall=4.86"

	A	rea (sf)	CN I	Description				
		1,014	98 I	Paved park	ing, HSG B	3		
*		3,037	98 l	Jnconnecte	ed pavemer	nt,sidewalk, HSG B		
		4,051	98 \	Veighted Average				
		4,051		100.00% In	npervious A	Area		
		3,037	7	74.97% Unconnected				
	_							
	Tc	Length	Slope		Capacity	Description		
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	1.2	143	0.0098	2.01		Shallow Concentrated Flow,		
						Paved Kv= 20.3 fps		

Subcatchment PS8: Court Street



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Summary for Reach 4R: Altus Model

0.041 ac,100.00% Impervious, Inflow Depth = 4.62" for 10 year event Inflow Area = Inflow = 0.2 cfs @ 12.07 hrs, Volume= 0.016 af Outflow 0.2 cfs @ 12.08 hrs, Volume= = 0.016 af, Atten= 1%, Lag= 0.8 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 2.68 fps, Min. Travel Time= 0.7 min Avg. Velocity = 0.88 fps, Avg. Travel Time= 2.1 min

Peak Storage= 8 cf @ 12.08 hrs Average Depth at Peak Storage= 0.17' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.3 cfs

8.0" Round Pipe n= 0.012 Length= 110.0' Slope= 0.0100 '/' Inlet Invert= 8.38', Outlet Invert= 7.28'



Hydrograph Inflow 0.22 Outflow 0.2 0.21 Inflow Area=0.041 ac 0.2 cfs 0.2 0.19 Avg. Flow Depth=0.17' 0.18-0.17 Max Vel=2.68 fps 0.16 0.15 8.0" 0.14 0.13 **Round Pipe** (cfs) 0.12 0.11 n=0.012 Flow 0.1 L=110.0' 0.09 0.08 S=0.0100 '/' 0.07 0.06 Capacity=1.3 cfs 0.05 0.04 0.03 0.02 0.01 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Reach 4R: Altus Model

Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018 Page 25



2790 Developed ConditionsType III 24-hr 10 year Rainfall=4.86"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 26

Summary for Reach 40R: Altus Model

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth =
 4.62" for 10 year event

 Inflow =
 0.6 cfs @
 12.07 hrs, Volume=
 0.050 af

 Outflow =
 0.6 cfs @
 12.07 hrs, Volume=
 0.050 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 4.74 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.59 fps, Avg. Travel Time= 0.1 min

Peak Storage= 1 cf @ 12.07 hrs Average Depth at Peak Storage= 0.27' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.9 cfs

8.0" Round Pipe n= 0.012 Length= 10.0' Slope= 0.0200 '/' Inlet Invert= 6.82', Outlet Invert= 6.62'



Hydrograph Inflow Outflow 0.6 0.65 Inflow Area=0.129 ac 0 0.6 Avg. Flow Depth=0.27' 0.55 Max Vel=4.74 fps 0.5 8.0" 0.45 **Round Pipe** 0.4 Flow (cfs) 0.35 n=0.012 0.3 L=10.0' 0 25 S=0.0200 '/' 0.2 Capacity=1.9 cfs 0.15 0.1 0.05 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Reach 40R: Altus Model

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Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018 C Page 27

Summary for Reach 41R: Altus Model

 Inflow Area =
 1.471 ac, 67.65% Impervious, Inflow Depth =
 2.83" for 10 year event

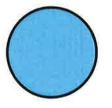
 Inflow =
 4.0 cfs @
 12.07 hrs, Volume=
 0.347 af

 Outflow =
 2.1 cfs @
 12.00 hrs, Volume=
 0.347 af, Atten= 48%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 3.03 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.29 fps, Avg. Travel Time= 1.0 min

Peak Storage= 64 cf @ 12.00 hrs Average Depth at Peak Storage= 1.00' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.1 cfs

12.0" Round Pipe n= 0.012 Length= 81.0' Slope= 0.0030 '/' Inlet Invert= 6.45', Outlet Invert= 6.21'



Hydrograph Inflow Outflow 4.0 cfs Inflow Area=1.471 ac Avg. Flow Depth=1.00' Max Vel=3.03 fps 12.0" 3 **Round Pipe** (cfs) 2.1 cfs n=0.012 Flow 2 L=81.0' S=0.0030 '/' Capacity=2.1 cfs 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

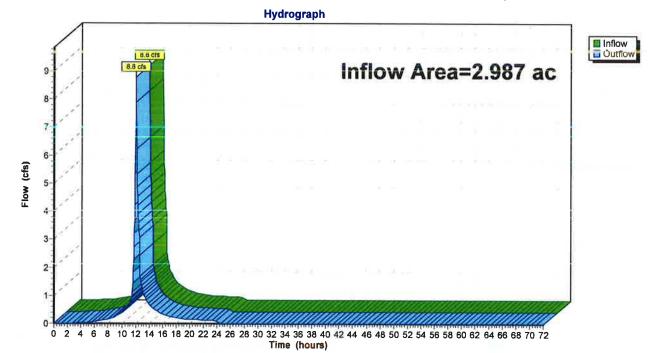
Reach 41R: Altus Model

Summary for Reach 300R: POA #3 - Existing CB (Altus Model)

Inflow Area	a =	2.987 ac, 49.88% Impervious, Inflow Depth = 3.37" for 10 year event
Inflow	=	8.8 cfs @ 12.06 hrs, Volume= 0.838 af
Outflow	=	8.8 cfs @ 12.06 hrs, Volume= 0.838 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Reach 300R: POA #3 - Existing CB (Altus Model)



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Summary for Pond 1P: OCS # 1 / SYSTEM # 1

Inflow Area =	0.280 ac, 68.25% Impervious, Inflow De	epth = 2.98" for 10 year event
Inflow =	0.9 cfs @ 12.07 hrs, Volume=	0.069 af
Outflow =	0.3 cfs @ 12.35 hrs, Volume=	0.069 af, Atten= 64%, Lag= 16.4 min
Discarded =	0.0 cfs @ 8.55 hrs, Volume=	0.033 af
Primary =	0.3 cfs @ 12.35 hrs, Volume=	0.036 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 12.43' @ 12.35 hrs Surf.Area= 0.015 ac Storage= 0.022 af

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 156.8 min (926.7 - 769.9)

Volume	Invert	Avail.Storage	e Storage Description
#1	10.50'	0.014 a	af 24.00'W x 27.00'L x 4.00'H Prismatoid
	44.00		0.060 af Overall - 0.025 af Embedded = 0.035 af x 40.0% Voids
#2	11.00'	0.025 a	
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
-			Row Length Adjustment= +0.44' x 6.45 sf x 6 rows
		0.039 a	af Total Available Storage
Device	Routing	Invert (Outlet Devices
#1	Primary	11.40' 1	I2.0" Round Culvert
		L	_= 14.0' CPP, square edge headwall, Ke= 0.500
		1	nlet / Outlet Invert= 11.40' / 11.33' S= 0.0050 '/' Cc= 0.900
		r	n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1		2.0" Vert. Orifice/Grate X 3.00 C= 0.600
#3	Device 1	14.50' 4	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Discarded		1.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.0 cfs @ 8.55 hrs HW=10.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.3 cfs @ 12.35 hrs HW=12.43' TW=8.50' (Dynamic Tailwater)

1=Culvert (Passes 0.3 cfs of 2.2 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.3 cfs @ 4.42 fps)

-3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

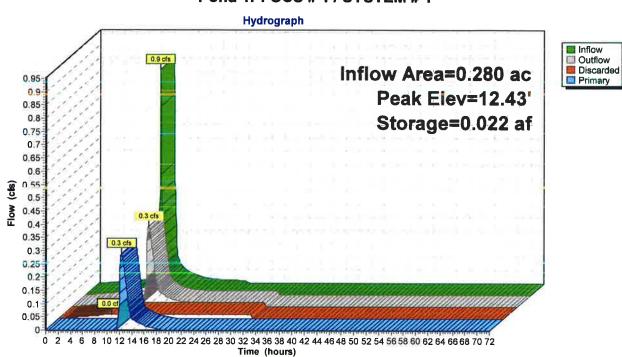
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 Type III 24-hr
 10 year Rainfall=4.86"

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Pond 1P: OCS # 1 / SYSTEM # 1

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Summary for Pond 3P: Existing CB (Altus Model)

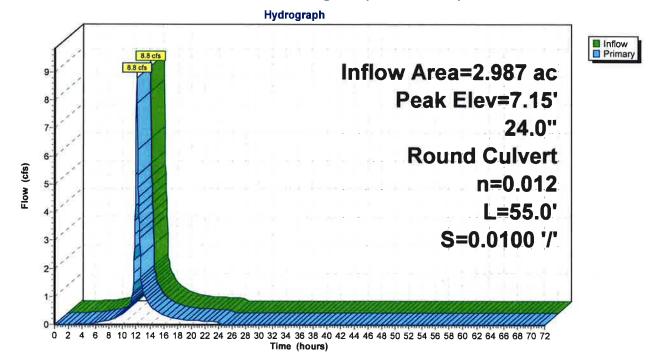
2.987 ac. 49.88% Impervious, Inflow Depth = 3.37" for 10 year event Inflow Area = Inflow 8.8 cfs @ 12.06 hrs, Volume= 0.838 af = Outflow 8.8 cfs @ 12.06 hrs, Volume= = 0.838 af, Atten= 0%, Lag= 0.0 min Primary Ξ 8.8 cfs @ 12.06 hrs, Volume= 0.838 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 7.15' @ 12.06 hrs Flood Elev= 8.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	5.76'	24.0" Round Culvert L= 55.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.76' / 5.21' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf

Primary OutFlow Max=8.7 cfs @ 12.06 hrs HW=7.14' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 8.7 cfs @ 5.28 fps)

Pond 3P: Existing CB (Altus Model)



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Summary for Pond 5P: CB#1

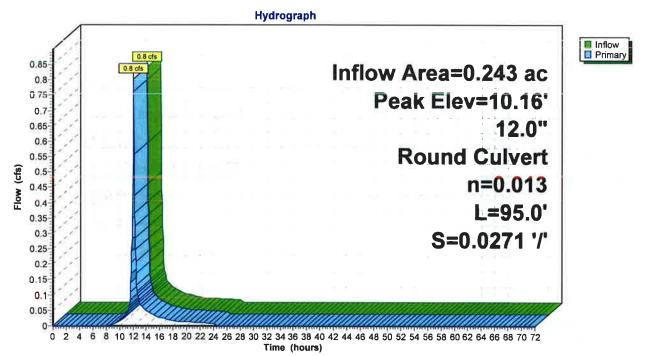
Inflow Area =	0.243 ac, 69.34% Impervious, Inflow Dept	th = 2.77" for 10 year event
inflow =	0.8 cfs @ 12.07 hrs, Volume= 0).056 af
Outflow =	0.8 cfs @ 12.07 hrs, Volume= 0	0.056 af, Atten= 0%, Lag= 0.0 min
Primary =	0.8 cfs @ 12.07 hrs, Volume= 0).056 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 10.16' @ 12.07 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	9.70'	12.0" Round Culvert
			L= 95.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 9.70' / 7.13' S= 0.0271 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.8 cfs @ 12.07 hrs HW=10.15' TW=8.18' (Dynamic Tailwater) -1=Culvert (Inlet Controls 0.8 cfs @ 2.28 fps)

Pond 5P: CB#1



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Type III 24-hr 10 year Rainfall=4.86" Printed 7/17/2018 C Page 33

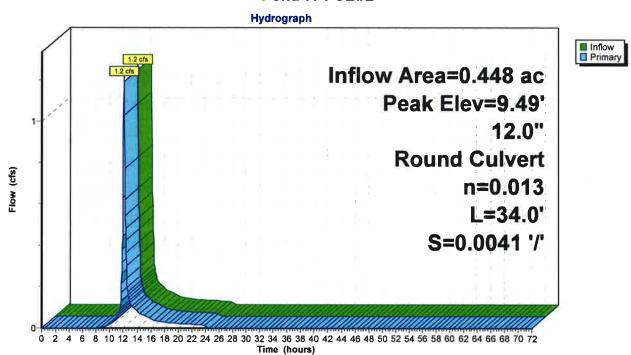
Summary for Pond 7P: CB#2

Inflow Area	a =	0.448 ac, 59.02% Impervious, Inflow Depth = 2.30" for 10 year e	event
Inflow	=	1.2 cfs @ 12.05 hrs, Volume= 0.086 af	
Outflow	=	1.2 cfs @ 12.05 hrs, Volume= 0.086 af, Atten= 0%, Lag=	= 0.0 min
Primary	=	1.2 cfs @ 12.05 hrs, Volume= 0.086 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.49' @ 12.20 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.03'	12.0" Round Culvert L= 34.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.03' / 6.89' S= 0.0041 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=8.05' TW=8.32' (Dynamic Tailwater)



Pond 7P: CB#2

2790 Developed Conditions 7	ype III 24-hr 10 year Rainfall=4.86"
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Summary for Pond 8P: CB#3

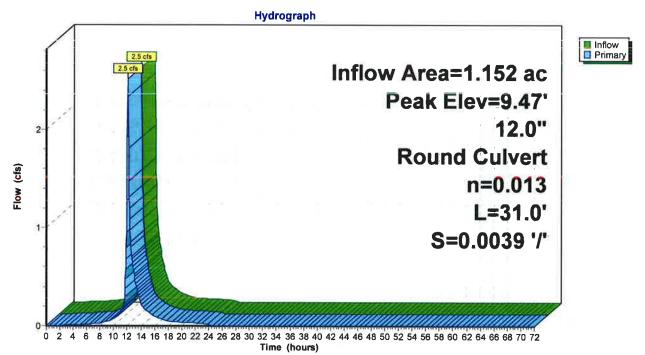
Inflow Area =	1.152 ac, 71.58% Impervious, Inflow Depth	= 2.38" for 10 year event
Inflow =	2.5 cfs @ 12.06 hrs, Volume= 0.2	228 af
Outflow =	2.5 cfs @ 12.06 hrs, Volume= 0.2	228 af, Atten= 0%, Lag= 0.0 min
Primary =	2.5 cfs @ 12.06 hrs, Volume= 0.2	228 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.47' @ 12.15 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	6.89'	12.0" Round Culvert
			L= 31.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.89' / 6.77' S= 0.0039 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.06 hrs HW=8.48' TW=8.77' (Dynamic Tailwater)

Pond 8P: CB#3



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Summary for Pond 9P: OCS # 2 / SYSTEM # 2

Inflow Area =	0.189 ac, 70.70% Impervious, Inflow Depth = 3.21" for 10 year event	
Inflow =	0.6 cfs @ 12.07 hrs, Volume= 0.051 af	
Outflow =	0.2 cfs @ 12.91 hrs, Volume= 0.051 af, Atten= 73%, Lag= 50.4 min	;
Discarded =	0.0 cfs @ 9.70 hrs, Volume= 0.035 af	
Primary =	0.1 cfs @ 12.91 hrs, Volume= 0.016 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 8.17' @ 12.51 hrs Surf Area= 0.019 ac Storage= 0.022 af

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 187.7 min (945.1 - 757.4)

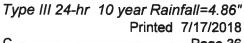
Volume	Invert	Avail.Stora	ge Storage Description			
#1	6.50'	0.019				
			0.074 af Overall - 0.026 af Embedded = 0.049 af x 40.0% Voids			
#2	7.00'	0.026				
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf			
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap Row Length Adjustment= +0.44' x 6.45 sf x 7 rows			
-		0.045				
		0.040				
Device	Routing	Invert	Outlet Devices			
#1	Primary	7.40'	12.0" Round Culvert			
			L= 5.0' CPP, square edge headwall, Ke= 0.500			
			nlet / Outlet Invert= 7.40' / 7.38' S= 0.0040 '/' Cc= 0.900			
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf			
#2	Device 1		.0" Vert. Orifice/Grate X 3.00 C= 0.600			
#3	Device 1	10.50'	.0' long x 0.5' breadth Broad-Crested Rectangular Weir			
			lead (feet) 0.20 0.40 0.60 0.80 1.00			
			Coef. (English) 2.80 2.92 3.08 3.30 3.32			
#4	Discarded	6.50'	1.000 in/hr Exfiltration over Surface area			

Discarded OutFlow Max=0.0 cfs @ 9.70 hrs HW=6.54' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.0 cfs)

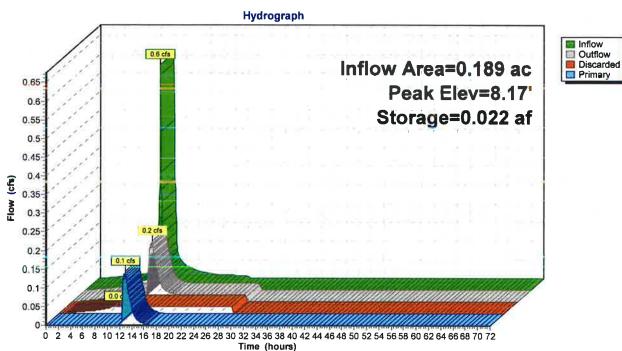
Primary OutFlow Max=0.1 cfs @ 12.91 hrs HW=8.00' TW=7.79' (Dynamic Tailwater) -1=Culvert (Passes 0.1 cfs of 0.9 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.1 cfs @ 2.24 fps) -3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Pond 9P: OCS # 2 / SYSTEM # 2

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Summary for Pond 10P: (new Pond)

Inflow Area =	0.028 ac, 0.00% Impervious, Inflow De	epth = 1.29" for 10 year event
Inflow =	0.0 cfs @ 12.09 hrs, Volume=	0.003 af
Outflow =	0.0 cfs @ 13.04 hrs, Volume=	0.003 af, Atten= 87%, Lag= 57.1 min
Discarded =	0.0 cfs @ 13.04 hrs, Volume=	0.003 af
Primary =	0.0 cfs @ 0.00 hrs, Volume=	0.000 af
Secondary =	0.0 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.22' @ 13.04 hrs Surf.Area= 214 sf Storage= 42 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 79.8 min (953.2 - 873.5)

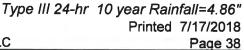
Volume	Invert	Avail.Ste	orage	Storage Description	n		
#1	9.00'	2	290 cf	0 cf Custom Stage Data (Irregular) Listed below (Recalc)			
Elevatio		urf.Area l (sq-ft)	Perim. Inc.Store (feet) (cubic-feet)		Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
9.0 10.0		164 438	77.4 103.9	0 290	0 290	164 557	
Device	Routing	Invert	Outi	et Devices			
#1	 #1 Primary 7.39' 6.0" Round Culvert L= 53.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.39' / 7.13' S= 0.0049 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.20 sf 				9 '/' Cc= 0.900		
#2	Device 1	9.50'	-				
#3	Secondary	9.75'	Hea 2.50 Coet				
#4	Discarded	9.00'	1.00	0 in/hr Exfiltration	over Surface area		
1000			- 10		·		

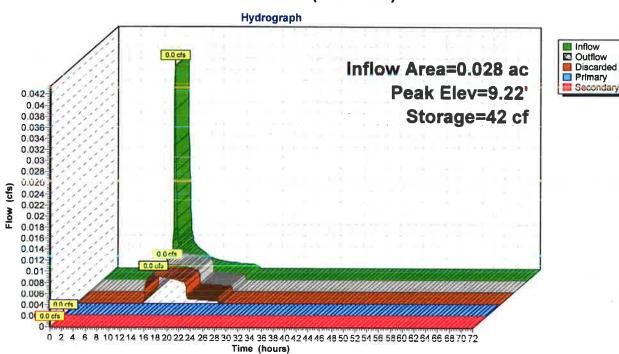
Discarded OutFlow Max=0.0 cfs @ 13.04 hrs HW=9.22' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 0.00 hrs HW=9.00' TW=7.03' (Dynamic Tailwater) 1=Culvert (Passes 0.0 cfs of 0.8 cfs potential flow) 2=Orifice/Grate (Controls 0.0 cfs)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=9.00' TW=0.00' (Dynamic Tailwater) -3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Pond 10P: (new Pond)

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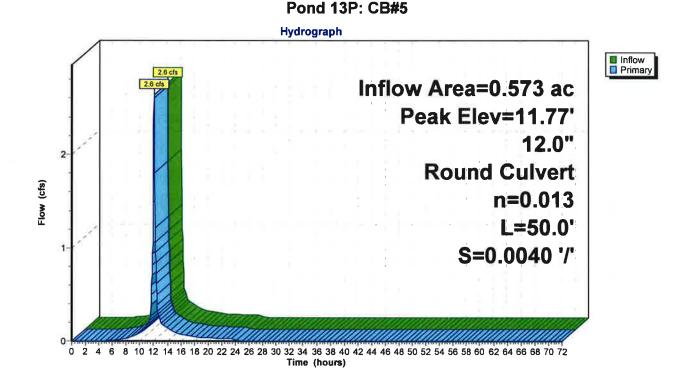
Summary for Pond 13P: CB#5

Inflow Area =	0.573 ac, 86.40% Impervious,	Inflow Depth = 3.74" for 10 year event	
Inflow =	2.6 cfs @ 12.04 hrs, Volum	ie= 0.179 af	
Outflow =	2.6 cfs @ 12.04 hrs, Volum	ie= 0.179 af, Atten= 0%, Lag= 0.0 mir	ı
Primary =	2.6 cfs @ 12.04 hrs, Volum	ne= 0.179 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 11.77' @ 12.21 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	8.06'	12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 8.06' / 7.86' S= 0.0040 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=9.43' TW=9.70' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs)



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Summary for Pond 15P: DMH#1

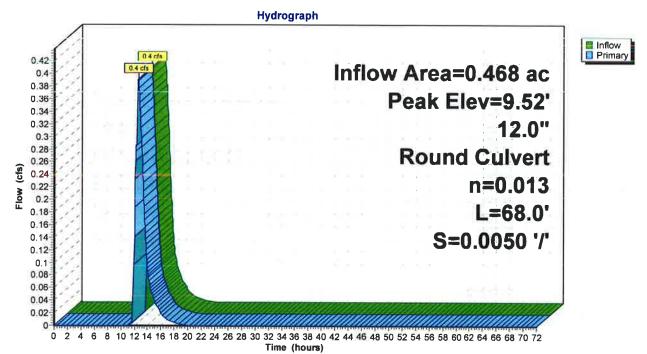
Inflow Area =	0.468 ac, 69.24% Impervious, Inflow	Depth = 1.33" for 10 year event
Inflow =	0.4 cfs @ 12.58 hrs, Volume=	0.052 af
Outflow =	0.4 cfs @ 12.58 hrs, Volume=	0.052 af, Atten= 0%, Lag= 0.0 min
Primary =	0.4 cfs @ 12.58 hrs, Volume=	0.052 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.52' @ 12.25 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.38'	12.0" Round Culvert
			L= 68.0' CPP, square edge headwaii, Ke= 0.500 Inlet / Outlet Invert= 7.38' / 7.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.5 cfs @ 12.58 hrs HW=7.96' TW=7.83' (Dynamic Tailwater)





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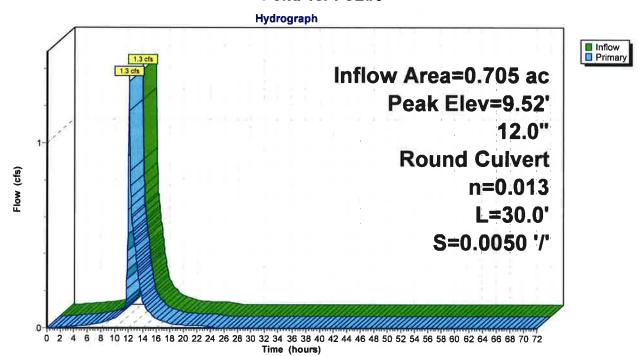
Summary for Pond 16P: CB#6

Inflow Area =	0.705 ac, 79.56% Impervious, Inflow D	Depth = 2.43" for 10 year event
Inflow =	1.3 cfs @ 12.08 hrs, Volume=	0.143 af
Outflow =	1.3 cfs @ 12.08 hrs, Volume=	0.143 af, Atten= 0%, Lag= 0.0 min
Primary =	1.3 cfs @ 12.08 hrs, Volume=	0.143 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.52' @ 12.20 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.04'	12.0" Round Culvert L= 30.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.04' / 6.89' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.08 hrs HW=8.24' TW=8.65' (Dynamic Tailwater)



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Pond 16P: CB#6

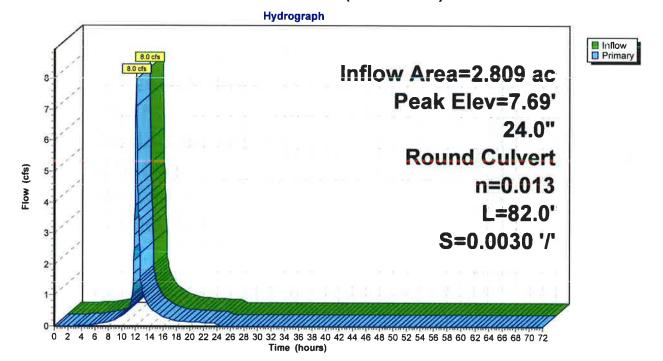
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Summary for Pond 30P: CB #1 (Altus Model)

Inflow Area = Inflow = Outflow = Primary =	2.809 ac, 53.04% Impervious, Inflow Depth = 3.31" for 10 year event 8.0 cfs @ 12.05 hrs, Volume= 0.774 af 8.0 cfs @ 12.05 hrs, Volume= 0.774 af, Atten= 0%, Lag= 0.0 min 8.0 cfs @ 12.05 hrs, Volume= 0.774 af
Routing by Dyn-Sto Peak Elev= 7.69' @ Flood Elev= 9.15'	or-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs ⊉ 12.07 hrs
Device Routing	Invert Outlet Devices
#1 Primary	6.11' 24.0" Round Culvert L= 82.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.11' / 5.86' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf
Primary OutFlow	Max=7.3 cfs @ 12.05 hrs HW=7.68' TW=7.14' (Dynamic Tailwater)

1=Culvert (Outlet Controls 7.3 cfs @ 3.78 fps)

Pond 30P: CB #1 (Altus Model)



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Summary for Pond 31P: CB #2 (Altus Model)

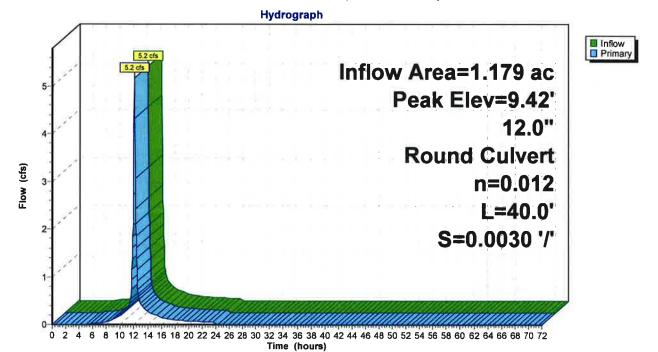
Inflow Area	=	1.179 ac, 4	1.96% Impervious,	, Inflow Depth = 3.8	30" for 10 year event
Inflow	=	5.2 cfs @	12.05 hrs, Volum	ie= 0.373 af	
Outflow	=	5.2 cfs @	12.05 hrs, Volum	ie= 0.373 af,	Atten= 0%, Lag= 0.0 min
Primary	=	5.2 cfs @	12.05 hrs, Volum	ie= 0.373 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.42' @ 12.06 hrs Flood Elev= 9.15'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.33'	12.0" Round Culvert L= 40.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.33' / 6.21' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=4.9 cfs @ 12.05 hrs HW=9.39' TW=7.68' (Dynamic Tailwater) -1=Culvert (Inlet Controls 4.9 cfs @ 6.30 fps)

Pond 31P: CB #2 (Altus Model)



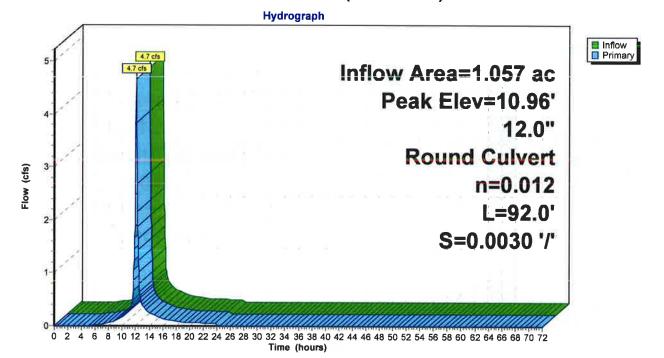
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Summary for Pond 32P: CB #3 (Altus Model)

		83% Impervious, Inflow Depth = 3.81" for 10 year event I2.05 hrs, Volume= 0.335 af
		12.05 hrs, Volume= 0.335 af, Atten= 0%, Lag= 0.0 min
Primary =	4.7 cfs @ 1	12.05 hrs, Volume= 0.335 af
Routing by Dyn-Stor- Peak Elev= 10.96' @ Flood Elev= 9.20'		Time Span= 0.00-72.00 hrs, dt= 0.05 hrs
Device Routing	Invert	Outlet Devices
#1 Primary	6.71'	12.0" Round Culvert L= 92.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.71' / 6.43' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf
Primary OutFlow Ma		2 12.05 hrs HW=10.70' TW=9.40' (Dynamic Tailwater)

-1=Culvert (Outlet Controls 3.6 cfs @ 4.59 fps)

Pond 32P: CB #3 (Altus Model)



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Summary for Pond 33P: CB #4 (Altus Model) - Relocated (CB5B)

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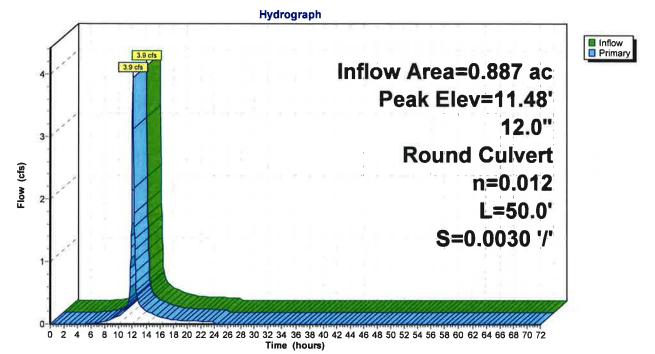
Inflow Area =	0.887 ac, 55.77% Impervious, Inflow E	Depth = 3.78" for 10 year event
Inflow =	3.9 cfs @ 12.05 hrs, Volume=	0.279 af
Outflow =	3.9 cfs @ 12.05 hrs, Volume=	0.279 af, Atten= 0%, Lag= 0.0 min
Primary =	3.9 cfs @ 12.05 hrs, Volume=	0.279 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 11.48' @ 12.12 hrs Flood Elev= 9.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.96'	12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.96' / 6.81' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=10.16' TW=10.59' (Dynamic Tailwater) -1=Culvert (Controls 0.0 cfs)





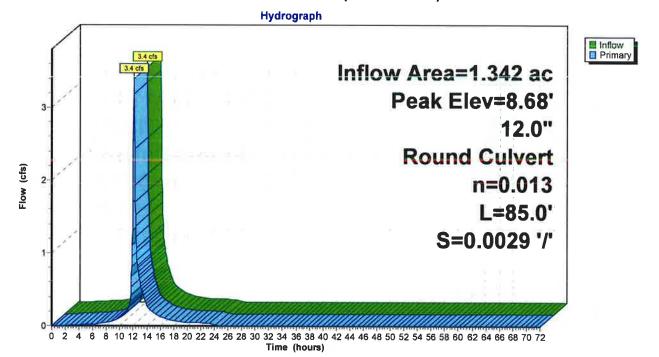
2790 Developed ConditionsType III 24-hr 10 year Rainfall=4.86"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 46

Summary for Pond 34P: CB #5 (Altus Model)

Inflow Area = Inflow =		54% Impervious, Inflow Depth = 2.66" for 10 year event 2.07 hrs, Volume=
Outflow =	3.4 cfs @ 12	2.07 hrs, Volume= 0.297 af, Atten= 0%, Lag= 0.0 min
Primary =	3.4 cfs @ 12	2.07 hrs, Volume= 0.297 af
Routing by Dyn-Sto Peak Elev= 8.68' @ Flood Elev= 8.68'		ime Span= 0.00-72.00 hrs, dt= 0.05 hrs
Device Routing	Invert	Outlet Devices
#1 Primary	5.83'	12.0" Round Culvert L= 85.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.83' / 5.58' S= 0.0029 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Primary OutFlow	Max=3.3 cfs @	12.07 hrs HW=8.58' TW=7.45' (Dynamic Tailwater)

1=Culvert (Outlet Controls 3.3 cfs @ 4.18 fps)

Pond 34P: CB #5 (Altus Model)



2790 Developed Conditions Type III 24-hr 10 year Rainfall=4.86" Prepared by Ambit Engineering, Inc. HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Summary for Pond AEI 6: Discharge Point 3 (Off Site Drainage)

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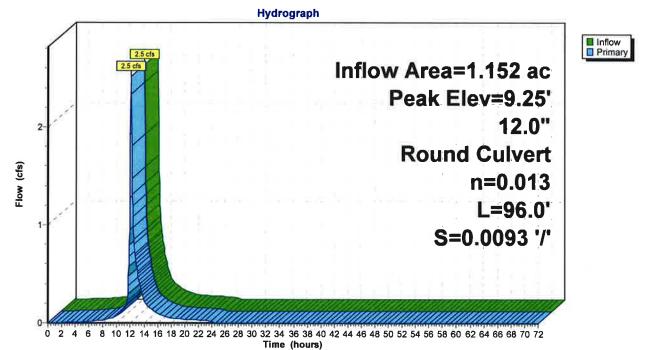
Inflow Area	a =	1.152 ac, 7	1.58% Impervious	, Inflow Depth = 2.	.38" for 10	year event
Inflow	=	2.5 cfs @	12.06 hrs, Volum	ne= 0.228 af	F	-
Outflow	=	2.5 cfs @	12.06 hrs, Volum	ne= 0.228 af	f, Atten= 0%,	Lag= 0.0 min
Primary	=	2.5 cfs @	12.06 hrs, Volum	ne= 0.228 af	F	•

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.25' @ 12.11 hrs Flood Elev= 10.77'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.77'	12.0" Round Culvert L= 96.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.77' / 5.88' S= 0.0093 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.3 cfs @ 12.06 hrs HW=8.77' TW=8.59' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.3 cfs @ 1.59 fps)





2790 Developed ConditionsType III 24-hr 10 year Rainfall=4.86"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 @ 2013 HydroCAD Software Solutions LLCPage 48

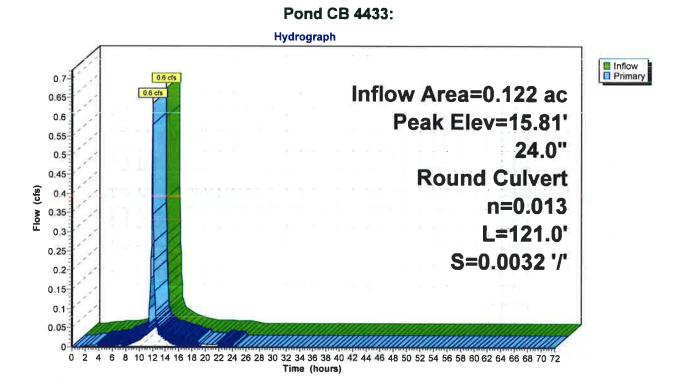
Summary for Pond CB 4433:

Inflow Area =	0.122 ac,100.00% Impervious, Inflow De	epth = 4.62" for 10 year event
Inflow =	0.6 cfs @ 12.01 hrs, Volume=	0.047 af
Outflow =	0.6 cfs @ 12.02 hrs, Volume=	0.047 af, Atten= 2%, Lag= 0.2 min
Primary =	0.6 cfs @ 12.02 hrs, Volume=	0.047 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.81' @ 12.07 hrs

#1 Primary 14.38' 24.0" Round Culvert	
L= 121.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.38' / 13.99' S= 0.0032 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf	

Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=15.76' TW=15.80' (Dynamic Tailwater)



2790 Developed Conditions Type III 24-hr 10 year Rainfall=4.86" Prepared by Ambit Engineering, Inc. HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Summary for Pond CB 4435:

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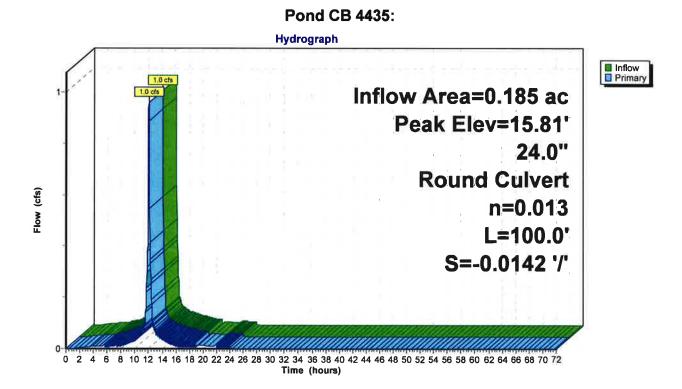
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Inflow Are	a =	0.185 ac,100.00% Impervious, Inflow Depth = 4.62" for 10 year event	
Inflow	=	1.0 cfs @ 12.02 hrs, Volume= 0.071 af	
Outflow	Ξ	1.0 cfs @ 12.02 hrs, Volume= 0.071 af, Atten= 0%, Lag= 0.0 m	nin
Primary	=	1.0 cfs @ 12.02 hrs, Volume= 0.071 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.81' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	15.41'	24.0" Round Culvert L= 100.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 13.99' / 15.41' S= -0.0142 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.9 cfs @ 12.02 hrs HW=15.80' TW=0.00' (Dynamic Tailwater)



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Summary for Pond CB 4560:

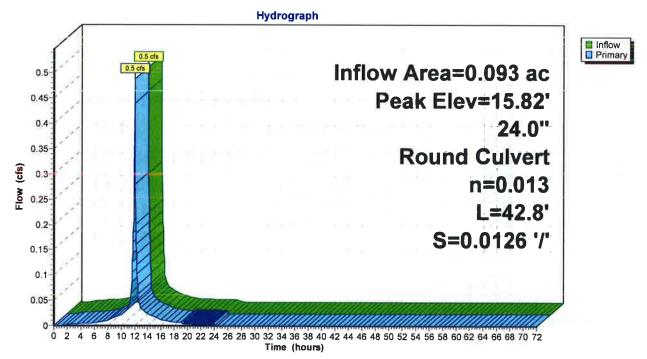
Inflow Area	=	0.093 ac,100.00% Impervious, Inflow Depth = 4.62" for 10 year event	
Inflow	=	0.5 cfs @ 12.02 hrs, Volume= 0.036 af	
Outflow	=	0.5 cfs @ 12.02 hrs, Volume= 0.036 af, Atten= 0%, Lag= 0.0 r	min
Primary	=	0.5 cfs @ 12.02 hrs, Volume= 0.036 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.82' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.92'	24.0" Round Culvert L= 42.8 CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.92' / 14.38' S= 0.0126 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=15.71' TW=15.76' (Dynamic Tailwater)

Pond CB 4560:



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Summary for Pond DP1A: CB#5A

Type III 24-hr 10 year Rainfall=4.86"

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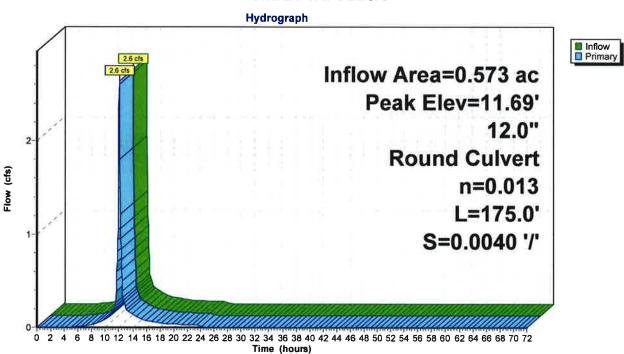
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Inflow Area =	0.573 ac, 86.40% Impervious, Inflow D	epth = 3.74" for 10 year event
Inflow =	2.6 cfs @ 12.04 hrs, Volume=	0.179 af
Outflow =	2.6 cfs @ 12.04 hrs, Volume=	0.179 af, Atten= 0%, Lag= 0.0 min
Primary =	2.6 cfs @ 12.04 hrs, Volume=	0.179 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 11.69' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.76'	12.0" Round Culvert L= 175.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.76' / 7.06' S= 0.0040 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=9.70' TW=9.85' (Dynamic Tailwater)



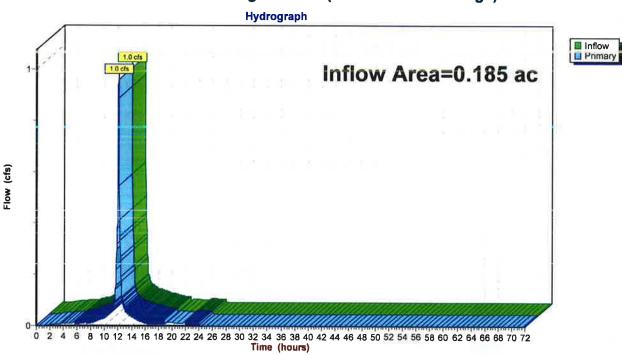
Pond DP1A: CB#5A

2790 Developed Conditions	Type III 24-hr 10 year Rainfall=4.86"
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Summary for Link 2L: Discharge Point 2 (Court Street Drainage)

Inflow Are	a =	0.185 ac,100.00% Impervious, Inflow Depth = 4.62" for 10 year event	
Inflow	=	1.0 cfs @ 12.02 hrs, Volume= 0.071 af	
Primary	=	1.0 cfs @ 12.02 hrs, Volume= 0.071 af, Atten= 0%, Lag= 0.0 min	J

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Link 2L: Discharge Point 2 (Court Street Drainage)

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Summary for Link 3L: Discharge Point 4 (DP4)

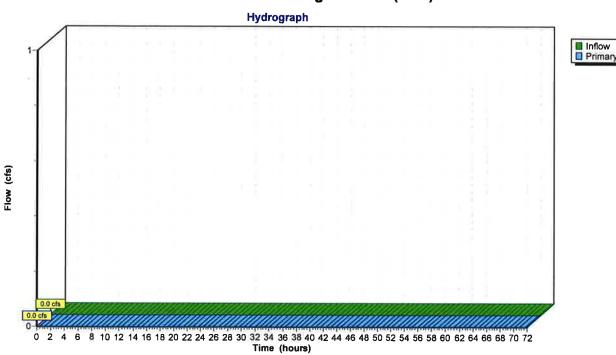
Type III 24-hr 10 year Rainfall=4.86"

Printed 7/17/2018

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Inflow	=	0.0 cfs @	0.00 hrs, Volume=	0.000 af
Primary	=	0.0 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



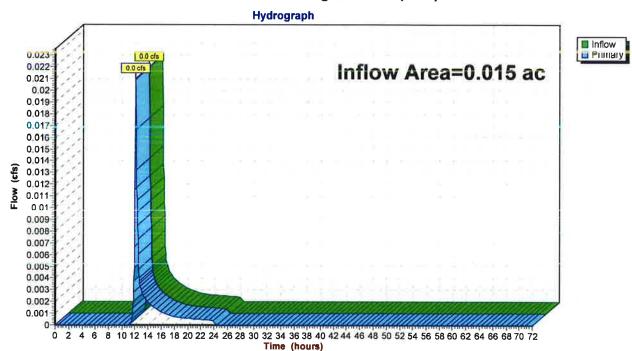
Link 3L: Discharge Point 4 (DP4)

2790 Developed Conditions Ty	/pe III 24-hr 10 year Rainfall=4.86"
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Summary for Link 4L: Discharge Point 5 (DP5)

Inflow Area	a =	0.015 ac,	0.00% Impervious,	Inflow Depth = 1.2	9" for 10 year event
Inflow	=	0.0 cfs @	12.09 hrs, Volume	= 0.002 af	
Primary	=	0.0 cfs @	12.09 hrs, Volume	= 0.002 af,	Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Link 4L: Discharge Point 5 (DP5)

Summary for Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)

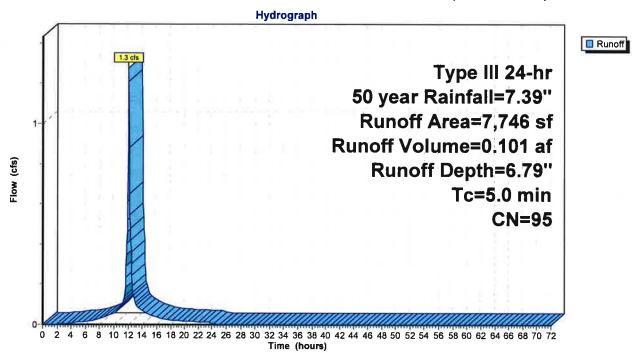
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Runoff 1.3 cfs @ 12.07 hrs, Volume= 0.101 af, Depth= 6.79" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN [Description		
*		7,746	95			
		7,746	1	00.00% P	ervious Are	28
	Тс	Length	Slope	Velocity	Capacity	Description
(!	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	5.0					Direct Entry,

Subcatchment 3S: East Side, On & Offsite to CB (Altus Model)



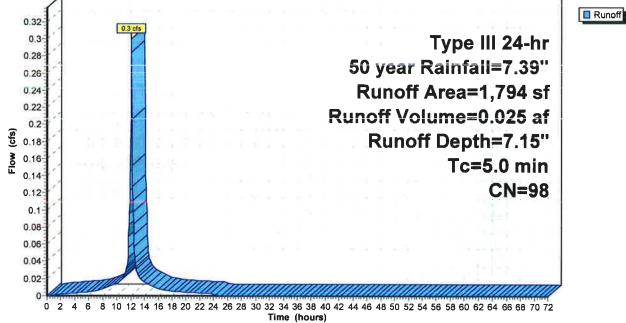
2790 Developed Conditions	Type III 24-hr 50 year Rainfall=7.39	1
Prepared by Ambit Engineering, Inc.	Printed 7/17/2018	3
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Summary for Subcatchment 4S: Existing Building (Altus Model)

Runoff = 0.3 cfs @ 12.07 hrs, Volume= 0.025 af, Depth= 7.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

A	rea (sf)	CN	Description		
k	1,794	98			
	1,794		100.00% In	npervious A	rea
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description
5.0					Direct Entry,
		Su	bcatchm	ent 4S: E	xisting Building (Altus Model)
				Hydro	graph
	1				



2790 Developed Conditions	Type III 24-hr	50 year Rainfall=7.39"
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Summary for Subcatchment 30S: West Parking Lot (Altus Model)

Runoff = 1.1 cfs @ 12.07 hrs, Volume= 0.087 af, Depth= 6.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

A	rea (sf)	CN	Description			
*	6,925	93				
-	6,925		100.00% Pe	ervious Are	a	
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description	
5.0					Direct Entry,	
Subcatchment 30S: West Parking Lot (Altus Model) Hydrograph						
Runof						
		1.1 cfs			Type III 24-hr	
1-	<				50 year Rainfall=7.39"	
Runoff Area=6,925 sf						
					Runoff Volume=0.087 af	
r (cfs)					Runoff Depth=6.56"	

Tc=5.0 min CN=93

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

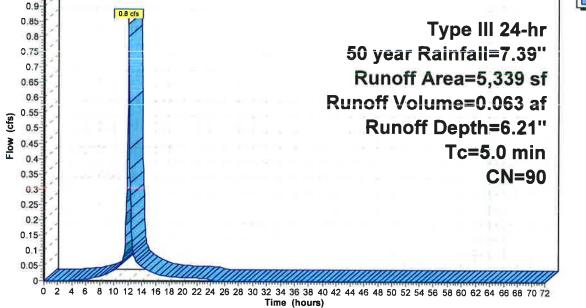
2790 Developed Conditions	Type III 24-hr	50 year Rain	fall=7.39"
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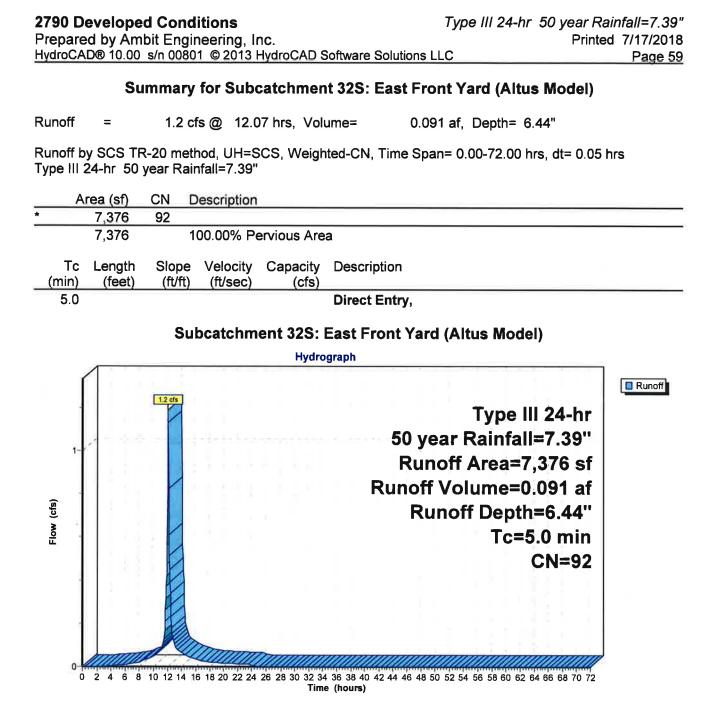
Summary for Subcatchment 31S: West Front Yard (Altus Model)

Runoff = 0.8 cfs @ 12.07 hrs, Volume= 0.063 af, Depth= 6.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7 39"

_	A	rea (sf)	CN [Description			
*		5,339	90				
		5,339	1	100.00% Pe	ervious Are	ea	
	Tc (min)	Length (feet)	Slope (îvît)		Capacity (cís)		
	5.0					Direct Entry,	
Subcatchment 31S: West Front Yard (Altus Model)							
					Hydro	ograph	
	0,9	[]	0.8 cfs				ıff
	0.85	1				Type III 24-hr	



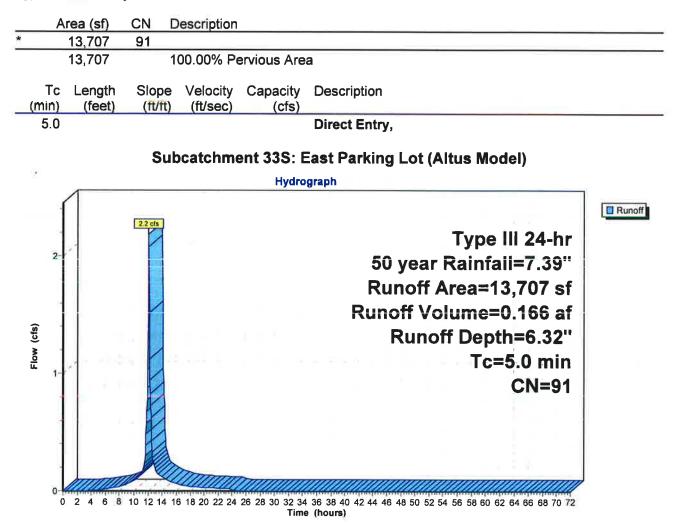


2790 Developed Conditions Type	e III 24-hr 50 year Rainfall=7.39"
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Summary for Subcatchment 33S: East Parking Lot (Altus Model)

Runoff = 2.2 cfs @ 12.07 hrs, Volume= 0.166 af, Depth= 6.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"



	l by Áml	oit Eng	ineering, li		Software Soluti				ainfall=7.39" ed 7/17/2018 Page 61
	Summary for Subcatchment 34S: North Parking Lot (Altus Model)								
Runoff	=	1.1	cfs @ 12.0)7 hrs, Vol	ume=	0.084	af, Depth=	6.79"	
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"									
Are	ea (sf)	CN	Description			30			
*	6,462	95							
-	6,462		100.00% Pe	ervious Are	a				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
5.0					Direct Entry	/,			
		Su	bcatchme	nt 34S: N	lorth Parkir	ng Lot	: (Altus Mo	del)	
				Hydro	graph				
1-		1.1 cfs					r Rainfa		Runoff
		10.3			F	Runo	off Area=	6,462 sf	

Runoff Volume=0.084 af

Runoff Depth=6.79"

Tc=5.0 min

CN=95

0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours) Ti

Flow (cfs)

2790 Developed Conditions T	ype III 24-hr	50 year Rain	fall=7.39"
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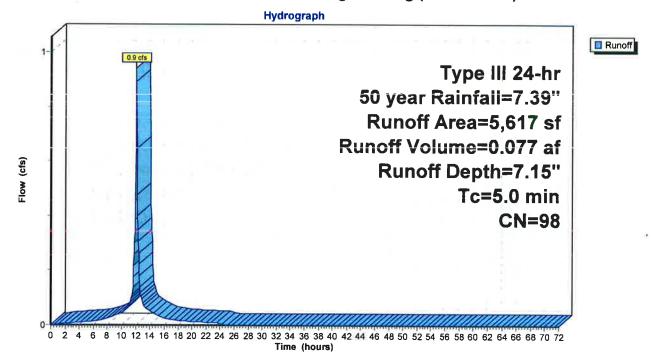
Summary for Subcatchment 40S: Existing Building (Altus Model)

Runoff = 0.9 cfs @ 12.07 hrs, Volume= 0.077 af, Depth= 7.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	Area (sf)	CN	Description			
*	5,617	98				
	5,617	100.00% Impervious Area				
To (min)		Slope (π/π)		Capacity (cfs)		
5.0		(IVII)	(IUSEC)	(015)	Direct Entry,	
					,,	

Subcatchment 40S: Existing Building (Altus Model)



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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 63

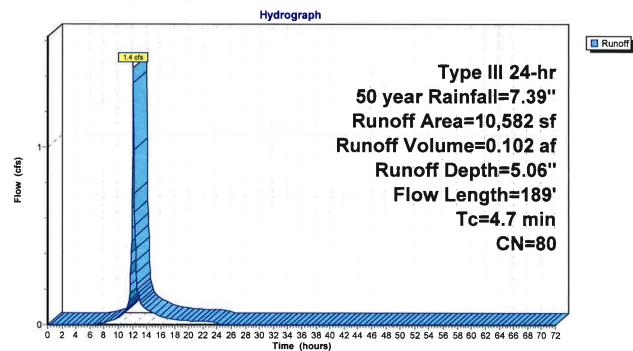
Summary for Subcatchment PS1:

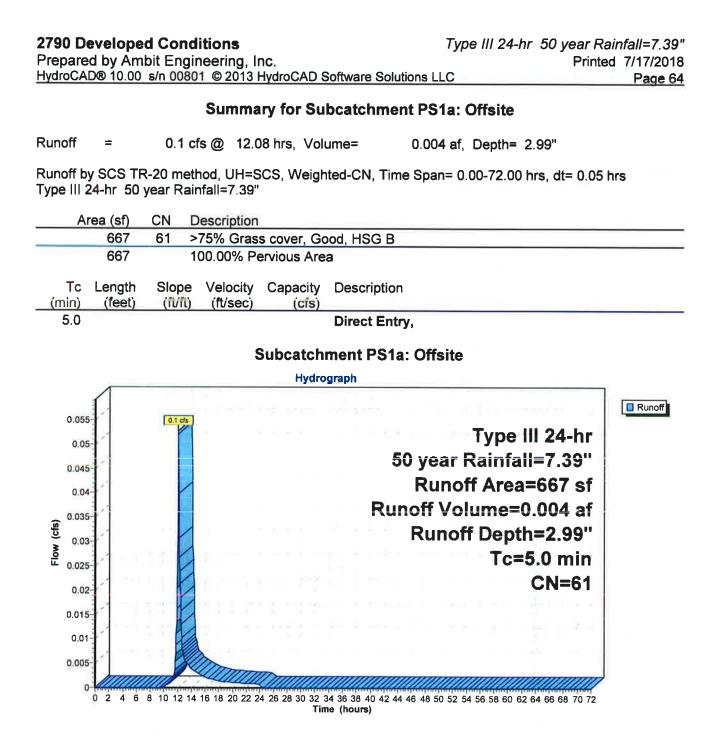
Runoff = 1.4 cfs @ 12.07 hrs, Volume= 0.102 af, Depth= 5.06"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	A	rea (sf)	CN [Description							
		6,399	98	98 Paved parking, HSG A							
*		939	98 I	Paved side	walks w/cu	rbs & sewers, HSG A					
		3,244	39 >	>75% Gras	s cover, Go	bod, HSG A					
		10,582	80 \	Neighted A	verage						
		3,244			vious Area						
		7,338	6	69.34% Imp	pervious Ar	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	3.9	32	0.0200	0.14		Sheet Flow,					
						Grass: Short n= 0.150 P2= 3.21"					
	0.8	157	0.0287	3.44		Shallow Concentrated Flow,					
						Paved Kv= 20.3 fps					
-	4.7	189	Total								

Subcatchment PS1:





2790 Developed Conditions	Type III 24-hr	50 year Rainfall=7.39"
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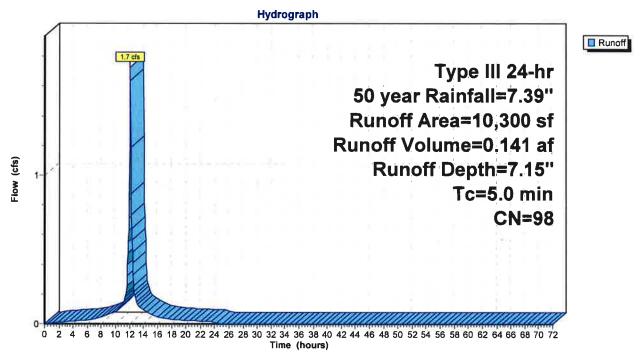
Summary for Subcatchment PS2: Existing Building Roof Drain

Runoff = 1.7 cfs @ 12.07 hrs, Volume= 0.141 af, Depth= 7.15"

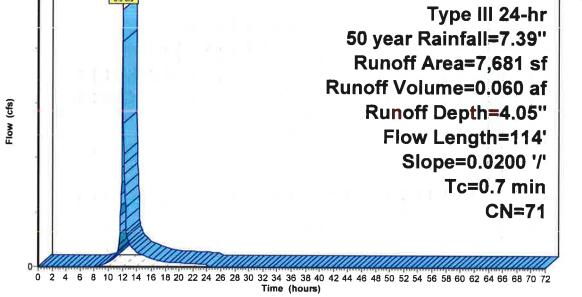
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

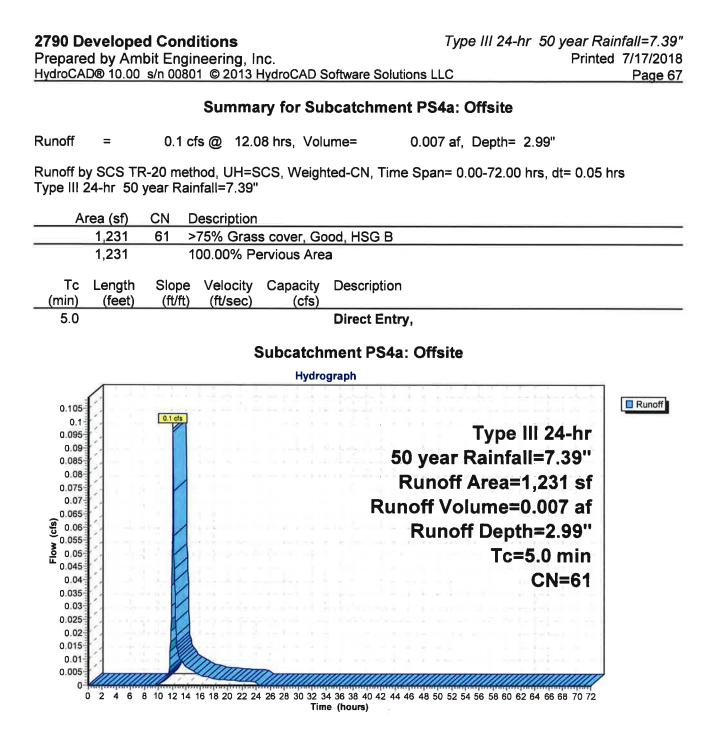
A	rea (sf)	CN I	Description			
	10,300	98 I	Roofs, HSG) A		
· · · · ·	10,300		100.00% Im	npervious A	Area	
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description	
5.0					Direct Entry,	

Subcatchment PS2: Existing Building Roof Drain



Prepared by A	ped Conditions Ambit Engineering, Inc. .00 s/n 00801 © 2013 HydroCAD Software Solut	Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 ions LLC Page 66							
	Summary for Subcatchment PS4:								
Runoff =	0.9 cfs @ 12.01 hrs, Volume=	0.060 af, Depth= 4.05"							
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"									
Area (s) CN Description								
3,51	3 39 >75% Grass cover, Good, HSG A								
4,16		GA							
7,68	1 71 Weighted Average								
3,51	3 45.74% Pervious Area								
4,16	8 54.26% Impervious Area								
Tc Leng (min) (fee									
0.7 1		ncentrated Flow,							
	Paved Kv=	= 20.3 fps							
Subcatchment PS4:									
Hydrograph									
1-	0.9 cfs								
		Type III 24-hr							





2790 Developed Conditions	Type III 24-hr 50 year Rainfall=7.39"
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Summary for Subcatchment	t PS5 [.]

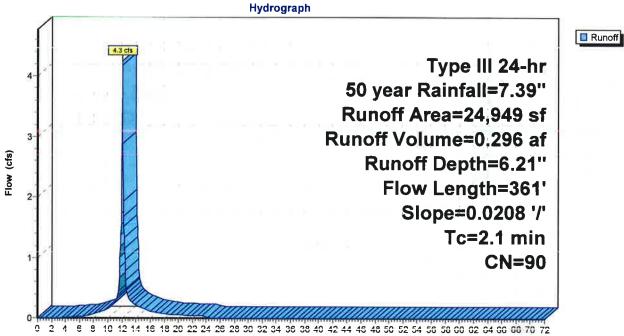
Runoff = 4.3 cfs @ 12.04 hrs, Volume= 0.296 af, Depth= 6.21"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	A	rea (sf)	CN [Description							
		19,373	98 F	Paved road	aved roads w/curbs & sewers, HSG A						
*		1,796	98 F	Paved sidewalks w/curbs & sewers, HSG A							
		388	98 F	Roofs, HSC	βA						
e		3,392	39 >	75% Gras	s cover, Go	bod, HSG A					
		24,949	90 1	J vveighted Average							
		3,392		13.60% Pe	rvious Area						
		21,557	8	36.40% lmp	pervious Ar	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	2.1	361	0.0208	2.93		Shallow Concentrated Flow,					
						David Ky 20.2 free					

Paved Kv= 20.3 fps

Subcatchment PS5:



Time (hours)

2790 Developed Conditions	Type III 24-hr 50 year Rainfall=7.3	9"
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Summary for Subcatchment PS5a: New Building Roof Drain

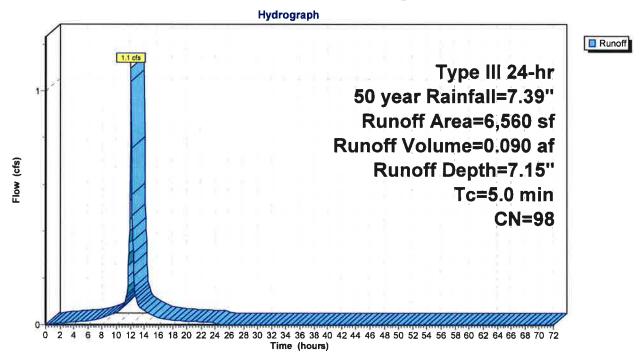
0.090 af, Depth= 7.15"

Runoff = 1.1 cfs @ 12.07 hrs, Volume=

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

ΑΑ	rea (sf)	CN I	Description					
	6,560	98 I	Roofs, HSG	A				
	6,560		100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
5.0					Direct Entry,			

Subcatchment PS5a: New Building Roof Drain



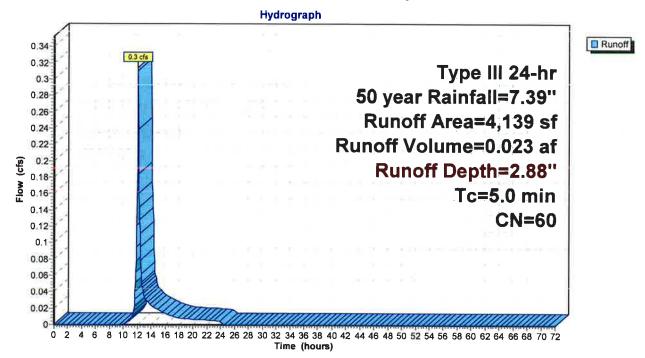
Summary for Subcatchment PS5aa: Landscaped Walk

Runoff = 0.3 cfs @ 12.08 hrs, Volume= 0.023 af, Depth= 2.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	Area (sf)	CN	Description	Description						
	2,666	39	>75% Gras	75% Grass cover, Good, HSG A						
	852	98	Roofs, HSC	Roofs, HSG A						
*	621	98	Paved side	aved sidewalks w/curbs & sewers, HSG A						
	4,139	60	Weighted A	/eighted Average						
	2,666		64.41% Pe	64.41% Pervious Area						
	1,473		35.59% lmj	35.59% Impervious Area						
(mi	Fc Length n) (feet)	Slop (ft/f		Capacity (cfs)	Description					
5	.0				Direct Entry,					

Subcatchment PS5aa: Landscaped Walk



2790 Developed Conditions	Type III 24-hr	50 year Rainfall=7.39"
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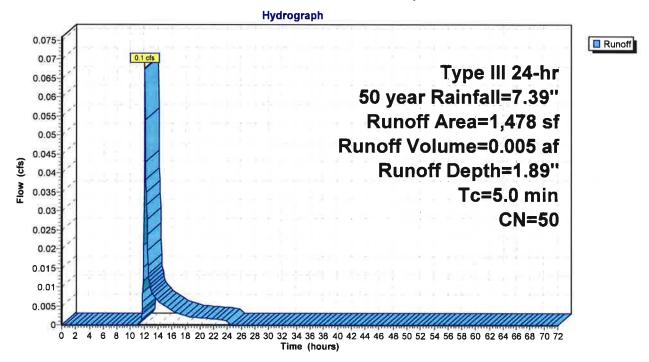
Summary for Subcatchment PS5aaa: Landscaped Walk

Runoff = 0.1 cfs @ 12.09 hrs, Volume= 0.005 af, Depth= 1.89	Runoff	=	0.1 cfs @	12.09 hrs,	Volume=	0.005 af, Depth= 1.89"	l.
---	--------	---	-----------	------------	---------	------------------------	----

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	A	rea (sf)	CN	Description					
		1,200	39	>75% Gras	>75% Grass cover, Good, HSG A				
*		278	98	Paved side	walk w/curk	bs & sewers, HSG A			
-		1,478 1,200 278	50	Weighted Average 81.19% Pervious Area 18.81% Impervious Area					
	Tc (min)	Length (feet)	Slop (ft/fi	· · · · · · · · · · · · · · · · · · ·	Capacity (cfs)	Description			
	5.0					Direct Entry,			

Subcatchment PS5aaa: Landscaped Walk



2790 Developed Conditions	Type III 24-hr	50 year Rair	nfall=7.39"
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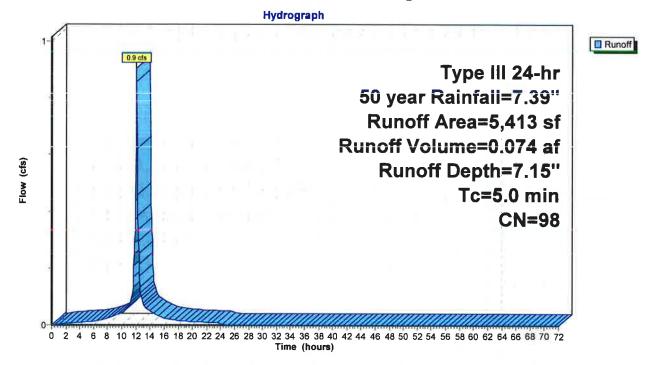
Summary for Subcatchment PS5b: New Building Roof Drain

Runoff = 0.9 cfs @ 12.07 hrs, Volume= 0.074 af, Depth= 7.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

A	rea (sf)	CN	Description	í		
	5,413	98	Roofs, HSC	G A		
	5,413		100.00% In	npervious A	rea	
Tc	Length	Slope			Description	
(min) 5.0	(féét)	(ft/ft) (ft/sec)	(cfs)	Direct Entry,	
0.0					Direct Entry,	

Subcatchment PS5b: New Building Roof Drain



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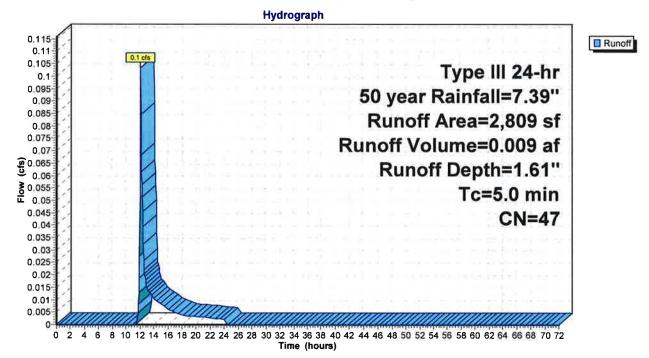
Summary for Subcatchment PS5bb: Landscaped Walk

Runoff = 0.1 cfs @ 12.10 hrs, Volume= 0.009 af, Depth= 1.61"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN	Description					
		2,409	39	>75% Gras	>75% Grass cover, Good, HSG A				
*		400	98	Paved side	Paved sidewalk w/curbs & sewers, HSG A				
		2,809	47	Weighted Average					
		2,409		85.76% Pervious Area					
		400		14.24% lm	14.24% Impervious Area				
(Tc min)	Length (feet)	Slop (ft/fl	,	Capacity (cfs)	Description			
	5.0					Direct Entry,			

Subcatchment PS5bb: Landscaped Walk



Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 73

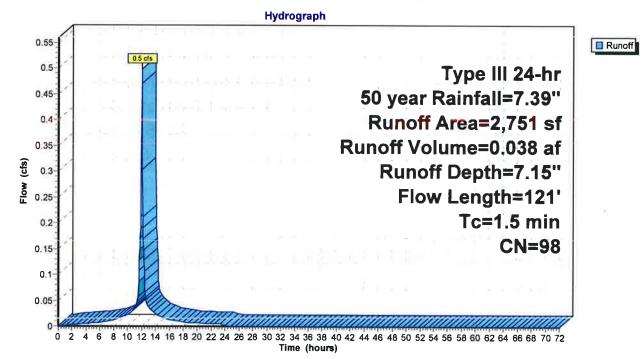
Summary for Subcatchment PS6: Court Street

Runoff = 0.5 cfs @ 12.02 hrs, Volume= 0.038 af, Depth= 7.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

_	A	rea (sf)	CN [Description			
		2,556	98 F	Paved park	ing, HSG B	3	
3		195	98 l	Jnconnecte	ed pavemer	nt, sidewalk, HSG B	
		2,751	98 \	Veighted A	verage		
		2,751	1	100.00% Im	pervious A	rea	
		195	7	.09% Unc	onnected		
	Тс	Length	Slope		Capacity	Description	
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	0.6	26	0.0096	0.69		Shallow Concentrated Flow,	
						Short Grass Pasture Kv= 7.0 fps	
	0.9	95	0.0078	1.79		Shallow Concentrated Flow,	
						Paved Kv= 20.3 fps	
	1.5	121	Total				

Subcatchment PS6: Court Street



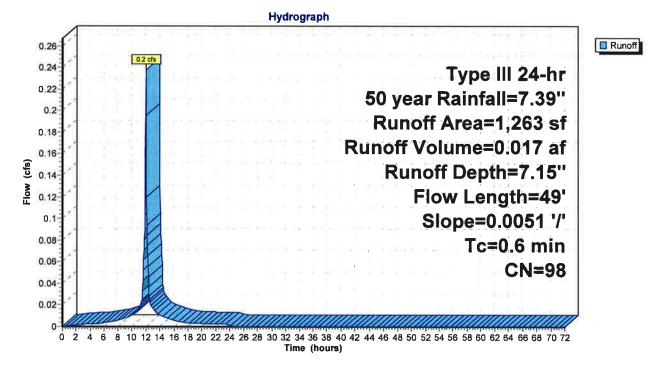
Summary for Subcatchment PS7: Court Street

Runoff 0.2 cfs @ 12.01 hrs, Volume= 0.017 af, Depth= 7.15" =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

	A	rea (sf)	CN	Description				
		922	98	Paved park	Paved parking, HSG B			
*		341	98	Unconnecte	ed pavemer	nt, sidewalk, HSG B		
		1,263	98	Weighted A	Veighted Average			
		1,263		100.00% Impervious Area				
		341	:	27.00% Unconnected				
	Та	Longth	Clana	Valasitu	Conneitu	Description		
	TC	Length	Slope		Capacity	Description		
-	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	0.6	49	0.0051	1.45		Shallow Concentrated Flow,		
						Paved Kv= 20.3 fps		

Subcatchment PS7: Court Street



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2790 Developed Conditions	Type III 24-hr	50 year Rainfall=7.39"
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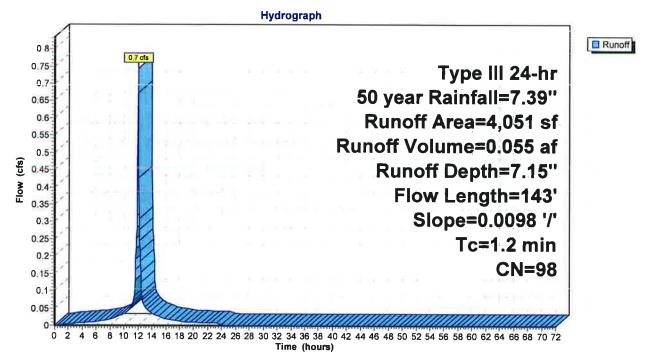
Summary for Subcatchment PS8: Court Street

Runoff = 0.7 cfs @ 12.02 hrs, Volume= 0.055 af, Depth= 7.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Type III 24-hr 50 year Rainfall=7.39"

-	A	rea (sf)	CN	Description	Ĕ	
		1,014	98	^D aved park	ing, HSG B	3
*		3,037	98	Jnconnecte	ed pavemer	nt,sidewalk, HSG B
		4,051	98	Neighted A	verage	
		4,051		100.00% In	npervious A	vrea
		3,037		74.97% Un	connected	
	_					
	TC	Length	Slope		Capacity	Description
a —	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	1.2	143	0.0098	2.01		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps

Subcatchment PS8: Court Street



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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 LC Page 77

Summary for Reach 4R: Altus Model

 Inflow Area =
 0.041 ac,100.00% Impervious, Inflow Depth =
 7.15" for 50 year event

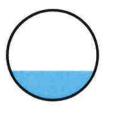
 Inflow =
 0.3 cfs @
 12.07 hrs, Volume=
 0.025 af

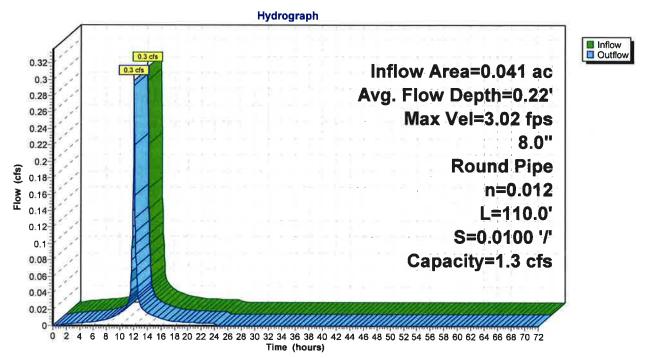
 Outflow =
 0.3 cfs @
 12.08 hrs, Volume=
 0.025 af, Atten= 1%, Lag= 0.7 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 3.02 fps, Min. Travel Time= 0.6 min Avg. Velocity = 1.01 fps, Avg. Travel Time= 1.8 min

Peak Storage= 11 cf @ 12.08 hrs Average Depth at Peak Storage= 0.22' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.3 cfs

8.0" Round Pipe n= 0.012 Length= 110.0' Slope= 0.0100 '/' Inlet Invert= 8.38', Outlet Invert= 7.28'





Reach 4R: Altus Model

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Summary for Reach 40R: Altus Model

 Inflow Area =
 0.129 ac,100.00% Impervious, Inflow Depth =
 7.15" for 50 year event

 Inflow =
 0.9 cfs @
 12.07 hrs, Volume=
 0.077 af

 Outflow =
 0.9 cfs @
 12.07 hrs, Volume=
 0.077 af, Atten= 0%, Lag= 0.0 min

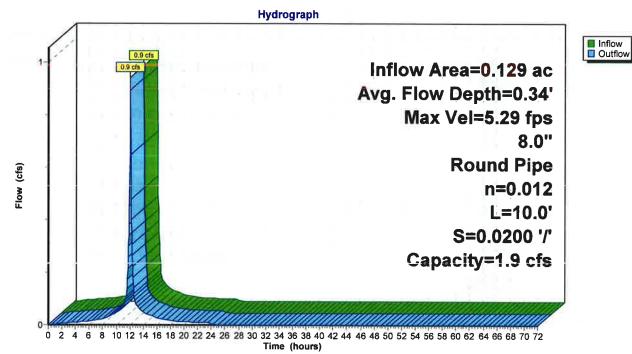
Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 5.29 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.81 fps, Avg. Travel Time= 0.1 min

Peak Storage= 2 cf @ 12.07 hrs Average Depth at Peak Storage= 0.34' Bank-Full Depth= 0.67' Flow Area= 0.3 sf, Capacity= 1.9 cfs

8.0" Round Pipe n= 0.012 Length= 10.0' Slope= 0.0200 '/' Inlet Invert= 6.82', Outlet Invert= 6.62'



Reach 40R: Altus Model



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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 79

Summary for Reach 41R: Altus Model

 Inflow Area =
 1.471 ac, 67.65% Impervious, Inflow Depth =
 4.99" for 50 year event

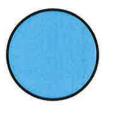
 Inflow =
 6.6 cfs @
 12.06 hrs, Volume=
 0.611 af

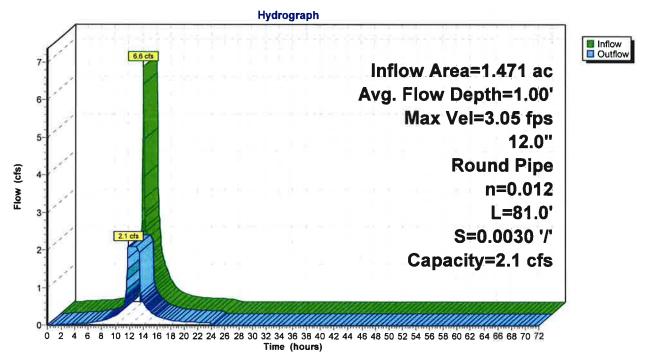
 Outflow =
 2.1 cfs @
 11.85 hrs, Volume=
 0.611 af, Atten= 68%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Max. Velocity= 3.05 fps, Min. Travel Time= 0.4 min Avg. Velocity = 1.50 fps, Avg. Travel Time= 0.9 min

Peak Storage= 64 cf @ 11.85 hrs Average Depth at Peak Storage= 1.00' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.1 cfs

12.0" Round Pipe n= 0.012 Length= 81.0' Slope= 0.0030 '/' Inlet Invert= 6.45', Outlet Invert= 6.21'



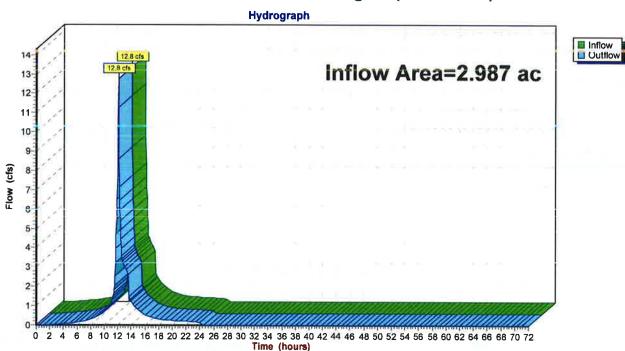


Reach 41R: Altus Model

Summary for Reach 300R: POA #3 - Existing CB (Altus Model)

Inflow Area	=	2.987 ac, 49.88% Impervious, Inflow Depth = 5.69" for 50 year event	
inflow :	=	12.8 cfs @ 12.05 hrs, Volume= 1.415 af	
Outflow	=	12.8 cfs @ 12.05 hrs, Volume= 1.415 af, Atten= 0%, Lag= 0.0 min	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Reach 300R: POA #3 - Existing CB (Altus Model)

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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 81

Summary for Pond 1P: OCS # 1 / SYSTEM # 1

Inflow Area =	0.280 ac, 68.25% Impervious, Inflow De	pth = 5.06" for 50 year event
Inflow =	1.5 cfs @ 12.07 hrs, Volume=	0.118 af
Outflow =	0.5 cfs @ 12.41 hrs, Volume=	0.118 af, Atten= 64%, Lag= 20.3 min
Discarded =	0.0 cfs @ 6.80 hrs, Volume=	0.037 af
Primary =	0.5 cfs @ 12.41 hrs, Volume=	0.081 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 14.33' @ 12.36 hrs Surf.Area= 0.015 ac Storage= 0.038 af

Plug-Flow detention time= 118.1 min calculated for 0.118 af (100% of inflow) Center-of-Mass det. time= 118.5 min (886.8 - 768.3)

Volume	Invert	Avail.Storage	Storage Description
#1	10.50'	0.014 af	24.00'W x 27.00'L x 4.00'H Prismatoid
			0.060 af Overall - 0.025 af Embedded = 0.035 af x 40.0% Voids
#2	11.00'	0.025 af	
			Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
<u> </u>			Row Length Adjustment= +0.44' x 6.45 sf x 6 rows
		0.039 af	Total Available Storage
Device	Routing	Invert Ou	utlet Devices
#1	Primary	11.40' 12	.0" Round Culvert
		L=	14.0' CPP, square edge headwall, Ke= 0.500
		Ini	et / Outlet Invert= 11.40' / 11.33' S= 0.0050 '/' Cc= 0.900
		n=	0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	11.50' 2.0	0" Vert. Orifice/Grate X 3.00 C= 0.600
#3	Device 1)' long x 0.5' breadth Broad-Crested Rectangular Weir
		He	ad (feet) 0.20 0.40 0.60 0.80 1.00
			ef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Discarded	10.50' 1.0	000 in/hr Exfiltration over Surface area

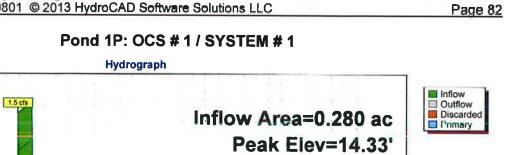
Discarded OutFlow Max=0.0 cfs @ 6.80 hrs HW=10.54' (Free Discharge)

Primary OutFlow Max=0.5 cfs @ 12.41 hrs HW=14.28' TW=9.22' (Dynamic Tailwater) 1=Culvert (Passes 0.5 cfs of 5.8 cfs potential flow) 2=Orifice/Grate (Orifice Controls 0.5 cfs @ 7.91 fps) 3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

2790 Developed Conditions

Flow (cfs)

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Type III 24-hr 50 year Rainfall=7.39"

Storage=0.038 af

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0.5 c

0.5

2790 Developed Conditions Type III 24-hr 50 year Rainfall=7.39" Prepared by Ambit Engineering, Inc. HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Summary for Pond 3P: Existing CB (Altus Model)

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Inflow Area = 2.987 ac. 49.88% Impervious. Inflow Depth = 5.69" for 50 year event Inflow 12.8 cfs @ 12.05 hrs, Volume= 1.415 af Ξ 12.8 cfs @ 12.05 hrs, Volume= 12.8 cfs @ 12.05 hrs, Volume= Outflow = 1.415 af, Atten= 0%, Lag= 0.0 min Primary 1.415 af Ξ

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 7.55' @ 12.05 hrs Flood Elev= 8.59'

Device	Routing	Invert	Outlet Devices
#1	Primary	5.76'	24.0" Round Culvert L= 55.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 5.76' / 5.21' S= 0.0100 '/' Cc= 0.900 n= 0.012, Flow Area= 3.14 sf

Primary OutFlow Max=12.6 cfs @ 12.05 hrs HW=7.53' TW=0.00' (Dynamic Tailwater) -1=Culvert (Barrel Controls 12.6 cfs @ 5.69 fps)

Hydrograph Inflow
Primary 14 12.8 cfs Inflow Area=2.987 ac 12.8 cf 13 12 Peak Elev=7.55' 11 24.0" 10 9 Round Culvert Flow (cfs) 8 n=0.012 7 L=55.0' 6 5 S=0.0100 '/' 4 3 2 1 D 0 246 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72

Time (hours)

Pond 3P: Existing CB (Altus Model)

2790 Developed ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 84

Summary for Pond 5P: CB#1

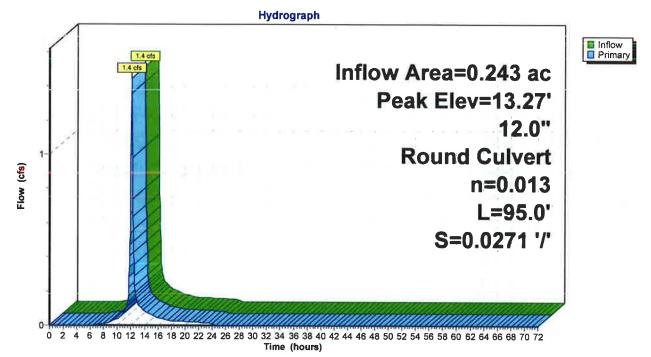
Inflow Area =	0.243 ac, 69.34% Impervious, Inflow	Depth = 5.06" for 50 year event	
Inflow =	1.4 cfs @ 12.07 hrs, Volume=	0.102 af	
Outflow =	1.4 cfs @ 12.07 hrs, Volume=	0.102 af, Atten= 0%, Lag= 0.0 mir	1
Primary =	1.4 cfs @ 12.07 hrs, Volume -	0.102 af	

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 13.27' @ 12.24 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	9.70'	12.0" Round Culvert L= 95.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 9.70' / 7.13' S= 0.0271 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.1 cfs @ 12.07 hrs HW=10.37' TW=10.37' (Dynamic Tailwater) -1=Culvert (Outlet Controls 0.1 cfs @ 0.17 fps)





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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 85

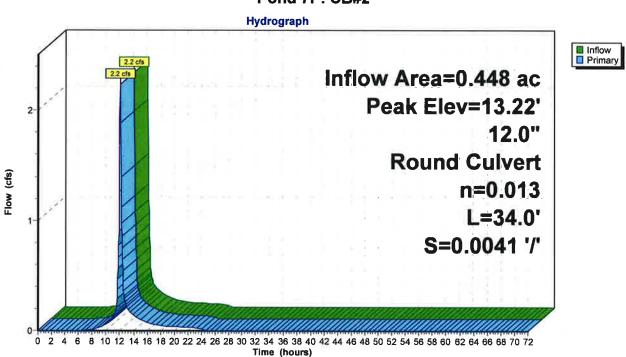
Summary for Pond 7P: CB#2

Inflow Area =	0.448 ac, 59.02% Impervious, Inflow E	Depth = 4.36" for 50 year event
Inflow =	2.2 cfs @ 12.05 hrs, Volume=	0.163 af
Outflow =	2.2 cfs @ 12.05 hrs, Volume=	0.163 af, Atten= 0%, Lag= 0.0 min
Primary =	2.2 cfs @ 12.05 hrs, Volume=	0.163 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 13.22' @ 12.19 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.03'	12.0" Round Culvert L= 34.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.03' / 6.89' S= 0.0041 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=9.79' TW=10.93' (Dynamic Tailwater) 1=Culvert (Controls 0.0 cfs)



Pond 7P: CB#2

2790 Developed ConditionsType III 24-hr50 year Rainfall=7.39"Prepared by Ambit Engineering, Inc.Printed 7/17/2018HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLCPage 86

Summary for Pond 8P: CB#3

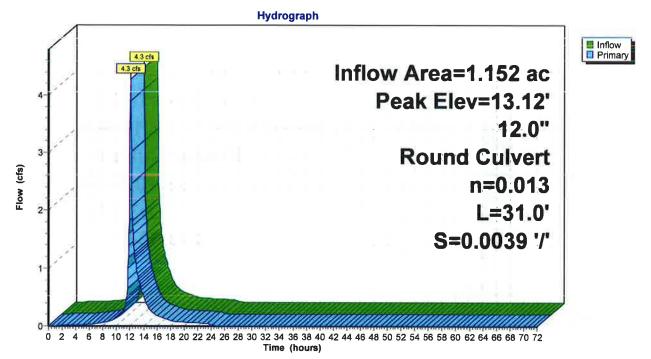
Inflow Area =	1.152 ac, 71.58% Impervious, Inflow D	epth = 4.44" for 50 year event
Inflow =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af
Outflow =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af, Atten= 0%, Lag= 0.0 min
Primary =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 13.12' @ 12.14 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 31.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.89' / 6.77' S= 0.0039 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.06 hrs HW=11.30' TW=11.69' (Dynamic Tailwater)

Pond 8P: CB#3



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Summary for Pond 9P: OCS # 2 / SYSTEM # 2

Inflow Area =	0.189 ac, 70.70% Impervious, Inflow De	epth = 5.26" for 50 year event
Inflow =	1.0 cfs @ 12.07 hrs, Volume=	0.083 af
Outflow =	0.3 cfs @ 12.76 hrs, Volume=	0.083 af, Atten= 68%, Lag= 41.5 min
Discarded =	0.0 cfs @ 8.40 hrs, Volume=	0.041 af
Primary =	0.3 cfs @ 12.76 hrs, Volume=	0.042 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.65' @ 12.47 hrs Surf.Area= 0.019 ac Storage= 0.039 af

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 164.3 min (920.6 - 756.3)

Volume	Invert	Avail.Storag	ge Storage Description
#1	6.50'	0.019 a	af 27.00'W x 30.00'L x 4.00'H Prismatoid
	7.00	0.000	0.074 af Overall - 0.026 af Embedded = 0.049 af x 40.0% Voids
#2	7.00'	0.026 a	af ADS_StormTech SC-740 x 24 Inside #1 Effective Size= 44.6"W x 30.0"H => 6.45 sf x 7.12'L = 45.9 cf
			Overall Size= 51.0"W x 30.0"H x 7.56'L with 0.44' Overlap
			Row Length Adjustment= +0.44' x 6.45 sf x 7 rows
S		0.045 a	af Total Available Storage
Device	Routing	Invert	Outlet Devices
#1	Primary	7.40'	12.0" Round Culvert
			L= 5.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 7.40' / 7.38' S= 0.0040 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#2	Device 1	7.50'	2.0" Vert. Orifice/Grate X 3.00 C= 0.600
#3	Device 1	10.50'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
		(Coef. (English) 2.80 2.92 3.08 3.30 3.32
#4	Discarded	6.50'	1.000 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.0 cfs @ 8.40 hrs HW=6.54' (Free Discharge)

Primary OutFlow Max=0.3 cfs @ 12.76 hrs HW=9.17' TW=8.18' (Dynamic Tailwater)

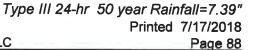
1=Culvert (Passes 0.3 cfs of 3.8 cfs potential flow)

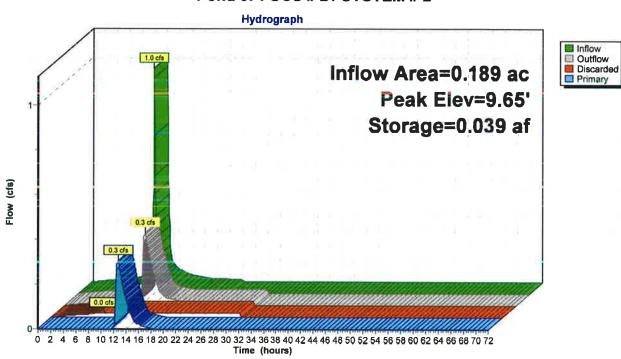
-2=Orifice/Grate (Orifice Controls 0.3 cfs @ 4.80 fps)

-3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)

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Pond 9P: OCS # 2 / SYSTEM # 2

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Summary for Pond 10P: (new Pond)

Inflow Area =	0.028 ac, 0.00% Impervious, Inflow De	epth = 2.99" for 50 year event
Inflow =	0.1 cfs @ 12.08 hrs, Volume=	0.007 af
Outflow =	0.0 cfs @ 12.49 hrs, Volume=	0.007 af, Atten= 73%, Lag= 24.7 min
Discarded =	0.0 cfs @ 12.49 hrs, Volume=	0.006 af
Primary =	0.0 cfs @ 12.49 hrs, Volume=	0.001 af
Secondary =	0.0 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 9.51' @ 12.49 hrs Surf.Area= 287 sf Storage= 114 cf

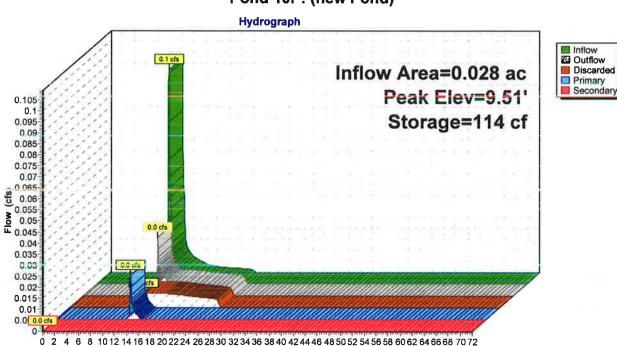
Plug-Flow detention time= 176.3 min calculated for 0.007 af (100% of inflow) Center-of-Mass det. time= 176.2 min (1,023.5 - 847.2)

Volume	Invert	Avail.Sto	orage	Storage Description		
#1	9.00'	2	90 cf	Custom Stage Data	(Irregular) Listed	below (Recalc)
Elevatio	et)	(sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
9.0 10.0		164	77.4	0	0	164
10.0	0	438	103.9	290	290	557
Device	Routing	Invert	Outle	et Devices		
#1	Primary	7.39'	6.0"	Round Culvert		
			Inlet	3.0' CPP, square ec / Outlet Invert= 7.39' .013 Corrugated PE,	7.13' S= 0.0049	9 '/' Cc= 0.900
#2	Device 1	9.50'		" Horiz. Orifice/Grate ted to weir flow at low		
#3	Secondary	9.75'	Hea 2.50 Coet	3.00 3.50 4.00 4.5	.60 0.80 1.00 1.2 0 5.00 5.50 0 2.70 2.68 2.68	20 1.40 1.60 1.80 2.00 2.66 2.65 2.65 2.65
#4	Discarded	9.00'	1.00	0 in/hr Exfiltration ov	ver Surface area	

Discarded OutFlow Max=0.0 cfs @ 12.49 hrs HW=9.51' (Free Discharge) **4=Exfiltration** (Exfiltration Controls 0.0 cfs)

Primary OutFlow Max=0.0 cfs @ 12.49 hrs HW=9.51' TW=8.51' (Dynamic Tailwater) 1=Culvert (Passes 0.0 cfs of 0.7 cfs potential flow) 2=Orifice/Grate (Weir Controls 0.0 cfs @ 0.32 fps)

Secondary OutFlow Max=0.0 cfs @ 0.00 hrs HW=9.00' TW=0.00' (Dynamic Tailwater) -3=Broad-Crested Rectangular Weir (Controls 0.0 cfs)



Time (hours)

Pond 10P: (new Pond)

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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 C Page 91

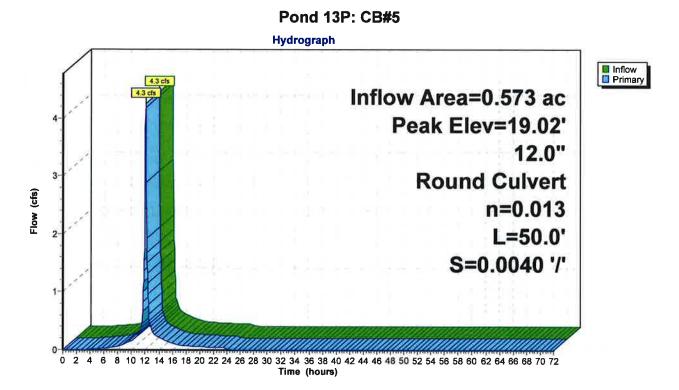
Summary for Pond 13P: CB#5

Inflow Area =	0.573 ac, 86.40% Impervious,	Inflow Depth = 6.21" for 50 year event
Inflow =	4.3 cfs @ 12.04 hrs, Volum	e= 0.296 af
Outflow =	4.3 cfs @ 12.04 hrs, Volum	e= 0.296 af, Atten= 0%, Lag= 0.0 min
Primary =	4.3 cfs @ 12.04 hrs, Volum	e= 0.296 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 19.02' @ 12.21 hrs

Device I	Routing	Invert	Outlet Devices
#1 1	Primary	8.06'	12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 8.06' / 7.86' S= 0.0040 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=12.98' TW=14.21' (Dynamic Tailwater)



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Summary for Pond 15P: DMH#1

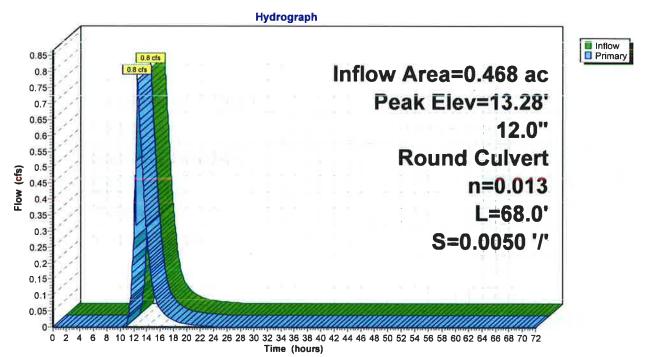
Inflow Area =	0.468 ac, 69.24% Impervious, Inflow	Depth = 3.14" for 50 year event
Inflow =	0.8 cfs @ 12.54 hrs, Volume=	0.123 af
Outflow =	0.8 cfs @ 12.54 hrs, Volume=	0.123 af, Atten= 0%, Lag= 0.0 min
Primary =	0.8 cfs @ 12.54 hrs, Volume=	0.123 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 13.28' @ 12.24 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 68.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.38' / 7.04' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.4 cfs @ 12.54 hrs HW=8.64' TW=8.47' (Dynamic Tailwater)

Pond 15P: DMH#1



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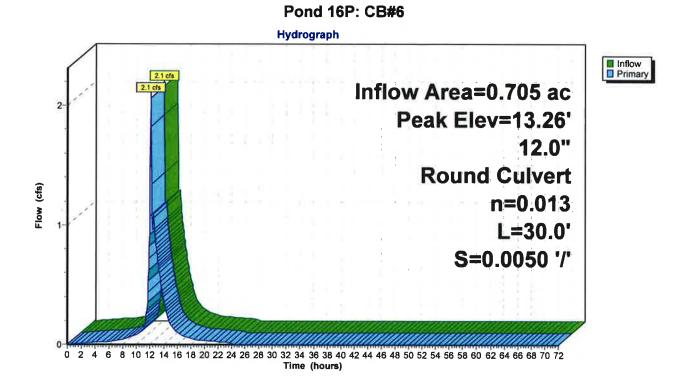
Summary for Pond 16P: CB#6

Inflow Area =	0.705 ac, 79.56% Impervious, Inflow De	epth = 4.49" for 50 year event
Inflow =	2.1 cfs @ 12.08 hrs, Volume=	0.264 af
Outflow =	2.1 cfs @ 12.08 hrs, Volume=	0.264 af, Atten= 0%, Lag= 0.0 min
Primary =	2.1 cfs @ 12.08 hrs, Volume=	0.264 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 13.26' @ 12.19 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.04'	12.0" Round Culvert L= 30.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.04' / 6.89' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.08 hrs HW=10.53' TW=11.79' (Dynamic Tailwater) **1=Culvert** (Controls 0.0 cfs)

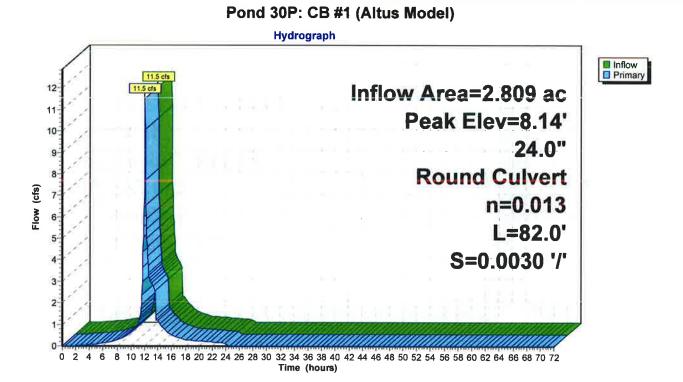


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Summary for Pond 30P: CB #1 (Altus Model)

2.809 ac, 53.04% Impervious, Inflow Depth = 5.62" for 50 year event Inflow Area = Inflow = 11.5 cfs @ 12.05 hrs, Volume= 1.315 af Outflow = 11.5 cfs @ 12.05 hrs, Volume= 1.315 af, Atten= 0%, Lag= 0.0 min Primary 11.5 cfs @ 12.05 hrs, Volume= = 1.315 af Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 8.14' @ 12.08 hrs Flood Elev= 9.15' Device Routing Invert Outlet Devices #1 Primary 6.11' 24.0" Round Culvert L= 82.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.11' / 5.86' S= 0.0030 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=10.0 cfs @ 12.05 hrs HW=8.10' TW=7.54' (Dynamic Tailwater)



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Summary for Pond 31P: CB #2 (Altus Model)

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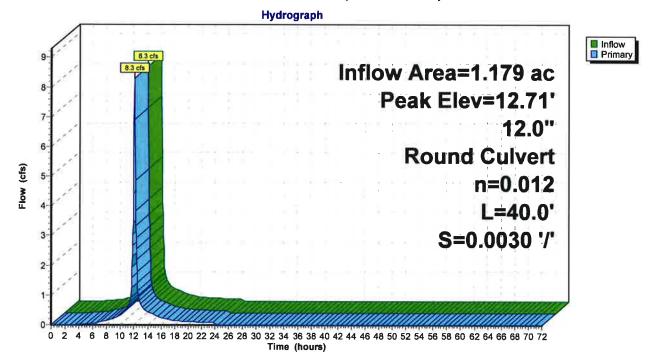
Inflow Area = 1.179 ac, 41.96% Impervious, Inflow Depth = 6.27" for 50 year event Inflow 8.3 cfs @ 12.05 hrs, Volume= = 0.616 af Outflow 8.3 cfs @ 12.05 hrs, Volume= 0.616 af, Atten= 0%, Lag= 0.0 min = Primary = 8.3 cfs @ 12.05 hrs, Volume= 0.616 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 12.71' @ 12.06 hrs Flood Elev= 9.15'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.33'	12.0" Round Culvert L= 40.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.33' / 6.21' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=8.1 cfs @ 12.05 hrs HW=12.67' TW=8.10' (Dynamic Tailwater) -1=Culvert (Inlet Controls 8.1 cfs @ 10.29 fps)

Pond 31P: CB #2 (Altus Model)



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Summary for Pond 32P: CB #3 (Altus Model)

1.057 ac, 46.83% Impervious, Inflow Depth = 6.28" for 50 year event Inflow Area = Inflow 7.5 cfs @ 12.05 hrs, Volume= = 0.553 af 7.5 cfs @ 12.05 hrs, Volume= Outflow Ξ 0.553 af, Atten= 0%, Lag= 0.0 min Primary = 7.5 cfs @ 12.05 hrs, Volume= 0.553 af Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 16.78' @ 12.08 hrs Flood Elev= 9.20' Device Routing Invert Outlet Devices #1 Primary 6.71' 12.0" Round Culvert L= 92.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.71' / 6.43' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=6.0 cfs @ 12.05 hrs HW=16.29' TW=12.66' (Dynamic Tailwater) 1=Culvert (Outlet Controls 6.0 cfs @ 7.68 fps)

Hydrograph Inflow Primary 7.5 cfr 8 Inflow Area=1.057 ac 7.5 cfs 7 Peak Elev=16.78' 12.0" 6 Round Culvert 5 Flow (cfs) n=0.012 4 L=92.0' 3 S=0.0030 '/' 2 1 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Pond 32P: CB #3 (Altus Model)

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Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 .C Page 97

Summary for Pond 33P: CB #4 (Altus Model) - Relocated (CB5B)

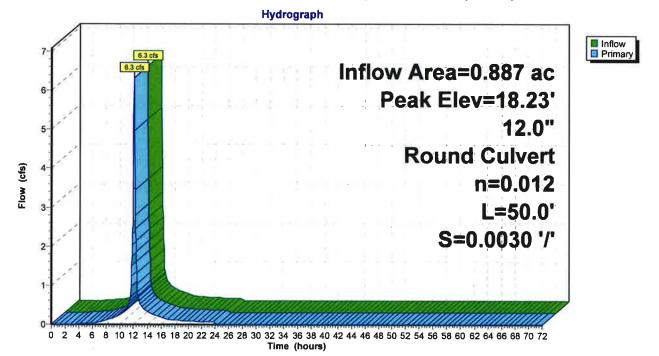
Inflow Area =	0.887 ac, 5	5.77% Impervious, In	flow Depth = 6.25"	for 50 year event
Inflow =	6.3 cfs @	12.05 hrs, Volume=	0.462 af	-
Outflow =	6.3 cfs @	12.05 hrs, Volume=	0.462 af, Att	en= 0%, Lag= 0.0 min
Primary =	6.3 cfs @	12.05 hrs, Volume=	0.462 af	•

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 18.23' @ 12.11 hrs Flood Elev= 9.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.96'	12.0" Round Culvert L= 50.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.96' / 6.81' S= 0.0030 '/' Cc= 0.900 n= 0.012, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.05 hrs HW=15.18' TW=16.03' (Dynamic Tailwater)





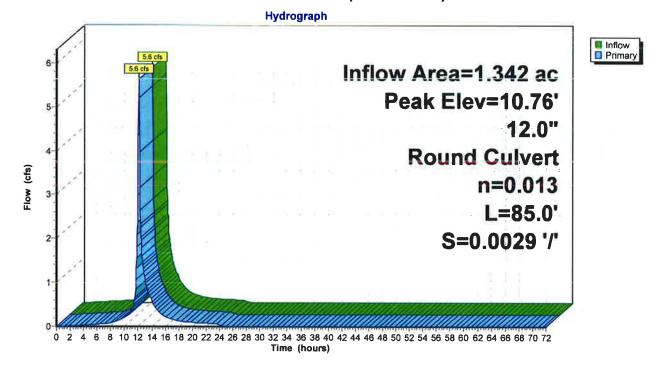
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Summary for Pond 34P: CB #5 (Altus Model)

Inflow Are	ea =	1.342 ac, 64.5	4% Impervious, Inflow Depth = 4.78" for 50 year event
Inflow	=	5.6 cfs @ 1	2.06 hrs, Volume= 0.535 af
Outflow	=	5.6 cfs @ 1	2.06 hrs, Volume= 0.535 af, Atten= 0%, Lag= 0.0 min
Primary	=	5.6 cfs @ 1	2.06 hrs, Volume= 0.535 af
	v= 10.76' (or-Ind method, T @ 12.06 hrs	ïme Span= 0.00-72.00 hrs, dt= 0.05 hrs
Device	Routing	Invert	Outlet Devices
#1	Primary	5.83'	12.0" Round Culvert
	-		L= 85.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 5.83' / 5.58' S= 0.0029 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
Determine	OUTEL		12 06 hrs HIM-10 60' TIM-7 4E' (Dynamic Tellusted)

Primary OutFlow Max=5.5 cfs @ 12.06 hrs HW=10.60' TW=7.45' (Dynamic Tailwater) 1=Culvert (Outlet Controls 5.5 cfs @ 6.97 fps)

Pond 34P: CB #5 (Altus Model)



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Summary for Pond AEI 6: Discharge Point 3 (Off Site Drainage)

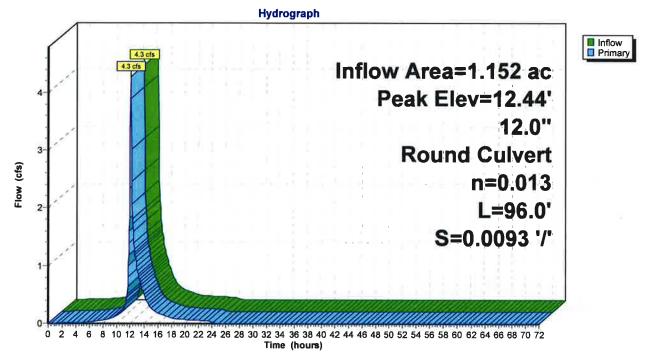
Inflow Area =	1.152 ac, 71.58% Impervious, Infl	ow Depth = 4.44" for 50 year event
Inflow =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af
Outflow =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af, Atten= 0%, Lag= 0.0 min
Primary =	4.3 cfs @ 12.06 hrs, Volume=	0.426 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 12.44' @ 12.10 hrs Flood Elev= 10.77'

Device	Routing	Invert	Outlet Devices
#1	Primary	6.77'	12.0" Round Culvert L= 96.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 6.77' / 5.88' S= 0.0093 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=3.1 cfs @ 12.06 hrs HW=11.69' TW=10.63' (Dynamic Tailwater) -1=Culvert (Outlet Controls 3.1 cfs @ 3.90 fps)





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Summary for Pond CB 4433:

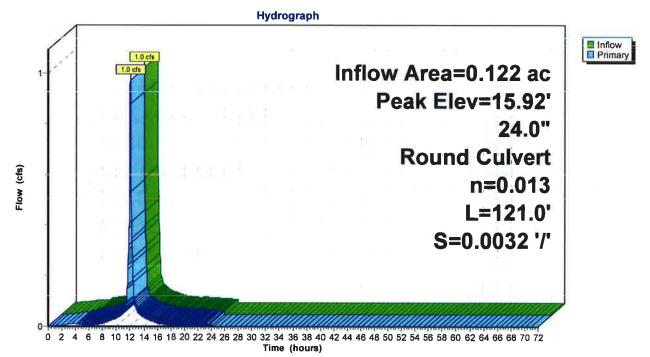
Inflow Area =	0.122 ac,100.00% Impervious,	Inflow Depth = 7.15" for 50 year event
Inflow =	1.0 cfs @ 12.01 hrs, Volume	e= 0.073 af
Outflow =	1.0 cfs @ 12.01 hrs, Volume	e= 0.073 af, Atten= 0%, Lag= 0.0 min
Primary =	1.0 cfs @ 12.01 hrs, Volume	e= 0.073 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.92' @ 12.06 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.38'	24.0" Round Culvert L= 121.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.38' / 13.99' S= 0.0032 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.0 cfs @ 12.01 hrs HW=15.85' TW=15.90' (Dynamic Tailwater)

Pond CB 4433:



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Summary for Pond CB 4435:

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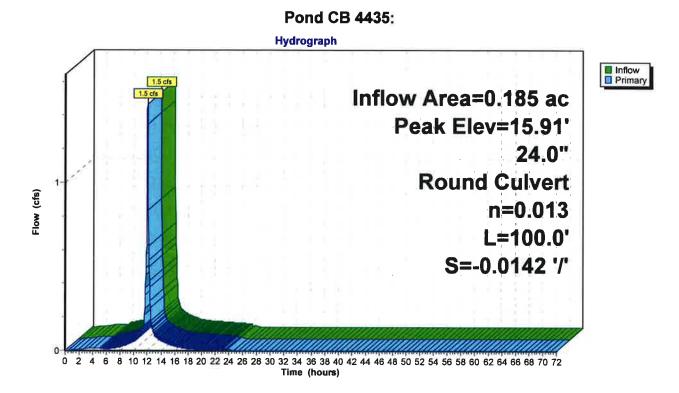
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Inflow Area =	0.185 ac,100.00% Impervious, Inflow E	Depth = 7.15" for 50 year event
Inflow =	1.5 cfs @ 12.02 hrs, Volume=	0.110 af
Outflow =	1.5 cfs @ 12.02 hrs, Volume=	0.110 af, Atten= 0%, Lag= 0.0 min
Primary =	1.5 cfs @ 12.02 hrs, Volume=	0.110 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.91' @ 12.02 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	15.41'	24.0" Round Culvert L= 100.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 13.99' / 15.41' S= -0.0142 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=1.4 cfs @ 12.02 hrs HW=15.90' TW=0.00' (Dynamic Tailwater) -1=Culvert (Inlet Controls 1.4 cfs @ 2.38 fps)



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Summary for Pond CB 4560:

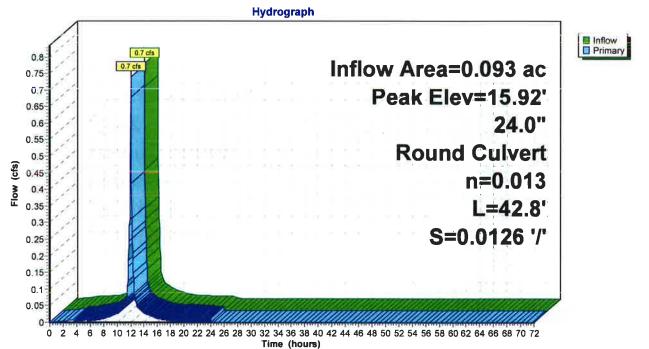
Inflow Area =	0.093 ac,100.00% Impervious, Inflow De	epth = 7.15" for 50 year event
Inflow =	0.7 cfs @ 12.02 hrs, Volume=	0.055 af
Outflow =	0.7 cfs @ 12.02 hrs, Volume=	0.055 af, Atten= 1%, Lag= 0.1 min
Primary =	0.7 cfs @ 12.02 hrs, Volume=	0 055 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 15.92' @ 12.11 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	14.92'	24.0" Round Culvert L= 42.8' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 14.92' / 14.38' S= 0.0126 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 3.14 sf

Primary OutFlow Max=0.0 cfs @ 12.02 hrs HW=15.79' TW=15.86' (Dynamic Tailwater)

Pond CB 4560:



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Summary for Pond DP1A: CB#5A

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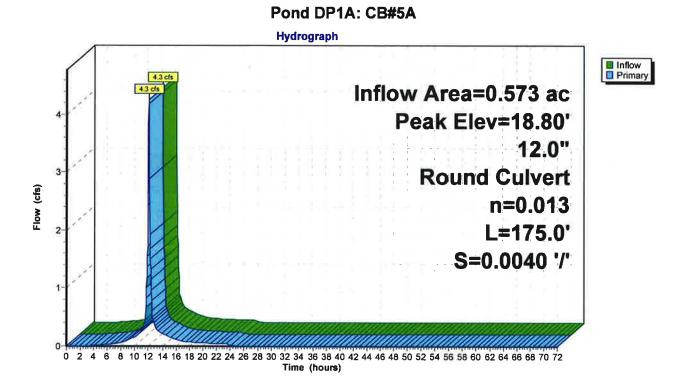
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Inflow Area	=	0.573 ac, 8	6.40% Impervious	, Inflow Depth =	6.21" for	50 year event
Inflow	=	4.3 cfs @	12.04 hrs, Volum	ne= 0.296	af	•
Outflow	=	4.3 cfs @	12.04 hrs, Volum	ie= 0.296	af, Atten=	0%, Lag= 0.0 min
Primary	=	4.3 cfs @	12.04 hrs, Volum	ne= 0.296	af	-

Routing by Dyn-Stor-Ind method, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs Peak Elev= 18.80' @ 12.16 hrs

Device	Routing	Invert	Outlet Devices
#1	Primary	7.76'	12.0" Round Culvert L= 175.0' CPP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 7.76' / 7.06' S= 0.0040 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.0 cfs @ 12.04 hrs HW=14.21' TW=14.43' (Dynamic Tailwater)



2790 Developed Conditions	Type III 24-hr 50 year Rainfall=7.39"
Prepared by Ambit Engineering, Inc.	Printed 7/17/2018
HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LL	C Page 104

Summary for Link 2L: Discharge Point 2 (Court Street Drainage)

Inflow Area =	0.185 ac,100.00% Impervious,	Inflow Depth = 7.15" for 50 year event
Inflow =	1.5 cfs @ 12.02 hrs, Volume	e= 0.110 af
Primary =	1.5 cfs @ 12.02 hrs, Volume	e= 0.110 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Flow (cfs)

0

Hydrograph Inflow Inflow Area=0.185 ac 1.5

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

Link 2L: Discharge Point 2 (Court Street Drainage)

2790 Developed Conditions Prepared by Ambit Engineering, Inc. HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software Solutions LLC

Type III 24-hr 50 year Rainfall=7.39" Printed 7/17/2018 Page 105

Summary for Link 3L: Discharge Point 4 (DP4)

Inflow	=	0.0 cfs @	0.00 hrs, Volume=	0.000 af
Primary	=	0.0 cfs @	0.00 hrs, Volume=	0.000 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs

Hydrograph Inflow Primary ⁼low (cfs) 0 0 2 4 6 8 10 12 14 16 18 20 22 24 26 28 30 32 34 36 38 40 42 44 46 48 50 52 54 56 58 60 62 64 66 68 70 72 Time (hours)

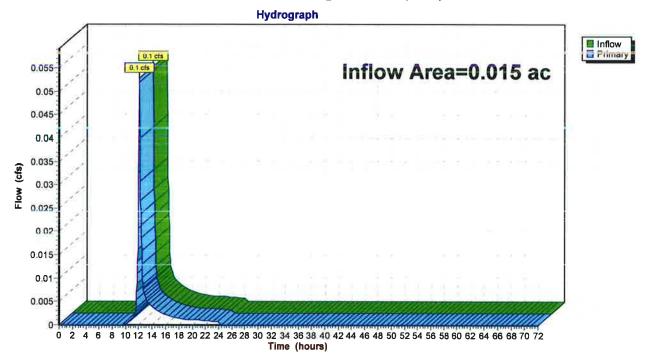
Link 3L: Discharge Point 4 (DP4)

2790 Developed Conditions	Type III 24-hr 50 year Rainfall=7.39"
Prepared by Ambit Engineering, Inc.	Printed 7/17/2018
HydroCAD® 10.00 s/n 00801 © 2013 HydroCAD Software So	lutions LLC Page 106

Summary for Link 4L: Discharge Point 5 (DP5)

Inflow Area =	0.015 ac, 0.00% Impervious, Inflow Depth = 2.99" for 50 year event
Inflow =	0.1 cfs @ 12.08 hrs, Volume= 0.004 af
Primary =	0.1 cfs @ 12.08 hrs, Volume= 0.004 af, Atten= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.00-72.00 hrs, dt= 0.05 hrs



Link 4L: Discharge Point 5 (DP5)

APPENDIX D

SOIL SURVEY INFORMATION

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USDA United States Department of Agriculture



Natural Resources Conservation Service

A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Rockingham **County, New** Hampshire



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

Custom Soil Resource Report

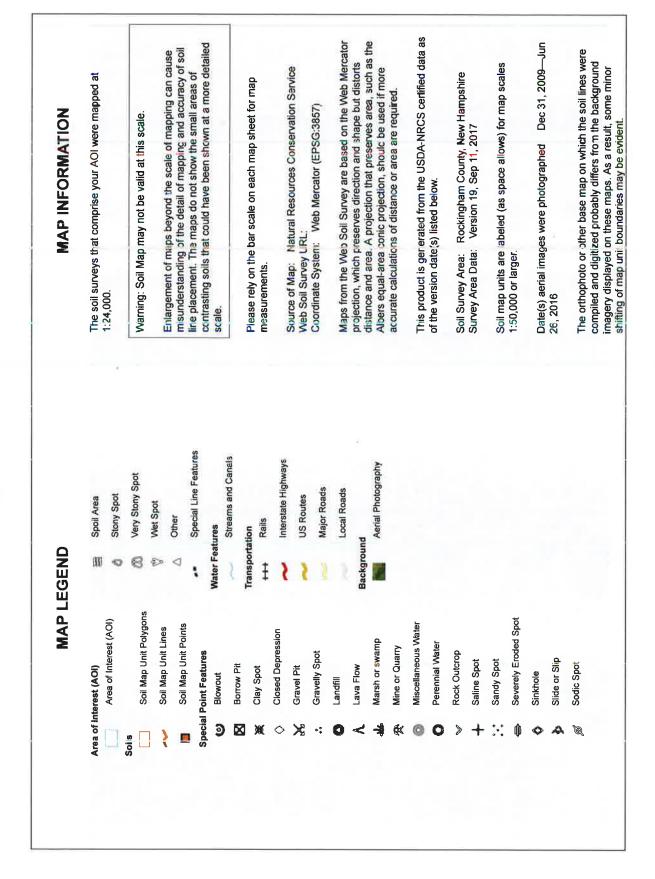
identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.



Custom Soil Rescurce Report



Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI		
699	Urban land	2.0	100.0%		
Totals for Area of Interest		2.0	100.0%		

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Rockingham County, New Hampshire

699—Urban land

Map Unit Composition

Urban land: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Minor Components

Not named

Percent of map unit: 15 percent Hydric soil rating: No

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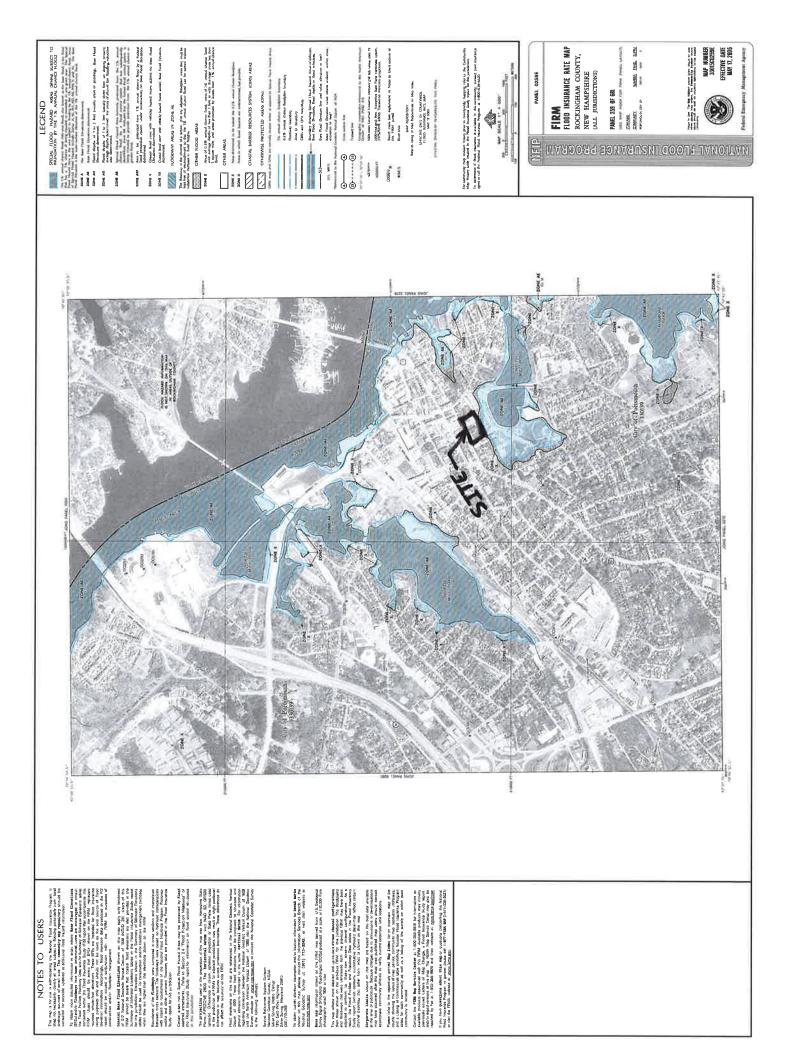
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APPENDIX E

FEMA FIRM MAP

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APPENDIX F

INSPECTION & MAINTENANCE PLAN

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STORMWATER MANAGEMENT INSPECTION & MAINTENANCE PLAN FOR PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET, PORTSMOUTH, NH

Introduction

that cover the inspection and maintenance requirements of the stormwater management system for the proposed redevelopment at the site. The intent of this plan is to provide Portsmouth Housing Authority located at 140 Court Street, Portsmouth, NH with a list of procedures

will be able to maintain the functional design of the stormwater management system. By installing and maintaining the drainage as shown on the approved site plan, Portsmouth Housing Authority will be able to maximize the system's ability to control the volume of runoff and measures will also help minimize potential environmental impacts. By following the enclosed procedures, Portsmouth Housing Authority The following inspection and maintenance program is necessary to keep the stormwater management system functioning properly. These remove sediment from site generated stormwater runoff.

Stormwater Management System Components

The Stormwater Management System is designed to comply with RSA 483 – B:9 V(g)(2). As a result, the design includes the following elements:

StormTech Subsurface Stormwater System

Roof runoff from the proposed structure and a portion of the parking lot will be captured in catch basins and directed to the proposed criteria. The system will release the stormwater to infiltrate 100% of the Water Quality Volume (WQV, also referred to as the "first Court Street and a new building to be constructed to the east. The design calls for two separate systems (System # 1 and System #2) that utilize 24 and 23 StormTech SC-740 chambers respectively with a single isolator row as recommended by StormTech design StormTech Subsurface Stormwater System located between the existing Portsmouth Housing Authority Building located at 140 flush") into the ground. It is also designed to attenuate peak flows for the Q10 and Q50 storm events as required by the City of Portsmouth.

BMP's	
on-Structural	
Ž	

capital inputs and are intended to provide protection against erosion of soils. Examples of non-structural BMP's on this project include Non-Structural best management practices (BMP's) include temporary and permanent measures that typically require less labor and but are not limited to: Temporary and permanent mulching, temporary and permanent grass cover, trees, shrubs and ground covers, miscellaneous landscape plantings, dust control, tree protection, topsoiling, sediment barriers, temporary storm drain inlet protection, and a stabilized construction entrance.

Structural BMP's

Structural BMP's are more labor and capital intensive structures or installations that require more specialized personnel to install. Examples on this project include but are not limited to: The rain garden located to the rear of Lot 3, associated inlet/outlet pipes, headwalls/end sections and emergency outlet/rip rap apron.

Inspection & Maintenance Checklist/Log

Authority and will serve as a guideline for performing the inspection and maintenance of the Stormwater Management System. This is a The following pages contain maintenance specifications, a Stormwater Management System Inspection & Maintenance Checklist, and a blank copy of the Stormwater Management System Inspection & Maintenance Log. The forms are provided to Portsmouth Housing guideline and should be periodically reviewed for conformance with current practice and standards.

STORMTECH SUBSURFACE STORMWATER SYSTEM MAINTENANCE

driveway runoff. This system is designed to accept and infiltrate the first inch of rainfall from a storm event. The system is also designed to In general, the intent of a subsurface leaching system is to provide for infiltration of runoff from developed areas, in this case the roof and stormwater run-off stream before the water reaches the rest of the subsurface system. The system should perform for many years without slow the peak runoff from a 50 year frequency rainfall event (7.39" of rain in a 24 hour period). In order to keep the subsurface leaching leaching systems would typically include an "Isolator Row". This is a row of chambers dedicated to settling out particulate matter in the system functioning properly, it is important to keep the system porous and unplugged by debris. Installation of a StormTech subsurface clogging. Regular inspection of the Isolator Row should be performed to avoid the need for system cleaning beyond the Isolator Row.

Specific Maintenance Procedures

Twice per year, during regular rains (less than 1 inch in 24 hours) inspect the overflow outlet to see if water is exiting the system. Run off exiting the system would indicate that the system is clogged and in need of replacement. Review the pipe outlet for any signs of rosion and stabilize if mecssary. Some water may be exiting the system, which is not designed for heavy rain safter long periods of drought may infiltrate into the soil and not show up. Lack of water exiting the system may indicate that the overflow pipe is clogged and not functioning. Check for animal activity and / or vegetation blockages. Extended periods of wetness at the ground surface above the chambers can also be a sign of system failure. If the subsurface leaching system is of functioning the system would be repaired by the removal of accumulated debris including sand and silfs) to return the subsurface leaching system to a functioning condition. Accumulated sediment can be removed with culvert cleaning device which will allow the removal of the accumulated debris by power washing the material back to the open end of the system for removal. Storm the subsurface leaching system to a functioning condition. Accumulated sediment can be removed with culvert cleaning device which will allow the removal of the accumulated debris by power washing the material back to the open end of the system for the over. Storm the subsurface leaching system to a functioning the system of the accumulated debris is of the accumulated debris is of the system of the system for the over. Storm the tender of the accumulated debris induction. Accumulated debris by power washing the material back to the open end of the system for tender or allow the removal. Storm the subsurface leaching system to a functioning condition. <th>rice per year, during regular rains (less than 1 in ting the system would indicate that the system i bilize if necessary. Some water may be exiting to iods of drought may infiltrate into the soil and 1 gged and not functioning. Check for animal act ove the chambers can also be a sign of system fa he subsurface leaching system is not functionin (s) to return the subsurface leaching system to a <i>lice</i> which will allow the removal of the accum noval.</th> <th>ch in 24 hours) inspect the overflow outlet to see if s clogged and in need of replacement. Review the p he system, which is not designed for heavy rain eve not show up. Lack of water exiting the system may i ivity and / or vegetation blockages. Extended period dilure. g the system would be repaired by the removal of ac functioning condition. Accumulated sediment can lated debris by power washing the material back to <i>Stormwater Management System</i></th> <th>water is exiting the system. Run off pipe outlet for any signs of erosion and ents, though heavy rains after long indicate that the overflow pipe is ds of wetness at the ground surface ccumulated debris including sand and be removed with culvert cleaning of the open end of the system for</th>	rice per year, during regular rains (less than 1 in ting the system would indicate that the system i bilize if necessary. Some water may be exiting to iods of drought may infiltrate into the soil and 1 gged and not functioning. Check for animal act ove the chambers can also be a sign of system fa he subsurface leaching system is not functionin (s) to return the subsurface leaching system to a <i>lice</i> which will allow the removal of the accum noval.	ch in 24 hours) inspect the overflow outlet to see if s clogged and in need of replacement. Review the p he system, which is not designed for heavy rain eve not show up. Lack of water exiting the system may i ivity and / or vegetation blockages. Extended period dilure. g the system would be repaired by the removal of ac functioning condition. Accumulated sediment can lated debris by power washing the material back to <i>Stormwater Management System</i>	water is exiting the system. Run off pipe outlet for any signs of erosion and ents, though heavy rains after long indicate that the overflow pipe is ds of wetness at the ground surface ccumulated debris including sand and be removed with culvert cleaning of the open end of the system for
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St Pe 140 Inspec Minimum	μ.	Stormwater Management System	
Inspec	T	<i>for</i> Portsmouth Housing Authority 40 Court Street, Portsmouth, NH	
Minimum	Insp	ection & Maintenance Checklist	
Component Inspection Frequency		Minimum Inspection Requirements	Maintenance/Cleanout Threshold
Stormtech Subsurface 2 times per year During Light Rains Inspect Outlet Functioning Chamber System Experiment of the system Experiment of the system	rface	During Light Rains Inspect Outlet Functioning	Repair / Clean as needed
Detention Basin Monthly Check for sediment clogging; leaks, excessive weed growth and sloughing of berms. Check plant vitality. Check for scouring near pipe inlet. Check for invasive s		Check for sediment clogging; leaks, excessive weed growth and sloughing of berms. Check plant vitality. Check for scouring near pipe inlet. Check for invasive	Repair leaks, scouring or sloughs, remove weeds and trash/debris; remove sediments regularly near pipe inlet.

4-

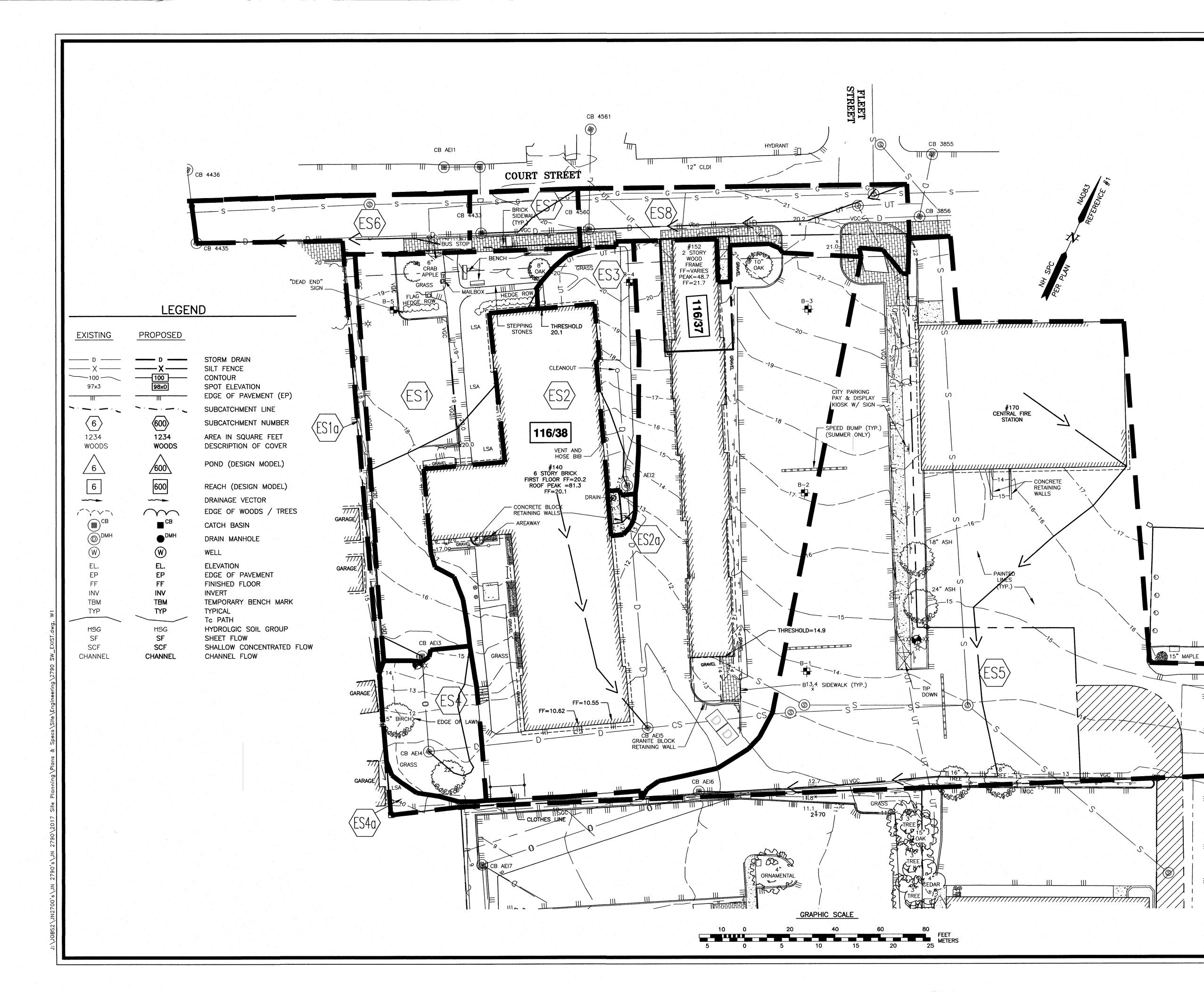
		species.	Replant dead or dying wetlands vegetation.
Catch Basins	Twice Yearly	Remove sediment and debris	Sediment within 6" of outlet pipe
Street Sweeping and Litter / Trash Removal	Twice Yearly	Visual Determination of Surface Conditions	Mechanical or Manual Sweeping as Needed

140 Court Street, Portsmouth, NH **Portsmouth Housing Authority** Stormwater Management System for

 Inspection & Maintenance Log

 (This log is to be submitted to the City of Dover Engineering Department on an annual basis, not later than December 15th of each year. The owner of record will be responsible for this ongoing maintenance and reporting.)

By					Τ
Performed By					
Date of Cleaning/Repair					
Cleaning/Repair Needed (List Items/Comments)					
Inspector					
Date Inspected					
BMP/System Component					





AMBIT ENGINEERING, INC. Civil Engineers & Land Surveyors

200 Griffin Road – Unit 3 Portsmouth, N.H. 03801–7114 Tel (603) 430–9282 Fax (603) 436-2315

PROJECT LOCATION 140 COURT STREET PORTSMOUTH, NH

PARCEL ID:

CITY OF PORTSMOUTH ASSESSOR'S MAP 116, LOTS 38 AND LOT 37.

OWNERS OF RECORD:

- 116/38 PORTSMOUTH HOUSING AUTHORITY
- 245 MIDDLE STREET
- PORTSMOUTH, NH 03801 R.C.R.D BK 1736, PG 386, BK 1797 PG 20 AND BK 1920, PG 47
- 116/37 ED PAC, LLC
- 242 CENTRAL AVENUE
- DOVER, NH 03820 BK 4679, PG 151

PARCEL 116/38 AND 116/37 ARE NOT IN A SPECIAL FLOOD HAZARD AREA AS SHOWN ON FIRM PANEL 3301SC0259E. EFFECTIVE 5/17/2005

NOTES:

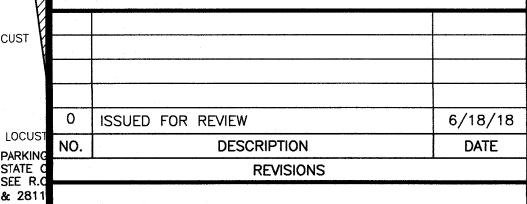
1) THIS PLAN IS INTENDED FOR RUNOFF ANALYSIS ONLY AND SHALL NOT BE USED FOR CONSTRUCTION.

2) THE CONTRACTOR SHALL NOTIFY DIG SAFE AT 1-888-DIG-SAFE (1-888-344-7233) AT LEAST 72 HOURS PRIOR TO COMMENCING ANY EXCAVATION ON PUBLIC OR PRIVATE PROPERTY.

3) UNDERGROUND UTILITY LOCATIONS ARE BASED UPON BEST AVAILABLE EVIDENCE AND ARE NOT FIELD VERIFIED. LOCATING AND PROTECTING ANY ABOVEGROUND OR UNDERGROUND UTILITIES IS THE SOLE RESPONSIBILITY OF THE CONTRACTOR AND/OR THE OWNER. UTILITY CONFLICTS SHOULD BE REPORTED AT ONCE TO THE DESIGN ENGINEER.

4) CONTRACTOR SHALL INSTALL AND MAINTAIN EROSION CONTROL MEASURES IN ACCORDANCE WITH THE "NEW HAMPSHIRE STORMWATER MANUAL, VOLUME 3, EROSION AND SEDIMENT CONTROLS DURING CONSTRUCTION. (NHDES DECEMBER 2008).

PORTSMOUTH HOUSING AUTHORITY 140 COURT STREET PORTSMOUTH, N.H.





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2790

SCALE: 1" = 20'

>--- PARKIN STATE SEE R.

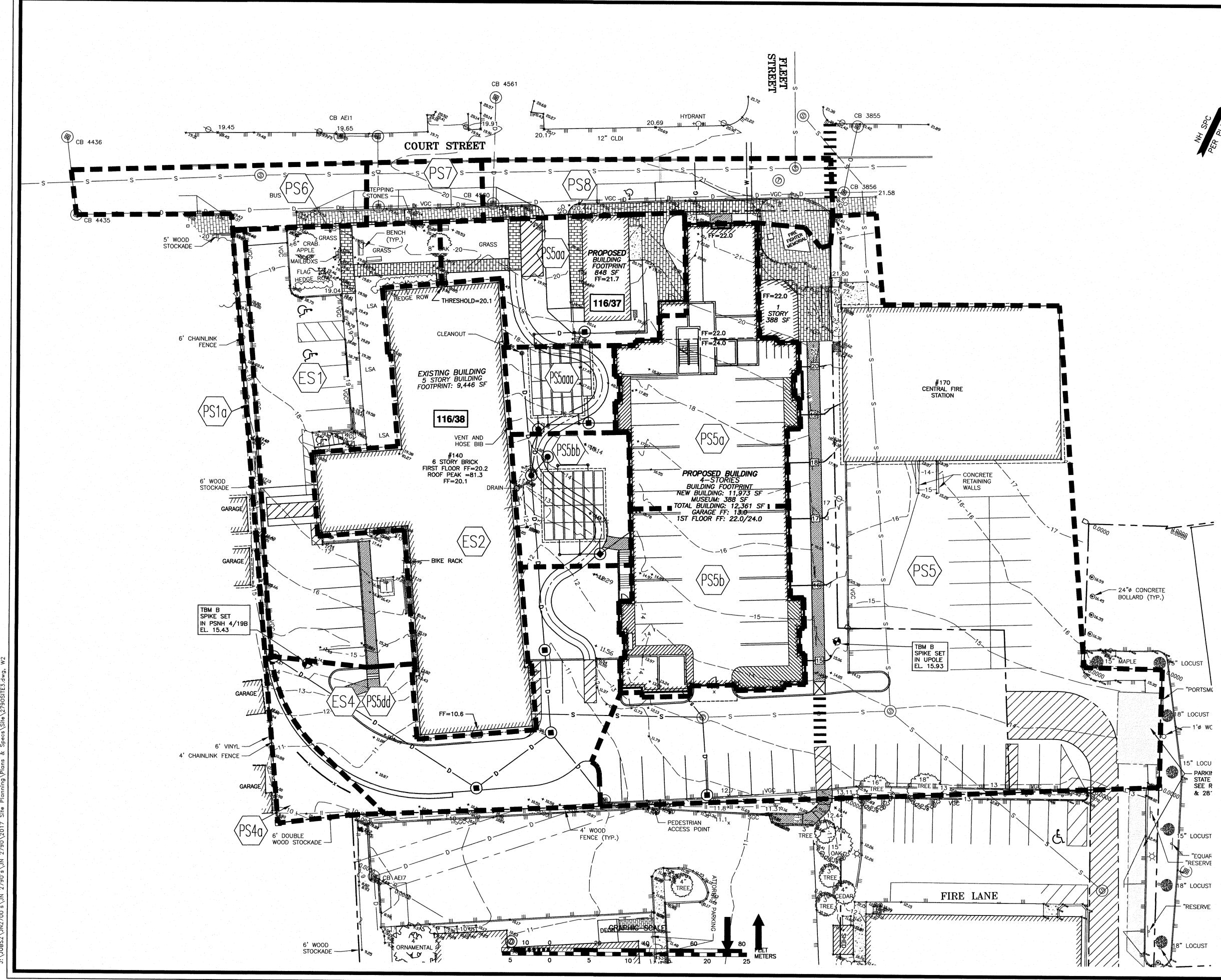
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18" LOCUST

PLAN OF EXISTING SUBCATCHMENTS







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