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May 24, 2022

Portsmouth Planning Department Attn. Peter Stith, Principal Planner 1 Junkins Avenue, Suite 3rd Floor Portsmouth, NH 03801

RE: Response Letter – Altus & Ambit Engineering and TAC Comments 1169 and 1171 Sagamore Ave, Portsmouth, NH Tax Map 224, Lots 14 & 15 JBE Project No. 21047

Dear Mr. Stith,

We are in receipt of comments from Eric Weinrieb, P.E., Altus Engineering dated April 29, 2022, John Chagnon, P.E., Ambit Engineering dated May 3, 2022 and TAC dated May 2, 2022. Review comments are listed below with our responses in bold.

ALTUS ENGINEERING:

GRADING AND DRAINAGE PLAN:

- 1. Note 29 indicates that the units will not have basements or foundation drains. This requirement is critical to premise of the stormwater management design. As such, it is recommended that this condition be documented on the approval. **RESPONSE: This is agreeable to the applicant.**
- 2. To the east of building unit 10 is a proposed 38.0 spot grade. It appears that the required grade should be closer to elevation 39.0.

 RESPONSE: The spot grade to the east of Unit 10 has been revised.
- 3. The revised plans depict a culvert under Sagamore Avenue that will drain the runoff from west side of Sagamore Avenue where the new sidewalk with raised curbing will be installed. Changing from open drainage along the Sagamore to a closed system supports the need for the culvert.

 RESPONSE: Agreed.

OFFSITE IMPROVEMENTS PLAN:

4. The Designer is proposing a 24-inch diameter culvert under Sagamore Avenue. Based on the drainage computations, it appears that a significantly smaller culvert will adequately handle the projected flows. A smaller diameter culvert will also reduce the potential for utility conflicts. The Designer should comment as to why a 24-inch culvert is proposed.

RESPONSE: The intent was to prevent the isolated depression from overflowing during the 50-Year, 24-Hour storm while also discharging as little as possible during the 2-Year 24-Hour storm, but this same result can be achieved with a 15" HDPE pipe and an invert out 0.2 ft lower, so the design has been modified accordingly.

5. The Designer should consider installing a Jellyfish or other approved treatment device at the culvert outfall.

RESPONSE: A Jellyfish filter has been added before the culvert outfall.

6. The Designer needs to confirm that the wetlands depicted on this plan has been delineated by a licensed wetlands scientist.

RESPONSE: The wetlands depicted on this plan have been delineated by a licensed wetlands scientist. Note #12 on Sheet C1 lists the wetland delineation standards that were used, and the same sheet has been stamped by the certified wetland scientist who delineated the wetlands.

7. It is understood that the applicant will need a Conditional Use Permit for the work on the city land and will need to obtain an easement to complete the work.

RESPONSE: We are applying for a conditional use permit and an easement will be prepared. A draft easement for the work on City land is shown on Sheet C2.

DETAIL SHEETS:

8. The city should decide if hoods should be installed on the catch basins outlet pipes on site and in the State right-of-way.

RESPONSE: No response needed.

9. The bioretention basin detail on Sheet D5 references notes 4 and 5 under design considerations. The plans are deficient note 5.

RESPONSE: The reference to Note 5 has been removed.

10. Concrete galley detail on Sheet D6 indicates that there will be a 6-inch crushed stone layer above the galleys. On System B, it appears that there will not be adequate cover above the stone to support vegetation.

RESPONSE: The plans and detail have been revised so that the minimum grade over System B is 38.6, leaving at least 6" of loam above the stone layer as required.



DRAINAGE ANALYSIS:

11. The Designer has addressed the increase in volume to the wetland at the northeast corner of the site by proposing a culvert that drains excess runoff towards the city land on the east side of Sagamore Avenue. It is our opinion that this culvert satisfactorily addresses the concerns regarding impacting the abutting properties to the north of the site.

RESPONSE: No response necessary.

STORMWATER MANAGEMENT OPERATION AND MAINTENANCE MANUAL:

12. This document should be included in the condominium documents and should be recorded at the Registry of Deeds to ensure that the association and all owners are aware of the requirements to maintain the site.

RESPONSE: The Stormwater Management Operation and Maintenance Manual will be included in the condominium documents and will be recorded at the Rockingham County Registry of Deeds.

AMBIT ENGINEERING - Comments on Behalf of Sea Star Cove Condominiums:

Existing Conditions Plan:

The Certified Soil Scientists should stamp the final plan.
 RESPONSE: The final plans will be stamped by a certified soil scientist.

2. The plan does not show benchmarks.

RESPONSE: A benchmark in the utility pole on the southeast corner of the subject parcel has been added to the plan.

3. The Exposed Ledge depiction has been removed from the Legend. RESPONSE: The ledge outcrop depiction has been added to the legend.

Demolition Plan DM-1:

- 4. The note to save the 12" Maple in the vicinity of the new headwall should be verified. **RESPONSE:** The tree is now noted to be removed.
- 5. Note 13: We doubt that any leach field components would be able to remain given the extensive site work.

RESPONSE: We believe this refers to Note 12 – There is no Note 13 on Sheet DM-1 – Note 12 has been revised to state that the leach field shall be removed.

6. The extent of old fill removal should extend beyond the property line if any fill was placed over the property line onto Sea Star Cove property.

RESPONSE: It is noted on Sheet DM-1 that any offsite fill shall be removed and the approximate extent of offsite fill is now shown.



7. The plan shows a "proposed tree line / limit of clearing" along the northerly property line at the west end of the property line. Trees marked in the field vary from this representation.

RESPONSE: The contractor is to clear trees up to the proposed treeline.

Condominium Site Plan C2:

- 8. The size of the bicycle pad should be confirmed by showing the layout of the racks. RESPONSE: The layout of the bicycle racks has been added to the bicycle rack detail on Sheet D1.
- Coverage calculation details should be on the plan.
 RESPONSE: Building coverage calculations have been added to Note 2 on Sheet C2.
- 10. The final Condominium Site Plans should show the plan view and note that maintenance will be required.

RESPONSE: The final condominium site plans will show the plan view and note that maintenance will be required.

Grading and Drainage Plan C3:

11. Show benchmarks. Clarify the intent of Note 2. Is the Contractor required to do a topographic survey of the property?

DESPONSE: A banchmark in the willity pole on the contract corpor of the su

RESPONSE: A benchmark in the utility pole on the southeast corner of the subject parcel has been added to the plan. Note 2 has been reworded to clarify the intent.

12. The elevation of the outlet pipe(s) from Concrete Galley Systems A and B are above the elevations of the collection system and will create a backflow in the collection piping network.

RESPONSE: System B is designed to infiltrate, and the outlet pipe is intended as an overflow only. The most frequent modelled storm during which this is activated is the 25-Year 24-Hour event. The underdrain on System A is at the bottom of the lined system and is intended to be the primary outflow from the system, below the collection piping network, from which detained outflow will discharge. The overflow pipe from this system is above the collection piping network, and the most frequent modelled storm during which it is activated is the 10-Year 24-Hour event.

The systems are designed to drain in a reasonable amount of time and tailwater modelling is set to be automatic throughout the entire HydroCAD model, so the potential for temporary backflow during peak storm events is taken into account and is not an issue.

13. The Stone Infiltration Bed overflow detail the overflow being at the gutter air brake. Note 27 indicates that locations may be adjusted, but the locations are key to the drainage analysis.

RESPONSE: Note 27 on Sheet C3 has been revised to instead say that final roof plans shall be reviewed by the project engineer prior to construction, so that it can be confirmed that the downspouts can still collect the water that they are intended to at the proposed locations.



14. The removal of the old fill will occur down to elevation which resembles the wetland elevation of the Sea Star Cove property. Could the pipe from Drain Manhole 3 be shortened and the grade lowered by the introduction of a retaining wall behind units 1 and 2 to provide some runoff storage on the 1169 / 1171 property?

RESPONSE: We have added a retaining wall and revised the proposed grading

15. There is a detail provided for the ledge removal for Galley System B; there should be one provided for Galley System A, and Bioretention 1 and 2.
RESPONSE: Ledge profiles for bioretention systems 1 & 2 have been added to Sheet D5 and a ledge profile for Galley System A has been added to D6 next to the one for Galley System B.

Landscape Plan L1:

behind units 1 and 2.

- 16. Are the 3 Ruby Spice Summer Sweet too close to run-off Gallery System B?

 RESPONSE: The 3 Ruby Spice Summer Sweet have been moved closer to Unit 4.
- 17. Will there be some trees remaining near the west end of the north property line? If not, can the developer add some plantings for a buffer?

 RESPONSE: Some additional trees have been added to the northwest corner of the property.

Detail Sheet D5:

18. Bioretention Detail Design Considerations Note 4 should align with the design requirements for elevation above ESHWT / ledge.

RESPONSE: Note 4 has been revised to say that ledge shall be removed to a depth of at least 2' below the bottom of the system.

Detail Sheet D6:

19. The Shea Concrete Galley System B Ledge Profile does not show the ledge under the system accurately.

RESPONSE: Any ledge profile will be an approximation; the ledge profile was based on test pits B1 and B2 and this is the most accurate depiction possible with the available data. More importantly, the contractor is to remove ledge to a depth of at least 2' below the bottom of the stone base, as noted.

Drainage Analysis Comments:

1. Pond 21P proposed (2P existing) is modelled after a wetland ponding area partially on the adjacent property. The pond in the proposed design receives a 0.11-foot higher peak elevation in the 2-year storm event. The other problems regarding peak volume from the last submission have been alleviated by a culvert crossing the street.

RESPONSE: With the revisions to the design per Altus comment #4, the 2-Year 24-Hour storm peak elevation is now lower than the existing.



2. The proposed infiltration practice at node 5P is designed to infiltrate the bulk of the stormwater volume reduction on site. While the test pit conducted at point B2 suggests a similar infiltration rate on the existing ground surface to that used in the model, the proposed infiltration device is located at least 4 feet below the ground surface. The proposed infiltration surface is within 1 inch of the ESHWT, and less than 2 feet from refusal of the test pit. If the refusal was due to the presence of ledge, then that further reduces the viability of the proposed infiltration device.

RESPONSE: The ledge is to be removed to an elevation at least 2 feet below the bottom of the stone backfill, and underneath approximately 57% of the proposed system, refusal is more than 2 feet below the proposed bottom of the stone already. Furthermore, the stone base material has a better percolation rate than the native soil it will be replacing, and the bottom of the actual infiltration chamber is at least 3' above the seasonal high water table as required. Infiltration is viable in a way that meets NHDES AOT standards.

TAC COMMENTS:

1. We assume all the prior comments were addressed, as there was no list of prior comments submitted.

RESPONSE: No response necessary.

Items to be addressed prior to Planning Board approval:

2. The culvert across Sagamore will need treatment before being discharged. DPW recommend a Jellyfish style filter.

RESPONSE: A Jellyfish filter has been added for the cross-culvert.

- 3. Add existing force main to drawing showing cross Sagamore culvert and add note regarding insulation of force main required near culvert.

 RESPONSE: The existing force main was already shown on Sheet C4. It is now noted on Sheet C4 that 2" of R-10 Foam Board insultation shall be provided between the existing forcemain and the proposed culvert.
- 4. The proposed culvert will need a temporary construction easement, permanent flowage easement, and permanent easement for the installation and placement of materials. RESONSE: The proposed culvert will require a temporary construction easement, permanent flowage easement and permanent easement for the installation and placement of materials from the city. A draft easement is shown on Sheet C2.
- 5. The proposed culvert will need City Council approval.

 RESPONSE: We will apply for City Council approval once approved by TAC.
- 6. The proposed culvert will require review by the Conservation Commission.

 RESPONSE: We will apply for a Conditional Use Permit once approved by TAC.
- 7. Please show that the proposed culvert and flowage meets the conservation restrictions of parcel 201/26.

RESPONSE: There are no conservation restrictions that would prevent the proposed flowage or culvert on parcel 201/26.



8. Staff are still waiting for the third-party review of the project.

RESPONSE: Responses to the third- and fourth-party review comments are included with this letter.

Included with this response letter are the following:

- 1. One (1) Full Size Revised Plan Set.
- 2. One (1) Revised Drainage Analysis.
- 3. Contech "Jellyfish" Maintenance Guide.
- 4. Conditional Use Application Cover Letter.
- 5. Current Deeds.
- 6. Letters of Authorization.

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Joseph Coronati Vice President

V 100 I Testaent

cc: \ Michael Garrepy (via email)

Mick Khavari (via email)

Tim Phoenix, Hoefle, Phoenix, Gormley & Roberts (via email)

Eric Weinrieb, Altus Engineering (via email and hand delivered)

John Chagnon, Ambit Engineering (via email and U.S. Mail)



City of Portsmouth, New Hampshire Site Plan Application Checklist

This site plan application checklist is a tool designed to assist the applicant in the planning process and for preparing the application for Planning Board review. The checklist is required to be completed and uploaded to the Site Plan application in the City's online permitting system. A preapplication conference with a member of the planning department is strongly encouraged as additional project information may be required depending on the size and scope. The applicant is cautioned that this checklist is only a guide and is not intended to be a complete list of all site plan review requirements. Please refer to the Site Plan review regulations for full details.

Applicant Responsibilities (Section 2.5.2): Applicable fees are due upon application submittal along with required attachments. The application shall be complete as submitted and provide adequate information for evaluation of the proposed site development. Waiver requests must be submitted in writing with appropriate justification.

Name of Applicant: The Sagamore Group, LLC	Date Submitted:	08/23/22		_	
Application # (in City's online permitting):LU-21-167					
Site Address: 1169 & 1171 Sagamore Ave.		Мар:	224	_ Lot:_	14&15

	Application Requirements		
M	Required Items for Submittal	Item Location (e.g. Page or Plan Sheet/Note #)	Waiver Requested
Х	Complete <u>application</u> form submitted via the City's web-based permitting program (2.5.2.1(2.5.2.3A)		N/A
X	All application documents, plans, supporting documentation and other materials uploaded to the application form in viewpoint in digital Portable Document Format (PDF). One hard copy of all plans and materials shall be submitted to the Planning Department by the published deadline. (2.5.2.8)		N/A

	Site Plan Review Application Required Information				
V	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested		
X	Statement that lists and describes "green" building components and systems. (2.5.3.1B)	Included			
X	Existing and proposed gross floor area and dimensions of all buildings and statement of uses and floor area for each floor. (2.5.3.1C)	C1 & C2	N/A		
X	Tax map and lot number, and current zoning of all parcels under Site Plan Review. (2.5.3.1D)	Cl	N/A		

	Site Plan Review Application Required Info	ormation	
V	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	Owner's name, address, telephone number, and signature. Name, address, and telephone number of applicant if different from owner. (2.5.3.1E)	Application	· N/A
X	Names and addresses (including Tax Map and Lot number and zoning districts) of all direct abutting property owners (including properties located across abutting streets) and holders of existing conservation, preservation or agricultural preservation restrictions affecting the subject property. (2.5.3.1F)	C1 & C2	N/A
x	Names, addresses and telephone numbers of all professionals involved in the site plan design. (2.5.3.16)	Cover Sheet	N/A
X	List of reference plans. (2.5.3.1H)	C1 & C2	N/A
x	List of names and contact information of all public or private utilities servicing the site. (2.5.3.1)	Cover Sheet	N/A

	Site Plan Specifications		
$\overline{\mathbf{A}}$	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	Full size plans shall not be larger than 22 inches by 34 inches with match lines as required, unless approved by the Planning Director (2.5.4.1A)	Required on all plan sheets	N/A
X	Scale: Not less than 1 inch = 60 feet and a graphic bar scale shall be included on all plans. (2.5.4.1B)	Required on all plan sheets	N/A
X	GIS data should be referenced to the coordinate system New Hampshire State Plane, NAD83 (1996), with units in feet. (2.5.4.1C)	C1 Note #15	N/A
x	Plans shall be drawn to scale and stamped by a NH licensed civil engineer. (2.5.4.1D)	Required on all plan sheets	N/A
X	Wetlands shall be delineated by a NH certified wetlands scientist and so stamped. (2.5.4.1E)	C1	N/A
X	Title (name of development project), north point, scale, legend. (2.5.4.2A)	Cover Sheet	N/A
х	Date plans first submitted, date and explanation of revisions. (2.5.4.2B)	All Sheets	N/A
X	Individual plan sheet title that clearly describes the information that is displayed. (2.5.4.2C)	Required on all plan sheets	N/A
X	Source and date of data displayed on the plan. (2.5.4.2D)	Cl	N/A

Site Plan Specifications – Required Exhibits and Data Required Items for Submittal Item Location Waive			Waiver
V.	required items for Submittal	(e.g. Page/line or Plan Sheet/Note #)	Requested
x	1. Existing Conditions: (2.5.4.3A)		
	Surveyed plan of site showing existing natural and built features;		
	Existing building footprints and gross floor area;		
	Existing parking areas and number of parking spaces provided;		
	Zoning district boundaries;		
	Existing, required, and proposed dimensional zoning	C 1	
	requirements including building and open space coverage, yards		
	and/or setbacks, and dwelling units per acre;		
	Existing impervious and disturbed areas;		
	Limits and type of existing vegetation;		
	Wetland delineation, wetland function and value assessment		
	(including vernal pools);		
	SFHA, 100-year flood elevation line and BFE data, as required.		
\mathbf{x}	2. Buildings and Structures: (2.5.4.3B)		
	Plan view: Use, size, dimensions, footings, overhangs, 1st fl.		
	elevation;		
	Elevations: Height, massing, placement, materials, lighting,		
	façade treatments;	Architectural Plans	
	Total Floor Area;		
	Number of Usable Floors;		
	Gross floor area by floor and use.		
X	3. Access and Circulation: (2.5.4.3C)		
	Location/width of access ways within site;		
	Location of curbing, right of ways, edge of pavement and		
	sidewalks;		
	Location, type, size and design of traffic signing (pavement partitions):	C2	
	markings);		
	 Names/layout of existing abutting streets; Driveway curb cuts for abutting prop. and public roads; 		
	If subdivision; Names of all roads, right of way lines and		
	easements noted;		
	AASHTO truck turning templates, description of minimum vehicle		
	allowed being a WB-50 (unless otherwise approved by TAC).	T1-T4	
X	4. Parking and Loading: (2.5.4.3D)		
	Location of off street parking/loading areas, landscaped	C2	
	areas/buffers;	C2	
_	Parking Calculations (# required and the # provided).		4
X	5. Water Infrastructure: (2.5.4.3E)		
	Size, type and location of water mains, shut-offs, hydrants &	C1 & C5	
	Engineering data;	Clacs	
	 Location of wells and monitoring wells (include protective radii). 		
X	6. Sewer Infrastructure: (2.5.4.3F)		
	Size, type and location of sanitary sewage facilities &	C1, C5, P1	
	Engineering data, including any onsite temporary facilities		

X	 7. Utilities: (2.5.4.3G) The size, type and location of all above & below ground utilities; Size type and location of generator pads, transformers and other fixtures. 	C1 & C5
X	8. Solid Waste Facilities: (2.5.4.3H)	
	The size, type and location of solid waste facilities.	C2 Note #22
X	 9. Storm water Management: (2.5.4.3I) The location, elevation and layout of all storm-water drainage. The location of onsite snow storage areas and/or proposed off-site snow removal provisions. Location and containment measures for any salt storage facilities Location of proposed temporary and permanent material storage locations and distance from wetlands, water bodies, and stormwater structures. 	C3 C2 C2 Note #35
X	 10. Outdoor Lighting: (2.5.4.3J) Type and placement of all lighting (exterior of building, parking lot and any other areas of the site) and photometric plan. 	L2
X	11. Indicate where dark sky friendly lighting measures have been implemented. (10.1)	L2
X	 12. Landscaping: (2.5.4.3K) Identify all undisturbed area, existing vegetation and that which is to be retained; 	L2
	Location of any irrigation system and water source.	C5
x	 13. Contours and Elevation: (2.5.4.3L) Existing/Proposed contours (2 foot minimum) and finished grade elevations. 	C1 & C3
X	 14. Open Space: (2.5.4.3M) Type, extent and location of all existing/proposed open space. 	C2
X	15. All easements, deed restrictions and non-public rights of ways. (2.5.4.3N)	C1 & C2
	 16. Character/Civic District (All following information shall be included): (2.5.4.3P) Applicable Building Height (10.5A21.20 & 10.5A43.30); Applicable Special Requirements (10.5A21.30); Proposed building form/type (10.5A43); Proposed community space (10.5A46). 	N/A
	The proposed development is consistent with the need to minimize flood damage; All public utilities and facilities are located and construction to minimize or eliminate flood damage; Adequate drainage is provided so as to reduce exposure to flood hazards.	N/A

	Other Required Information			
V	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested	
X	Traffic Impact Study or Trip Generation Report, as required. (3.2.1-2)	Previously Submitted		
Х	Indicate where Low Impact Development Design practices have been incorporated. (7.1)	C3		
х	Indicate whether the proposed development is located in a wellhead protection or aquifer protection area. Such determination shall be approved by the Director of the Dept. of Public Works. (7.3.1)	Not in Either		
X	Stormwater Management and Erosion Control Plan. (7.4)	Included		
X	Inspection and Maintenance Plan (7.6.5)	Included		

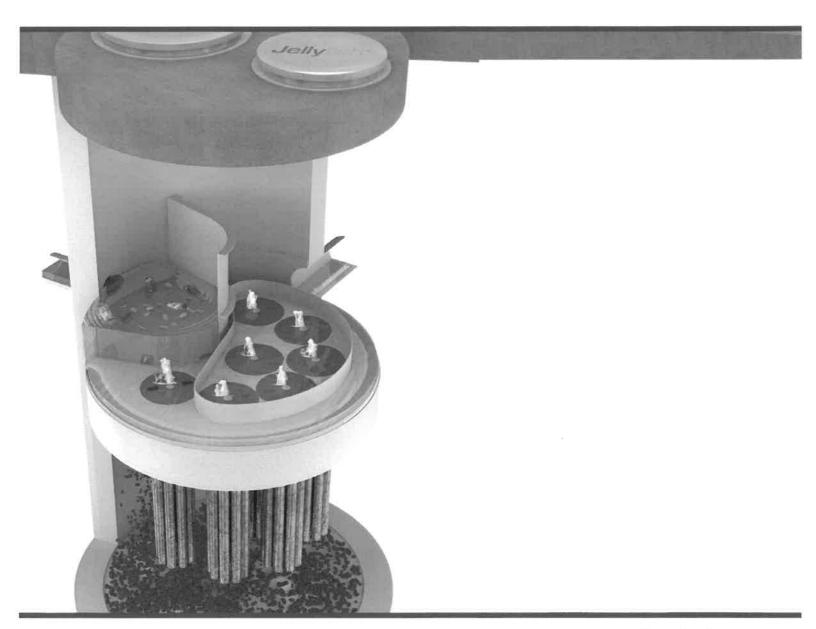
V	Final Site Plan Approval Required Info	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	All local approvals, permits, easements and licenses required, including but not limited to:	Easements shown on C1 & C2	
X	Exhibits, data, reports or studies that may have been required as part of the approval process, including but not limited to: Calculations relating to stormwater runoff; Information on composition and quantity of water demand and wastewater generated; Information on air, water or land pollutants to be discharged, including standards, quantity, treatment and/or controls; Estimates of traffic generation and counts pre- and post-construction; Estimates of noise generation; A Stormwater Management and Erosion Control Plan; Endangered species and archaeological / historical studies; Wetland and water body (coastal and inland) delineations; Environmental impact studies. (2.5.3.2B)	Enclosed	
	A document from each of the required private utility service providers indicating approval of the proposed site plan and indicating an ability to provide all required private utilities to the site. (2.5.3.2D)	Pending	

	Final Site Plan Approval Required Info	mation	
A	Required Items for Submittal	Item Location (e.g. Page/line or Plan Sheet/Note #)	Waiver Requested
X	A list of any required state and federal permit applications required for the project and the status of same. (2.5.3.2E)	C2 Note #5	
X	A note shall be provided on the Site Plan stating: "All conditions on this Plan shall remain in effect in perpetuity pursuant to the requirements of the Site Plan Review Regulations." (2.5.4.2E)	C2 Note #19	N/A
	For site plans that involve land designated as "Special Flood Hazard Areas" (SFHA) by the National Flood Insurance Program (NFIP) confirmation that all necessary permits have been received from those governmental agencies from which approval is required by Federal or State law, including Section 404 of the Federal Water Pollution Control Act Amendments of 1972, 33 U.S.C. 1334. (2.5.4.2F)	N/A	
X	Plan sheets submitted for recording shall include the following notes: a. "This Site Plan shall be recorded in the Rockingham County Registry of Deeds." b. "All improvements shown on this Site Plan shall be constructed and maintained in accordance with the Plan by the property owner and all future property owners. No changes shall be made to this Site Plan without the express approval of the Portsmouth Planning Director." (2.13.3)	C2 Notes #20 & #21	N/A

Applicant's Signature: Phum (5 agot) Date: 3/22/22



Jellyfish® Filter Maintenance Guide





JELLYFISH® FILTER INSPECTION & MAINTENANCE GUIDE

Jellyfish units are often just one of many structures in a more comprehensive stormwater drainage and treatment system.

In order for maintenance of the Jellyfish filter to be successful, it is imperative that all other components be properly maintained. The maintenance and repair of upstream facilities should be carried out prior to Jellyfish maintenance activities.

In addition to considering upstream facilities, it is also important to correct any problems identified in the drainage area. Drainage area concerns may include: erosion problems, heavy oil loading, and discharges of inappropriate materials.

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1.0 Inspection and Maintenance Overview

The primary purpose of the Jellyfish® Filter is to capture and remove pollutants from stormwater runoff. As with any filtration system, these pollutants must be removed to maintain the filter's maximum treatment performance. Regular inspection and maintenance are required to insure proper functioning of the system.

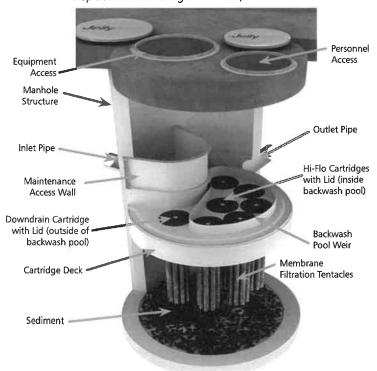
Maintenance frequencies and requirements are site specific and vary depending on pollutant loading. Additional maintenance activities may be required in the event of non-storm event runoff, such as base-flow or seasonal flow, an upstream chemical spill or due to excessive sediment loading from site erosion or extreme runoff events. It is a good practice to inspect the system after major storm events.

Inspection activities are typically conducted from surface observations and include:

- Observe if standing water is present
- Observe if there is any physical damage to the deck or cartridge lids
- Observe the amount of debris in the Maintenance Access Wall (MAW) or inlet bay for vault systems

Maintenance activities include:

- Removal of oil, floatable trash and debris
- Removal of collected sediments
- Rinsing and re-installing the filter cartridges
- Replace filter cartridge tentacles, as needed



Note: Separator Skirt not shown

2.0 Inspection Timing

Inspection of the Jellyfish Filter is key in determining the maintenance requirements for, and to develop a history of, the site's pollutant loading characteristics. In general, inspections should be performed at the times indicated below; or per the approved project stormwater quality documents (if applicable), whichever is more frequent.

- A minimum of quarterly inspections during the first year of operation to assess the sediment and floatable pollutant accumulation, and to ensure proper functioning of the system.
- Inspection frequency in subsequent years is based on the inspection and maintenance plan developed in the first year of operation. Minimum frequency should be once per year.
- 3. Inspection is recommended after each major storm event.
- Inspection is required immediately after an upstream oil, fuel or other chemical spill.

3.0 Inspection Procedure

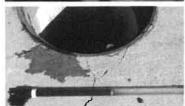
The following procedure is recommended when performing inspections:

- 1. Provide traffic control measures as necessary.
- Inspect the MAW or inlet bay for floatable pollutants such as trash, debris, and oil sheen.
- Measure oil and sediment depth in several locations, by lowering a sediment probe until contact is made with the floor of the structure. Record sediment depth, and presences of any oil layers.
- Inspect cartridge lids. Missing or damaged cartridge lids to be replaced.
- Inspect the MAW (where appropriate), cartridge deck and receptacles, and backwash pool weir, for damaged or broken components.

3.1 Dry weather inspections

- Inspect the cartridge deck for standing water, and/or sediment on the deck.
- No standing water under normal operating conditions.
- Standing water inside the backwash pool, but not outside the backwash pool indicates, that the filter cartridges need to be rinsed.





Inspection Utilizing Sediment Probe

- Standing water outside the backwash pool is not anticipated and may indicate a backwater condition caused by high water elevation in the receiving water body, or possibly a blockage in downstream infrastructure.
- Any appreciable sediment (≥1/16") accumulated on the deck surface should be removed.

3.2 Wet weather inspections

- Observe the rate and movement of water in the unit.
 Note the depth of water above deck elevation within the MAW or inlet bay.
- Less than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges (i.e. cartridges located outside the backwash pool).
- Greater than 6 inches, flow should be exiting the cartridge lids of each of the draindown cartridges and each of the hi-flo cartridges (i.e. cartridges located inside the backwash pool), and water should be overflowing the backwash pool weir.
- 18 inches or greater and relatively little flow is exiting the cartridge lids and outlet pipe, this condition indicates that the filter cartridges need to be rinsed.

4.0 Maintenance Requirements

Required maintenance for the Jellyfish Filter is based upon results of the most recent inspection, historical maintenance records, or the site specific water quality management plan; whichever is more frequent. In general, maintenance requires some combination of the following:

- Sediment removal for depths reaching 12 inches or greater, or within 3 years of the most recent sediment cleaning, whichever occurs sooner.
- 2. Floatable trash, debris, and oil removal.
- 3. Deck cleaned and free from sediment.
- 4. Filter cartridges rinsed and re-installed as required by the most recent inspection results, or within 12 months of the most recent filter rinsing, whichever occurs sooner.
- Replace tentacles if rinsing does not restore adequate hydraulic capacity, remove accumulated sediment, or if damaged or missing. It is recommended that tentacles should remain in service no longer than 5 years before replacement.
- Damaged or missing cartridge deck components must be repaired or replaced as indicated by results of the most recent inspection.
- The unit must be cleaned out and filter cartridges inspected immediately after an upstream oil, fuel, or chemical spill.
 Filter cartridge tentacles should be replaced if damaged or compromised by the spill.

5.0 Maintenance Procedure

The following procedures are recommended when maintaining the Jellyfish Filter:

- 1. Provide traffic control measures as necessary.
- Open all covers and hatches. Use ventilation equipment as required, according to confined space entry procedures.
 Caution: Dropping objects onto the cartridge deck may cause damage.

- 3. Perform Inspection Procedure prior to maintenance activity.
- 4. To access the cartridge deck for filter cartridge service, descend into the structure and step directly onto the deck. Caution: Do not step onto the maintenance access wall (MAW) or backwash pool weir, as damage may result. Note that the cartridge deck may be slippery.
- 5. Maximum weight of maintenance crew and equipment on the cartridge deck not to exceed 450 lbs.

5.1 Filter Cartridge Removal

- 1. Remove a cartridge lid.
- Remove cartridges from the deck using the lifting loops in the cartridge head plate. Rope or a lifting device (available from Contech) should be used. Caution: Should a snag occur, do not force the cartridge upward as damage to the tentacles may result. Wet cartridges typically weigh between 100 and 125 lbs.
- 3. Replace and secure the cartridge lid on the exposed empty receptacle as a safety precaution. Contech does not recommend exposing more than one empty cartridge receptacle at a time.

5.2 Filter Cartridge Rinsing

 Remove all 11 tentacles from the cartridge head plate. Take care not to lose or damage the O-ring seal as well as the plastic threaded nut and connector.



- Position tentacles in a container (or over the MAW), with the threaded connector (open end) facing down, so rinse water is flushed through the membrane and captured in the container.
- 3. Using the Jellyfish rinse tool (available from Contech) or a low-pressure garden hose sprayer, direct water spray onto the tentacle membrane, sweeping from top to bottom along the length of the tentacle. Rinse until all sediment is removed from the membrane. Caution: Do not use a high pressure sprayer or focused stream of water on the membrane. Excessive water pressure may damage the membrane.

- 4. Collected rinse water is typically removed by vacuum hose.
- 5. Reassemble cartridges as detailed later in this document. Reuse O-rings and nuts, ensuring proper placement on each tentacle.

5.3 Sediment and Flotables Extraction

- Perform vacuum cleaning of the Jellyfish Filter only after filter cartridges have been removed from the system. Access the lower chamber for vacuum cleaning only through the maintenance access wall (MAW) opening. Be careful not to damage the flexible plastic separator skirt that is attached to the underside of the deck on manhole systems. Do not lower the vacuum wand through a cartridge receptacle, as damage to the receptacle will result.
- 2. Vacuum floatable trash, debris, and oil, from the MAW opening or inlet bay. Alternatively, floatable solids may be removed by a net or skimmer.



Vacuuming Sump Through MAW

- 3. Pressure wash cartridge deck and receptacles to remove all sediment and debris. Sediment should be rinsed into the sump area. Take care not to flush rinse water into the outlet pipe.
- Remove water from the sump area. Vacuum or pump equipment should only be introduced through the MAW or inlet bay.
- Remove the sediment from the bottom of the unit through the MAW or inlet bay opening.



Vacuuming Sump Through MAW

6. For larger diameter Jellyfish Filter manholes (≥8-ft) and some vaults complete sediment removal may be facilitated by removing a cartridge lid from an empty receptacle and inserting a jetting wand (not a vacuum wand) through the receptacle. Use the sprayer to rinse loosened sediment toward the vacuum hose in the MAW opening, being careful not to damage the receptacle.

5.4 Filter Cartridge Reinstallation and Replacement

- Cartridges should be installed after the deck has been cleaned.
 It is important that the receptacle surfaces be free from grit and debris.
- Remove cartridge lid from deck and carefully lower the filter cartridge into the receptacle until head plate gasket is seated squarely in receptacle. Caution: Do not force the cartridge downward; damage may occur.
- Replace the cartridge lid and check to see that both male threads are properly seated before rotating approximately 1/3 of a full rotation until firmly seated. Use of an approved rim gasket lubricant may facilitate installation. See next page for additional details.
- 4. If rinsing is ineffective in removing sediment from the tentacles, or if tentacles are damaged, provisions must be made to replace the spent or damaged tentacles with new tentacles. Contact Contech to order replacement tentacles.

5.5 Chemical Spills

Caution: If a chemical spill has been captured, do not attempt maintenance. Immediately contact the local hazard response agency and contact Contech.

5.6 Material Disposal

The accumulated sediment found in stormwater treatment and conveyance systems must be handled and disposed of in accordance with regulatory protocols. It is possible for sediments to contain measurable concentrations of heavy metals and organic chemicals (such as pesticides and petroleum products). Areas with the greatest potential for high pollutant loading include industrial areas and heavily traveled roads. Sediments and water must be disposed of in accordance with all applicable waste disposal regulations. When scheduling maintenance, consideration must be made for the disposal of solid and liquid wastes. This typically requires coordination with a local landfill for solid waste disposal. For liquid waste disposal a number of options are available including a municipal vacuum truck decant facility, local waste water treatment plant or on-site treatment and discharge.

Jellyfish Filter Components & Filter Cartridge Assembly and Installation

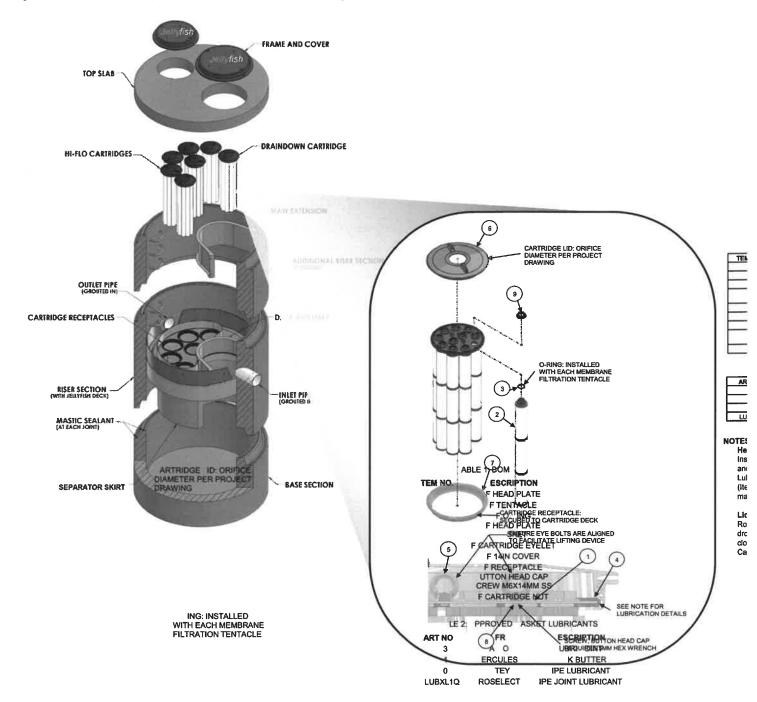


TABLE 1: BOM

17 DEL (, DOM		
ITEM NO.	DESCRIPTION	
1	JF HEAD PLATE	
2	JF TENTACLE	
3	JF O-RING	
4	JF HEAD PLATE GASKET	
5	JF CARTRIDGE EYELET	
6 _{ADTDI}	OCE DIE 14IN COVER	
₫EC! ID!	n TAIF RECERTACHEOU	
	BUTTON HEAD CAP	
8	SCREW M6X14MM SS	
9	JF CARTRIDGE NUT	

TABLE 2: APPROVED GASKET LUBRICANTS

PART NO.	MFR	DESCRIPTION
78713	LA-CO	LUBRI-JOINT
40501	HERCULES	DUCK BUTTER
30600	OATEY	PIPE LUBRICANT
PSLUBXL10	PROSELECT	PIPE JOINT LUBRICANT

NOTES:

Head Plate Gasket Installation:

Install Head Plate Gasket (Item 4) onto the Head Plate (Item 1) and liberally apply a lubricant from Table 2: Approved Gasket Lubricants onto the gasket where it contacts the Receptacle (Item 7) and Cartridge Lide (ITem 6). Follow Lubricant manufacturer's instructions.

Lid Assembly:

Rotate Cartridge Lid counter-clockwise until both male threads drop down and properly seat. Then rotate Cartridge Lid clock-wise approximately one-third of a full rotation until Cartridge Lid is firmly secured, creating a watertight seal.

	Jellyfish	Filter Inspe	ction and M	laintenance Lo	og	
Owner:				Jellyfish Model No:		
Location:				GPS Coordinates:		
Land Use:	Commercial:		Industrial:		Service Station:	
R	oadway/Highway:		Airport:		Residential:	
Date/Time:						
Inspector:						
Maintenance Contractor:						
Visible Oil Present: (Y/N)						
Oil Quantity Removed:						
Floatable Debris Present: (Y/N)						
Floatable Debris Removed: (Y/N)						
Water Depth in Backwash Pool						
Draindown Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Draindown Cartridges: (Y/N)						
Hi-Flo Cartridges externally rinsed and recommissioned: (Y/N)						
New tentacles put on Hi-Flo Cartridges: (Y/N)						
Sediment Depth Measured: (Y/N)						
Sediment Depth (inches or mm):						
Sediment Removed: (Y/N)						
Cartridge Lids intact: (Y/N)						
Observed Damage:						
Comments:						



Jellyfish®

CINTECH ENGINEERED SOLUTIONS

800.338.1122 www.ContechES.com

Support

- Drawings and specifications are available at www.conteches.com/jellyfish.
- Site-specific design support is available from Contech Engineered Solutions.
- Find a Certified Maintenance Provider at www.conteches.com/ccmp

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85 Portsmouth Avenue, PO Box 219, Stratham, NH 03885 603.772.4746 - JonesandBeach.com

May 24, 2022

Portsmouth Planning Board Attn: Board Members 1 Junkins Avenue, Suite 3rd Floor Portsmouth, NH 03801

RE: Conditional Use Application 1169 & 1171 Sagamore Avenue, Portsmouth, NH Tax Map 224, Lots 14 & 15, and Tax Map 201, Lot 26 JBE Project No. 21047

Dear Board Members,

Jones & Beach Engineers, Inc., respectfully submits a Conditional Use Application for the above-referenced properties on behalf of the applicant, The Sagamore Group, LLC. The intent of this project is to remove existing structures on the subject parcels and construct 10 condominium units. Runoff from impervious surfaces will be treated and detained on-site, and some of it infiltrated. Then, it is discharged toward a depression with an isolated wetland in the northeast corner of the subject parcel. Peak rates of runoff toward the depression will be reduced in the proposed condition compared with the existing condition during all analyzed storm events.

After discussions with the Technical Advisory Committee and with the abutters, we have agreed to install a cross-culvert under Sagamore Avenue to connect the wetlands on either side. Although no one could find a culvert in the field an old culvert in the field or on old plans, it was agreed that one should be located here. The culvert also collects and treats roadway drainage with catch basins and a proprietary treatment device called a Jellyfish.

The culvert will drain toward a larger wetland located across the street on City-owned property (Tax Map 201, Lot 26). The intent of the proposed culvert is to reduce peak water elevations within the depression in the proposed condition and to mitigate the potential for flooding during larger storm events, as modelled. The culvert will unavoidably need to be within the buffer of the larger wetland and therefore triggers the need for a Conditional Use Permit. The smaller wetland on Lot 15 is under 10,000 S.F. in area and therefore too small to have a buffer of its own. Proposed temporary buffer impacts are as follows (whereas work within the right of way is exempt from the requirement for a CUP):

- 300 S.F. on Lot 15 (Proposed Condominium Site)
- 270 S.F. on Lot 26 (City Owned Property)
- 570 S.F. Total

Additionally, because a new sidewalk is being proposed as requested by the City, runoff from a $460^{\circ} \pm long$ stretch of the southbound side of Sagamore Avenue which currently drains via sheet flow is proposed to be directed into a closed drainage system. This closed drainage system is proposed to be tied into the proposed cross-culvert. Road runoff will be treated via a "Jellyfish" filtration device before being discharged toward the larger wetland on Lot 26. Runoff from the proposed condominium development will be treated on-site.

10.1017.50 Criteria for Approval of Conditional Use Applications:

- 1. The land is reasonably suited to the use, activity or alteration.

 RESPONSE: As agreed to by the Technical Advisory Committee, the wetland located on Map 201, Lot 26 has much more available flood storage than the depression surrounding the isolated wetland in the corner of the subject parcel on which the condominium units are proposed. The large wetland on this City-owned property is able to handle the runoff better than the isolated depression surrounding the smaller wetland across the street, and it should be noted that peak rates of runoff toward that isolated depression are reduced in the proposed conditions and the intent of the proposed culvert is to act as an overflow. The City-owned land is in conservation and therefore won't be developed and provides excellent stormwater attenuation.
- There is no alternative location outside the wetland buffer that is feasible and reasonable for the proposed use, activity or alteration.
 RESPONSE: It is not possible to build this culvert outside of the wetland buffer.
 The culvert directly provides an overflow from a smaller wetland to drain toward a larger one; therefore, it must be located in the wetland buffer.
- 3. There will be no adverse impact on the wetland functional values of the site or surrounding properties.

 RESPONSE: In the existing condition, the runoff from Sagamore Ave and from the subject parcel reach a wetland untreated. In the proposed condition, all runoff will be treated before reaching the wetland on the City-owned property. Runoff from the proposed condominium development will be treated on-site and runoff from the road will be treated with a proposed Jellyfish filtration device.
- 4. Alteration of the natural vegetative state or managed woodland will occur only to the extent necessary to achieve construction goals.
 RESPONSE: A very minimal amount of vegetation will need to be cleared for the proposed culvert. It will be primarily underneath the roadway and only the inlet and outlet with associated erosion control measures will be in existing vegetated areas. Existing vegetation will only be disturbed on the side slope of the road for the installation of the culvert and of the rip rap. Grass and naturally occurring shrubs may be allowed to grow back over the proposed culvert along the side slope of the road, but trees should not be allowed to grow over it.



5. The proposal is the alternative with the least adverse impact to areas and environments under the jurisdiction of this Section.

RESPONSE: There will be minimal temporary impact for the installation of the culvert. In the existing condition, stormwater enters the wetland untreated. In the proposed condition, the runoff from the condominium development and the roadway will be treated, which mitigates the potential for degradation of water quality downstream. The culvert is to be installed within the wetland buffer, not the wetland itself. Proposed temporary impacts to the wetland buffer are as noted above. There will be no permanent impacts to the wetland buffer.

6. Any area within the vegetated buffer strip will be returned to a natural state to the extent feasible.

RESPONSE: The installation of the culvert results in only temporary disturbance. Grass may be allowed to grow back over the culvert. For maintenance purposes, trees should not be allowed to grow over the culvert, but the remainder of the wooded area within the wetland buffer will remain wooded.

The following information is additionally required for Conditional Use Applications:

- Total area of inland wetland (both on and off subject parcel): 521 S.F. *
- Distance of proposed activity to wetland requiring CUP: 7' (Only the wetland on Lot 26 is large enough to require a CUP)
- Wetland buffer total area on lot: 1,354 S.F. *
- Wetland buffer area to be disturbed: See Above
- Inland wetland total area on lot: 257 S.F.
- Inland wetland area to be disturbed: 0 S.F.

The following items are provided in support of this Application:

If you have any questions or need any additional information, please feel free to contact our office. Thank you very much for your time.

Very truly yours,

JONES & BEACH ENGINEERS, INC.

Joseph A. Coronati

Vice President

^{*} Responses with asterisk refer only to Tax Map 224, Lot 15; Tax Map 201, Lot 26 has not been fully surveyed, only the portion shown on the plans.

KNOW ALL MEN BY THESE PRESENTS

2299-1707

THAT the Mark H. Wentworth Home for Chronic Invalids, a voluntary corporation duly established by law and having a usual place of business in Portsmouth Rockingham County, State of

New Hampshire, for consideration paid, grant to the City of Portsmouth, a municipal corporation

in the County of Rockingham and State of New Hampshire

County-State-of-x

, with WARRANTY COVENANTS,

(Description and incumbrances, if any)

A certain tract of land situate on the Easterly side of Sagamore Avenue and the Southerly side of Wentworth Road, also known as Wentworth House Road in said Portsmouth and more particularly bounded as follows:

Beginning at a point in the Southerly sideline of Wentworth Road at the Northeasterly corner of land of Harold and Katherine Abbott and running Easterly along the Southerly sideline of Wentworth Road 464 feet more or less to land of Herman and Bertraude L. Odiorne; thence turning and running Southerly by said Odiornes, land of Mike Kuchtey and land of Helen F. Mulcahy 605 feet more or less to the Portsmouth-Rye town line; thence turning and running Southwesterly by said Portsmouth-Rye town line 1090 feet more or less to the Westerly sideline of Sagamore Avenue; thence turning and running Northerly by said Sagamore Avenue 1200 feet more or less to an iron pipe in the ground at land of Richard and Kathryn Cooper; thence turning and running Easterly by said land of Cooper 100 feet to an iron pipe in the ground; thence turning and running Northerly by said land of Cooper 100 feet to a drill hole in a ledge; thence continuing Northerly by land of Richard Cooper and others 80 feet to a corner at land of Valley Oil Company; thence turning and running Easterly by land of said Oil Company 49 feet more or less to an iron pipe at land of said Abbotts; thence continuing in an Easterly direction by land of Abbotts 100 feet more or less to an iron pipe; thence turning and running Northerly by said land of said Abbotts 139 feet more or less to Wentworth Road and the point of beginning. Containing by estimation 16.5 acres.

Being the same premises acquired by deed of Charles J. Griffin Executor of the will of Henry Kenney dated October 17, 1939, recorded in Rockingham County Registry of Deeds Book 963 Page 375 less a certain lot conveyed to Richard Cooper and Kathryn E. Cooper by deed dated September 27, 1956, recorded in Rockingham County Registry of Deeds Book 1410 Page 350. instrument

d beautical and other interest there is x orate this 27 day of September , 19 77 WITNESS hand the Mark H. W State of New Humpshire September Rockingham,

Then personally appeared the above named Wyman P. Boynton, President of the Board of Trustees of the Mark H. Wentwork Chronic Invalids, and for this purpose duly authorvoluntary act and d and acknowledged the foregoing in said corporation, before me a

Notary Public -

ized

Mark H. Wentworth Home for Chronic Invalids

Meeting of the Board of Trustees of the Mark H. Wentworth Home for Chronic Invalids held at the Home on December 3, 1976, with a quorum of the Trustees present.

President, Wyman P. Boynton, presided.

On motion it was

VOTED: To sell the Sagamore Avenue property of the Home to the City of Portsmouth for the sum of \$40,000.00, together with the appraisers fee and the abatement of the 1976 taxes; and further that the President be authorized to execute all deeds and other instruments required.

A true extract from the reco

Richard E. Winslow,

Approved

KNOW ALL MEN BY THESE PRESENTS, That Norman J. Smith, of P.O. Box 95, Portsmouth, County of Rockingham and State of New Hampshire,

8 2418 PO173

for consideration paid, grant to Colleen M. Hebert of 1169 Sagamore Avenue, Portsmouth, County of Rockingham and State of New Hampshire,

with warranty covenants

A certain parcel of land, together with the buildings thereon, situate on the Westerly side of Sagamore Avenue, so-called, in Portsmouth in the County of Rockingham and State of New Hampshire, more particularly bounded and described as follows:

Beginning in the Westerly sideline of the Avenue at land now or formerly of Haven L. Joy; thence running Westerly by other land of Joy, Two Hundred Ninety-three and Five Tenths (293.5) feet to land now or formerly of Ralph W. Junkins Est. et als; thence turning and running Norterly by other land of Junkins et als One Hundred Twenty-six and Thirty-two Hundredths (126.32) feet to a point at other land now or formerly of John J. and Harriet Scammon; thence turning and running Easterly by other land of Scammon Three Hundred (300) feet, more or less, to the Westerly sideline of the Avenue, thence running Southerly by the sideline Forty-seven and Sixty-five Hundredths (47.65) feet to a point, thence running Southeasterly by the sideline Fortynine and Eight Hundredths (49.08) feet to land of Joy which is the point of beginning.

Being the same premises conveyed to Norman J. Smith and Janet S. Smith by deed of John J. Scammon et ai dated July 24, 1954 and recorded in the Rockingham County Registry of Deeds in Book 1323 Page 324.



Norman J. Smith, being single . husband MORROWN MORK WHINGONS IN IT IN THE and granter all rights of contest done cand home stead and other interests therein

my. Witness, hand XXXXXXX thr. 29th Jy 82.

Julito a. Gile

LS

State of Nem Hampshire

88.7

Rockingham

duly 29 VD II

Personally appeared Norman J. Smit.

known to me, or satisfuctionly process to be the person

or here ment

subscribed to the foregoing instrument and acknowledged that

secuted the same

for the purposes their mecontained

Returne Jedets a. Siles





WARRANTY DEED

KNOW ALL PERSONS BY THESE PRESENTS THAT I, ROBERT F.

SCAMMON, JR., single and not a party to a civil union, of 1169 Sagamore Avenue, Portsmouth, New Hampshire, 03801

For consideration paid, grant to **JOHN J. HEBERT AND COLLEEN HEBERT**, husband and wife, of 54 Pioneer Road, Rye, New Hampshire, 03870, as joint tenants with rights of survivorship,

With Warranty Covenants, the following described premises situate in Portsmouth, Rockingham County, New Hampshire:

A certain lot or parcel of land with the buildings thereon situate on Sagamore Avenue, City of Portsmouth, County Rockingham and State of New Hampshire, bounded and described as follows:

Beginning at the concrete bound at the Northeasterly corner of the within described lot, the said bound being Four Hundred Seventy-nine (479) feet southerly along said Sagamore Avenue from the southeasterly corner of land now or formerly of Charles F. Moody; thence running Southerly twenty-four (24) degrees thirty-four (34) minutes west along said Sagamore Avenue one hundred (100) feet to a stake in the stone wall at other land now or formerly of Allen B. Keen; thence turning and running N 83° 43' W by other land of said Keen 300 feet to a stake; thence turning and running N 24° 30' E 100 feet by land now or formerly of Frank E. Brooks, etals; thence turning and running S 83° 43' E by land of said Brooks and other 300 feet to Sagamore Avenue and being the point of beginning.

Also a parcel of land situated on Sagamore Avenue in said Portsmouth adjoining and lying on the northerly side of the above described parcel and bounded and described as follows: Beginning at a concrete bound at the southeasterly corner of these premises at land described above, said bound being 479 feet southerly along said Sagamore Avenue from the southeasterly corner of land now or formerly of Charles F. Moody; thence running N 83° 43' W by the above described parcel 300 feet to a point of land now or formerly of Frank E Brooks et als; thence turning and running N 24° 30' E by other land of said Brooks and others 300 feet, more or less to

said Sagamore Avenue; thence turning and running southerly along said Sagamore Avenue 50 feet to said concrete bound and being the point of beginning.

Also a parcel of land situated on Sagamore Avenue in said Portsmouth and bounded and described as follows: Beginning at the northeasterly corner of the herein described parcel at the intersection of the westerly sideline of said Sagamore Avenue and land now or formerly of Allen B. Keen, said point being 100 feet S 24° 34' W along said Sagamore Avenue from the concrete bound aforementioned; thence running southerly along said Avenue 25 feet to land now or formerly of Frank E. Brooks, et als; thence turning and running N 83° 43' W by land now or formerly Frank E. Brooks, et als 300 feet, more or less, to a point; thence turning and running N 24° 30' E 25 feet by land of said Brooks, et als, to a stake at other land now or formerly of Allen B. Keen; thence turning and running Southeast 83° 43' E by other land of said Keen 300 feet to Sagamore Avenue and being the point of beginning. This parcel adjoining and lying on the southerly side of the first described parcel herein.

Being the same premises conveyed to the within Grantor by deed of Barbara Scammon dated April 25, 1995, recorded in Rockingham County Registry of Deeds, Book 3097, Page 1715.

Signed this 30th day of November, 2012.

Robert F. Scammon, Jr.

STATE OF NEW HAMPSHIRE ROCKINGHAM COUNTY

Personally appea	ared this 30th day of November	, 2012,	Robert F.
Scammon, Jr.	, who acknowledged tha	at he/she/they exe	cuted the
foregoing instrument as	his/her/their free act and deed for the	e purposes contain	ned herein.

Before me.

Lori Hebert, Notary Public

My commission expires: 05/09/2017

Letter of Authorization

The Sagamore Group, LLC, 4 Merrill Industrial Drive, Hampton, NH, 03842, USA, developer of property located in Portsmouth, NH, known as Tax Map 224, Lots 14 & 15, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on our behalf concerning the subject properties. The parcels are located at 1169 & 1171 Sagamore Avenue in Portsmouth, NH.

We hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

The Sagamore Group, LLC

Daniel Jackson, Member

Duly authorized

 $\frac{5/4/21}{\text{Date}}$

dotloop signature verification:

Letter of Authorization

We, John & Colleen Hebert, 54 Pioneer Road, Rye, NH 03870, owners of property located in Portsmouth, NH, known as Tax Map 224, Lot 15, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on my behalf concerning the previously-mentioned property. The parcel is located on 1169 Sagamore Avenue in Portsmouth, NH.

We hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

	Inla J Habout	05/04/21 2:47 PM EDT 5510-MUAR-1SWP-P2NG	
Witness	John Hebert	Date	
	College Hobert	dolloop verified 05/04/21 2:49 PM EDT ()BG-7/M M-LUFK-BAFX	
Witness	Colleen Hebe		Date

Letter of Authorization

I, Colleen Hebert, 54 Pioneer Road, Rye, NH 03870, owner of property located in Portsmouth, NH, known as Tax Map 224, Lot 14, do hereby authorize Jones & Beach Engineers, Inc., PO Box 219, Stratham, NH, to act on my behalf concerning the previously-mentioned property. The parcel is located on 1171 Sagamore Avenue in Portsmouth, NH.

I hereby appoint Jones & Beach Engineers, Inc., as my agent to act on my behalf in the review process, to include any required signatures.

	dolloop verified OS/O4/21 2:49 PM EDT RISS-STAZ-YMFI-YURD			
Witness	Colleen He	1	Date	

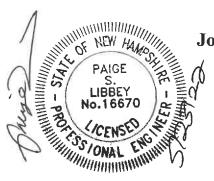
DRAINAGE ANALYSIS

SEDIMENT AND EROSION CONTROL PLAN

Sagamore Avenue Condominiums 1169 & 1171 Sagamore Ave. Portsmouth, NH 03801 Tax Map 224, Lots 14 & 15

Prepared for:

The Sagamore Group, LLC P.O. Box 430 Hampton, NH 03842



Jones & Beach Engineers, Inc.
85 Portsmouth Avenue
P.O. Box 219
Stratham, NH 03885
(603) 772-4746
August 23, 2021
Revised October 5, 2021
Revised December 28, 2021
Revised February 9, 2022
Revised March 22, 2022
Revised April 18, 2022
Revised May 10, 2022
JBE Project No. 21047

EXECUTIVE SUMMARY

The Sagamore Group, LLC proposes to construct ten (10) residential condominium units on a 1.83-acre parcel of land located at 1169 & 1171 Sagamore Avenue in Portsmouth, NH. In the existing condition, the two lots to be consolidated are home to single-family residences with multiple sheds and paved driveways, a pool, and a gravel driveway running through the lots.

A drainage analysis of the entire site was conducted for the purpose of estimating the peak rate of stormwater runoff and to subsequently design adequate drainage structures. Two models were compiled, one for the area in its existing (pre-construction) condition, and a second for its proposed (post-construction) condition. The analysis was conducted using data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events using the USDA SCS TR-20 method within the HydroCAD Stormwater Modeling System environment. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region. A summary of the existing and proposed conditions peak rates of runoff in units of cubic feet per second (cfs) is as follows:

Analysis Point	2 Year		10 Year		25 Year		50 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.60	0.31	1.40	0.87	2.11	1.40	2.80	1.92
Analysis Point #2	0.86	0.72	1.53	1.25	2.06	1.68	2.56	2.07
Analysis Point #3	1.20	0.22	2.24	0.53	3.14	0.80	3.98	1.07
Analysis Point #4	0.24	0.21	0.50	0.40	0.73	0.56	0.94	0.70
Analysis Point #5	N/A	0.69	N/A	1.05	N/A	1.50	N/A	2.40

A similar summary of the existing and proposed peak volumes in units of acre-feet is as follows:

Analysis Point	2 Year		10 Year		25 Year		50 Year	
	Pre	Post	Pre	Post	Pre	Post	Pre	Post
Analysis Point #1	0.063	0.036	0.140	0.089	0.208	0.139	0.275	0.189
Analysis Point #2	0.072	0.067	0.127	0.117	0.172	0.158	0.215	0.196
Analysis Point #3	0.086	0.017	0.228	0.039	0.402	0.058	0.573	0.077
Analysis Point #4	0.022	0.019	0.045	0.037	0.064	0.051	0.083	0.065
Analysis Point #5	N/A	0.082	N/A	0.206	N/A	0.343	N/A	0.478

The subject parcels are located in the Mixed Residential / Office (MRO) Zoning District. The subject parcels currently consist of the aforementioned single-family residences with associated driveways, sheds, and a pool, all of which is proposed to be demolished. The topography and ledge outcrops on the site as well as a stretch of Sagamore Ave. that is considered in this analysis define six (6) subcatchments, which drain to four (4) analysis points. Subcatchments 2S-4S drain directly toward their respective analysis points while subcatchment 6S drains directly toward Analysis Point #1, subcatchment 1S drains directly toward an isolated wetland which overflows toward both Analysis Points 1&3, and subcatchment 5S drains toward a shallow depression straddling the two properties, modelled as a pond, before cresting over a "berm" and running off toward the northerly abutter's detention pond (Analysis Point 3). The neighboring "Westwind Townhomes of Portsmouth" site to the south stands topographically prominent to this parcel, so some runoff from this development reaches

the southeast corner of the subject parcel although most of it drains directly into the Sagamore Avenue right of way. The runoff reaching this corner of the property (Analysis Point 2) then continues south along Sagamore Avenue. The majority of the site drains to the north in the existing condition, reaching either the abutting "Sea Star Cove Condominium" detention pond (Analysis Point 3) or the adjacent depression (Analysis Point 1) after overflowing from the isolated wetland in the rear of the site. Also included in Subcatchment 1S, which drains toward Analysis Point 1, is a stretch of Sagamore Ave with a low point at a horseshoe shaped driveway for an abutter to the subject property. Runoff from this stretch of the road sheet flows across the abutter's property in the proposed condition before ultimately reaching either the isolated wetland or a wooded depression defined as Analysis Point 1.

The proposed site development consists of the aforementioned ten (10) condominium units with associated paved roadway and individual driveways. The addition of the proposed impervious paved areas and buildings causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c), the net result being a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to mitigate this possibility. The proposed site development divides the site into nineteen (19) subcatchments, representing both the periphery of the site that will continue its existing flow pattern toward the aforementioned analysis points as well as the developed portions that will be routed into the site's stormwater management system for treatment and reduction of peak flows. The proposed stormwater management system for the front of the site consists of two (2) bioretention systems to filter runoff and a downstream concrete galley field that will detain runoff and release it slowly, allowing for peak flow rates to be reduced. The proposed stormwater management system for the rear of the site consists of two catch basins as well as several yard drains draining into a concrete galley field designed for infiltration, from which overflow will be routed to the concrete galley field in the center of the site that is designed for detention. Through the use of these practices, the peak rate and volume of runoff is reduced toward Analysis Points #1-4 during all analyzed storm events.

Otherwise, some roof runoff will be infiltrated through subsurface stone beds. These systems, in combination with the concrete galley field designed for infiltration, will help to reduce volumes of runoff below the existing condition and promote groundwater recharge.

Additionally, although the system has been designed to reduce the amount of flooding on to abutting properties in the proposed condition, a cross-street culvert is proposed as an overflow from the depression surrounding the isolated wetland. As modelled, this culvert protects against flooding on to adjacent properties during all analyzed storm events. This culvert outlets across the street into a larger wetland area, so new Analysis Point 5 is introduced in the proposed condition for the runoff that is captured by this culvert.

The use of Best Management Practices per the NHDES <u>Stormwater Manual</u> have been applied to the design of this drainage system and will be observed during all stages of construction. All land disturbed during construction will be stabilized within thirty days of groundbreaking and abutting property owners will suffer minimal adversity resultant of this development.

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1.0 RAINFALL CHARACTERISTICS

This drainage report includes an existing conditions analysis of the area involved in the proposed development, as well as a proposed condition, or post-construction analysis, of the same location. These analyses were accomplished using the USDA SCS TR-20 Method within the HydroCAD Stormwater Modeling System. The curve numbers were developed using the SCS TR-55 Runoff Curve numbers for Urban Areas. A Type III SCS 24-hour rainfall distribution was utilized in analyzing the data for the 2 Year – 24 Hour (3.70"), 10 Year – 24 Hour (5.61"), 25 Year – 24 Hour (7.12"), and 50 Year – 24 Hour (8.53") storm events. This data was taken from the Extreme Precipitation Tables developed by the Northeast Regional Climate Center (NRCC), and the values have been increased by 15% due to the project being within the Coastal/Great Bay Region.

The peak rates of runoff will be reduced from the existing condition, thereby minimizing any potential for a negative impact on abutting properties or erosion of the wetland system. This is accomplished through treatment of stormwater runoff and attenuation of peak flows and volumes resulting from storm events.

2.0 EXISTING CONDITIONS ANALYSIS

The two existing single-family residential properties feature three houses, two sheds, a pool, two paved driveways and a gravel driveway running through the site in addition to a paved island in the center of the site. The site is otherwise covered by both woods and grass, with sporadic ledge outcrops. A small section of the southern part of the site is sloped toward the south, while the majority of it is sloped toward the north.

The area draining toward the north is split into three subcatchments; Subcatchments 1S, 3S, and 5S. Subcatchment 1S drains into an isolated wetland near the northeast corner of the site. Subcatchment 1S includes the entire on and off-site contributing watershed area toward the isolated wetland, which includes parts of abutting properties as well as a stretch of Sagamore Avenue. Subcatchment 3S drains into Analysis Point #3 (AP3) representing the abutting condominium property's private detention pond. Subcatchment 5S drains toward a shallow depression straddling the two existing subject parcels, represented as 1P, and once the depression fills it crests over a berm and drains across Subcatchment 3S toward Analysis Point #3.

Two additional subcatchments were defined for the area draining toward the south; Subcatchment 2S and Subcatchment 4S. Subcatchment 2S is directed toward Analysis Point #2 (AP2), representing the shoulder of Sagamore Avenue. Runoff in this direction combines with runoff from the edge of the abutting property and continues south. Subcatchment 4S, which is separated from 3S by a ledge outcrop, a building roof, and otherwise a subtle inflection in the surface topography, is located in the southwestern corner of the property and this small area drains directly into the Sea Star Cove Condiminium property, represented by Analysis Point #4 (AP4).

There are two berms on the isolated wetland in the northeast corner of the subject site. A lower berm carries overflow toward the abutter's detention pond and a higher, 70' long x 10' wide berm carries any extreme overflow toward a depression in the woods represented as Analysis Point AP1. Additionally, a stretch of the road and areas of abutting properties drain directly toward Analysis Point AP1 and are represented as Subcatchment 6S.

Existing soil types were determined through a High Intensity Soil Survey (HISS) conducted by a Certified Soil Scientist. A Site-Specific Soil Map (SSSM) conversion table was provided along with the report that was generated based on the results of the HISS. These soils are categorized into Hydrologic Soil Groups (HSG) B and D. Areas surrounding ledge outcrops are categorized into HSG D while the remainder of the upland area of the site is mostly categorized into HSG B. Specifically, the upland soil types include the Hollis-Rock Outcrop Complex, Made Land – Similar to Canton, Newfields, and Chatfield Variant. According to "Ksat Values for New Hampshire Soils" sponsored by the Society of Soil Scientists of Northern New England SSSNNE Special Publication No. 5, the saturated hydraulic conductivity (Ksat) value for Canton soils ranges from 2 to 6 inches/hour within the B horizon and 6 to 20 inches/hour within the C horizon; the Ksat value for Newfields soils ranges from 0.6 to 2 inches per hour within both the B and C horizons, and the Ksat value for both Chatfield Variant and Hollis soils ranges from 0.6 to 6 inches/hour within both the B and C horizons.

3.0 PROPOSED CONDITIONS ANALYSIS

The addition of the proposed impervious paved areas and buildings causes an increase in the curve number (C_n) and a decrease in the time of concentration (T_c), the result being a potential increase in peak rates of runoff from the site. A stormwater management system was designed in order to mitigate this possibility. The proposed development, consisting of the aforementioned ten (10) condominium units with associated paved roadway and driveways as well as stormwater management features divide the subject parcel into nineteen (19) subcatchments. Subcatchments 2S-4S drain directly into their respective Analysis Points, AP2-AP4, as previously outlined. Subcatchments 5S-6S will drain into the two bioretention systems in the front of the site, and after receiving treatment in the bioretention systems, runoff will be piped into concrete "Galley" chambers for underground detention. Subcatchments 7S-8S represent the rear of the site and runoff from here is graded toward two catch basins in sequence from which a closed drainage network feeds into another Galley chamber system, except that this one is designed for infiltration. Overflow from this will be piped into the Galley chamber system in the center of the site that is designed for detention only. Subcatchments 9S-12S represent lawn areas that are proposed to drain toward yard drains. Subcatchments 13S-15S represent roof subcatchments from which runoff will be infiltrated through subsurface stone infiltration beds in lawn areas. Subcatchments 16S, 17S, and 18S represent three stretches of Sagamore Avenue that are to drain toward proposed deep sump catch basins, the purpose of which is to pre-treat roadway runoff and drain it to the wetland across the street. The three proposed catch basins drain toward a proposed "Jellyfish" filtration system for treatment. Finally, Subcatchment 19S represents the sections of adjacent properties draining directly toward the wooded depression to the north of the site represented as AP1. As explained in the executive summary, the proposed stormwater management features help to reduce off-site peak rates and volumes toward AP1-AP4 below the existing condition.

As stated in the executive summary, a new cross street culvert is proposed to be installed as an overflow to prevent runoff from cresting on to adjacent properties after filling the depression surrounding the isolated wetland. Because this culvert carries water across the road, a new analysis point is introduced, represented as Analysis Point 5 to delineate the runoff that enters the larger wetland across the street. The three proposed catch basins along Sagamore Ave feed into a "Jellyfish" filtration system which intercepts the cross-street culvert and treats runoff directed toward it, and therefore the roadway runoff that enters the proposed catch basin also directly reaches Analysis Point AP5 after being treated.

As modelled, this proposed culvert reduces the peak elevation within the depression surrounding the isolated wetland and reduces the potential for flooding during peak storm events. A summary of the peak elevations during each analyzed storm event are as follows, noting that the flood elevation is situated at 31.3:

	2 Year	10 Year	25 Year	50 Year
Existing	30.48	31.32 (Flooding)	31.36 (Flooding)	31.44 (Flooding)
Proposed	30.42	30.65	30.96	31.18

After passing through the bioretention systems and concrete "Galley" chambers, treated and attenuated runoff will gradually drain toward the isolated wetland in the northeast corner of the site, from which any overflow will drain across the street via the proposed culvert during all analyzed storm events. The peak rates and volumes of runoff will be reduced in all analyzed storm events toward Analysis Points 1-4 in the proposed condition compared to the existing condition.

The site will be graded such that runoff from all impervious areas, with the exception of clean roof, patio, and deck runoff, will be treated, detained, and some of it infiltrated to groundwater, by way of bioretention systems and subsurface infiltration and detention chambers. The two bioretention systems in the front of the site cannot be used for infiltration due to the presence of ledge in the area where they are proposed, therefore they shall be lined and underdrained. The proposed concrete Galley chambers in the center of the site will also lined and underdrained due to the presence of groundwater while the proposed concrete Galley chambers in the northwest corner of the site are designed as a subsurface infiltration basin, with at least 3' between the bottom of the chamber and the SHWT.

The Ksat values stated at the end of the Existing Conditions Analysis were used to determine the design infiltration rates of each stormwater practice. The lower Ksat for each soil type was divided by 2 to develop a design infiltration rate of 0.3 or 1 inches/hour for each stormwater practice depending on what soil type they are located in. When a practice is located within multiple soil types, a weighted average is taken. For example, the underground stone infiltration bed in back of Units 1 and 2 straddles two soil types, one with each aforementioned design infiltration rate, so the two rates were averaged and a design infiltration rate of 0.65 inches/hour was ultimately used.

By reducing the peak rate and volume of stormwater runoff toward the neighbor's detention pond, the functioning of the overall drainage system between the two properties is improved resultant to this development. The outfall is in an optimal location as the treated and attenuated runoff will be released toward an existing wetland, a rip rap outlet protection apron is proposed in order to dissipate any concentrated flows that result, and a proposed cross-street culvert will work to reduce the potential for flooding on adjacent properties. The contours surrounding the isolated wetland in the northeastern corner of the site are modelled as a pond, 21P, in the proposed condition, where it is modelled as 2P in the existing condition.

According to the NH Stormwater Manual, bioretention systems provide a pollutant removal efficiency of 90% for TSS and 65% for nitrogen, and infiltration basins (including subsurface ones) provide a removal efficiency of 90% for TSS and 60% for nitrogen provided that there is 3' of soil or stone separating the bottom of the chamber from the seasonal high water table and that the chamber is at least 75' from surface water. Runoff from all impervious surfaces with the exception of roofs is being directed toward one of these two types of treatment systems. The City of Portsmouth Site Plan Review Regulations stipulate that stormwater BMPs should either be designed for 80% TSS removal and 50%

nitrogen removal, OR to retain and treat the Water Quality Volume. This plan exceeds the requirements for pollutant removal because appropriate treatment / groundwater recharge systems are used and the Water Quality Volume is retained and treated.

5.0 CONCLUSION

This proposed site development will have minimal adverse effect on abutting infrastructures, properties, and wetlands by way of stormwater runoff or siltation. Appropriate steps will be taken to eliminate erosion and sedimentation; these will be accomplished through the construction of a drainage system consisting of site grading, catch basins, drain manholes, yard drains, bioretention systems, concrete "Galley" chambers, subsurface stone infiltration beds, rip rap outlet protection, a "Jellyfish" filtration system for road runoff, and a proposed cross-street culvert as well as temporary erosion control measures including but not limited to silt fence and the use of a stabilized construction entrance. The drainage outfall is in its optimal location and the rate and the volume of runoff reaching the abutter's detention pond from the subject site will be reduced. Best Management Practices developed by the State of New Hampshire have been utilized in the design of this system and their application will be enforced throughout the construction process. Peak rates and volumes of runoff from the site will be reduced toward all analysis points during all analyzed storm events.

This project disturbs less than 100,000 S.F. and does <u>not</u> require a NHDES Alteration of Terrain Permit.

Respectfully Submitted,

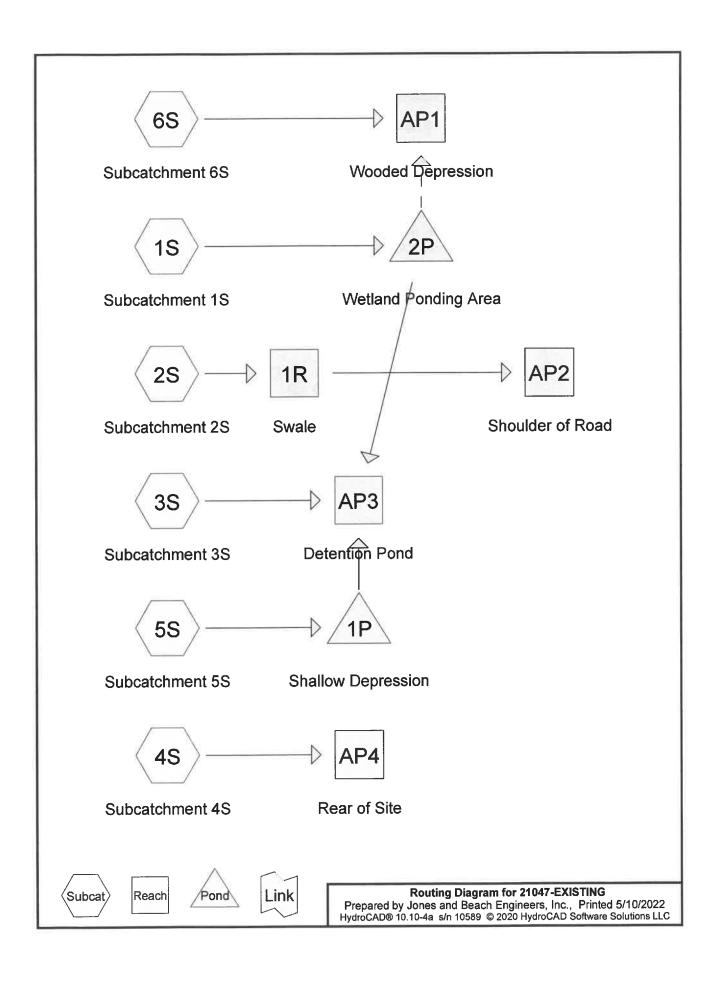
JONES & BEACH ENGINEERS, INC.

Daniel Meditz, E.I.T Project Engineer

APPENDIX I

EXISTING CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.644	61	>75% Grass cover, Good, HSG B (1S, 3S, 4S, 5S, 6S)
0.448	80	>75% Grass cover, Good, HSG D (1S, 2S, 3S, 4S, 5S)
0.135	96	Gravel surface, HSG B (1S, 5S)
0.107	96	Gravel surface, HSG D (1S, 2S, 3S, 4S, 5S)
0.156	98	Ledge Outcrop, HSG D (1S, 2S, 3S, 4S, 5S)
0.228	98	Paved parking, HSG B (5S, 6S)
0.047	98	Paved roads w/curbs & sewers, HSG B (1S)
0.040	98	Paved roads w/curbs & sewers, HSG D (1S, 2S)
0.064	98	Roofs, HSG B (1S, 4S, 5S, 6S)
0.103	98	Roofs, HSG D (1S, 2S, 4S, 5S)
0.861	55	Woods, Good, HSG B (1S, 3S, 4S, 5S, 6S)
0.088	77	Woods, Good, HSG D (1S, 3S, 4S, 5S)
2.921	74	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
0.000	HSG A	
1.980	HSG B	1S, 3S, 4S, 5S, 6S
0.000	HSG C	
0.941	HSG D	1S, 2S, 3S, 4S, 5S
0.000	Other	
2.921		TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S

Runoff Area=34,729 sf 15.46% Impervious Runoff Depth>1.25"
Flow Length=112' Tc=20.1 min CN=72 Runoff=0.75 cfs 0.083 af

Subcatchment2S: Subcatchment2S Runoff Area=16,495 sf 25.67% Impervious Runoff Depth>2.27"

Flow Length=45' Slope=0.0400 '/' Tc=6.0 min CN=86 Runoff=0.99 cfs 0.072 af

Subcatchment3S: Subcatchment3S

Runoff Area=16,448 sf 0.17% Impervious Runoff Depth>0.61"

Flow Length=180' Tc=24.1 min CN=60 Runoff=0.13 cfs 0.019 af

Subcatchment4S: Subcatchment4S

Runoff Area=7,905 sf 42.56% Impervious Runoff Depth>1.44"

Flow Length=68' Slope=0.0290 '/' Tc=12.6 min CN=75 Runoff=0.24 cfs 0.022 af

Subcatchment5S: Subcatchment5S

Runoff Area=22,358 sf 25.08% Impervious Runoff Depth>1.87"
Flow Length=87' Tc=7.2 min CN=81 Runoff=1.07 cfs 0.080 af

Subcatchment6S: Subcatchment6S

Runoff Area=29,310 sf 31.34% Impervious Runoff Depth>1.13"
Flow Length=137' Tc=16.7 min CN=70 Runoff=0.60 cfs 0.063 af

Reach 1R: Swale

Avg. Flow Depth=0.43' Max Vel=0.52 fps Inflow=0.99 cfs 0.072 af n=0.150 L=140.0' S=0.0214'/' Capacity=8.19 cfs Outflow=0.86 cfs 0.072 af

Reach AP1: Wooded Depression Inflow=0.60 cfs 0.063 af Outflow=0.60 cfs 0.063 af

Reach AP2: Shoulder of Road Inflow=0.86 cfs 0.072 af Outflow=0.86 cfs 0.072 af

Reach AP3: Detention Pond Inflow=1.20 cfs 0.086 af Outflow=1.20 cfs 0.086 af

Reach AP4: Rear of Site

Inflow=0.24 cfs 0.022 af
Outflow=0.24 cfs 0.022 af

Pond 1P: Shallow Depression Peak Elev=37.14' Storage=590 cf Inflow=1.07 cfs 0.080 af

Outflow=1.16 cfs 0.067 af

Pond 2P: Wetland Ponding Area Peak Elev=30.48' Storage=3,609 cf Inflow=0.75 cfs 0.083 af Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Outflow=0.00 cfs 0.000 af

Total Runoff Area = 2.921 ac Runoff Volume = 0.339 af Average Runoff Depth = 1.39"
78.16% Pervious = 2.283 ac 21.84% Impervious = 0.638 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S Runoff Area=34,729 sf 15.46% Impervious Runoff Depth>2.67" Flow Length=112' Tc=20.1 min CN=72 Runoff=1.67 cfs 0.177 af

Subcatchment2S: Subcatchment2S Runoff Area=16,495 sf 25.67% Impervious Runoff Depth>4.04" Flow Length=45' Slope=0.0400 '/' Tc=6.0 min CN=86 Runoff=1.72 cfs 0.127 af

Subcatchment3S: Subcatchment3S

Runoff Area=16,448 sf 0.17% Impervious Runoff Depth>1.66"
Flow Length=180' Tc=24.1 min CN=60 Runoff=0.43 cfs 0.052 af

Subcatchment4S: Subcatchment4S Runoff Area=7,905 sf 42.56% Impervious Runoff Depth>2.95" Flow Length=68' Slope=0.0290 '/' Tc=12.6 min CN=75 Runoff=0.50 cfs 0.045 af

Subcatchment5S: Subcatchment5S

Runoff Area=22,358 sf 25.08% Impervious Runoff Depth>3.53"
Flow Length=87' Tc=7.2 min CN=81 Runoff=2.00 cfs 0.151 af

Subcatchment6S: Subcatchment6S

Runoff Area=29,310 sf 31.34% Impervious Runoff Depth>2.49"
Flow Length=137' Tc=16.7 min CN=70 Runoff=1.40 cfs 0.140 af

Reach 1R: Swale

Avg. Flow Depth=0.53' Max Vel=0.60 fps Inflow=1.72 cfs 0.127 af n=0.150 L=140.0' S=0.0214 '/' Capacity=8.19 cfs Outflow=1.53 cfs 0.127 af

Reach AP1: Wooded Depression Inflow=1.40 cfs 0.140 af Outflow=1.40 cfs 0.140 af

Reach AP2: Shoulder of Road Inflow=1.53 cfs 0.127 af
Outflow=1.53 cfs 0.127 af

Reach AP3: Detention Pond Inflow=2.24 cfs 0.228 af Outflow=2.24 cfs 0.228 af Outflow=2.24 cfs 0.228 af

Reach AP4: Rear of Site

Inflow=0.50 cfs 0.045 af
Outflow=0.50 cfs 0.045 af

Pond 1P: Shallow Depression Peak Elev=37.17' Storage=590 cf Inflow=2.00 cfs 0.151 af

Outflow=2.06 cfs 0.138 af

Pond 2P: Wetland Ponding Area Peak Elev=31.32' Storage=6,101 cf Inflow=1.67 cfs 0.177 af Primary=0.10 cfs 0.038 af Secondary=0.00 cfs 0.000 af Outflow=0.10 cfs 0.038 af

Total Runoff Area = 2.921 ac Runoff Volume = 0.692 af Average Runoff Depth = 2.84" 78.16% Pervious = 2.283 ac 21.84% Impervious = 0.638 ac Prepared by Jones and Beach Engineers, Inc.

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 1.67 cfs @ 12.29 hrs, Volume= 0.177 af, Depth> 2.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

A	Area (sf)	CN	Description						
	4,202	55	Woods, Go	Voods, Good, HSG B					
	191	61	>75% Gras	75% Grass cover, Good, HSG B					
	9,900	61	>75% Gras	s cover, Go	ood, HSG B				
	4,049	96	Gravel surfa	ace, HSG E	3				
	2,054	98	Paved road	s w/curbs &	& sewers, HSG B				
	5,450	55	Woods, Go	od, HSG B					
	745	98	Roofs, HSC	BB					
*	1,274	98	Ledge Outo	rop, HSG [
	1,901		Woods, Go						
	666		Gravel surfa						
	3,000	80	>75% Gras	s cover, Go	ood, HSG D				
	534				& sewers, HSG D				
-	763	98	Roofs, HSC	D D					
	34,729	72	Weighted A	verage					
	29,359		84.54% Pe	vious Area	l				
	5,370		15.46% Imp	pervious Ar	ea				
Tc	Length	Slope		Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
20.0	100	0.0200	0.08		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 3.70"				
0.1	12	0.3300	2.87		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
20.1	112	Total							

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 1.72 cfs @ 12.09 hrs, Volume= 0.127 af, Depth> 4.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Area (sf)	CN	Description
*	401	Ledge Outcrop, HSG D	
	1,855	96	Gravel surface, HSG D
	7,620	80	>75% Grass cover, Good, HSG D
	1,200	98	Paved roads w/curbs & sewers, HSG D
	908	98	Roofs, HSG D
	2,786	80	>75% Grass cover, Good, HSG D
	1,725	98	Roofs, HSG D
	16,495	86	Weighted Average
	12,261		74.33% Pervious Area
	4,234		25.67% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
3.6	45	0.0400	0.21		Sheet Flow, Grass: Short	n= 0.150	P2= 3.70"	

3.6 45 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 0.43 cfs @ 12.37 hrs, Volume=

0.052 af, Depth> 1.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Δ	rea (sf)	CN I	Description		
*		28)		
		660		Ledge Outo Gravel surfa		
		1,114		Woods, Go		•
		291		,	,	ood, HSG D
		4,820				ood, HSG B
		9,535		Woods, Go		
		16,448		Weighted A		
		16,420		99.83% Pei		
		28	(0.17% lmpe	ervious Area	a
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)		(cfs)	
	1.5	11	0.0230	0.12		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	5.4	18	0.0167	0.06		Sheet Flow,
		40	0.0400	0.40		Woods: Light underbrush n= 0.400 P2= 3.70"
	3.2	19	0.0100	0.10		Sheet Flow, Grass: Short n= 0.150 P2= 3.70"
	4.0	22	0.0540	0.09		Sheet Flow,
	4.0	22	0.0540	0.03		Woods: Light underbrush n= 0.400 P2= 3.70"
	8.0	30	0.0180	0.06		Sheet Flow,
	0.0	00	0.0100	0.00		Woods: Light underbrush n= 0.400 P2= 3.70"
	2.0	80	0.0180	0.67		Shallow Concentrated Flow,
			3.0.00			Woodland Kv= 5.0 fps
	24.1	180	Total			

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 0.50 cfs @ 12.18 hrs, Volume= 0.04

0.045 af, Depth> 2.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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	Area (sf)	CN	Description					
*	2,545	98	Ledge Outcrop, HSG D					
	27	96	Gravel surfa	ace, HSG D				
	21	98	Roofs, HSC	S D				
	111	77	Woods, Go	od, HSG D				
	174	80	>75% Gras	s cover, Go	ood, HSG D			
	798	98	Roofs, HSG B					
	1,028	61	>75% Grass cover, Good, HSG B					
	3,201	55	Woods, Go	od, HSG B				
	7,905	75	Weighted A	verage				
	4,541		57.44% Pei	vious Area				
	3,364		42.56% lmp	pervious Ar	ea			
To (min)		Slope (ft/ft		Capacity (cfs)	Description			
12.6	68	0.0290	0.09		Sheet Flow, Woods: Light underbrush	n= 0.400	P2= 3.70"	

Summary for Subcatchment 5S: Subcatchment 5S

Runoff 2.00 cfs @ 12.10 hrs, Volume= 0.151 af, Depth> 3.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Area (sf)	CN	Description
*	2,532	98	Ledge Outcrop, HSG D
	1,442	96	Gravel surface, HSG D
	59	98	Roofs, HSG D
	715	77	Woods, Good, HSG D
	3,730	80	>75% Grass cover, Good, HSG D
	1,158	98	Roofs, HSG B
	852	98	Paved parking, HSG B
	1,842	96	Gravel surface, HSG B
	6,869	61	>75% Grass cover, Good, HSG B
	256	55	Woods, Good, HSG B
	1,896	80	>75% Grass cover, Good, HSG D
	1,007	98	Roofs, HSG D
	22,358 81		Weighted Average
	16,750		74.92% Pervious Area
	5,608		25.08% Impervious Area
	5,608		25.08% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.7	6	0.0500	0.15		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.2	15	0.0200	1.01		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.70"
	3.8	31	0.0167	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.9	14	0.1400	0.27		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	1.6	21	0.0676	0.22		Sheet Flow,
		-				Grass: Short n= 0.150 P2= 3.70"
-	7.2	87	Total			

Summary for Subcatchment 6S: Subcatchment 6S

1.40 cfs @ 12.24 hrs, Volume= 0.140 af, Depth> 2.49" Runoff

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Α	rea (sf)	CN [Description					
		9,085	98 F	Paved parking, HSG B					
		5,246	61 >	75% Gras	s cover, Go	ood, HSG B			
		14,877	55 N	Voods, Go	od, HSG B				
		102	98 F	Roofs, HSG	6 B				
-		29,310 70 Weighted Average							
	20,123 68.66% Pervious Area				vious Area				
		9,187	3	31.34% Imp	ervious Ar	ea			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	16.0	100	0.0350	0.10		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 3.70"			
	0.7	37	0.0300	0.87		Shallow Concentrated Flow,			
-						Woodland Kv= 5.0 fps			
	16.7	137	Total						

Summary for Reach 1R: Swale

0.379 ac, 25.67% Impervious, Inflow Depth > 4.04" for 10 Yr 24 Hr(+15%) event Inflow Area =

1.72 cfs @ 12.09 hrs, Volume= 1.53 cfs @ 12.13 hrs, Volume= 0.127 af Inflow

0.127 af, Atten= 11%, Lag= 2.7 min Outflow

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.60 fps, Min. Travel Time= 3.9 min Avg. Velocity = 0.24 fps, Avg. Travel Time= 9.6 min

Peak Storage= 358 cf @ 12.13 hrs Average Depth at Peak Storage= 0.53', Surface Width= 9.59' Bank-Full Depth= 1.00' Flow Area= 9.0 sf, Capacity= 8.19 cfs

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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0.00' x 1.00' deep channel, n= 0.150 Sheet flow over Short Grass Side Slope Z-value= 10.0 8.0 '/' Top Width= 18.00'

Length= 140.0' Slope= 0.0214 '/'

Inlet Invert= 40.00', Outlet Invert= 37.00'



Summary for Reach AP1: Wooded Depression

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.673 ac, 31.34% Impervious, Inflow Depth > 2.49" for 10 Yr 24 Hr(+15%) event

Inflow = 1.40 cfs @ 12.24 hrs, Volume= 0.140 af

Outflow = 1.40 cfs @ 12.24 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Shoulder of Road

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.379 ac. 25.67% Impervious. Inflow Depth > 4.03" for 10 Yr 24 Hr(+15%) event

Inflow = 1.53 cfs @ 12.13 hrs, Volume= 0.127 af

Outflow = 1.53 cfs @ 12.13 hrs, Volume= 0.127 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Detention Pond

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.688 ac, 14.97% Impervious, Inflow Depth > 1.62" for 10 Yr 24 Hr(+15%) event

Inflow = 2.24 cfs @ 12.11 hrs, Volume= 0.228 af

Outflow = 2.24 cfs @ 12.11 hrs, Volume= 0.228 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Rear of Site

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.181 ac, 42.56% Impervious, Inflow Depth > 2.95" for 10 Yr 24 Hr(+15%) event

Inflow = 0.50 cfs @ 12.18 hrs, Volume= 0.045 af

Outflow = 0.50 cfs @ 12.18 hrs, Volume= 0.045 af, Atten= 0%, Lag= 0.0 min

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Shallow Depression

[93] Warning: Storage range exceeded by 0.09'

[90] Warning: Qout>Qin may require smaller dt or Finer Routing

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=39)

0.513 ac, 25.08% Impervious, Inflow Depth > 3.53" for 10 Yr 24 Hr(+15%) event Inflow Area =

2.00 cfs @ 12.10 hrs, Volume= 2.06 cfs @ 12.10 hrs, Volume= 0.151 af Inflow

0.138 af, Atten= 0%, Lag= 0.0 min Outflow

2.06 cfs @ 12.10 hrs, Volume= 0.138 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.17' @ 12.10 hrs Surf Area= 3,088 sf Storage= 590 cf

Plug-Flow detention time= 64.1 min calculated for 0.138 af (91% of inflow)

Center-of-Mass det. time= 20.8 min (835.5 - 814.7)

Volume	Inve	ert Avail.Sto	rage Storage	e Description	
#1	36.7	75' 59	90 cf Custor	n Stage Data (Pris	smatic)Listed below (Recalc)
Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
36.75		417	0	0	
36.88	}	1,613	132	132	
37.00)	2,380	240	372	
37.08	3	3,088	219	590	
Device I	Routing	Invert	Outlet Device	es	
#1	Primary	37.07'			ad-Crested Rectangular Weir
			Head (feet)	0.20 0.40 0.60 0	.80 1.00 1.20 1.40 1.60 1.80 2.00
				.50 4.00 4.50	
					8 2.67 2.65 2.64 2.64 2.68 2.68
			2.72 2.81 2	.92 2.97 3.07 3.3	32

Primary OutFlow Max=2.04 cfs @ 12.10 hrs HW=37.17' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 2.04 cfs @ 0.77 fps)

Summary for Pond 2P: Wetland Ponding Area

Inflow Area =	0.797 ac, 15.46% Impervious, Inflow De	epth > 2.67" for 10 Yr 24 Hr(+15%) event
Inflow =	1.67 cfs @ 12.29 hrs, Volume=	0.177 af
Outflow =	0.10 cfs @ 16.12 hrs, Volume=	0.038 af, Atten= 94%, Lag= 230.1 min
	0.10 cfs @ 16.12 hrs, Volume=	0.038 af
	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 31.32' @ 16.12 hrs Surf.Area= 4,120 sf Storage= 6,101 cf

Plug-Flow detention time= 438.2 min calculated for 0.038 af (21% of inflow)

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Center-of-Mass det. time= 299.4 min (1,146.8 - 847.3)

Volume	Invert	t Avail.Storage		Storage Description			_
#1	28.00	6,9	968 cf	Custom Stage Date	a (Irregular)Listed	below (Recalc)	
Elevation (fee		urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)	
28.0	00	619	194.0	0	0	619	
29.0	00	1,245	250.0	914	914	2,610	
30.0	00	2,036	357.0	1,624	2,538	7,787	
31.0	00	2,891	433.0	2,451	4,989	12,582	
31.5	50	4,916	435.0	1,929	6,919	12,839	
31.	51	4,916	435.0	49	6,968	12,843	
Device	Routing	Invert	Outle	et Devices			_
#1	Secondary	31.50	70.0	long x 10.0' bread	th Broad-Crested	Rectangular Weir	
			Head	d (feet) 0.20 0.40 0	.60 0.80 1.00 1.2	0 1.40 1.60	
			Coef	. (English) 2.49 2.5	6 2.70 2.69 2.68	2.69 2.67 2.64	
#2	Primary	31.30		long x 4.0' breadtl			
			Head	d (feet) 0.20 0.40 0	.60 0.80 1.00 1.2	0 1.40 1.60 1.80 2.00	
				3.00 3.50 4.00 4.5			
			Coef	. (English) 2.38 2.5	4 2.69 2.68 2.67	2.67 2.65 2.66 2.66	
			2.68	2.72 2.73 2.76 2.7	79 2.88 3.07 3.32		

Primary OutFlow Max=0.10 cfs @ 16.12 hrs HW=31.32' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 0.10 cfs @ 0.33 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S

Runoff Area=34,729 sf 15.46% Impervious Runoff Depth>3.92"
Flow Length=112' Tc=20.1 min CN=72 Runoff=2.46 cfs 0.260 af

Flow Length=112 1C=20.1 min CN=72 Runoii=2.46 cis 0.260 ai

Subcatchment2S: Subcatchment2S Runoff Area=16,495 sf 25.67% Impervious Runoff Depth>5.48"

Flow Length=45' Slope=0.0400 '/' Tc=6.0 min CN=86 Runoff=2.30 cfs 0.173 af

Subcatchment3S: Subcatchment3S

Runoff Area=16,448 sf 0.17% Impervious Runoff Depth>2.67"
Flow Length=180' Tc=24.1 min CN=60 Runoff=0.72 cfs 0.084 af

Subcatchment4S: Subcatchment4S Runoff Area=7,905 sf 42.56% Impervious Runoff Depth>4.25"

Flow Length=68' Slope=0.0290 '/' Tc=12.6 min CN=75 Runoff=0.73 cfs 0.064 af

Subcatchment5S: Subcatchment5S

Runoff Area=22,358 sf 25.08% Impervious Runoff Depth>4.91"
Flow Length=87' Tc=7.2 min CN=81 Runoff=2.77 cfs 0.210 af

Subcatchment6S: Subcatchment6S

Runoff Area=29,310 sf 31.34% Impervious Runoff Depth>3.71"
Flow Length=137' Tc=16.7 min CN=70 Runoff=2.11 cfs 0.208 af

Reach 1R: Swale Avg. Flow Depth=0.60' Max Vel=0.64 fps Inflow=2.30 cfs 0.173 af

n=0.150 L=140.0' S=0.0214 '/' Capacity=8.19 cfs Outflow=2.06 cfs 0.172 af

Reach AP1: Wooded Depression Inflow=2.11 cfs 0.208 af

Outflow=2.11 cfs 0.208 af

Reach AP2: Shoulder of Road Inflow=2.06 cfs 0.172 af
Outflow=2.06 cfs 0.172 af

Reach AP3: Detention Pond Inflow=3.14 cfs 0.402 af Outflow=3.14 cfs 0.402 af

People AD4: Boar of Site

Reach AP4: Rear of Site Inflow=0.73 cfs 0.064 af Outflow=0.73 cfs 0.064 af

Pond 1P: Shallow Depression Peak Elev=37.19' Storage=590 cf Inflow=2.77 cfs 0.210 af

Outflow=2.81 cfs 0.197 af

Pond 2P: Wetland Ponding Area Peak Elev=31.36' Storage=6,271 cf Inflow=2.46 cfs 0.260 af Primary=0.55 cfs 0.121 af Secondary=0.00 cfs 0.000 af Outflow=0.55 cfs 0.121 af

Total Runoff Area = 2.921 ac Runoff Volume = 0.999 af Average Runoff Depth = 4.11"
78.16% Pervious = 2.283 ac 21.84% Impervious = 0.638 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment 1S: Subcatchment 1S Runoff Area=34,729 sf 15.46% Impervious Runoff Depth>5.14"

Flow Length=112' Tc=20.1 min CN=72 Runoff=3.23 cfs 0.342 af

Subcatchment2S: Subcatchment2S Runoff Area=16,495 sf 25.67% Impervious Runoff Depth>6.84"

Flow Length=45' Slope=0.0400 '/' Tc=6.0 min CN=86 Runoff=2.84 cfs 0.216 af

Subcatchment3S: Subcatchment3S Runoff Area=16,448 sf 0.17% Impervious Runoff Depth>3.72"

Flow Length=180' Tc=24.1 min CN=60 Runoff=1.01 cfs 0.117 af

Subcatchment4S: Subcatchment4S Runoff Area=7,905 sf 42.56% Impervious Runoff Depth>5.51"

Flow Length=68' Slope=0.0290 '/' Tc=12.6 min CN=75 Runoff=0.94 cfs 0.083 af

Subcatchment5S: Subcatchment5S Runoff Area=22,358 sf 25.08% Impervious Runoff Depth>6.24"

Flow Length=87' Tc=7.2 min CN=81 Runoff=3.48 cfs 0.267 af

Subcatchment6S: Subcatchment6S Runoff Area=29,310 sf 31.34% Impervious Runoff Depth>4.91"

Flow Length=137' Tc=16.7 min CN=70 Runoff=2.80 cfs 0.275 af

Reach 1R: Swale Avg. Flow Depth=0.65' Max Vel=0.68 fps Inflow=2.84 cfs 0.216 af

n=0.150 L=140.0' S=0.0214 '/' Capacity=8.19 cfs Outflow=2.56 cfs 0.215 af

Reach AP1: Wooded Depression Inflow=2.80 cfs 0.275 af

Outflow=2.80 cfs 0.275 af

Reach AP2: Shoulder of Road Inflow=2.56 cfs 0.215 af

Outflow=2.56 cfs 0.215 af

Reach AP3: Detention Pond Inflow=3.98 cfs 0.573 af

Outflow=3.98 cfs 0.573 af

Reach AP4: Rear of Site Inflow=0.94 cfs 0.083 af

Outflow=0.94 cfs 0.083 af

Pond 1P: Shallow Depression Peak Elev=37.21' Storage=590 cf Inflow=3.48 cfs 0.267 af

Outflow=3.48 cfs 0.253 af

Pond 2P: Wetland Ponding Area Peak Elev=31.44' Storage=6.611 cf Inflow=3.23 cfs 0.342 af

Primary=1.90 cfs 0.202 af Secondary=0.00 cfs 0.000 af Outflow=1.90 cfs 0.202 af

Total Runoff Area = 2.921 ac Runoff Volume = 1.300 af Average Runoff Depth = 5.34"
78.16% Pervious = 2.283 ac 21.84% Impervious = 0.638 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 3.23 cfs @ 12.28 hrs, Volume=

0.342 af, Depth> 5.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

Δ	rea (sf)	CN [Description						
	4,202		Voods, Go	od. HSG B					
	191		75% Grass cover, Good, HSG B						
	9,900		75% Grass cover, Good, HSG B						
	4,049	96 (Gravel surface, HSG B						
	2,054				k sewers, HSG B				
	5,450		Voods, Go						
	745		Roofs, HSG B						
*	1,274		Ledge Outcrop, HSG D						
	1,901			od, HSG D					
	666			ace, HSG [
	3,000				ood, HSG D				
	534				& sewers, HSG D				
	763		Roofs, HSC						
	34,729		Weighted A						
	29,359			vious Area					
	5,370		15.46% IM	pervious Ar	ea				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)		(cfs)					
20.0		0.0200			Sheet Flow,				
20.0		3.0230	2.30		Woods: Light underbrush n= 0.400 P2= 3.70"				
0.1	12	0.3300	2.87		Shallow Concentrated Flow,				
					Woodland Kv= 5.0 fps				
20.1	112	Total							

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 2.84 cfs @ 12.09 hrs, Volume=

0.216 af, Depth> 6.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

	Area (sf)	CN	Description
* 401 98 Le			Ledge Outcrop, HSG D
	1,855	96	Gravel surface, HSG D
	7,620	80	>75% Grass cover, Good, HSG D
	1,200	98	Paved roads w/curbs & sewers, HSG D
	908	98	Roofs, HSG D
	2,786	80	>75% Grass cover, Good, HSG D
	1,725	98	Roofs, HSG D
	16,495	86	Weighted Average
	12,261		74.33% Pervious Area
	4,234		25.67% Impervious Area

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•			
3.6	45	0.0400	0.21		Sheet Flow,			
					Grass: Short	n= 0.150	P2= 3.70"	
3.6	45	Total	Increased t	o minimum	$T_C = 6.0 \text{ min}$			

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 1.01 cfs @ 12.35 hrs, Volume=

0.117 af, Depth> 3.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN [Description		
*	28	98 L	.edge Outo	rop, HSG E	
	660			ace, HSG D	
	1,114	77 \	Noods, Go	od, HSG D	
	291	80 >	>75% Gras	s cover, Go	ood, HSG D
	4,820	61 >	>75% Gras	s cover, Go	ood, HSG B
	9,535	55 \	Noods, Go	od, HSG B	
	16,448	60 \	Neighted A	verage	
	16,420			vious Area	
	28	(0.17% Impe	ervious Area	a
			•		
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
1.5	11	0.0230	0.12		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
5.4	18	0.0167	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
3.2	19	0.0100	0.10		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
4.0	22	0.0540	0.09		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
8.0	30	0.0180	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
2.0	80	0.0180	0.67		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
24.1	180	Total			

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 0.94 cfs @ 12.17 hrs, Volume= 0.083 af, Depth> 5.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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	Area (sf)	CN	Description						
*	2,545	98	Ledge Outo	rop, HSG [)				
	27	96	Gravel surfa						
	21	98	Roofs, HSG	D D					
	111	77	Woods, Go	Noods, Good, HSG D					
	174	80	>75% Gras	75% Grass cover, Good, HSG D					
	798	98		oofs, HSG B					
	1,028	61	>75% Gras	75% Grass cover, Good, HSG B					
	3,201	55	Woods, Go	Woods, Good, HSG B					
	7,905	75	Weighted A	verage					
	4,541		57.44% Pei	vious Area	1				
	3,364		42.56% Imp	ervious Ar	ea				
	Tc Length	Slop	e Velocity	Capacity	Description				
(m	in) (feet)	(ft/f	t) (ft/sec)	(cfs)					
12	2.6 68	0.029	0.09		Sheet Flow,				

Woods: Light underbrush n= 0.400 P2= 3.70"

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 3.48 cfs @ 12.10 hrs, Volume=

0.267 af, Depth> 6.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

	Area (sf)	CN	Description
*	2,532	98	Ledge Outcrop, HSG D
	1,442	96	Gravel surface, HSG D
	59	98	Roofs, HSG D
	715	77	Woods, Good, HSG D
	3,730	80	>75% Grass cover, Good, HSG D
	1,158	98	Roofs, HSG B
	852	98	Paved parking, HSG B
	1,842	96	Gravel surface, HSG B
	6,869	61	>75% Grass cover, Good, HSG B
	256	55	Woods, Good, HSG B
	1,896	80	>75% Grass cover, Good, HSG D
	1,007	98	Roofs, HSG D
3	22,358	81	Weighted Average
	16,750		74.92% Pervious Area
	5,608		25.08% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-					(CIS)	
	0.7	6	0.0500	0.15		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.2	15	0.0200	1.01		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.70"
	3.8	31	0.0167	0.13		Sheet Flow,
	0.0	•	0.0.0.	00		Grass: Short n= 0.150 P2= 3.70"
	0.9	1.4	0.1400	0.27		Sheet Flow,
	0.5	17	0.1400	0.27		•
						Grass: Short n= 0.150 P2= 3.70"
	1.6	21	0.0676	0.22		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	7.2	87	Total			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 2.80 cfs @ 12.23 hrs, Volume= 0.275 af, Depth> 4.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

ΑΑ	rea (sf)	CN E	Description				
	9,085	98 F	aved park	ing, HSG B			
	5,246	61 >	75% Gras	s cover, Go	ood, HSG B		
	14,877	55 V	Voods, Go	od, HSG B			
	102	98 F	Roofs, HSG B				
	29,310	70 V	Veighted A	verage			
	20,123	6	8.66% Per	vious Area			
	9,187	3	1.34% Imp	ervious Ar	ea		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
16.0	100	0.0350	0.10		Sheet Flow,		
					Woods: Light underbrush n= 0.400 P2= 3.70"		
0.7	37	0.0300	0.87		Shallow Concentrated Flow,		
					Woodland Kv= 5.0 fps		
16.7	137	Total					

Summary for Reach 1R: Swale

Inflow Area = 0.379 ac, 25.67% Impervious, Inflow Depth > 6.84" for 50 Yr 24 Hr(+15%) event

Inflow = 2.84 cfs @ 12.09 hrs, Volume= 0.216 af

Outflow = 2.56 cfs @ 12.13 hrs, Volume= 0.215 af, Atten= 10%, Lag= 2.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.68 fps, Min. Travel Time= 3.4 min Avg. Velocity = 0.27 fps, Avg. Travel Time= 8.6 min

Peak Storage= 527 cf @ 12.13 hrs

Average Depth at Peak Storage= 0.65', Surface Width= 11.65'

Bank-Full Depth= 1.00' Flow Area= 9.0 sf, Capacity= 8.19 cfs

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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0.00' x 1.00' deep channel, n= 0.150 Sheet flow over Short Grass

Side Slope Z-value= 10.0 8.0 '/' Top Width= 18.00'

Length= 140.0' Slope= 0.0214 '/'

Inlet Invert= 40.00', Outlet Invert= 37.00'



Summary for Reach AP1: Wooded Depression

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.673 ac, 31.34% Impervious, Inflow Depth > 4.91" for 50 Yr 24 Hr(+15%) event

Inflow = 2.80 cfs @ 12.23 hrs, Volume= 0.275 af

Outflow = 2.80 cfs @ 12.23 hrs, Volume= 0.275 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Shoulder of Road

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.379 ac, 25.67% Impervious, Inflow Depth > 6.83" for 50 Yr 24 Hr(+15%) event

Inflow = 2.56 cfs @ 12.13 hrs, Volume= 0.215 af

Outflow = 2.56 cfs @ 12.13 hrs, Volume= 0.215 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Detention Pond

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.688 ac, 14.97% Impervious, Inflow Depth > 4.07" for 50 Yr 24 Hr(+15%) event

Inflow = 3.98 cfs @ 12.11 hrs, Volume= 0.573 af

Outflow = 3.98 cfs @ 12.11 hrs, Volume= 0.573 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Rear of Site

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.181 ac, 42.56% Impervious, Inflow Depth > 5.51" for 50 Yr 24 Hr(+15%) event

Inflow = 0.94 cfs @ 12.17 hrs, Volume= 0.083 af

Outflow = 0.94 cfs @ 12.17 hrs, Volume= 0.083 af, Atten= 0%, Lag= 0.0 min

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Shallow Depression

[93] Warning: Storage range exceeded by 0.13'

Inflow Area = 0.513 ac, 25.08% Impervious, Inflow Depth > 6.24" for 50 Yr 24 Hr(+15%) event

Inflow 3.48 cfs @ 12.10 hrs, Volume= 0.267 af

3.48 cfs @ 12.10 hrs, Volume= 3.48 cfs @ 12.10 hrs, Volume= Outflow = 0.253 af. Atten= 0%. Lag= 0.0 min

Primary 0.253 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.21' @ 12.10 hrs Surf.Area= 3,088 sf Storage= 590 cf

Plug-Flow detention time= 43.0 min calculated for 0.253 af (95% of inflow)

Center-of-Mass det. time= 15.6 min (814.3 - 798.7)

Volume	Invert	Avail.Storage	Storage	Description	
#1	36.75'	590 cf	Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (feet)			c.Store ic-feet)	Cum.Store (cubic-feet)	
36.75		417	0	0	
36.88		1,613	132	132	
37.00		2,380	240	372	
37.08		3,088	219	590	

Device	Routing	Invert	Outlet Devices
#1	Primary	37.07'	27.0' long x 3.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50
			Coef. (English) 2.44 2.58 2.68 2.67 2.65 2.64 2.64 2.68 2.68
			272 281 292 297 307 332

Primary OutFlow Max=3.45 cfs @ 12.10 hrs HW=37.21' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Weir Controls 3.45 cfs @ 0.91 fps)

Summary for Pond 2P: Wetland Ponding Area

Inflow Area =	0.797 ac, 15.46% Impervious, Inflow De	epth > 5.14" for 50 Yr 24 Hr(+15%) event
Inflow =	3.23 cfs @ 12.28 hrs, Volume=	0.342 af
Outflow =	1.90 cfs @ 12.57 hrs, Volume=	0.202 af, Atten= 41%, Lag= 17.7 min
Primary =	1.90 cfs @ 12.57 hrs, Volume=	0.202 af
Secondary =	0.00 cfs @ 0.00 hrs. Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 31.44' @ 12.57 hrs Surf.Area= 4,625 sf Storage= 6,611 cf

Plug-Flow detention time= 192.9 min calculated for 0.202 af (59% of inflow) Center-of-Mass det. time= 88.0 min (916.6 - 828.7)

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Volume	Invert	Avail.St	orage	Storage Description		
#1	28.00'	6,9	968 cf	Custom Stage Data	a (Irregular)Listed	below (Recalc)
Elevation (fee	10	urf.Area (sq-ft)	Perim. (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	Wet.Area (sq-ft)
28.0	00	619	194.0	0	0	619
29.0	00	1,245	250.0	914	914	2,610
30.0	00	2,036	357.0	1,624	2,538	7,787
31.0	00	2,891	433.0	2,451	4,989	12,582
31.5	50	4,916	435.0	1,929	6,919	12,839
31.	51	4,916	435.0	49	6,968	12,843
Device	Routing	Invert	Outle	et Devices		
#1	Secondary	31.50'	70.0	long x 10.0' bread	th Broad-Crested	Rectangular Weir
	•			d (feet) 0.20 0.40 0		
			Coef	f. (English) 2.49 2.50	6 2.70 2.69 2.68	2.69 2.67 2.64
#2	Primary	31.30'	16.0	long x 4.0' breadth	n Broad-Crested R	lectangular Weir
			Head	d (feet) 0.20 0.40 0	.60 0.80 1.00 1.2	0 1.40 1.60 1.80 2.00
			2.50	3.00 3.50 4.00 4.5	50 5.00 5.50	
			Coef	f. (English) 2.38 2.54	4 2.69 2.68 2.67	2.67 2.65 2.66 2.66
			2.68	2.72 2.73 2.76 2.7	79 2.88 3.07 3.32	

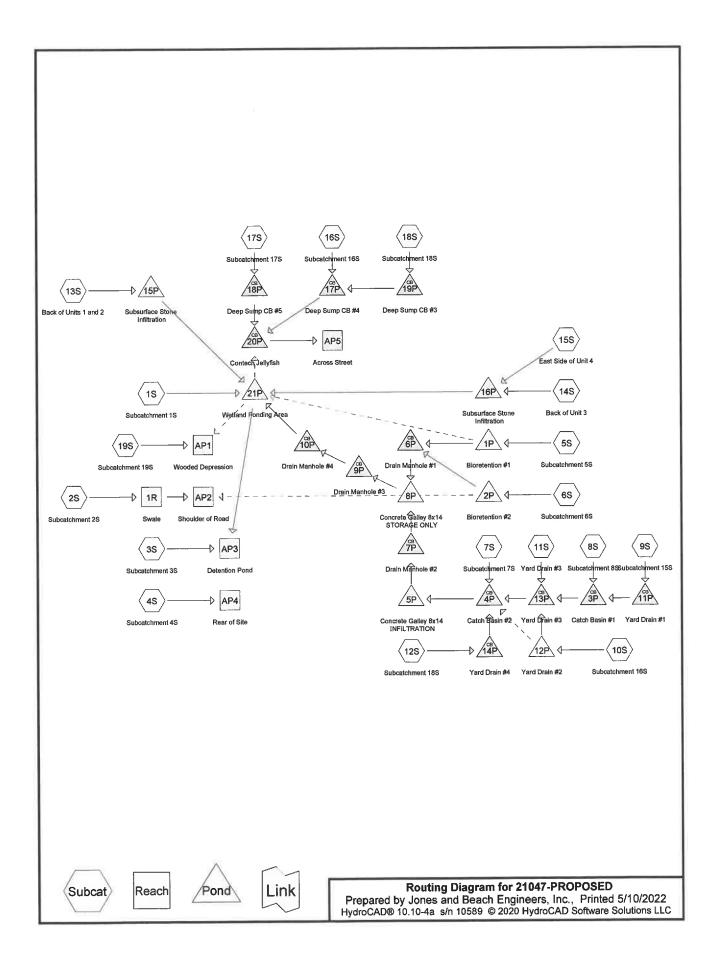
Primary OutFlow Max=1.86 cfs @ 12.57 hrs HW=31.43' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Weir Controls 1.86 cfs @ 0.87 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

APPENDIX II

PROPOSED CONDITIONS DRAINAGE ANALYSIS

Summary 2 YEAR Complete 10 YEAR Summary 25 YEAR Complete 50 YEAR



Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
0.673	61	>75% Grass cover, Good, HSG B (1S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 19S)
0.400	80	>75% Grass cover, Good, HSG D (1S, 2S, 6S, 7S, 8S, 9S, 10S, 12S)
0.095	98	Ledge Outcrop, HSG D (2S, 4S, 8S)
0.522	98	Paved parking, HSG B (5S, 6S, 7S, 8S, 17S, 18S, 19S)
0.136	98	Paved parking, HSG D (5S, 6S, 7S, 8S, 17S)
0.042	98	Paved roads w/curbs & sewers, HSG B (1S, 16S)
0.007	98	Paved roads w/curbs & sewers, HSG D (2S)
0.257	98	Roofs, HSG B (1S, 3S, 4S, 5S, 7S, 8S, 9S, 11S, 12S, 13S, 15S, 19S)
0.289	98	Roofs, HSG D (1S, 2S, 6S, 7S, 8S, 9S, 12S, 14S, 15S)
0.487	55	Woods, Good, HSG B (1S, 3S, 4S, 19S)
0.014	77	Woods, Good, HSG D (1S, 4S)
2.921	80	TOTAL AREA

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Soil Listing (all nodes)

Area	Soil	Subcatchment
(acres)	Group	Numbers
0.000	HSG A	
1.980	HSG B	1S, 3S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 11S, 12S, 13S, 15S, 16S, 17S, 18S, 19S
0.000	HSG C	
0.941	HSG D	1S, 2S, 4S, 5S, 6S, 7S, 8S, 9S, 10S, 12S, 14S, 15S, 17S
0.000	Other	
2.921		TOTAL AREA

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3 Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,938 sf 18.32% Impervious Runoff Depth>0.96" Flow Length=48' Tc=6.6 min CN=67 Runoff=0.31 cfs 0.026 af
Subcatchment 2S: Subcatchment 2S	Runoff Area=14,773 sf 41.02% Impervious Runoff Depth>2.36" Flow Length=126' Tc=12.0 min CN=87 Runoff=0.76 cfs 0.067 af
Subcatchment3S: Subcatchment3S	Runoff Area=8,436 sf 21.48% Impervious Runoff Depth>1.07" Tc=6.0 min CN=69 Runoff=0.22 cfs 0.017 af
Subcatchment4S: Subcatchment4S	Runoff Area=5,429 sf 56.24% Impervious Runoff Depth>1.87" Flow Length=87' Tc=13.2 min CN=81 Runoff=0.21 cfs 0.019 af
Subcatchment5S: Subcatchment5S	Runoff Area=6,946 sf 73.74% Impervious Runoff Depth>2.45" Tc=6.0 min CN=88 Runoff=0.44 cfs 0.033 af
Subcatchment6S: Subcatchment6S	Runoff Area=10,412 sf 62.71% Impervious Runoff Depth>2.63" Flow Length=60' Tc=6.0 min CN=90 Runoff=0.71 cfs 0.052 af
Subcatchment7S: Subcatchment7S	Runoff Area=9,749 sf 83.39% Impervious Runoff Depth>2.93" Flow Length=135' Tc=6.0 min CN=93 Runoff=0.72 cfs 0.055 af
Subcatchment8S: Subcatchment8S	Runoff Area=13,276 sf 70.01% Impervious Runoff Depth>2.63" Flow Length=86' Tc=11.2 min CN=90 Runoff=0.77 cfs 0.067 af
Subcatchment 9S: Subcatchment 15S Flow Length=67	Runoff Area=3,072 sf 26.66% Impervious Runoff Depth>1.58" ' Slope=0.0160 '/' Tc=7.2 min CN=77 Runoff=0.12 cfs 0.009 af
Subcatchment 10S: Subcatchment 16S Flow Length=83'	Runoff Area=3,155 sf 0.00% Impervious Runoff Depth>0.71" Slope=0.0060 '/' Tc=12.7 min CN=62 Runoff=0.04 cfs 0.004 af
Subcatchment11S: Yard Drain #3 Flow Length=60	Runoff Area=2,881 sf 15.97% Impervious Runoff Depth>0.96" ' Slope=0.0150 '/' Tc=6.8 min CN=67 Runoff=0.06 cfs 0.005 af
Subcatchment 12S: Subcatchment 18S Flow Length=37	Runoff Area=1,341 sf 25.58% Impervious Runoff Depth>2.03" ' Slope=0.0190 '/' Tc=6.0 min CN=83 Runoff=0.07 cfs 0.005 af
Subcatchment 13S: Back of Units 1 and 2	Runoff Area=918 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.07 cfs 0.006 af
Subcatchment 14S: Back of Unit 3	Runoff Area=310 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.03 cfs 0.002 af
Subcatchment 15S: East Side of Unit 4	Runoff Area=502 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment 16S: Subcatchment 16S	Runoff Area=1,247 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.10 cfs 0.008 af

21047-PROPOSED	Type III 24-hr 2 Yr 24 Hr (+15%) Rainfall=3.70"	,
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Subcatchment17S: Subcatchment17S Runoff Area=2,806 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.019 af
Subcatchment 18S: Subcatchment 18S Runoff Area=4,475 sf 100.00% Impervious Runoff Depth>3.46" Tc=6.0 min CN=98 Runoff=0.36 cfs 0.030 af
Subcatchment 19S: Subcatchment 19S Runoff Area=23,588 sf 18.01% Impervious Runoff Depth>0.80" Flow Length=137' Tc=16.7 min CN=64 Runoff=0.31 cfs 0.036 af
Reach 1R: Swale Avg. Flow Depth=0.61' Max Vel=0.64 fps Inflow=0.76 cfs 0.067 af n=0.150 L=140.0' S=0.0214 '/' Capacity=2.65 cfs Outflow=0.72 cfs 0.067 af
Reach AP1: Wooded Depression Inflow=0.31 cfs 0.036 af Outflow=0.31 cfs 0.036 af
Reach AP2: Shoulder of Road Inflow=0.72 cfs 0.067 af Outflow=0.72 cfs 0.067 af
Reach AP3: Detention Pond Inflow=0.22 cfs 0.017 af Outflow=0.22 cfs 0.017 af
Reach AP4: Rear of Site Inflow=0.21 cfs 0.019 af Outflow=0.21 cfs 0.019 af
Reach AP5: Across Street Inflow=0.69 cfs 0.082 af Outflow=0.69 cfs 0.082 af
Pond 1P: Bioretention#1 Peak Elev=35.21' Storage=137 cf Inflow=0.44 cfs 0.033 af Primary=0.44 cfs 0.030 af Secondary=0.00 cfs 0.000 af Outflow=0.44 cfs 0.030 af
Pond 2P: Bioretention#2 Peak Elev=35.40' Storage=218 cf Inflow=0.71 cfs 0.052 af Primary=0.60 cfs 0.051 af Secondary=0.00 cfs 0.000 af Outflow=0.60 cfs 0.051 af
Pond 3P: Catch Basin #1 Peak Elev=35.59' Inflow=0.89 cfs 0.076 af 15.0" Round Culvert n=0.013 L=47.0' S=0.0053 '/' Outflow=0.89 cfs 0.076 af
Pond 4P: Catch Basin #2 Peak Elev=35.08' Inflow=1.70 cfs 0.145 af 15.0" Round Culvert n=0.013 L=36.0' S=0.0056 '/' Outflow=1.70 cfs 0.145 af
Pond 5P: Concrete Galley 8x14 INFILTRATIONPeak Elev=34.18' Storage=0.050 af Inflow=1.70 cfs 0.145 af Discarded=0.46 cfs 0.144 af Primary=0.00 cfs 0.000 af Outflow=0.46 cfs 0.144 af
Pond 6P: Drain Manhole #1 Peak Elev=34.70' Inflow=1.02 cfs 0.081 af 12.0" Round Culvert n=0.013 L=48.0' S=0.0056 '/' Outflow=1.02 cfs 0.081 af
Pond 7P: Drain Manhole #2 Peak Elev=34.20' Inflow=0.00 cfs 0.000 af 12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.00 cfs 0.000 af
Pond 8P: Concrete Galley 8x14 STORAGE Peak Elev=33.77' Storage=0.021 af Inflow=1.02 cfs 0.081 af Primary=0.38 cfs 0.080 af Secondary=0.00 cfs 0.000 af Outflow=0.38 cfs 0.080 af

Pond 9P: Drain Manhole #3

Peak Elev=31.97' Inflow=0.38 cfs 0.080 af

12.0" Round Culvert n=0.013 L=85.0' S=0.0059'/ Outflow=0.38 cfs 0.080 af

21	047-I		DOS	ED
~ "	U4/-I	- 12 (FUJ	

Type III 24-hr 2 Yr 24 Hr (+15%) Rainfall=3.70"

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Pond 10P: Drain Manhole #4 Peak Elev=31.47' Inflow=0.38 cfs 0.080 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.38 cfs 0.080 af

Pond 11P: Yard Drain #1 Peak Elev=36.03' Inflow=0.12 cfs 0.009 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0055 '/' Outflow=0.12 cfs 0.009 af

Pond 12P: Yard Drain #2 Peak Elev=39.02' Storage=1 cf Inflow=0.04 cfs 0.004 af

Primary=0.04 cfs 0.004 af Secondary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.004 af

Pond 13P: Yard Drain #3 Peak Elev=35.31' Inflow=0.98 cfs 0.086 af

15.0" Round Culvert n=0.013 L=48.0' S=0.0052 '/' Outflow=0.98 cfs 0.086 af

Pond 14P: Yard Drain #4 Peak Elev=36.66' Inflow=0.07 cfs 0.005 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0100 '/' Outflow=0.07 cfs 0.005 af

Pond 15P: Subsurface Stone Infiltration Peak Elev=29.07' Storage=0.002 af Inflow=0.07 cfs 0.006 af

Discarded=0.01 cfs 0.006 af Primary=0.00 cfs 0.000 af Outflow=0.01 cfs 0.006 af

Pond 16P: Subsurface Stone Infiltration Peak Elev=32.44' Storage=0.002 af Inflow=0.07 cfs 0.005 af

Discarded=0.02 cfs 0.005 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.005 af

Pond 17P: Deep Sump CB #4 Peak Elev=29.99' Inflow=0.46 cfs 0.038 af

12.0" Round Culvert n=0.013 L=67.0' S=0.0060 '/' Outflow=0.46 cfs 0.038 af

Pond 18P: Deep Sump CB #5 Peak Elev=29.53' Inflow=0.23 cfs 0.019 af

12.0" Round Culvert n=0.013 L=3.0' S=0.0167 '/' Outflow=0.23 cfs 0.019 af

Pond 19P: Deep Sump CB #3 Peak Elev=30.20' Inflow=0.36 cfs 0.030 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.36 cfs 0.030 af

Pond 20P: Contech Jellyfish Peak Elev=29.41' Inflow=0.69 cfs 0.082 af

15.0" Round Culvert n=0.013 L=42.0' S=0.0060 '/' Outflow=0.69 cfs 0.082 af

Pond 21P: Wetland Ponding Area
Peak Elev=30.42' Storage=3,584 cf Inflow=0.63 cfs 0.106 af Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Tertiary=0.05 cfs 0.026 af Outflow=0.05 cfs 0.026 af

Total Runoff Area = 2.921 ac Runoff Volume = 0.464 af Average Runoff Depth = 1.91"
53.89% Pervious = 1.574 ac 46.11% Impervious = 1.347 ac

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,938 sf 18.32% Impervious Runoff Depth>2.24" Flow Length=48' Tc=6.6 min CN=67 Runoff=0.80 cfs 0.060 af
Subcatchment 2S: Subcatchment 2S	Runoff Area=14,773 sf 41.02% Impervious Runoff Depth>4.14" low Length=126' Tc=12.0 min CN=87 Runoff=1.32 cfs 0.117 af
Subcatchment3S: Subcatchment3S	Runoff Area=8,436 sf 21.48% Impervious Runoff Depth>2.41" Tc=6.0 min CN=69 Runoff=0.53 cfs 0.039 af
Subcatchment4S: Subcatchment4S	Runoff Area=5,429 sf 56.24% Impervious Runoff Depth>3.52" Flow Length=87' Tc=13.2 min CN=81 Runoff=0.40 cfs 0.037 af
Subcatchment5S: Subcatchment5S	Runoff Area=6,946 sf 73.74% Impervious Runoff Depth>4.25" Tc=6.0 min CN=88 Runoff=0.75 cfs 0.056 af
Subcatchment6S: Subcatchment6S	Runoff Area=10,412 sf 62.71% Impervious Runoff Depth>4.46" Flow Length=60' Tc=6.0 min CN=90 Runoff=1.17 cfs 0.089 af
Subcatchment7S: Subcatchment7S	Runoff Area=9,749 sf 83.39% Impervious Runoff Depth>4.79" Flow Length=135' Tc=6.0 min CN=93 Runoff=1.15 cfs 0.089 af
Subcatchment8S: Subcatchment8S	Runoff Area=13,276 sf 70.01% Impervious Runoff Depth>4.46" Flow Length=86' Tc=11.2 min CN=90 Runoff=1.28 cfs 0.113 af
Subcatchment 9S: Subcatchment 15S Flow Length=67	Runoff Area=3,072 sf 26.66% Impervious Runoff Depth>3.14" Slope=0.0160 '/' Tc=7.2 min CN=77 Runoff=0.25 cfs 0.018 af
Subcatchment 10S: Subcatchment 16S Flow Length=83'	Runoff Area=3,155 sf 0.00% Impervious Runoff Depth>1.82" Slope=0.0060 '/' Tc=12.7 min CN=62 Runoff=0.12 cfs 0.011 af
Subcatchment 11S: Yard Drain #3 Flow Length=60	Runoff Area=2,881 sf 15.97% Impervious Runoff Depth>2.24" Slope=0.0150 '/' Tc=6.8 min CN=67 Runoff=0.16 cfs 0.012 af
Subcatchment 12S: Subcatchment 18S Flow Length=37	Runoff Area=1,341 sf 25.58% Impervious Runoff Depth>3.73" Slope=0.0190 '/' Tc=6.0 min CN=83 Runoff=0.13 cfs 0.010 af
Subcatchment 13S: Back of Units 1 and 2	Runoff Area=918 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.11 cfs 0.009 af
Subcatchment 14S: Back of Unit 3	Runoff Area=310 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.04 cfs 0.003 af
Subcatchment 15S: East Side of Unit 4	Runoff Area=502 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment16S: Subcatchment16S	Runoff Area=1,247 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.15 cfs 0.013 af

21047-PROPOSED	Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Subcatchment17S: Subcatchment17S	Runoff Area=2,806 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.35 cfs 0.029 af
Subcatchment18S: Subcatchment18S	Runoff Area=4,475 sf 100.00% Impervious Runoff Depth>5.37" Tc=6.0 min CN=98 Runoff=0.55 cfs 0.046 af

Subcatchment 19S: Subcatchment 19S

Runoff Area=23,588 sf 18.01% Impervious Runoff Depth>1.98"
Flow Length=137' Tc=16.7 min CN=64 Runoff=0.87 cfs 0.089 af

Reach 1R: Swale

Avg. Flow Depth=0.76' Max Vel=0.73 fps Inflow=1.32 cfs 0.117 af n=0.150 L=140.0' S=0.0214 '/' Capacity=2.65 cfs Outflow=1.25 cfs 0.117 af

Reach AP1: Wooded Depression	Inflow=0.87 cfs 0.089 af Outflow=0.87 cfs 0.089 af
Reach AP2: Shoulder of Road	Inflow=1.25 cfs 0.117 af Outflow=1.25 cfs 0.117 af

Reach AP3: Detention Pond Inflow=0.53 cfs 0.039 af Outflow=0.53 cfs 0.039 af

Reach AP4: Rear of Site Inflow=0.40 cfs 0.037 af
Outflow=0.40 cfs 0.037 af

Reach AP5: Across Street Inflow=1.05 cfs 0.206 af
Outflow=1.05 cfs 0.206 af

Pond 1P: Bioretention #1 Peak Elev=35.60' Storage=155 cf Inflow=0.75 cfs 0.056 af Primary=0.73 cfs 0.054 af Secondary=0.00 cfs 0.000 af Outflow=0.73 cfs 0.054 af

Pond 2P: Bioretention #2 Peak Elev=36.19' Storage=303 cf Inflow=1.17 cfs 0.089 af Primary=1.03 cfs 0.087 af Secondary=0.00 cfs 0.000 af Outflow=1.03 cfs 0.087 af

Pond 3P: Catch Basin #1 Peak Elev=35.87' Inflow=1.50 cfs 0.132 af 15.0" Round Culvert n=0.013 L=47.0' S=0.0053 '/' Outflow=1.50 cfs 0.132 af

Pond 4P: Catch Basin #2 Peak Elev=35.75' Inflow=2.93 cfs 0.254 af

15.0" Round Culvert n=0.013 L=36.0' S=0.0056 '/' Outflow=2.93 cfs 0.254 af

Pond 5P: Concrete Galley 8x14 INFILTRATIONPeak Elev=35.72' Storage=0.094 af Inflow=2.93 cfs 0.254 af Discarded=0.67 cfs 0.251 af Primary=0.00 cfs 0.000 af Outflow=0.68 cfs 0.251 af

Pond 6P: Drain Manhole #1 Peak Elev=34.96' Inflow=1.76 cfs 0.141 af 12.0" Round Culvert n=0.013 L=48.0' S=0.0056 '/' Outflow=1.76 cfs 0.141 af

Pond 7P: Drain Manhole #2

Peak Elev=34.71' Inflow=0.00 cfs 0.000 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.00 cfs 0.000 af

Pond 8P: Concrete Galley 8x14 STORAGE Peak Elev=34.73' Storage=0.041 af Inflow=1.76 cfs 0.141 af Primary=0.50 cfs 0.140 af Secondary=0.00 cfs 0.000 af Outflow=0.50 cfs 0.140 af

Pond 9P: Drain Manhole #3

Peak Elev=32.03' Inflow=0.50 cfs 0.140 af

12.0" Round Culvert n=0.013 L=85.0' S=0.0059 '/' Outflow=0.50 cfs 0.140 af

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Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Pond 10P: Drain Manhole #4 Peak Elev=31.53' Inflow=0.50 cfs 0.140 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.50 cfs 0.140 af

Pond 11P: Yard Drain #1 Peak Elev=36.14' Inflow=0.25 cfs 0.018 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0055 '/' Outflow=0.25 cfs 0.018 af

Pond 12P: Yard Drain #2 Peak Elev=39.04' Storage=2 cf Inflow=0.12 cfs 0.011 af

Primary=0.12 cfs 0.011 af Secondary=0.00 cfs 0.000 af Outflow=0.12 cfs 0.011 af

Pond 13P: Yard Drain #3 Peak Elev=35.76' Inflow=1.76 cfs 0.155 af

15.0" Round Culvert n=0.013 L=48.0' S=0.0052 '/' Outflow=1.76 cfs 0.155 af

Pond 14P: Yard Drain #4 Peak Elev=36.72' Inflow=0.13 cfs 0.010 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0100 '/' Outflow=0.13 cfs 0.010 af

Pond 15P: Subsurface Stone Infiltration Peak Elev=30.07' Storage=0.004 af Inflow=0.11 cfs 0.009 af

Discarded=0.02 cfs 0.009 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.009 af

Pond 16P: Subsurface Stone Infiltration Peak Elev=32.81' Storage=0.003 af Inflow=0.10 cfs 0.008 af

Discarded=0.03 cfs 0.008 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.008 af

Pond 17P: Deep Sump CB #4 Peak Elev=30.09' Inflow=0.70 cfs 0.059 af

12.0" Round Culvert n=0.013 L=67.0' S=0.0060 '/' Outflow=0.70 cfs 0.059 af

Pond 18P: Deep Sump CB #5 Peak Elev=29.64 Inflow=0.35 cfs 0.029 af

12.0" Round Culvert n=0.013 L=3.0' S=0.0167 '/' Outflow=0.35 cfs 0.029 af

Pond 19P: Deep Sump CB #3 Peak Elev=30.31' Inflow=0.55 cfs 0.046 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.55 cfs 0.046 af

Pond 20P: Contech Jellyfish Peak Elev=29.53' Inflow=1.05 cfs 0.206 af

15.0" Round Culvert n=0.013 L=42.0' S=0.0060 '/' Outflow=1.05 cfs 0.206 af

Pond 21P: Wetland Ponding Area Peak Elev=30.65' Storage=4,209 cf Inflow=1.19 cfs 0.200 af

Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Tertiary=0.44 cfs 0.119 af Outflow=0.44 cfs 0.119 af

Total Runoff Area = 2.921 ac Runoff Volume = 0.846 af Average Runoff Depth = 3.48" 53.89% Pervious = 1.574 ac 46.11% Impervious = 1.347 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 0.80 cfs @ 12.10 hrs, Volume= 0.060 af, Depth> 2.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

Α	rea (sf)	CN I	Description								
	586	98	Paved roads w/curbs & sewers, HSG B								
	1,864	55	Noods, Go	Voods, Good, HSG B							
	3,396	61 :	>75% Gras	75% Grass cover, Good, HSG B							
	611	80 :	>75% Grass cover, Good, HSG D								
	541	77	Noods, Go	od, HSG D							
	3,408	55	Noods, Go	od, HSG B							
	1,564	61	>75% Gras	s cover, Go	ood, HSG B						
	1,600	98 I	Roofs, HSG B								
	368	98 I	Roofs, HSG D								
13,938 67 Weighted Average											
	11,384		31.68% Pe	rvious Area	1						
	2,554	•	18.32% Imp	pervious Ar	ea						
Tc	Length	Slope	Velocity	Capacity	Description						
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
5.1	32	0.0625	0.10		Sheet Flow,						
					Woods: Light underbrush	n= 0.400	P2= 3.70"				
1.5	16	0.3300	0.18		Sheet Flow,						
					Woods: Light underbrush	n= 0.400	P2= 3.70"				
6.6	48	Total									

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 1.32 cfs @ 12.16 hrs, Volume= 0.117 af, Depth> 4.14"

	Area (sf)	CN	Description					
	4,812	80	>75% Grass cover, Good, HSG D					
	319	98	Paved roads w/curbs & sewers, HSG D					
	2,823	98	,					
*	186	98	Ledge Outcrop, HSG D					
	3,901	80	>75% Grass cover, Good, HSG D					
	2,732	98	Roofs, HSG D					
	14,773	87	Weighted Average					
	8,713		58.98% Pervious Area					
	6,060		41.02% Impervious Area					

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	2.2	38	0.1000	0.29		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.7	17	0.3300	0.39		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	9.1	71	0.0100	0.13		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
-	12.0	126	Total			

Summary for Subcatchment 3S: Subcatchment 3S

Runoff = 0.53 cfs @ 12.10 hrs, Volume=

0.039 af, Depth> 2.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

Α	rea (sf)	CN	Description	escription								
	6,481	61	>75% Gras	75% Grass cover, Good, HSG B								
	143	55	Woods, Go	oods, Good, HSG B								
	1,812	98	Roofs, HSG	oofs, HSG B								
	8,436	69	Weighted Average									
	6,624		78.52% Pervious Area									
	1,812		21.48% Impervious Area									
Tc (min)	Length (feet)	Slope (ft/ft	,	Capacity (cfs)	Description							
6.0					Direct Entry,							

Summary for Subcatchment 4S: Subcatchment 4S

Runoff = 0.40 cfs @ 12.18 hrs, Volume=

0.037 af, Depth> 3.52"

	Area (sf)	CN	Description				
*	2,343	98	Ledge Outcrop, HSG D				
	73	77	Woods, Good, HSG D				
	917	55	Woods, Good, HSG B				
	1,386 61 >75% Grass cover, Good, HSG B						
	710	98	Roofs, HSG B				
	5,429	81	Weighted Average				
	2,376		43.76% Pervious Area				
	3,053		56.24% Impervious Area				

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.2	38	0.2100	3.12		Sheet Flow,
					Smooth surfaces n= 0.011 P2= 3.70"
8.0	7	0.2860	0.14		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
12.2	42	0.0120	0.06		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
13.2	87	Total	·		

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 0.75 cfs @ 12.09 hrs, Volume=

0.056 af, Depth> 4.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

A	rea (sf)	CN	Description	Description								
	1,824	61	>75% Gras	75% Grass cover, Good, HSG B								
	14	98	Paved park	aved parking, HSG D								
	3,268	98	Paved park	aved parking, HSG B								
	1,840	98	Roofs, HSG	oofs, HSG B								
	6,946	88	Weighted A	verage								
	1,824		26.26% Pervious Area									
	5,122		73.74% lmp	pervious Ar	ea							
_												
Tc	Length	Slope		Capacity	Description							
(min)_	(feet)	(ft/ft	(ft/sec)	(cfs)								
6.0					Direct Entry,							

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 1.17 cfs @ 12.09 hrs, Volume=

0.089 af, Depth> 4.46"

ΑΑ	rea (sf)	CN	Description			
	687	61	>75% Grass cover, Good, HSG B			
	1,334	98	Paved parking, HSG B			
	2,813 98 Paved parking, HSG D					
	3,196	80	>75% Grass cover, Good, HSG D			
	2,382	98	Roofs, HSG D			
	10,412 90 Weighted Average 3,883 37.29% Pervious Area		Weighted Average			
	6,529		62.71% Impervious Area			

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	1.7	20	0.0500	0.19		Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.7	40	0.0100	0.93		Sheet Flow,
12						Smooth surfaces n= 0.011 P2= 3.70"
	2.4	60	Total, I	ncreased t	o minimum	Tc = 6.0 min

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 1.15 cfs @ 12.09 hrs, Volume=

0.089 af, Depth> 4.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

A	rea (sf)	CN E	escription						
	1,935	98 F	Roofs, HSG	В					
	2,857			ng, HSG B					
	1,047				ood, HSG B				
	857		Roofs, HSG						
	2,481		Paved parking, HSG D >75% Grass cover, Good, HSG D						
	572				ood, HSG D				
	9,749		Veighted A						
	1,619	-	16.61% Pervious Area						
	8,130	8	3.39% lmp	ervious Are	ea				
_					Describetion				
Tc	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
4.6	40	0.0175	0.14		Sheet Flow,				
					Grass: Short n= 0.150 P2= 3.70"				
1.0	60	0.0100	1.01		Sheet Flow,				
					Smooth surfaces n= 0.011 P2= 3.70"				
0.3	35	0.0100	2.03		Shallow Concentrated Flow,				
(=====================================					Paved Kv= 20.3 fps				
5.9	135	Total, I	ncreased t	o minimum	Tc = 6.0 min				

Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 1.28 cfs @ 12.15 hrs, Volume=

0.113 af, Depth> 4.46"

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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	P	Area (sf)	CN_	Description							
		1,788	61	>75% Gras	s cover, Go	ood, HSG B					
		4,412	98	Paved park	ing, HSG B	}					
		1,219	98	Roofs, HSC	B						
		2,194				ood, HSG D					
*		1,608	98 I	_edge Outo	rop, HSG [)					
		39	98 I	8 Paved parking, HSG D							
		2,016	98 I								
		13,276	90 \	Veighted A							
		3,982		29.99% Per							
		9,294	•	70.01% lmp	pervious Are	ea					
	Тс	Length	Slope	Velocity	Capacity	Description					
1	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	3.3	40	0.0400	0.20		Sheet Flow,					
						Grass: Short	n= 0.150	P2= 3.70"			
	2.5	20	0.0200	0.13		Sheet Flow,					
						Grass: Short	n= 0.150	P2= 3.70"			
	5.4	26	0.0050	0.08		Sheet Flow,					
						Grass: Short	n= 0.150	P2= 3.70"			
	11.2	86	Total								

Summary for Subcatchment 9S: Subcatchment 15S

Runoff = 0.25 cfs @ 12.11 hrs, Volume=

0.018 af, Depth> 3.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Α	rea (sf)	CN	Description	escription								
		1,238	61	>75% Gras	75% Grass cover, Good, HSG B								
		1,015	80	>75% Gras	75% Grass cover, Good, HSG D								
		72	98	Roofs, HSG	Roofs, HSG B Roofs, HSG D								
		747	98	Roofs, HSG									
		3,072	77	Weighted Average									
		2,253		73.34% Pervious Area									
		819		26.66% lmp	ervious Ar	ea							
	_												
	Tc	Length	Slope		Capacity	Description							
1	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)								
	7.2	67	0.0160	0.15		Sheet Flow,							
						Grass: Short	n= 0.150	P2= 3.70"					

Summary for Subcatchment 10S: Subcatchment 16S

Runoff = 0.12 cfs @ 12.19 hrs, Volume= 0.011 af, Depth> 1.82"

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	Aı	rea (sf)	CN	Description	Description Description						
-		2,918	61	>75% Gras	75% Grass cover, Good, HSG B						
		237	80	>75% Gras	75% Grass cover, Good, HSG D						
		3,155	62	Weighted A	eighted Average						
		3,155		100.00% Pe	00.00% Pervious Area						
	Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description					
	12.7	83	0.006	0 0.11		Sheet Flow, Grass: Short	n= 0.150	P2= 3.70"			

Summary for Subcatchment 11S: Yard Drain #3

Runoff

0.16 cfs @ 12.11 hrs, Volume=

0.012 af, Depth> 2.24"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	A	rea (sf)	CN	Description					
		2,421	61	>75% Grass cover, Good, HSG B					
		460	98	Roofs, HSG B					
		2,881	67	Weighted Average					
		2,421		84.03% Pervious Area					
		460		15.97% lmp	ervious Ar	ea			
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	. Nov. 100	(cfs)				
8	6.8	60	0.0150	0.15		Sheet Flow,			
						Grass: Short	n= 0.150	P2= 3.70"	

Summary for Subcatchment 12S: Subcatchment 18S

Runoff

0.13 cfs @ 12.09 hrs, Volume=

0.010 af, Depth> 3.73"

Area (sf)	CN	Description				
94	61	>75% Grass cover, Good, HSG B				
904	80 >75% Grass cover, Good, HSG D					
11 98 Roofs, HSG B						
332	98	Roofs, HSG D				
1,341	83	Weighted Average				
998		74.42% Pervious Area				
343		25.58% Impervious Area				

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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		Length			Capacity	Description			
7.2	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	4.2	37	0.0190	0.15		Sheet Flow,			
						Grass: Short	n= 0.150	P2= 3.70"	
	4.2	37	Total, I	ncreased to	o minimum	Tc = 6.0 min			

Summary for Subcatchment 13S: Back of Units 1 and 2

Runoff = 0.11 cfs @ 12.09 hrs, Volume=

0.009 af, Depth> 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	A	rea (sf)	CN [Description							
		918	98 F	8 Roofs, HSG B							
		918	918 100.00% Impervious Area								
	_	_									
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
_	6.0					Direct Entry.					

Summary for Subcatchment 14S: Back of Unit 3

Runoff = 0.04 cfs @ 12.09 hrs, Volume=

0.003 af, Depth> 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfali=5.61"

-	Α	rea (sf)	CN I	Description						
13		310	310 98 Roofs, HSG D							
		310	310 100.00% Impervious Area							
(m	Tc nin)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	6.0					Direct Entry.				

Summary for Subcatchment 15S: East Side of Unit 4

Runoff = 0.06 cfs @ 12.09 hrs, Volume=

0.005 af, Depth> 5.37"

Area (sf)	CN	Description
500	98	Roofs, HSG B
 2	98	Roofs, HSG D
502	98	Weighted Average
502		100.00% Impervious Area

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Tc (min)	Length (feet)		Velocity (ft/sec)	Capacity (cfs)	Description	
(HIIII)	(leet)	(IVIL)	(10360)	(013)		
6.0					Direct Entry,	

Summary for Subcatchment 16S: Subcatchment 16S

Runoff = 0.15 cfs @ 12.09 hrs, Volume=

0.013 af, Depth> 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	Α	rea (sf)	CN [Description						
1,247 98 Paved roads w/curbs & sewers, HSG B										
		1,247	1,247 100.00% Impervious Area							
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
	6.0					Direct Entry,				

Summary for Subcatchment 17S: Subcatchment 17S

Runoff = 0.35 cfs @ 12.09 hrs, Volume=

0.029 af, Depth> 5.37"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

Α	rea (sf)	CN	Description					
	2,230	98	Paved park	ing, HSG B				
	576	98	Paved park	ing, HSG D				
	2,806	98	3 Weighted Average					
	2,806		100.00% Impervious Area					
Tc	Length	Slope	n or •0	Capacity	Description			
(min)	(feet)	(ft/ft	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 18S: Subcatchment 18S

Runoff = 0.55 cfs @ 12.09 hrs, Volume=

0.046 af, Depth> 5.37"

Area (sf)	CN	Description
4,475	98	Paved parking, HSG B
4,475		100.00% Impervious Area

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0	Direct Entry,				

Summary for Subcatchment 19S: Subcatchment 19S

Runoff = 0.87 cfs @ 12.25 hrs, Volume=

0.089 af, Depth> 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

	rea (sf)	CN E	escription		
	4,147	98 F	aved park	ing, HSG B	
	4,462	61 >	75% Gras	s cover, Go	ood, HSG B
	102	98 F	Roofs, HSG	В	
	14,877	55 V	Voods, Go	od, HSG B	
-	23,588	64 V	Veighted A	verage	
	19,339	81.99% Pervious Area			
	4,249	1	8.01% Imp	ervious Ar	ea
_					
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
16.0	100	0.0350	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
0.7	37	0.0300	0.87		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
16.7	137	Total			

Summary for Reach 1R: Swale

Inflow Area = 0.339 ac, 41.02% Impervious, Inflow Depth > 4.14" for 10 Yr 24 Hr(+15%) event

Inflow = 1.32 cfs @ 12.16 hrs, Volume= 0.117 af

Outflow = 1.25 cfs @ 12.21 hrs, Volume= 0.117 af, Atten= 5%, Lag= 2.6 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.73 fps, Min. Travel Time= 3.2 min

Avg. Velocity = 0.30 fps, Avg. Travel Time= 7.7 min

Peak Storage= 240 cf @ 12.21 hrs

Average Depth at Peak Storage= 0.76', Surface Width= 4.53'

Bank-Full Depth= 1.00' Flow Area= 3.0 sf, Capacity= 2.65 cfs

0.00' x 1.00' deep channel, n= 0.150 Sheet flow over Short Grass

Side Slope Z-value= 3.0 '/' Top Width= 6.00'

Length= 140.0' Slope= 0.0214 '/'

Inlet Invert= 40.00', Outlet Invert= 37.00'

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61" Printed 5/10/2022

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Summary for Reach AP1: Wooded Depression

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.542 ac, 18.01% Impervious, Inflow Depth > 1.98" for 10 Yr 24 Hr(+15%) event

Inflow = 0.87 cfs @ 12.25 hrs, Volume= 0.089 af

Outflow = 0.87 cfs @ 12.25 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Shoulder of Road

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.339 ac, 41.02% Impervious, Inflow Depth > 4.13" for 10 Yr 24 Hr(+15%) event

Inflow = 1.25 cfs @ 12.21 hrs, Volume= 0.117 af

Outflow = 1.25 cfs @ 12.21 hrs, Volume= 0.117 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Detention Pond

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.720 ac, 49.10% Impervious, Inflow Depth > 0.27" for 10 Yr 24 Hr(+15%) event

Inflow = 0.53 cfs @ 12.10 hrs, Volume= 0.039 af

Outflow = 0.53 cfs @ 12.10 hrs, Volume= 0.039 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Rear of Site

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.125 ac, 56.24% Impervious, Inflow Depth > 3.52" for 10 Yr 24 Hr(+15%) event

Inflow = 0.40 cfs @ 12.18 hrs, Volume= 0.037 af

Outflow = 0.40 cfs @ 12.18 hrs, Volume= 0.037 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

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Summary for Reach AP5: Across Street

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.196 ac,100.00% Impervious, Inflow Depth > 12.64" for 10 Yr 24 Hr(+15%) event

Inflow = 1.05 cfs @ 12.09 hrs, Volume= 0.206 af

Outflow = 1.05 cfs @ 12.09 hrs, Volume= 0.206 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention #1

Inflow Area =	0.159 ac, 73.74% Impervious, Inflow Do	epth > 4.25" for 10 Yr 24 Hr(+15%) event
Inflow =	0.75 cfs @ 12.09 hrs, Volume=	0.056 af
Outflow =	0.73 cfs @ 12.11 hrs, Volume=	0.054 af, Atten= 3%, Lag= 1.1 min
Primary =	0.73 cfs @ 12.11 hrs, Volume=	0.054 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 35.60' @ 12.11 hrs Surf.Area= 315 sf Storage= 155 cf

Plug-Flow detention time= 39.0 min calculated for 0.054 af (96% of inflow)

Center-of-Mass det. time= 15.9 min (809.2 - 793.3)

Volume	Invert	<u> Ava</u>	il.Stora	ge Storage Descr	ription	
#1	33.99'		694	cf Custom Stage	e Data (Prismatic)Listed below (Recalc)
Elevation		.Area			Cum.Store	
(fee	et)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
33.9	99	315	0.0	0	0	
34.0	00	315	40.0	1	1	
34.9	99	315	40.0	125	126	
35.0	00	315	15.0	0	126	
36.4	19	315	15.0	70	197	
36.5	50	315	100.0	3	200	
37.0	00	484	100.0	200	400	
37.5	50	668	100.0	288	688	
37.5	51	668	100.0	7	694	
Device	Routing	In	vert	Outlet Devices		
#1	Primary	34	.58'	8.0" Round Culver	rt	
	•			L= 40.0' CPP, proj	ecting, no headwa	III, Ke= 0.900
				Inlet / Outlet Invert=	34.58' / 34.40' S	s= 0.0045 '/' Cc= 0.900
				n= 0.013 Corrugate	ed PE, smooth inte	erior, Flow Area= 0.35 sf
#2	Device 1	34				Limited to weir flow at low heads
#3	Device 1	37	'.30'	18.0" Horiz. Orifice	e/Grate C= 0.600	ı
				Limited to weir flow	at low heads	
#4	Secondary	37	'.50'	31.0' long x 4.0' br	readth Broad-Cre	sted Rectangular Weir
	•			Head (feet) 0.20 0	.40 0.60 0.80 1.0	00 1.20 1.40 1.60 1.80 2.00
				2.50 3.00 3.50 4.0		
						2.67 2.67 2.65 2.66 2.66
				2.68		

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Primary OutFlow Max=0.72 cfs @ 12.11 hrs HW=35.58' TW=34.94' (Dynamic Tailwater)

-1=Culvert (Passes 0.72 cfs of 1.00 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.72 cfs @ 3.68 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=33.99' TW=28.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: Bioretention #2

Inflow Area =	0.239 ac, 62.71% Impervious, Inflow D	Depth > 4.46" for 10 Yr 24 Hr(+15%) event
Inflow =	1.17 cfs @ 12.09 hrs, Volume=	0.089 af
Outflow =	1.03 cfs @ 12.13 hrs, Volume=	0.087 af, Atten= 12%, Lag= 2.7 min
Primary =	1.03 cfs @ 12.13 hrs, Volume=	0.087 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 36.19' @ 12.13 hrs Surf.Area= 600 sf Storage= 303 cf

Plug-Flow detention time= 24.2 min calculated for 0.087 af (98% of inflow) Center-of-Mass det. time= 12.3 min (798.7 - 786.4)

Volume	Inve	ert Ava	il.Storage	Storage Descri	ption	
#1	34.4	9'	1,249 cf	Custom Stage	Data (Prismatic)L	isted below (Recalc)
					0 0	
Elevatio	n	Surf.Area	Voids	Inc.Store	Cum.Store	
(fee	t)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)	
34.4	9	600	0.0	0	0	
34.5	0	600	40.0	2	2	
35.4	9	600	40.0	238	240	
35.5	0	600	15.0	1	241	
36.9	9	600	15.0	134	375	
37.0	0	600	100.0	6	381	
38.0	0	1,113	100.0	857	1,237	
38.0	1	1,113	100.0	11	1,249	
			_			
Device	Routing	In	<u>ivert Ou</u>	tlet Devices		
#1	Primary	34		" Round Culver 33.0' CPP, proje	t ecting, no headwall,	, Ke= 0.900

#1	Primary	34.58'	8.0" Round Culvert
	•		L= 33.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.58' / 34.40' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Device 1	34.75'	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	37.70'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	38.00'	13.0' long x 4.0' breadth Broad-Crested Rectangular Weir
	,		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50
			Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66
			2 68 2 72 2 73 2 76 2 79 2 88 3 07 3 32

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Primary OutFlow Max=1.02 cfs @ 12.13 hrs HW=36.15' TW=34.94' (Dynamic Tailwater)

-1=Culvert (Passes 1.02 cfs of 1.46 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.02 cfs @ 5.17 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=34.49' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: Catch Basin #1

Inflow Area = 0.375 ac, 61.86% Impervious, Inflow Depth > 4.21" for 10 Yr 24 Hr(+15%) event

Inflow = 1.50 cfs @ 12.15 hrs, Volume= 0.132 af

Outflow = 1.50 cfs @ 12.15 hrs, Volume= 0.132 af, Atten= 0%, Lag= 0.0 min

Primary = 1.50 cfs @ 12.15 hrs, Volume= 0.132 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 35.87' @ 12.13 hrs

Flood Elev= 38.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	35.00'	15.0" Round Culvert
			L= 47.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 35.00' / 34.75' S= 0.0053 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=1.49 cfs @ 12.15 hrs HW=35.86' TW=35.61' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.49 cfs @ 2.33 fps)

Summary for Pond 4P: Catch Basin #2

Inflow Area = 0.768 ac, 56.90% Impervious, Inflow Depth > 3.97" for 10 Yr 24 Hr(+15%) event

Inflow = 2.93 cfs @ 12.11 hrs, Volume= 0.254 af

Outflow = 2.93 cfs @ 12.11 hrs, Volume= 0.254 af, Atten= 0%, Lag= 0.0 min

Primary = 2.93 cfs @ 12.11 hrs, Volume= 0.254 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 35.75' @ 12.55 hrs

Flood Elev= 38.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	34.30'	15.0" Round Culvert
			L= 36.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.30' / 34.10' S= 0.0056 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=2.88 cfs @ 12.11 hrs HW=35.38' TW=34.39' (Dynamic Tailwater) —1=Culvert (Barrel Controls 2.88 cfs @ 3.42 fps)

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Summary for Pond 5P: Concrete Galley 8x14 INFILTRATION

Inflow Area =	0.768 ac, 56.90% Impervious, Inflow	Depth > 3.97" for 10 Yr 24 Hr(+15%) event
Inflow =	2.93 cfs @ 12.11 hrs, Volume=	0.254 af
Outflow =	0.68 cfs @ 12.57 hrs, Volume=	0.251 af, Atten= 77%, Lag= 27.6 min
Discarded =	0.67 cfs @ 12.57 hrs, Volume=	0.251 af
Primary =	0.00 cfs @ 12.57 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 35.72' @ 12.57 hrs Surf.Area= 0.071 ac Storage= 0.094 af

Plug-Flow detention time= 79.0 min calculated for 0.251 af (99% of inflow) Center-of-Mass det. time= 71.3 min (865.5 - 794.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	33.90'	0.000 af	24.00'W x 42.00'L x 3.67'H Field A
			0.085 af Overall - 0.085 af Embedded = 0.000 af x 40.0% Voids
#2A	33.90'	0.062 af	Shea Leaching Chamber 8x14x3.7 x 9 Inside #1
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf
			9 Chambers in 3 Rows
#3	30.90'	0.035 af	28.00'W x 46.00'L x 3.00'H Prismatoid
			0.089 af Overall x 40.0% Voids
#4	30.90'	0.007 af	8.00'W x 32.00'L x 3.00'H Prismatoid
			0.018 af Overall x 40.0% Voids
#5	33.90'	0.010 af	2.00'W x 148.00'L x 3.67'H Prismatoid
			0.025 af Overall x 40.0% Voids
#6B	33.90'	0.000 af	8.00'W x 28.00'L x 3.67'H Field B
			0.019 af Overall - 0.019 af Embedded = 0.000 af x 40.0% Voids
#7B	33.90'	0.014 af	Shea Leaching Chamber 8x14x3.7 x 2 Inside #6
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf

0.128 af Total Available Storage

Storage Group A created with Chamber Wizard Storage Group B created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	30.90'	0.300 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 30.82' Phase-In= 0.01'
#2	Primary	35.70'	12.0" Round Culvert
	,		L= 60.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 35.70' / 34.30' S= 0.0233 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Primary	37.56'	160.0' long x 1.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Discarded OutFlow Max=0.67 cfs @ 12.57 hrs HW=35.72' (Free Discharge) 1=Exfiltration (Controls 0.67 cfs)

Primary OutFlow Max=0.00 cfs @ 12.57 hrs HW=35.72' TW=34.69' (Dynamic Tailwater)

-2=Culvert (Inlet Controls 0.00 cfs @ 0.39 fps)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Drain Manhole #1

Inflow Area = 0.398 ac, 67.12% Impervious, Inflow Depth > 4.25" for 10 Yr 24 Hr(+15%) event

Inflow = 1.76 cfs @ 12.12 hrs, Volume= 0.141 af

Outflow = 1.76 cfs (a) 12.12 hrs, Volume= 0.141 af, Atten= 0%, Lag= 0.0 min

Primary = 1.76 cfs @ 12.12 hrs, Volume= 0.141 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 34.96' @ 12.12 hrs

Flood Elev= 38.90'

Device	Routing	Invert	Outlet Devices
#1	Primary	34.07'	12.0" Round Culvert
	-		L= 48.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.07' / 33.80' S= 0.0056 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.71 cfs @ 12.12 hrs HW=34.94' TW=33.93' (Dynamic Tailwater) 1=Culvert (Barrel Controls 1.71 cfs @ 3.16 fps)

Summary for Pond 7P: Drain Manhole #2

Inflow Area = 0.768 ac, 56.90% Impervious, Inflow Depth = 0.00" for 10 Yr 24 Hr(+15%) event

Inflow = 0.00 cfs @ 12.57 hrs, Volume= 0.000 af

Outflow = 0.00 cfs @ 12.57 hrs, Volume= 0.000 af, Atten= 0%, Lag= 0.0 min

Primary = 0.00 cfs @ 12.57 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 34.71' @ 12.54 hrs

Flood Elev= 39.20'

Device	Routing	Invert	Outlet Devices
#1	Primary	34.20'	12.0" Round Culvert
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.20' / 34.00' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.00 cfs @ 12.57 hrs HW=34.69' TW=34.71' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

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Summary for Pond 8P: Concrete Galley 8x14 STORAGE ONLY

[92] Warning: Device #4 is above defined storage

[80] Warning: Exceeded Pond 7P by 0.41' @ 12.70 hrs (0.46 cfs 0.010 af)

Inflow Area =	1.167 ac, 60.39% Impervious, Inflow D	Depth > 1.45" for 10 Yr 24 Hr(+15%) event
Inflow =	1.76 cfs @ 12.12 hrs, Volume=	0.141 af
Outflow =	0.50 cfs @ 12.50 hrs, Volume=	0.140 af, Atten= 72%, Lag= 22.8 min
Primary =	0.50 cfs @ 12.50 hrs, Volume=	0.140 af
Secondary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 34.73' @ 12.50 hrs Surf.Area= 0.055 ac Storage= 0.041 af

Plug-Flow detention time= 38.0 min calculated for 0.140 af (99% of inflow) Center-of-Mass det. time= 32.6 min (835.3 - 802.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	33.30'	0.000 af	16.00'W x 56.00'L x 3.67'H Field A
			0.075 af Overall - 0.075 af Embedded = 0.000 af x 40.0% Voids
#2A	33.30'	0.055 af	Shea Leaching Chamber 8x14x3.7 x 8 Inside #1
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf
			8 Chambers in 2 Rows
#3	32.30'	0.011 af	= *· · · · · · · · · · · · · · · · · ·
			0.028 af Overall x 40.0% Voids
#4	33.30'	0.010 af	2.00'W x 144.00'L x 3.67'H Prismatoid
			0.024 af Overall x 40.0% Voids
		0.076 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	32.30'	4.0" Round Culvert L= 3.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 32.30' / 32.27' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Device 1	32.30'	4.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary	34.70'	8.0" Round Culvert L= 3.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 34.70' / 34.67' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#4	Secondary	39.80'	160.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Primary OutFlow Max=0.50 cfs @ 12.50 hrs HW=34.73' TW=32.03' (Dynamic Tailwater)

1=Culvert (Inlet Controls 0.50 cfs @ 5.72 fps)

2=Orifice/Grate (Passes 0.50 cfs of 0.63 cfs potential flow)

-3=Culvert (Barrel Controls 0.00 cfs @ 0.60 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=32.30' TW=31.60' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 9P: Drain Manhole #3

Inflow Area = 1.167 ac, 60.39% Impervious, Inflow Depth > 1.44" for 10 Yr 24 Hr(+15%) event

Inflow = 0.50 cfs @ 12.50 hrs, Volume= 0.140 af

Outflow = 0.50 cfs @ 12.50 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Primary = 0.50 cfs @ 12.50 hrs, Volume= 0.140 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 32.03' @ 12.50 hrs

Flood Elev= 39.90'

Device Routing Invert Outlet Devices

#1 Primary

31.60'

12.0" Round Culvert

L= 85.0' CPP, projecting, no headwall, Ke= 0.900
Inlet / Outlet Invert= 31.60' / 31.10' S= 0.0059 '/' Cc= 0.900

n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.50 cfs @ 12.50 hrs HW=32.03' TW=31.53' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.50 cfs @ 2.30 fps)

Summary for Pond 10P: Drain Manhole #4

Inflow Area = 1.167 ac, 60.39% Impervious, Inflow Depth > 1.44" for 10 Yr 24 Hr(+15%) event

Inflow = 0.50 cfs @ 12.50 hrs, Volume= 0.140 af

Outflow = 0.50 cfs (a) 12.50 hrs, Volume= 0.140 af, Atten= 0%, Lag= 0.0 min

Primary = 0.50 cfs @ 12.50 hrs, Volume= 0.140 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 31.53' @ 12.50 hrs

Flood Elev= 36.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	31.10'	12.0" Round Culvert
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 31.10' / 30.90' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.50 cfs @ 12.50 hrs HW=31.53' TW=30.20' (Dynamic Tailwater) 1=Culvert (Barrel Controls 0.50 cfs @ 2.28 fps)

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Summary for Pond 11P: Yard Drain #1

Inflow Area = 0.071 ac, 26.66% Impervious, Inflow Depth > 3.14" for 10 Yr 24 Hr(+15%) event

Inflow = 0.25 cfs @ 12.11 hrs, Volume= 0.018 af

Outflow = 0.25 cfs @ 12.11 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Primary = 0.25 cfs @ 12.11 hrs, Volume= 0.018 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 36.14' @ 12.12 hrs

Flood Elev= 39.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	35.80'	8.0" Round Culvert L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 35.80' / 35.58' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf

Primary OutFlow Max=0.24 cfs @ 12.11 hrs HW=36.13' TW=35.85' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.24 cfs @ 1.98 fps)

Summary for Pond 12P: Yard Drain #2

Inflow Area =	0.072 ac,	0.00% Impervious, Inflow D	epth > 1.82" for 10 Yr 24 Hr(+15%) event
Inflow =	0.12 cfs @	12.19 hrs, Volume=	0.011 af
Outflow =	0.12 cfs @	12.20 hrs, Volume=	0.011 af, Atten= 0%, Lag= 0.4 min
Primary =	0.12 cfs @	12.20 hrs, Volume=	0.011 af
Secondary =	0.00 cfs @	0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 39.04' @ 12.20 hrs Surf.Area= 107 sf Storage= 2 cf

Plug-Flow detention time= 0.2 min calculated for 0.011 af (100% of inflow) Center-of-Mass det. time= 0.2 min (866.4 - 866.2)

VolumeInvertAvail.StorageStorage Description#139.00'1,358 cfCustom Stage Data (Prismatic)Listed below (Recalc)

		.,		•	•		,	
Elevation (fee	. 91	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
39.0	00	5	0	0				
40.0		2,685	1,358	1,358				
		,						
Device	Routing	Invert	Outlet Devices					
#1	Primary	36.00'	8.0" Round Cu	ulvert				
			L= 50.0' CPP,	projecting, no h	neadwall, K	(e= 0.900		
			Inlet / Outlet Inv	ert= 36.00' / 35	.33' S= 0.	0134 '/' (Cc = 0.900	
			n= 0.013 Corru	igated PE, smo	oth interior,	Flow Are	e= 0.35	sf
#2	Device 1	39.00'	18.0" Horiz. Or	ifice/Grate C=	= 0.600			
			Limited to weir					
#3	Secondary	40.00'	100.0' long x 2					
	•		Head (feet) 0.2	0 0.40 0.60 0	.80 1.00 1	.20 1.40	1.60 1.8	30 2.00

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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2.50 3.00 3.50

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88

2.85 3.07 3.20 3.32

Primary OutFlow Max=0.12 cfs @ 12.20 hrs HW=39.04' TW=35.55' (Dynamic Tailwater)

1=Culvert (Passes 0.12 cfs of 2.18 cfs potential flow)

2=Orifice/Grate (Weir Controls 0.12 cfs @ 0.64 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=39.00' TW=34.30' (Dynamic Tailwater) = 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 13P: Yard Drain #3

Inflow Area = 0.514 ac, 47.23% Impervious, Inflow Depth > 3.62" for 10 Yr 24 Hr(+15%) event

Inflow = 1.76 cfs @ 12.14 hrs, Volume= 0.155 af

Outflow = 1.76 cfs @ 12.14 hrs, Volume= 0.155 af, Atten= 0%, Lag= 0.0 min

Primary = 1.76 cfs @ 12.14 hrs, Volume= 0.155 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 35.76' @ 12.53 hrs

Flood Elev= 38.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	34.65'	15.0" Round Culvert
			L= 48.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.65' / 34.40' S= 0.0052 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior. Flow Area= 1.23 sf

Primary OutFlow Max=1.74 cfs @ 12.14 hrs HW=35.61' TW=35.36' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.74 cfs @ 2.38 fps)

Summary for Pond 14P: Yard Drain #4

Inflow Area = 0.031 ac, 25.58% Impervious, Inflow Depth > 3.73" for 10 Yr 24 Hr(+15%) event

Inflow = 0.13 cfs @ 12.09 hrs, Volume= 0.010 af

Outflow = 0.13 cfs @ 12.09 hrs, Volume= 0.010 af, Atten= 0%, Lag= 0.0 min

Primary = 0.13 cfs @ 12.09 hrs, Volume= 0.010 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 36.72' @ 12.09 hrs

Flood Elev= 39.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	36.50'	8.0" Round Culvert
	•		L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 36.50' / 36.10' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior. Flow Area= 0.35 sf

Primary OutFlow Max=0.13 cfs @ 12.09 hrs HW=36.72' TW=35.37' (Dynamic Tailwater) 1=Culvert (Inlet Controls 0.13 cfs @ 1.26 fps)

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Summary for Pond 15P: Subsurface Stone Infiltration

Inflow Area =	0.021 ac,100.00% Impervious, Inflow Do	epth > 5.37" for 10 Yr 24 Hr(+15%) event
Inflow =	0.11 cfs @ 12.09 hrs, Volume=	0.009 af
Outflow =	0.02 cfs @ 12.58 hrs, Volume=	0.009 af, Atten= 85%, Lag= 29.4 min
Discarded =	0.02 cfs @ 12.58 hrs, Volume=	0.009 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 30.07' @ 12.58 hrs Surf.Area= 0.004 ac Storage= 0.004 af

Plug-Flow detention time= 111.7 min calculated for 0.009 af (100% of inflow) Center-of-Mass det. time= 111.0 min (856.8 - 745.7)

Invert Avail.Storage Storage Description

#1	27.50'	0.007	af 4.00'W x 40.00'L x 4.51'H Prismatoid 0.017 af Overall x 40.0% Voids
Device	Routing	Invert	Outlet Devices
#1	Discarded		0.650 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 27.08' Phase-In= 0.01'
#2	Primary		88.0' long x 1.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Discarded OutFlow Max=0.02 cfs @ 12.58 hrs HW=30.07' (Free Discharge) **1=Exfiltration** (Controls 0.02 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=27.50' TW=28.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 16P: Subsurface Stone Infiltration

Inflow Area =	0.019 ac,100.00% Impervious, Inflow Do	epth > 5.37" for 10 Yr 24 Hr(+15%) event
Inflow =	0.10 cfs @ 12.09 hrs, Volume=	0.008 af
Outflow =	0.03 cfs @ 12.44 hrs, Volume=	0.008 af, Atten= 73%, Lag= 21.3 min
Discarded =	0.03 cfs @ 12.44 hrs, Volume=	0.008 af
Primary =	0.00 cfs @ 0.00 hrs, Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 32.81' @ 12.44 hrs Surf.Area= 0.006 ac Storage= 0.003 af

Plug-Flow detention time= 51.1 min calculated for 0.008 af (100% of inflow) Center-of-Mass det. time= 50.1 min (795.8 - 745.7)

Volume	Invert	Avail.Storage	Storage Description	
#1	31.80'	0.004 af	8.00'W x 35.00'L x 1.71'H Prismatoid	

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Device	Routing	Invert	Outlet Devices
#1	Discarded	31.80'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 31.72' Phase-In= 0.01'
#2	Primary	33.50'	86.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.44 hrs HW=32.81' (Free Discharge) 1=Exfiltration (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=31.80' TW=28.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Deep Sump CB #4

Inflow Area = 0.131 ac,100.00% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr(+15%) event

Inflow = 0.70 cfs @ 12.09 hrs, Volume= 0.059 af

Outflow = 0.70 cfs @ 12.09 hrs, Volume= 0.059 af, Atten= 0%, Lag= 0.0 min

Primary = 0.70 cfs @ 12.09 hrs, Volume= 0.059 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 30.09' @ 12.09 hrs

Flood Elev= 33.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	29.60'	12.0" Round Culvert
			L= 67.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 29.60' / 29.20' S= 0.0060 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.69 cfs @ 12.09 hrs HW=30.08' TW=29.52' (Dynamic Tailwater) 1=Culvert (Barrel Controls 0.69 cfs @ 2.66 fps)

Summary for Pond 18P: Deep Sump CB #5

Inflow Area = 0.064 ac,100.00% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr(+15%) event

Inflow = 0.35 cfs @ 12.09 hrs, Volume= 0.029 af

Outflow = 0.35 cfs @ 12.09 hrs, Volume= 0.029 af, Atten= 0%, Lag= 0.0 min

Primary = 0.35 cfs @ 12.09 hrs, Volume= 0.029 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 29.64' @ 12.09 hrs

Flood Elev= 34.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	29.25'	12.0" Round Culvert
			L= 3.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 29.25' / 29.20' S= 0.0167 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Type III 24-hr 10 Yr 24 Hr(+15%) Rainfall=5.61"

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Primary OutFlow Max=0.34 cfs @ 12.09 hrs HW=29.63' TW=29.52' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.34 cfs @ 1.84 fps)

Summary for Pond 19P: Deep Sump CB #3

Inflow Area = 0.103 ac,100.00% Impervious, Inflow Depth > 5.37" for 10 Yr 24 Hr(+15%) event

Inflow = 0.55 cfs @ 12.09 hrs, Volume= 0.046 af

Outflow = 0.55 cfs @ 12.09 hrs, Volume= 0.046 af, Atten= 0%, Lag= 0.0 min

Primary = 0.55 cfs @ 12.09 hrs, Volume= 0.046 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 30.31' @ 12.09 hrs

Flood Elev= 33.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	20.00	12.0" Round Culvert L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 29.80' / 29.60' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.54 cfs @ 12.09 hrs HW=30.30' TW=30.08' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.54 cfs @ 1.99 fps)

Summary for Pond 20P: Contech Jellyfish

Inflow Area = 0.196 ac,100.00% Impervious, Inflow Depth > 12.64" for 10 Yr 24 Hr(+15%) event

Inflow = 1.05 cfs @ 12.09 hrs, Volume= 0.206 af

Outflow = 1.05 cfs @ 12.09 hrs, Volume= 0.206 af, Atten= 0%, Lag= 0.0 min

Primary = 1.05 cfs @ 12.09 hrs, Volume= 0.206 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 29.53' @ 12.09 hrs

Flood Elev= 33.60'

Device	Routing	Invert	Outlet Devices
#1	Primary		15.0" Round Culvert L= 42.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 28.95' / 28.70' S= 0.0060 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=1.02 cfs @ 12.09 hrs HW=29.52' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 1.02 cfs @ 2.76 fps)

Summary for Pond 21P: Wetland Ponding Area

Volume

Invert

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1.527 ac, 52.60% Impervious, Inflow Depth > 1.57" for 10 Yr 24 Hr(+15%) event Inflow 1.19 cfs @ 12.11 hrs, Volume= 0.200 af 0.44 cfs @ 13.61 hrs, Volume= 0.00 cfs @ 0.00 hrs, Volume= Outflow = 0.119 af, Atten= 63%, Lag= 90.1 min Primary 0.000 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Tertiary 0.44 cfs @ 13.61 hrs, Volume= 0.119 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 30.65' @ 13.61 hrs Surf.Area= 2.746 sf Storage= 4.209 cf

Plug-Flow detention time= 216.1 min calculated for 0.119 af (59% of inflow) Center-of-Mass det. time= 112.2 min (951.6 - 839.4)

Avail.Storage Storage Description

#1	28.00'	7,	242 cf	Custom Stage Dat	a (Irregular)Listed I	pelow (Recalc)
Elevation	on St	ırf.Area	Perim.	Inc.Store	Cum.Store	Wet.Area
(fee	et)	(sq-ft)	(feet)	(cubic-feet)	(cubic-feet)	(sq-ft)
28.0	00	619	194.0	0	0	619
29.0	00	1,245	250.0	914	914	2,610
30.0	00	2,174	307.0	1,688	2,602	5,152
31.0		3,074	298.0	2,611	5,213	5,680
31.5		4,916	435.0	1,980	7,193	13,674
31.5	51	4,916	435.0	49	7,242	13,678
Device	Routing	Inver	t Outle	et Devices		
#1	Secondary	31.50	70.0	long x 10.0' bread	th Broad-Crested	Rectangular Weir
				d (feet) 0.20 0.40 0		
				f. (English) 2.49 2.5		
#2	Primary			long x 4.0' breadt		
						0 1.40 1.60 1.80 2.00
				3.00 3.50 4.00 4.5		
						2.67 2.65 2.66 2.66
4 0	Tartian.	20.20		2.72 2.73 2.76 2.7	79 2.88 3.07 3.32	
#3	Tertiary	30.30		" Round Culvert	des besidend IV-	0.500
				4.0' CPP, square e		
				/ Outlet Invert= 30.3		
			n= 0.	.013 Corrugated PE	., smooth interior, 🕒	iow Area= 1.23 st

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Tertiary OutFlow Max=0.44 cfs @ 13.61 hrs HW=30.65' TW=29.34' (Dynamic Tailwater) 3=Culvert (Barrel Controls 0.44 cfs @ 2.30 fps)

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method - Pond routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,938 sf 18.32% Impervious Runoff Depth>3.40" Flow Length=48' Tc=6.6 min CN=67 Runoff=1.23 cfs 0.091 af
Subcatchment 2S: Subcatchment 2S	Runoff Area=14,773 sf 41.02% Impervious Runoff Depth>5.59" Flow Length=126' Tc=12.0 min CN=87 Runoff=1.75 cfs 0.158 af
Subcatchment3S: Subcatchment3S	Runoff Area=8,436 sf 21.48% Impervious Runoff Depth>3.61" Tc=6.0 min CN=69 Runoff=0.80 cfs 0.058 af
Subcatchment4S: Subcatchment4S	Runoff Area=5,429 sf 56.24% Impervious Runoff Depth>4.91" Flow Length=87' Tc=13.2 min CN=81 Runoff=0.56 cfs 0.051 af
Subcatchment5S: Subcatchment5S	Runoff Area=6,946 sf 73.74% Impervious Runoff Depth>5.71" Tc=6.0 min CN=88 Runoff=1.00 cfs 0.076 af
Subcatchment6S: Subcatchment6S	Runoff Area=10,412 sf 62.71% Impervious Runoff Depth>5.94" Flow Length=60' Tc=6.0 min CN=90 Runoff=1.53 cfs 0.118 af
Subcatchment7S: Subcatchment7S	Runoff Area=9,749 sf 83.39% Impervious Runoff Depth>6.29" Flow Length=135' Tc=6.0 min CN=93 Runoff=1.48 cfs 0.117 af
Subcatchment8S: Subcatchment8S	Runoff Area=13,276 sf 70.01% Impervious Runoff Depth>5.93" Flow Length=86' Tc=11.2 min CN=90 Runoff=1.68 cfs 0.151 af
Subcatchment 9S: Subcatchment 15S Flow Length=67	Runoff Area=3,072 sf 26.66% Impervious Runoff Depth>4.47" ' Slope=0.0160 '/' Tc=7.2 min CN=77 Runoff=0.35 cfs 0.026 af
Subcatchment 10S: Subcatchment 16S Flow Length=83'	Runoff Area=3,155 sf 0.00% Impervious Runoff Depth>2.88" Slope=0.0060 '/' Tc=12.7 min CN=62 Runoff=0.19 cfs 0.017 af
Subcatchment 11S: Yard Drain #3 Flow Length=60	Runoff Area=2,881 sf 15.97% Impervious Runoff Depth>3.40" ' Slope=0.0150 '/' Tc=6.8 min CN=67 Runoff=0.25 cfs 0.019 af
Subcatchment 12S: Subcatchment 18S Flow Length=37	Runoff Area=1,341 sf 25.58% Impervious Runoff Depth>5.14" ' Slope=0.0190 '/' Tc=6.0 min CN=83 Runoff=0.18 cfs 0.013 af
Subcatchment 13S: Back of Units 1 and 2	Runoff Area=918 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.14 cfs 0.012 af
Subcatchment 14S: Back of Unit 3	Runoff Area=310 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.05 cfs 0.004 af
Subcatchment15S: East Side of Unit 4	Runoff Area=502 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.08 cfs 0.007 af
Subcatchment 16S: Subcatchment 16S	Runoff Area=1,247 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.20 cfs 0.016 af

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Type III 24-hr 25 Yr 24 Hr(+15%) Rainfall=7.12"

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Subcatchment 17S: Subcatchment 17S

Runoff Area=2,806 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.44 cfs 0.037 af

Subcatchment 18S: Subcatchment 18S

Runoff Area=4,475 sf 100.00% Impervious Runoff Depth>6.88" Tc=6.0 min CN=98 Runoff=0.70 cfs 0.059 af

Subcatchment 19S: Subcatchment 19S

Runoff Area=23,588 sf 18.01% Impervious Runoff Depth>3.08"

Flow Length=137' Tc=16.7 min CN=64 Runoff=1.40 cfs 0.139 af

Reach 1R: Swale

Avg. Flow Depth=0.84' Max Vel=0.79 fps Inflow=1.75 cfs 0.158 af n=0.150 L=140.0' S=0.0214'/' Capacity=2.65 cfs Outflow=1.68 cfs 0.158 af

Reach AP1: Wooded Depression

Inflow=1.40 cfs 0.139 af Outflow=1.40 cfs 0.139 af

Reach AP2: Shoulder of Road

Inflow=1.68 cfs 0.158 af Outflow=1.68 cfs 0.158 af

Reach AP3: Detention Pond

Inflow=0.80 cfs 0.058 af Outflow=0.80 cfs 0.058 af

Reach AP4: Rear of Site

Inflow=0.56 cfs 0.051 af Outflow=0.56 cfs 0.051 af

Reach AP5: Across Street

Inflow=1.50 cfs 0.343 af Outflow=1.50 cfs 0.343 af

Pond 1P: Bioretention #1

Peak Elev=36.08' Storage=178 cf Inflow=1.00 cfs 0.076 af

Primary=0.93 cfs 0.073 af Secondary=0.00 cfs 0.000 af Outflow=0.93 cfs 0.073 af

Pond 2P: Bioretention #2

Peak Elev=37.00' Storage=382 cf Inflow=1.53 cfs 0.118 af Primary=1.30 cfs 0.116 af Secondary=0.00 cfs 0.000 af Outflow=1.30 cfs 0.116 af

Pond 3P: Catch Basin #1

Peak Elev=36.58' Inflow=1.99 cfs 0.177 af 15.0" Round Culvert n=0.013 L=47.0' S=0.0053 '/' Outflow=1.99 cfs 0.177 af

Pond 4P: Catch Basin #2

Peak Elev=36.51' Inflow=3.93 cfs 0.343 af

15.0" Round Culvert n=0.013 L=36.0' S=0.0056 '/' Outflow=3.93 cfs 0.343 af

Pond 5P: Concrete Galley 8x14 INFILTRATIONPeak Elev=36.33' Storage=0.110 af Inflow=3.93 cfs 0.343 af Discarded=0.76 cfs 0.306 af Primary=1.10 cfs 0.033 af Outflow=1.86 cfs 0.339 af

Pond 6P: Drain Manhole #1

Peak Elev=35.66' Inflow=2.22 cfs 0.190 af

12.0" Round Culvert n=0.013 L=48.0' S=0.0056 '/' Outflow=2.22 cfs 0.190 af

Pond 7P: Drain Manhole #2

Peak Elev=35.71' Inflow=1.10 cfs 0.033 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=1.10 cfs 0.033 af

Pond 8P: Concrete Galley 8x14 STORAGE

Peak Elev=35.60' Storage=0.059 af Inflow=2.22 cfs 0.223 af Primary=1.59 cfs 0.222 af Secondary=0.00 cfs 0.000 af Outflow=1.59 cfs 0.222 af

Pond 9P: Drain Manhole #3 Peak Elev=32.48' Inflow=1.59 cfs 0.222 af

12.0" Round Culvert n=0.013 L=85.0' S=0.0059 '/' Outflow=1.59 cfs 0.222 af

210	47-P	ROP	OSED

Type III 24-hr 25 Yr 24 Hr(+15%) Rainfall=7.12"

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Peak Elev=31.95' Inflow=1.59 cfs 0.222 af Pond 10P: Drain Manhole #4 12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=1.59 cfs 0.222 af

Peak Elev=36.67' Inflow=0.35 cfs 0.026 af Pond 11P: Yard Drain #1 8.0" Round Culvert n=0.013 L=40.0' S=0.0055 '/' Outflow=0.35 cfs 0.026 af

Peak Elev=39.05' Storage=4 cf Inflow=0.19 cfs 0.017 af Pond 12P: Yard Drain #2 Primary=0.19 cfs 0.017 af Secondary=0.00 cfs 0.000 af Outflow=0.19 cfs 0.017 af

Peak Elev=36.62' Inflow=2.39 cfs 0.213 af Pond 13P: Yard Drain #3 15.0" Round Culvert n=0.013 L=48.0' S=0.0052 '/' Outflow=2.39 cfs 0.213 af

Peak Elev=36.76' Inflow=0.18 cfs 0.013 af Pond 14P: Yard Drain #4 8.0" Round Culvert n=0.013 L=40.0' S=0.0100 '/' Outflow=0.18 cfs 0.013 af

Peak Elev=30.87' Storage=0.005 af Inflow=0.14 cfs 0.012 af Pond 15P: Subsurface Stone Infiltration Discarded=0.02 cfs 0.012 af Primary=0.00 cfs 0.000 af Outflow=0.02 cfs 0.012 af

Peak Elev=33.11' Storage=0.003 af Inflow=0.13 cfs 0.011 af Pond 16P: Subsurface Stone Infiltration Discarded=0.03 cfs 0.011 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.011 af

Peak Elev=30.16' Inflow=0.90 cfs 0.075 af Pond 17P: Deep Sump CB #4

12.0" Round Culvert n=0.013 L=67.0' S=0.0060 '/' Outflow=0.90 cfs 0.075 af

Peak Elev=29.72' Inflow=0.44 cfs 0.037 af Pond 18P: Deep Sump CB #5

12.0" Round Culvert n=0.013 L=3.0' S=0.0167 '/' Outflow=0.44 cfs 0.037 af

Peak Elev=30.39' Inflow=0.70 cfs 0.059 af Pond 19P: Deep Sump CB #3

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.70 cfs 0.059 af

Peak Elev=29.66' Inflow=1.50 cfs 0.343 af Pond 20P: Contech Jellyfish

15.0" Round Culvert n=0.013 L=42.0' S=0.0060 '/' Outflow=1.50 cfs 0.343 af

Peak Elev=30.96' Storage=5,086 cf Inflow=2.00 cfs 0.312 af Pond 21P: Wetland Ponding Area Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Tertiary=1.35 cfs 0.230 af Outflow=1.35 cfs 0.230 af

> Total Runoff Area = 2.921 ac Runoff Volume = 1.169 af Average Runoff Depth = 4.80" 53.89% Pervious = 1.574 ac 46.11% Impervious = 1.347 ac

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Time span=0.00-24.00 hrs, dt=0.05 hrs, 481 points x 3
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Dyn-Stor-Ind method

Subcatchment1S: Subcatchment1S	Runoff Area=13,938 sf 18.32% Impervious Runoff Depth>4.56" Flow Length=48' Tc=6.6 min CN=67 Runoff=1.65 cfs 0.122 af
Subcatchment2S: Subcatchment2S	Runoff Area=14,773 sf 41.02% Impervious Runoff Depth>6.95" Flow Length=126' Tc=12.0 min CN=87 Runoff=2.16 cfs 0.197 af
Subcatchment3S: Subcatchment3S	Runoff Area=8,436 sf 21.48% Impervious Runoff Depth>4.80" Tc=6.0 min CN=69 Runoff=1.07 cfs 0.077 af
Subcatchment4S: Subcatchment4S	Runoff Area=5,429 sf 56.24% Impervious Runoff Depth>6.23" Flow Length=87' Tc=13.2 min CN=81 Runoff=0.70 cfs 0.065 af
Subcatchment5S: Subcatchment5S	Runoff Area=6,946 sf 73.74% Impervious Runoff Depth>7.08" Tc=6.0 min CN=88 Runoff=1.22 cfs 0.094 af
Subcatchment6S: Subcatchment6S	Runoff Area=10,412 sf 62.71% Impervious Runoff Depth>7.32" Flow Length=60' Tc=6.0 min CN=90 Runoff=1.87 cfs 0.146 af
Subcatchment7S: Subcatchment7S	Runoff Area=9,749 sf 83.39% Impervious Runoff Depth>7.68" Flow Length=135' Tc=6.0 min CN=93 Runoff=1.79 cfs 0.143 af
Subcatchment8S: Subcatchment8S	Runoff Area=13,276 sf 70.01% Impervious Runoff Depth>7.32" Flow Length=86' Tc=11.2 min CN=90 Runoff=2.05 cfs 0.186 af
Subcatchment9S: Subcatchment15S Flow Length=67	Runoff Area=3,072 sf 26.66% Impervious Runoff Depth>5.76" Slope=0.0160 '/' Tc=7.2 min CN=77 Runoff=0.45 cfs 0.034 af
Subcatchment 10S: Subcatchment 16S Flow Length=83'	Runoff Area=3,155 sf 0.00% Impervious Runoff Depth>3.96" Slope=0.0060 '/' Tc=12.7 min CN=62 Runoff=0.27 cfs 0.024 af
Subcatchment11S: Yard Drain #3 Flow Length=60	Runoff Area=2,881 sf 15.97% Impervious Runoff Depth>4.56" Slope=0.0150 '/' Tc=6.8 min CN=67 Runoff=0.34 cfs 0.025 af
Subcatchment 12S: Subcatchment 18S Flow Length=37	Runoff Area=1,341 sf 25.58% Impervious Runoff Depth>6.48" Slope=0.0190 '/' Tc=6.0 min CN=83 Runoff=0.22 cfs 0.017 af
Subcatchment 13S: Back of Units 1 and 2	Runoff Area=918 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.17 cfs 0.015 af
Subcatchment 14S: Back of Unit 3	Runoff Area=310 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.06 cfs 0.005 af
Subcatchment 15S: East Side of Unit 4	Runoff Area=502 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.09 cfs 0.008 af
Subcatchment 16S: Subcatchment 16S	Runoff Area=1,247 sf 100.00% Impervious Runoff Depth>8.28" Tc=6.0 min CN=98 Runoff=0.23 cfs 0.020 af

all=8.53"
4/

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Runoff Area=2,806 sf 100.00% Impervious Runoff Depth>8.28" Subcatchment 17S: Subcatchment 17S Tc=6.0 min CN=98 Runoff=0.53 cfs 0.044 af

Runoff Area=4,475 sf 100.00% Impervious Runoff Depth>8.28" Subcatchment 18S: Subcatchment 18S Tc=6.0 min CN=98 Runoff=0.84 cfs 0.071 af

Runoff Area=23,588 sf 18.01% Impervious Runoff Depth>4.19" Subcatchment 19S: Subcatchment 19S Flow Length=137' Tc=16.7 min CN=64 Runoff=1.92 cfs 0.189 af

Avg. Flow Depth=0.91' Max Vel=0.83 fps Inflow=2.16 cfs 0.197 af Reach 1R: Swale n=0.150 L=140.0' S=0.0214 '/' Capacity=2.65 cfs Outflow=2.07 cfs 0.196 af

Inflow=1.92 cfs 0.189 af **Reach AP1: Wooded Depression** Outflow=1.92 cfs 0.189 af

Inflow=2.07 cfs 0.196 af Reach AP2: Shoulder of Road Outflow=2.07 cfs 0.196 af

Inflow=1.07 cfs 0.077 af Reach AP3: Detention Pond Outflow=1.07 cfs 0.077 af

Inflow=0.70 cfs 0.065 af Reach AP4: Rear of Site Outflow=0.70 cfs 0.065 af

Inflow=2.40 cfs 0.478 af Reach AP5: Across Street Outflow=2.40 cfs 0.478 af

Peak Elev=36.75' Storage=289 cf Inflow=1.22 cfs 0.094 af Pond 1P: Bioretention #1 Primary=1.06 cfs 0.092 af Secondary=0.00 cfs 0.000 af Outflow=1.06 cfs 0.092 af

Peak Elev=37.27' Storage=561 cf Inflow=1.87 cfs 0.146 af Pond 2P: Bioretention #2

Primary=1.29 cfs 0.144 af Secondary=0.00 cfs 0.000 af Outflow=1.29 cfs 0.144 af

Peak Elev=37.51' Inflow=2.44 cfs 0.220 af Pond 3P: Catch Basin #1 15.0" Round Culvert n=0.013 L=47.0' S=0.0053 '/' Outflow=2.44 cfs 0.220 af

Peak Elev=37.27' Inflow=4.86 cfs 0.429 af Pond 4P: Catch Basin #2 15.0" Round Culvert n=0.013 L=36.0' S=0.0056 '/' Outflow=4.86 cfs 0.429 af

Pond 5P: Concrete Galley 8x14 INFILTRATIONPeak Elev=36.86' Storage=0.125 af Inflow=4.86 cfs 0.429 af

Peak Elev=36.79' Inflow=2.35 cfs 0.236 af

Pond 6P: Drain Manhole #1 12.0" Round Culvert n=0.013 L=48.0' S=0.0056 '/' Outflow=2.35 cfs 0.236 af

Peak Elev=36.75' Inflow=1.90 cfs 0.070 af Pond 7P: Drain Manhole #2 12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=1.90 cfs 0.070 af

Peak Elev=36.26' Storage=0.073 af Inflow=3.62 cfs 0.305 af Pond 8P: Concrete Galley 8x14 STORAGE Primary=2.10 cfs 0.304 af Secondary=0.00 cfs 0.000 af Outflow=2.10 cfs 0.304 af

Peak Elev=32.75' Inflow=2.10 cfs 0.304 af Pond 9P: Drain Manhole #3

12.0" Round Culvert n=0.013 L=85.0' S=0.0059'/ Outflow=2.10 cfs 0.304 af

Discarded=0.83 cfs 0.353 af Primary=1.90 cfs 0.070 af Outflow=2.70 cfs 0.423 af

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Pond 10P: Drain Manhole #4 Peak Elev=32.13' Inflow=2.10 cfs 0.304 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=2.10 cfs 0.304 af

Pond 11P: Yard Drain #1 Peak Elev=37.85' Inflow=0.45 cfs 0.034 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0055 '/' Outflow=0.45 cfs 0.034 af

Pond 12P: Yard Drain #2 Peak Elev=39.07' Storage=6 cf Inflow=0.27 cfs 0.024 af

Primary=0.27 cfs 0.024 af Secondary=0.00 cfs 0.000 af Outflow=0.27 cfs 0.024 af

Pond 13P: Yard Drain #3 Peak Elev=37.69' Inflow=3.00 cfs 0.269 af

15.0" Round Culvert n=0.013 L=48.0' S=0.0052 '/' Outflow=3.00 cfs 0.269 af

Pond 14P: Yard Drain #4 Peak Elev=37.28' Inflow=0.22 cfs 0.017 af

8.0" Round Culvert n=0.013 L=40.0' S=0.0100 '/' Outflow=0.22 cfs 0.017 af

Pond 15P: Subsurface Stone Infiltration Peak Elev=31.61' Storage=0.006 af Inflow=0.17 cfs 0.015 af

Discarded=0.03 cfs 0.014 af Primary=0.00 cfs 0.000 af Outflow=0.03 cfs 0.014 af

Pond 16P: Subsurface Stone Infiltration Peak Elev=33.39' Storage=0.004 af Inflow=0.15 cfs 0.013 af

Discarded=0.04 cfs 0.013 af Primary=0.00 cfs 0.000 af Outflow=0.04 cfs 0.013 af

Pond 17P: Deep Sump CB #4 Peak Elev=30.24' Inflow=1.07 cfs 0.091 af

12.0" Round Culvert n=0.013 L=67.0' S=0.0060'/' Outflow=1.07 cfs 0.091 af

Pond 18P: Deep Sump CB #5 Peak Elev=29.90' Inflow=0.53 cfs 0.044 af

12.0" Round Culvert n=0.013 L=3.0' S=0.0167 '/' Outflow=0.53 cfs 0.044 af

Pond 19P: Deep Sump CB #3 Peak Elev=30.47' Inflow=0.84 cfs 0.071 af

12.0" Round Culvert n=0.013 L=40.0' S=0.0050 '/' Outflow=0.84 cfs 0.071 af

Pond 20P: Contech Jellyfish Peak Elev=29.89' Inflow=2.40 cfs 0.478 af

15.0" Round Culvert n=0.013 L=42.0' S=0.0060'/' Outflow=2.40 cfs 0.478 af

Pond 21P: Wetland Ponding Area Peak Elev=31.18' Storage=5,810 cf Inflow=2.73 cfs 0.426 af Primary=0.00 cfs 0.000 af Secondary=0.00 cfs 0.000 af Tertiary=2.20 cfs 0.343 af Outflow=2.20 cfs 0.343 af

Total Runoff Area = 2.921 ac Runoff Volume = 1.481 af Average Runoff Depth = 6.08" 53.89% Pervious = 1.574 ac 46.11% Impervious = 1.347 ac

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Summary for Subcatchment 1S: Subcatchment 1S

Runoff = 1.65 cfs @ 12.10 hrs, Volume=

0.122 af, Depth> 4.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

Α	rea (sf)	CN [Description					
	586	98 F	Paved roads w/curbs & sewers, HSG B					
	1,864	55 \	Noods, Go	od, HSG B				
	3,396				ood, HSG B			
	611	80 >	>75% Gras	s cover, Go	ood, HSG D			
	541			od, HSG D				
	3,408		Noods, Go					
	1,564	61 :	>75% Gras	s cover, Go	ood, HSG B			
	1,600		Roofs, HSG					
	368	98 I	Roofs, HSG	3 D				
	13,938	67 \	Neighted A	verage				
	11,384	8	31.68% Pei	rvious Area				
	2,554	•	18.32% Imp	pervious Ar	ea			
Tç	Length	Slope		Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
5.1	32	0.0625	0.10		Sheet Flow,			
					Woods: Light underbrush	n= 0.400	P2= 3.70"	
1.5	16	0.3300	0.18		Sheet Flow,			
					Woods: Light underbrush	n= 0.400	P2= 3.70"	
6.6	48	Total						

Summary for Subcatchment 2S: Subcatchment 2S

Runoff = 2.16 cfs @ 12.16 hrs, Volume=

0.197 af, Depth> 6.95"

	Area (sf)	CN	Description
	4,812	80	>75% Grass cover, Good, HSG D
	319	Paved roads w/curbs & sewers, HSG D	
	2,823	98	Roofs, HSG D
*	186	98	Ledge Outcrop, HSG D
	3,901	80	>75% Grass cover, Good, HSG D
	2,732	98	Roofs, HSG D
	14,773	87	Weighted Average
	8,713		58.98% Pervious Area
	6,060		41.02% Impervious Area

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.2	38	0.1000	0.29		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
0.7	17	0.3300	0.39		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
9.1	71	0.0100	0.13		Sheet Flow,
					Grass: Short n= 0.150 P2= 3.70"
12.0	126	Total			

Summary for Subcatchment 3S: Subcatchment 3S

Runoff =

1.07 cfs @ 12.09 hrs, Volume=

0.077 af, Depth> 4.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN	Description						
	6,481	61	>75% Gras	75% Grass cover, Good, HSG B					
	143	55	Woods, Go	Voods, Good, HSG B					
	1,812	98	Roofs, HSC	Roofs, HSG B					
	8,436	69	Weighted Average						
	6,624		78.52% Per	vious Area					
	1,812		21.48% Imp	21.48% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft		Capacity (cfs)	Description				
6.0			2007		Direct Entry,				

Summary for Subcatchment 4S: Subcatchment 4S

Runoff =

0.70 cfs @ 12.18 hrs, Volume=

0.065 af, Depth> 6.23"

	Area (sf)	CN	Description
*	2,343	98	Ledge Outcrop, HSG D
	73	77	Woods, Good, HSG D
	917	55	Woods, Good, HSG B
	1,386	61	>75% Grass cover, Good, HSG B
	710	98	Roofs, HSG B
-	5,429	81	Weighted Average
	2,376		43.76% Pervious Area
	3,053		56.24% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.2	38	0.2100	3.12		Sheet Flow,
0.8	7	0.2860	0.14		Smooth surfaces n= 0.011 P2= 3.70" Sheet Flow,
0.0	•	0.2000	0.11		Woods: Light underbrush n= 0.400 P2= 3.70"
12.2	42	0.0120	0.06		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 3.70"
13.2	87	Total			VVOOds. Light underbrush in o. 100 1 2 0.70

Summary for Subcatchment 5S: Subcatchment 5S

Runoff = 1.22 cfs @ 12.09 hrs, Volume=

0.094 af, Depth> 7.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN	Description					
	1,824	61	>75% Grass cover, Good, HSG B					
	14		Paved park					
	3,268	98	Paved parking, HSG B					
	1,840	98	Roofs, HSG B					
	6,946	88	88 Weighted Average					
	1,824		26.26% Pervious Area					
	5,122		73.74% lmp					
Tc	Length	Slope		Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Summary for Subcatchment 6S: Subcatchment 6S

Runoff = 1.87 cfs @ 12.09 hrs, Volume=

0.146 af, Depth> 7.32"

Area (sf)	CN	Description
687	61	>75% Grass cover, Good, HSG B
1,334	98	Paved parking, HSG B
2,813	98	Paved parking, HSG D
3,196	80	>75% Grass cover, Good, HSG D
2,382	98	Roofs, HSG D
10,412	90	Weighted Average
3,883		37.29% Pervious Area
6,529		62.71% Impervious Area

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
•	1.7	20	0.0500	0.19	3/	Sheet Flow,
						Grass: Short n= 0.150 P2= 3.70"
	0.7	40	0.0100	0.93		Sheet Flow,
						Smooth surfaces n= 0.011 P2= 3.70"
	2.4	60	Total, I	ncreased t	o minimum	Tc = 6.0 min

Summary for Subcatchment 7S: Subcatchment 7S

Runoff = 1.79 cfs @ 12.09 hrs, Volume=

0.143 af, Depth> 7.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN [Description				
	1,935	98 F	Roofs, HSG B				
	2,857	98 F	Paved parking, HSG B				
	1,047	61 >	·75% Gras	s cover, Go	ood, HSG B		
	857		Roofs, HSG				
	2,481		Paved parking, HSG D				
	572	80 >	75% Gras	s cover, Go	ood, HSG D		
	9,749	93 V	Veighted A	verage			
	1,619			vious Area			
	8,130	8	13.39% lmp	pervious Ar	ea		
_							
		01		<u> </u>	5		
Tc	Length	Slope	Velocity	Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	Capacity (cfs)	Description		
10 . 25					Sheet Flow,		
(min) 4.6	(feet) 40	(ft/ft) 0.0175	(ft/sec) 0.14		Sheet Flow, Grass: Short n= 0.150 P2= 3.70"		
(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow, Grass: Short n= 0.150 P2= 3.70" Sheet Flow,		
(min) 4.6 1.0	(feet) 40 60	(ft/ft) 0.0175 0.0100	0.14 1.01		Sheet Flow, Grass: Short n= 0.150 P2= 3.70" Sheet Flow, Smooth surfaces n= 0.011 P2= 3.70"		
(min) 4.6	(feet) 40	(ft/ft) 0.0175	(ft/sec) 0.14		Sheet Flow, Grass: Short n= 0.150 P2= 3.70" Sheet Flow, Smooth surfaces n= 0.011 P2= 3.70" Shallow Concentrated Flow,		
(min) 4.6 1.0	(feet) 40 60	(ft/ft) 0.0175 0.0100 0.0100	(ft/sec) 0.14 1.01 2.03	(cfs)	Sheet Flow, Grass: Short n= 0.150 P2= 3.70" Sheet Flow, Smooth surfaces n= 0.011 P2= 3.70"		

Summary for Subcatchment 8S: Subcatchment 8S

Runoff = 2.05 cfs @ 12.15 hrs, Volume=

0.186 af, Depth> 7.32"

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	A	rea (sf)	CN E	Description								
		1,788	61 >	51 >75% Grass cover, Good, HSG B								
		4,412	98 F	Paved parki	ing, HSG B	,						
		1,219	98 F	Roofs, HSG	βB							
		2,194	80 >									
*		1,608	98 L	98 Ledge Outcrop, HSG D								
		39	98 F	98 Paved parking, HSG D								
		2,016	98 F	98 Roofs, HSG D								
		13,276	90 V	90 Weighted Average								
		3,982	2	29.99% Pervious Area								
		9,294	7	70.01% Impervious Area								
	Тс	_	Slope	Velocity	Capacity	Description						
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)							
	3.3	40	0.0400	0.20		Sheet Flow,						
						Grass: Short	n= 0.150	P2= 3.70"				
	2.5	20	0.0200	0.13		Sheet Flow,						
						Grass: Short	n= 0.150	P2= 3.70"				
	5.4	26	0.0050	0.08		Sheet Flow,		DO 0 70"				
_						Grass: Short	n= 0.150	P2= 3.70"				
	11.2	86	Total									

Summary for Subcatchment 9S: Subcatchment 15S

Runoff = 0.45 cfs @ 12.10 hrs, Volume=

0.034 af, Depth> 5.76"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN	Description							
	1,238	61	>75% Gras	s cover, Go	ood, HSG B					
	1,015	80	>75% Grass cover, Good, HSG D							
	72	98	Roofs, HSG B							
	747	98	8 Roofs, HSG D							
	3,072	77	77 Weighted Average							
	2,253		73.34% Per	vious Area	l					
	819		26.66% Imp	pervious Ar	ea					
Tc	Length	Slope		Capacity	Description					
(min)	(feet)	(ft/ft) (ft/sec)	(cfs)						
7.2	67	0.0160	0.15		Sheet Flow,					
					Grass: Short	n= 0.150	P2= 3.70"			

Summary for Subcatchment 10S: Subcatchment 16S

Runoff = 0.27 cfs @ 12.18 hrs, Volume=

0.024 af, Depth> 3.96"

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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	Area (sf)	CN	Description								
8	2,918	61	>75% Gras	75% Grass cover, Good, HSG B							
	237	80	>75% Gras	75% Grass cover, Good, HSG D							
	3,155	62	Weighted A	Veighted Average							
	3,155		100.00% Pervious Area								
	Tc Length	Slope	,	Capacity	Description						
(m	n) (feet)	(ft/ft) (ft/sec)	(cfs)							
12	2.7 83	0.0060	0.11		Sheet Flow,						
					Grass: Short	n= 0.150	P2= 3.70"				

Summary for Subcatchment 11S: Yard Drain #3

Runoff = 0.34 cfs @ 12.10 hrs, Volume=

0.025 af, Depth> 4.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

A	rea (sf)	CN	Description									
	2,421	61	>75% Gras	75% Grass cover, Good, HSG B								
	460	98	Roofs, HSG	Roofs, HSG B								
	2,881	67	Veighted Average									
	2,421		84.03% Pervious Area									
	460		15.97% lmp									
To	Longth	Clone	\/olooitr	Conocity	Description							
Tc	Length	Slope		Capacity	Description							
(min)	(feet)	(ft/ft)		(cfs)								
6.8	60	0.0150	0.15		Sheet Flow,							
					Grass: Short	n= 0.150	P2= 3.70"					

Summary for Subcatchment 12S: Subcatchment 18S

Runoff = 0.22 cfs @ 12.09 hrs, Volume=

0.017 af, Depth> 6.48"

Area (sf)	CN	Description			
94	>75% Grass cover, Good, HSG B				
904 80 >75% Grass cover, Good, HSG D					
11	Roofs, HSG B				
 332	Roofs, HSG D				
1,341	83	Weighted Average			
998		74.42% Pervious Area			
343		25.58% Impervious Area			

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
4.2	37	0.0190	0.15		Sheet Flow, Grass: Short n= 0.150 P2= 3.70"

4.2 37 Total, Increased to minimum Tc = 6.0 min

Summary for Subcatchment 13S: Back of Units 1 and 2

Runoff = 0.17 cfs @ 12.09 hrs, Volume=

0.015 af, Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

	Α	rea (sf)	CN I	Description					
		918	98	Roofs, HSG	B				
		918 100.00% Impervious Area							
(n	Tc nin)	Length (feet)	Slope (ft/ft)	•	Capacity (cfs)	Description			
	6.0					Direct Entry,			

Summary for Subcatchment 14S: Back of Unit 3

Runoff = 0.06 cfs @ 12.09 hrs, Volume=

0.005 af, Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

	Α	rea (sf)	CN [Description					
-		310	98 F	Roofs, HSC	G D				
-		310 100.00% Impervious Area							
	Тс	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	6.0					Direct Entry.			

Summary for Subcatchment 15S: East Side of Unit 4

Runoff = 0.09 cfs @ 12.09 hrs, Volume=

0.008 af, Depth> 8.28"

Area (sf)	CN		
500	98	Roofs, HSG B	
2	98	Roofs, HSG D	
502 98 Weighted Average 502 100.00% Impervious Are		Weighted Average 100.00% Impervious Area	

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Тс	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.0		Direct Entry,			

Summary for Subcatchment 16S: Subcatchment 16S

Runoff = 0.23 cfs @ 12.09 hrs, Volume=

0.020 af, Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

Α	rea (sf)	CN [Description					
	1,247	98 F	aved road	aved roads w/curbs & sewers, HSG B				
	1,247	1	100.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
6.0					Direct Entry,			

Summary for Subcatchment 17S: Subcatchment 17S

Runoff = 0.53 cfs @ 12.09 hrs, Volume=

0.044 af, Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

ΑΑ	rea (sf)	CN	Description						
:17	2,230	98	Paved park	aved parking, HSG B					
	576	98	Paved park	aved parking, HSG D					
	2,806	98	Weighted A	eighted Average					
	2,806		100.00% lm	00.00% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft	tract Date: Control	Capacity (cfs)	Description				
	(leet)	(IVII) (10560)	(CIS)		_			
6.0					Direct Entry,				

Summary for Subcatchment 18S: Subcatchment 18S

Runoff = 0.84 cfs @ 12.09 hrs, Volume=

0.071 af. Depth> 8.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

Area (sf)	CN	Description	
4,475	98	Paved parking, HSG B	
4,475		100.00% Impervious Area	

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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		Velocity (ft/sec)	Description
6.0			Direct Entry

Summary for Subcatchment 19S: Subcatchment 19S

Runoff =

1.92 cfs @ 12.24 hrs, Volume=

0.189 af, Depth> 4.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

Α	rea (sf)	CN D	escription		
	4,147	98 F	aved park	ing, HSG B	
	4,462	61 >	75% Grass	s cover, Go	ood, HSG B
	102	98 F	Roofs, HSG	ВВ	
	14,877	55 V	Voods, Go	od, HSG B	
	23,588	64 V	Veighted A	verage	
	19,339	-		vious Area	
	4,249	1	8.01% lmp	pervious Ar	ea
Tc	Length	Slope	Velocity	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
16.0	100	0.0350	0.10		Sheet Flow,
					Woods: Light underbrush n= 0.400 P2= 3.70"
0.7	37	0.0300	0.87		Shallow Concentrated Flow,
					Woodland Kv= 5.0 fps
16.7	137	Total			

Summary for Reach 1R: Swale

Inflow Area =

0.339 ac, 41.02% Impervious, Inflow Depth > 6.95" for 50 Yr 24 Hr(+15%) event

Inflow = Outflow =

2.16 cfs @ 12.16 hrs, Volume= 2.07 cfs @ 12.20 hrs, Volume= 0.197 af 0.196 af, Atten= 4%, Lag= 2.3 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Max. Velocity= 0.83 fps, Min. Travel Time= 2.8 min

Avg. Velocity = 0.34 fps, Avg. Travel Time= 6.9 min

Peak Storage= 349 cf @ 12.20 hrs

Average Depth at Peak Storage= 0.91', Surface Width= 5.47' Bank-Full Depth= 1.00' Flow Area= 3.0 sf, Capacity= 2.65 cfs

0.00' x 1.00' deep channel, n= 0.150 Sheet flow over Short Grass

Side Slope Z-value= 3.0 '/' Top Width= 6.00'

Length= 140.0' Slope= 0.0214 '/'

Inlet Invert= 40.00', Outlet Invert= 37.00'

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Summary for Reach AP1: Wooded Depression

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.542 ac, 18.01% Impervious, Inflow Depth > 4.19" for 50 Yr 24 Hr(+15%) event

Inflow = 1.92 cfs @ 12.24 hrs, Volume= 0.189 af

Outflow = 1.92 cfs @ 12.24 hrs, Volume= 0.189 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP2: Shoulder of Road

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.339 ac, 41.02% Impervious, Inflow Depth > 6.94" for 50 Yr 24 Hr(+15%) event

Inflow = 2.07 cfs @ 12.20 hrs, Volume= 0.196 af

Outflow = 2.07 cfs @ 12.20 hrs, Volume= 0.196 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP3: Detention Pond

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.720 ac, 49.10% Impervious, Inflow Depth > 0.54" for 50 Yr 24 Hr(+15%) event

Inflow = 1.07 cfs @ 12.09 hrs, Volume= 0.077 af

Outflow = 1.07 cfs @ 12.09 hrs, Volume= 0.077 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Reach AP4: Rear of Site

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.125 ac, 56.24% Impervious, Inflow Depth > 6.23" for 50 Yr 24 Hr(+15%) event

Inflow = 0.70 cfs @ 12.18 hrs, Volume= 0.065 af

Outflow = 0.70 cfs @ 12.18 hrs, Volume= 0.065 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs. dt= 0.05 hrs / 3

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Summary for Reach AP5: Across Street

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.196 ac,100.00% Impervious, Inflow Depth > 29.31" for 50 Yr 24 Hr(+15%) event

Inflow = 2.40 cfs @ 12.52 hrs, Volume= 0.478 af

Outflow = 2.40 cfs @ 12.52 hrs, Volume= 0.478 af, Atten= 0%, Lag= 0.0 min

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Summary for Pond 1P: Bioretention #1

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=1)

Inflow Area = 0.159 ac, 73.74% Impervious, Inflow Depth > 7.08" for 50 Yr 24 Hr(+15%) event

Inflow = 1.22 cfs @ 12.09 hrs, Volume= 0.094 af

Outflow = 1.06 cfs @ 12.10 hrs, Volume= 0.092 af, Atten= 13%, Lag= 0.5 min

Primary = 1.06 cfs @ 12.10 hrs, Volume= 0.092 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 36.75' @ 12.49 hrs Surf.Area= 400 sf Storage= 289 cf

Plug-Flow detention time= 28.5 min calculated for 0.092 af (97% of inflow)

Center-of-Mass det. time= 13.5 min (793.2 - 779.6)

Volume	Invert Ava	il.Storage	Storage Descripti	ion	
#1	33.99'	694 cf	Custom Stage D	ata (Prismatic)	Listed below (Recalc)
Elevation	Surf.Area	Voids	Inc.Store	Cum.Store	
Elevation				(cubic-feet)	
(feet)	(sq-ft)	(%)	(cubic-feet)	(cubic-leet)	
33.99	315	0.0	0	0	
34.00	315	40.0	1	1	
34.99	315	40.0	125	126	
35.00	315	15.0	0	126	
36.49	315	15.0	70	197	
36.50	315	100.0	3	200	
37.00	484	100.0	200	400	
37.50	668	100.0	288	688	
37.51	668	100.0	7	694	
Device Rou	uting In	vert Out	let Devices		
			Pound Culvert		

Device	Routing	Invert	Outlet Devices
#1	Primary	34.58'	8.0" Round Culvert
	•		L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.58' / 34.40' S= 0.0045 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Device 1	34.75	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	37.30'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	37.50'	31.0' long x 4.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00 3.50 4.00 4.50 5.00 5.50

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Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32

Primary OutFlow Max=1.06 cfs @ 12.10 hrs HW=36.49' TW=35.24' (Dynamic Tailwater)

-1=Culvert (Passes 1.06 cfs of 1.48 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.06 cfs @ 5.38 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=33.99' TW=28.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: Bioretention #2

[87] Warning: Oscillations may require smaller dt or Finer Routing (severity=3)

Inflow Area = 0.239 ac, 62.71% Impervious, Inflow Depth > 7.32" for 50 Yr 24 Hr(+15%) event 1.87 cfs @ 12.09 hrs, Volume= 0.146 af

Outflow = 1.29 cfs @ 12.09 hrs, Volume= 0.144 af, Atten= 31%, Lag= 0.3 min

Primary = 1.29 cfs @ 12.09 hrs, Volume= 0.144 af

Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 37.27' @ 12.22 hrs Surf.Area= 738 sf Storage= 561 cf

Plug-Flow detention time= 19.5 min calculated for 0.144 af (99% of inflow) Center-of-Mass det. time= 11.5 min (785.1 - 773.6)

Volume	Invert Ava	il.Storage	Storage Descrip	tion		
#1	34.49'	1,249 cf	Custom Stage	Data (Prismatic)Listed	below (Recalc)	
Elevation	Surf.Area	Voids	Inc.Store	Cum.Store		
(feet)	(sq-ft)	(%)	(cubic-feet)	(cubic-feet)		
34.49	600	0.0	0	0		
34.50	600	40.0	2	2		
35.49	600	40.0	238	240		
35.50	600	15.0	1	241		
36.99	600	15.0	134	375		
37.00	600	100.0	6	381		
38.00	1,113	100.0	857	1,237		
38.01	1,113	100.0	11	1,249		
Device Routing Invert Outlet Devices						

Device	Routing	invert	Outlet Devices
#1	Primary	34.58'	8.0" Round Culvert
			L= 33.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.58' / 34.40' S= 0.0055 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf
#2	Device 1	34.75'	6.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Device 1	37.70'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	38.00'	13.0' long x 4.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50, 3.00, 3.50, 4.00, 4.50, 5.00, 5.50

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Coef. (English) 2.38 2.54 2.69 2.68 2.67 2.67 2.65 2.66 2.66 2.68 2.72 2.73 2.76 2.79 2.88 3.07 3.32

Primary OutFlow Max=1.28 cfs @ 12.09 hrs HW=37.06' TW=35.23' (Dynamic Tailwater)

-1=Culvert (Passes 1.28 cfs of 1.80 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 1.28 cfs @ 6.52 fps)

-3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=34.49' TW=0.00' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: Catch Basin #1

[80] Warning: Exceeded Pond 11P by 0.20' @ 12.10 hrs (0.59 cfs 0.005 af)

0.375 ac, 61.86% Impervious, Inflow Depth > 7.02" for 50 Yr 24 Hr(+15%) event Inflow Area =

2.44 cfs @ 12.14 hrs, Volume= 0.220 af Inflow

2.44 cfs @ 12.14 hrs, Volume= 0.220 af, Atten= 0%, Lag= 0.0 min Outflow

2.44 cfs @ 12.14 hrs, Volume= 0.220 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.51' @ 12.20 hrs

Flood Elev= 38.50'

Device	Routing	Invert	Outlet Devices
#1	Primary		15.0" Round Culvert L= 47.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 35.00' / 34.75' S= 0.0053'/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=0.00 cfs @ 12.14 hrs HW=37.34' TW=37.59' (Dynamic Tailwater) -1=Culvert (Controls 0.00 cfs)

Summary for Pond 4P: Catch Basin #2

[80] Warning: Exceeded Pond 14P by 0.01' @ 12.30 hrs (0.12 cfs 0.001 af)

0.768 ac, 56.90% Impervious, Inflow Depth > 6.69" for 50 Yr 24 Hr(+15%) event Inflow Area =

4.86 cfs @ 12.11 hrs, Volume= 0.429 af Inflow

4.86 cfs @ 12.11 hrs, Volume= 0.429 af, Atten= 0%, Lag= 0.0 min Outflow

0.429 af 4.86 cfs @ 12.11 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.27' @ 12.18 hrs

Flood Elev= 38.80'

Device	Routing	Invert	Outlet Devices
#1	Primary	•	15.0" Round Culvert L= 36.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 34.30' / 34.10' S= 0.0056 '/' Cc= 0.900 n= 0.013 Corrugated PE smooth interior. Flow Area= 1.23 sf

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Primary OutFlow Max=4.77 cfs @ 12.11 hrs HW=36.94' TW=35.90' (Dynamic Tailwater) 1=Culvert (Inlet Controls 4.77 cfs @ 3.89 fps)

Summary for Pond 5P: Concrete Galley 8x14 INFILTRATION

[80] Warning: Exceeded Pond 4P by 0.01' @ 12.50 hrs (0.51 cfs 0.002 af)

Inflow Area = 0.768 ac, 56.90% Impervious, Inflow Depth > 6.69" for 50 Yr 24 Hr(+15%) event lnflow = 4.86 cfs @ 12.11 hrs, Volume= 0.429 af Outflow = 2.70 cfs @ 12.22 hrs, Volume= 0.423 af, Atten= 44%, Lag= 6.2 min 0.83 cfs @ 12.40 hrs, Volume= 0.353 af Primary = 1.90 cfs @ 12.21 hrs, Volume= 0.070 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 36.86' @ 12.40 hrs Surf.Area= 0.071 ac Storage= 0.125 af

Plug-Flow detention time= 69.4 min calculated for 0.422 af (98% of inflow) Center-of-Mass det. time= 61.1 min (843.7 - 782.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	33.90'	0.000 af	24.00'W x 42.00'L x 3.67'H Field A
			0.085 af Overall - 0.085 af Embedded = 0.000 af x 40.0% Voids
#2A	33.90'	0.062 af	Shea Leaching Chamber 8x14x3.7 x 9 Inside #1
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf
			9 Chambers in 3 Rows
#3	30.90'	0.035 af	28.00'W x 46.00'L x 3.00'H Prismatoid
			0.089 af Overall x 40.0% Voids
#4	30.90'	0.007 af	8.00'W x 32.00'L x 3.00'H Prismatoid
			0.018 af Overall x 40.0% Voids
#5	33.90'	0.010 af	2.00'W x 148.00'L x 3.67'H Prismatoid
			0.025 af Overall x 40.0% Voids
#6B	33.90'	0.000 af	8.00'W x 28.00'L x 3.67'H Field B
			0.019 af Overall - 0.019 af Embedded = 0.000 af \times 40.0% Voids
#7B	33.90'	0.014 af	Shea Leaching Chamber 8x14x3.7 x 2 Inside #6
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf
		0.400 - 6	Talaka Nati Ot

0.128 af Total Available Storage

Storage Group A created with Chamber Wizard Storage Group B created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	30.90'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 30.82' Phase-In= 0.01'
#2	Primary	35.70'	12.0" Round Culvert
			L= 60.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 35.70' / 34.30' S= 0.0233 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf
#3	Primary	37.56'	160.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00

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2.50 3.00

Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

Discarded OutFlow Max=0.83 cfs @ 12.40 hrs HW=36.86' (Free Discharge) 1=Exfiltration (Controls 0.83 cfs)

Primary OutFlow Max=1.96 cfs @ 12.21 hrs HW=36.63' TW=35.99' (Dynamic Tailwater)

-2=Culvert (Inlet Controls 1.96 cfs @ 2.59 fps)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 6P: Drain Manhole #1

[80] Warning: Exceeded Pond 1P by 0.04' @ 12.50 hrs (0.20 cfs 0.001 af)

Inflow Area = 0.398 ac, 67.12% Impervious, Inflow Depth > 7.10" for 50 Yr 24 Hr(+15%) event

Inflow = 2.35 cfs @ 12.09 hrs, Volume= 0.236 af

Outflow = 2.35 cfs @ 12.09 hrs, Volume= 0.236 af, Atten= 0%, Lag= 0.0 min

Primary = 2.35 cfs @ 12.09 hrs, Volume= 0.236 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 36.79' @ 12.50 hrs

Flood Elev= 38.90'

Device	Routing	Invert	Outlet Devices
#1	Primary		12.0" Round Culvert L= 48.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 34.07' / 33.80' S= 0.0056 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.39 cfs @ 12.09 hrs HW=35.23' TW=34.59' (Dynamic Tailwater)
—1=Culvert (Inlet Controls 2.39 cfs @ 3.04 fps)

Summary for Pond 7P: Drain Manhole #2

Inflow Area = 0.768 ac, 56.90% Impervious, Inflow Depth = 1.09" for 50 Yr 24 Hr(+15%) event

Inflow = 1.90 cfs @ 12.21 hrs, Volume= 0.070 af

Outflow = 1.90 cfs @ 12.21 hrs, Volume= 0.070 af, Atten= 0%, Lag= 0.0 min

Primary = 1.90 cfs @ 12.21 hrs, Volume= 0.070 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 36.75' @ 12.50 hrs

Flood Elev= 39.20'

Device	Routing	Invert	Outlet Devices		
#1	Primary	34.20'	12.0" Round Culvert		
	•		L= 40.0' CPP, projecting, no headwall, Ke= 0.900		
			Inlet / Outlet invert= 34.20' / 34.00' S= 0.0050 '/' Cc= 0.900		
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf		

Primary OutFlow Max=1.91 cfs @ 12.21 hrs HW=35.99' TW=35.58' (Dynamic Tailwater) 1=Culvert (Inlet Controls 1.91 cfs @ 2.43 fps)

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Summary for Pond 8P: Concrete Galley 8x14 STORAGE ONLY

[92] Warning: Device #4 is above defined storage

[80] Warning: Exceeded Pond 6P by 0.01' @ 12.70 hrs (0.31 cfs 0.004 af) [80] Warning: Exceeded Pond 7P by 0.61' @ 13.30 hrs (0.91 cfs 0.022 af)

Inflow Area = 1.167 ac, 60.39% Impervious, Inflow Depth > 3.14" for 50 Yr 24 Hr(+15%) event 1.167 ac, 60.39% Impervious, Inflow Depth > 3.14" for 50 Yr 24 Hr(+15%) event 0.305 af 0.304 af, Atten= 42%, Lag= 14.4 min

Primary = 2.10 cfs @ 12.44 hrs, Volume= 0.304 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 36.26' @ 12.44 hrs Surf.Area= 0.055 ac Storage= 0.073 af

Plug-Flow detention time= 31.6 min calculated for 0.304 af (99% of inflow) Center-of-Mass det. time= 28.4 min (807.3 - 779.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	33.30'	0.000 af	16.00'W x 56.00'L x 3.67'H Field A
			0.075 af Overall - 0.075 af Embedded = 0.000 af x 40.0% Voids
#2A	33.30'	0.055 af	
			Inside= 84.0"W x 36.0"H => 23.08 sf x 13.00'L = 300.0 cf
			Outside= 96.0"W x 44.0"H => 29.36 sf x 14.00'L = 411.0 cf
			8 Chambers in 2 Rows
#3	32.30'	0.011 af	20.00'W x 60.00'L x 1.00'H Prismatoid
			0.028 af Overall x 40.0% Voids
#4	33.30'	0.010 af	2.00'W x 144.00'L x 3.67'H Prismatoid
s			0.024 af Overall x 40.0% Voids
		0.076 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	32.30'	4.0" Round Culvert
			L= 3.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 32.30' / 32.27' S= 0.0100 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.09 sf
#2	Device 1	32.30'	4.0" Vert. Orifice/Grate C= 0.600 Limited to weir flow at low heads
#3	Primary	34.70'	
			L= 3.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 34.70' / 34.67' S= 0.0100 '/' Cc= 0.900
#4	Secondary	39.80'	
			3.30 3.31 3.32
#4	Secondary	39.80'	L= 3.0° CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 34.70′ / 34.67′ S= 0.0100 ′/ Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf 160.0′ long x 1.0′ breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2. 2.50 3.00 Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31 3.30 3.31 3.32

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Primary OutFlow Max=2.09 cfs @ 12.44 hrs HW=36.25' TW=32.70' (Dynamic Tailwater)

1=Culvert (Inlet Controls 0.63 cfs @ 7.16 fps)
2=Orifice/Grate (Passes 0.63 cfs of 0.79 cfs potential flow)

-3=Culvert (Inlet Controls 1.47 cfs @ 4.20 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=32.30' TW=31.60' (Dynamic Tailwater) 4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 9P: Drain Manhole #3

1.167 ac, 60.39% Impervious, Inflow Depth > 3.13" for 50 Yr 24 Hr(+15%) event Inflow Area =

Inflow 2.10 cfs @ 12.44 hrs, Volume= 0.304 af

0.304 af, Atten= 0%, Lag= 0.0 min 2.10 cfs @ 12.44 hrs, Volume= Outflow =

0.304 af 2.10 cfs @ 12.44 hrs, Volume= Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 32.75' @ 12.49 hrs

Flood Elev= 39.90'

Device Routing Invert Outlet Devices 12.0" Round Culvert #1 Primary 31.60' L= 85.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 31.60' / 31.10' S= 0.0059 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.12 cfs @ 12.44 hrs HW=32.70' TW=32.13' (Dynamic Tailwater) 1=Culvert (Outlet Controls 2.12 cfs @ 3.05 fps)

Summary for Pond 10P: Drain Manhole #4

1.167 ac, 60.39% Impervious, Inflow Depth > 3.13" for 50 Yr 24 Hr(+15%) event Inflow Area =

2.10 cfs @ 12.44 hrs, Volume= 0.304 af inflow

0.304 af, Atten= 0%, Lag= 0.0 min 2.10 cfs @ 12.44 hrs, Volume= Outflow =

2.10 cfs @ 12.44 hrs, Volume= 0.304 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 32.13' @ 12.44 hrs

Flood Elev= 36.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	• • • • • • • • • • • • • • • • • • • •	12.0" Round Culvert L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 31.10' / 30.90' S= 0.0050 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=2.09 cfs @ 12.44 hrs HW=32.13' TW=31.11' (Dynamic Tailwater) 1=Culvert (Barrel Controls 2.09 cfs @ 3.21 fps)

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Summary for Pond 11P: Yard Drain #1

Inflow Area = 0.071 ac, 26.66% Impervious, Inflow Depth > 5.76" for 50 Yr 24 Hr(+15%) event

0.45 cfs @ 12.10 hrs, Volume= Inflow 0.034 af

0.45 cfs @ 12.10 hrs, Volume= 0.45 cfs @ 12.10 hrs, Volume= 0.034 af, Atten= 0%, Lag= 0.0 min Outflow =

Primary = 0.034 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.85' @ 12.20 hrs

Flood Elev= 39.00'

Device	Routing	Invert	Outlet Devices	
#1	Primary	35.80'	8.0" Round Culvert	
			L= 40.0' CPP, projecting, no headwall, Ke= 0.900	
			Inlet / Outlet Invert= 35.80' / 35.58' S= 0.0055 '/' Cc= 0.900	
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf	

Primary OutFlow Max=0.00 cfs @ 12.10 hrs HW=36.78' TW=36.94' (Dynamic Tailwater) 1=Culvert (Controls 0.00 cfs)

Summary for Pond 12P: Yard Drain #2

Inflow Area =	0.072 ac,	0.00% Impervious, Inflow De	epth > 3.96" for 50 Yr 24 Hr(+15%) event
Inflow =	0.27 cfs @	12.18 hrs, Volume=	0.024 af
Outflow =	0.27 cfs @	12.19 hrs, Volume=	0.024 af, Atten= 0%, Lag= 0.6 min
Primary =	0.27 cfs @	12.19 hrs, Volume=	0.024 af
Secondary =	0.00 cfs @	0.00 hrs. Volume=	0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 39.07' @ 12.19 hrs Surf.Area= 183 sf Storage= 6 cf

Plug-Flow detention time= 0.3 min calculated for 0.024 af (100% of inflow)

Center-of-Mass det. time= 0.2 min (843.5 - 843.2)

Volume	Invert			Description		
#1	39.00'	1,3	58 cf Custom	Stage Data (Pi	Prismatic) Listed below (Recalc)	
Elevation (fee	20	urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
39.0	-	5	0	0		
40.0)1	2,685	1,358	1,358		
Device	Routing	Invert	Outlet Devices	i		
#1	Primary	36.00'	8.0" Round C	ulvert		
					headwall, Ke= 0.900	
					35.33' S= 0.0134 '/' Cc= 0.900	
				•	nooth interior, Flow Area= 0.35	sf
#2	Device 1	39.00'		rifice/Grate C		
				flow at low hea		
#3	Secondary	40.00'			Broad-Crested Rectangular Wo 0.80 1.00 1.20 1.40 1.60 1.8	

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2.50 3.00 3.50

Coef. (English) 2.54 2.61 2.61 2.60 2.66 2.70 2.77 2.89 2.88 2.85 3.07 3.20 3.32

Primary OutFlow Max=0.26 cfs @ 12.19 hrs HW=39.07' TW=37.60' (Dynamic Tailwater)

-1=Culvert (Passes 0.26 cfs of 1.58 cfs potential flow)
-2=Orifice/Grate (Weir Controls 0.26 cfs @ 0.84 fps)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=39.00' TW=34.30' (Dynamic Tailwater) —3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 13P: Yard Drain #3

[80] Warning: Exceeded Pond 3P by 0.32' @ 12.10 hrs (2.64 cfs 0.032 af)

Inflow Area = 0.514 ac, 47.23% Impervious, Inflow Depth > 6.28" for 50 Yr 24 Hr(+15%) event

Inflow = 3.00 cfs @ 12.14 hrs, Volume= 0.269 af

Outflow = 3.00 cfs @ 12.14 hrs, Volume= 0.269 af, Atten= 0%, Lag= 0.0 min

Primary = 3.00 cfs @ 12.14 hrs, Volume= 0.269 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.69' @ 12.17 hrs

Flood Elev= 38.50'

Device	Routing	Invert	Outlet Devices
#1	Primary	34.65'	15.0" Round Culvert L= 48.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 34.65' / 34.40' S= 0.0052 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf

Primary OutFlow Max=2.96 cfs @ 12.14 hrs HW=37.58' TW=37.17' (Dynamic Tailwater) 1=Culvert (Inlet Controls 2.96 cfs @ 2.41 fps)

Summary for Pond 14P: Yard Drain #4

Inflow Area = 0.031 ac, 25.58% Impervious, Inflow Depth > 6.48" for 50 Yr 24 Hr(+15%) event

Inflow = 0.22 cfs @ 12.09 hrs, Volume= 0.017 af

Outflow = 0.22 cfs @ 12.09 hrs, Volume= 0.017 af, Atten= 0%, Lag= 0.0 min

Primary = 0.22 cfs @ 12.09 hrs, Volume= 0.017 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 37.28' @ 12.18 hrs

Flood Elev= 39.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	36.50'	8.0" Round Culvert L= 40.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 36.50' / 36.10' S= 0.0100 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.35 sf

Primary OutFlow Max=0.31 cfs @ 12.09 hrs HW=36.91' TW=36.65' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.31 cfs @ 1.99 fps)

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Summary for Pond 15P: Subsurface Stone Infiltration

Inflow Area = 0.021 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr(+15%) event Inflow 0.17 cfs @ 12.09 hrs, Volume= 0.015 af 0.03 cfs @ 12.58 hrs, Volume= Outflow 0.014 af, Atten= 85%, Lag= 29.4 min = 0.03 cfs @ 12.58 hrs, Volume= Discarded = 0.014 af 0.000 af Primary 0.00 cfs @ 0.00 hrs, Volume=

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 31.61' @ 12.58 hrs Surf.Area= 0.004 ac Storage= 0.006 af

Plug-Flow detention time= 130.4 min calculated for 0.014 af (99% of inflow) Center-of-Mass det. time= 122.9 min (862.9 - 740.0)

Volume	Invert	Avail.Storage	Storage Description
#1	27.50'	0.007 af	4.00'W x 40.00'L x 4.51'H Prismatoid 0.017 af Overall x 40.0% Voids
Device	Routing	Invert Ou	utlet Devices
#1	Discarded	27.50' 0. 6	650 in/hr Exfiltration over Surface area
			onductivity to Groundwater Elevation = 27.08' Phase-In= 0.01'
#2	Primary		.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			50 3.00
		Co	pef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
		3.3	30 3.31 3.32

Discarded OutFlow Max=0.03 cfs @ 12.58 hrs HW=31.61' (Free Discharge) 1=Exfiltration (Controls 0.03 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=27.50' TW=28.00' (Dynamic Tailwater) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 16P: Subsurface Stone Infiltration

Inflow Area = 0.019 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr(+15%) event Inflow 0.15 cfs @ 12.09 hrs, Volume= 0.013 af Outflow = 0.04 cfs @ 12.44 hrs, Volume= 0.013 af, Atten= 73%, Lag= 21.3 min 0.04 cfs @ 12.44 hrs, Volume= Discarded = 0.013 af Primary 0.00 cfs @ 0.00 hrs, Volume= 0.000 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 33.39' @ 12.44 hrs Surf.Area= 0.006 ac Storage= 0.004 af

Plug-Flow detention time= 56.9 min calculated for 0.013 af (100% of inflow) Center-of-Mass det. time= 55.9 min (796.0 - 740.0)

Volume	Invert	Avail.Storage	Storage Description	
#1	31.80'	0.004 af	8.00'W x 35.00'L x 1.71'H Prismatoid	
			0.011 af Overall x 40.0% Voids	

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

21047-PROPOSED

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Device	Routing	Invert	Outlet Devices
#1	Discarded	31.80'	0.300 in/hr Exfiltration over Surface area
			Conductivity to Groundwater Elevation = 31.72' Phase-In= 0.01'
#2	Primary	33.50'	86.0' long x 1.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00
			2.50 3.00
			Coef. (English) 2.69 2.72 2.75 2.85 2.98 3.08 3.20 3.28 3.31
			3.30 3.31 3.32

Discarded OutFlow Max=0.04 cfs @ 12.44 hrs HW=33.39' (Free Discharge) **1=Exfiltration** (Controls 0.04 cfs)

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=31.80' TW=28.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Deep Sump CB #4

0.131 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr(+15%) event Inflow Area =

1.07 cfs @ 12.09 hrs, Volume= 0.091 af Inflow

1.07 cfs @ 12.09 hrs, Volume= 0.091 af, Atten= 0%, Lag= 0.0 min Outflow =

1.07 cfs @ 12.09 hrs, Volume= 0.091 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 30.24' @ 12.09 hrs

Flood Elev= 33.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	29.60'	12.0" Round Culvert L= 67.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 29.60' / 29.20' S= 0.0060 '/' Cc= 0.900 n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=1.05 cfs @ 12.09 hrs HW=30.23' TW=29.70' (Dynamic Tailwater) 1=Culvert (Outlet Controls 1.05 cfs @ 2.88 fps)

Summary for Pond 18P: Deep Sump CB #5

0.064 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr(+15%) event Inflow Area =

0.53 cfs @ 12.09 hrs, Volume= 0.044 af Inflow

0.044 af, Atten= 0%, Lag= 0.0 min 0.53 cfs @ 12.09 hrs, Volume= Outflow =

0.53 cfs @ 12.09 hrs, Volume= 0.044 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 29.90' @ 12.51 hrs

Flood Elev= 34.00'

Device	Routing	Invert	Outlet Devices
#1	Primary	29.25'	12.0" Round Culvert
	•		L= 3.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 29.25' / 29.20' S= 0.0167 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Type III 24-hr 50 Yr 24 Hr(+15%) Rainfall=8.53"

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Primary OutFlow Max=0.51 cfs @ 12.09 hrs HW=29.79' TW=29.70' (Dynamic Tailwater) —1=Culvert (Inlet Controls 0.51 cfs @ 1.17 fps)

Summary for Pond 19P: Deep Sump CB #3

Inflow Area = 0.103 ac,100.00% Impervious, Inflow Depth > 8.28" for 50 Yr 24 Hr(+15%) event

Inflow 0.84 cfs @ 12.09 hrs, Volume= 0.071 af

0.84 cfs @ 12.09 hrs, Volume= 0.84 cfs @ 12.09 hrs, Volume= Outflow = 0.071 af, Atten= 0%, Lag= 0.0 min

0.071 af Primary

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 30.47' @ 12.09 hrs

Flood Elev= 33.10'

Device	Routing	Invert	Outlet Devices
#1	Primary	29.80'	12.0" Round Culvert
	-		L= 40.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 29.80' / 29.60' S= 0.0050 '/' Cc= 0.900
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 0.79 sf

Primary OutFlow Max=0.82 cfs @ 12.09 hrs HW=30.45' TW=30.23' (Dynamic Tailwater) 1=Culvert (Outlet Controls 0.82 cfs @ 2.14 fps)

Summary for Pond 20P: Contech Jellyfish

Inflow Area = 0.196 ac,100.00% Impervious, Inflow Depth > 29.31" for 50 Yr 24 Hr(+15%) event

Inflow 2.40 cfs @ 12.52 hrs, Volume= 0.478 af

Outflow = 2.40 cfs @ 12.52 hrs, Volume= 0.478 af, Atten= 0%, Lag= 0.0 min

Primary 2.40 cfs @ 12.52 hrs, Volume= 0.478 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3

Peak Elev= 29.89' @ 12.52 hrs

Flood Elev= 33.60'

Device	Routing	Invert	Outlet Devices		
#1	Primary	28.95'	15.0" Round Culvert		
			.= 42.0' CPP, projecting, no headwall, Ke= 0.900		
			Inlet / Outlet Invert= 28.95' / 28.70' S= 0.0060 '/' Cc= 0.900		
			n= 0.013 Corrugated PE, smooth interior, Flow Area= 1.23 sf		

Primary OutFlow Max=2.39 cfs @ 12.52 hrs HW=29.89' TW=0.00' (Dynamic Tailwater) 1=Culvert (Barrel Controls 2.39 cfs @ 3.35 fps)

Summary for Pond 21P: Wetland Ponding Area

Volume

Invert

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1.527 ac, 52.60% Impervious, Inflow Depth > 3.34" for 50 Yr 24 Hr(+15%) event Inflow Area = 2.73 cfs @ 12.33 hrs, Volume= Inflow 0.426 af 2.20 cfs @ 12.69 hrs. Volume= Outflow = 0.343 af. Atten= 19%, Lag= 21.7 min Primary = 0.00 cfs @ 0.00 hrs. Volume= 0.000 af Secondary = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af Tertiary 2.20 cfs @ 12.69 hrs, Volume= 0.343 af

Routing by Dyn-Stor-Ind method, Time Span= 0.00-24.00 hrs, dt= 0.05 hrs / 3 Peak Elev= 31.18' @ 12.69 hrs Surf.Area= 3,677 sf Storage= 5,810 cf

Plug-Flow detention time= 121.0 min calculated for 0.343 af (81% of inflow) Center-of-Mass det. time= 56.5 min (869.7 - 813.3)

Avail.Storage Storage Description

cf Custom Stage Data (Irregular)Listed below (Recalc)			
/eir			
4			
eir			
.80 2.00			
6 2.66			
00			
sf			
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			

Primary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 0.00 hrs HW=28.00' TW=0.00' (Dynamic Tailwater) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Tertiary OutFlow Max=2.20 cfs @ 12.69 hrs HW=31.18' TW=29.89' (Dynamic Tailwater)
—3=Culvert (Barrel Controls 2.20 cfs @ 3.37 fps)

APPENDIX III

Test Pit Logs



GOVE ENVIRONMENTAL SERVICES, INC.

TEST PIT DATA

Project 1169 &1171 Sagamore Avenue, Portsmouth, NH

Client Garrepy Planning Consultants, LLC

GES Project No. 2021039

MM/DD/YY Staff 03-23-2021 JP Gove, CSS # 004

Depth	Color	Texture	Structure	Consistence	Redox
Fill - 0-12"	10YR3/2	SL	Gr	Fr	None
Fill – 12-35"	10YR3/3	SL	Gr	Fr	None
Apb – 35-45"	10YR3/2	SL	Gr	Fr	None
Bwb - 45-60"	10YR4/3	SL	Om	Fr	None
Bedrock-60"					

Test Pit No.	2	Lot No.:
ESHWT:	None Observed	WSPCD Group:
Termination @	55"	Roots to:
Refusal:	Yes	SCS Soil:
Obs. Water:	none	HIS Type:

Depth	Color	Texture	Structure	Consistence	Redox
Ap - 0-10"	10YR3/2	SL	Gr	Fr	None
Bw - 10-55"	7.5YR3/4	SL	Gr	Fr	None
Rinnable Redr	ock - 55"				

Test Pit No. ESHWT: Termination @ Refusal:	3 31" 51" Yes	Lot No.: WSPCD Group: Roots to: SCS Soil:
Obs. Water:	none	HIS Type:

Depth	Color	Texture	Structure	Consistence	Redox
Ap - 0-11"	10YR3/3	SL	Gr	Fr	None
Bw - 11-31"	10YR4/4	GRLS	Gr	Fr	None
Bw2-31-51"	7.5YR5/4	CBSL	Om	Fr	Yes
Rippable Bedro	ock – 51"				

Test Pit No.

4

Lot No.:

ESHWT:

None Observed 33"

WSPCD Group:

Termination @ Refusal:

Yes

Roots to: SCS Soil:

Obs. Water:

none

HIS Type:

Depth Ap - 0-11"

Color 10YR3/2

Texture Structure SL

Consistence Fr

Redox None

Bw - 11-33"

10YR4/4

Gr **CBSL** Gr

Fr

None

Bedrock - 33"

Test Pit No.

None Observed

Lot No.: WSPCD Group:

ESHWT: Termination @ Refusal:

22" Yes

Roots to: SCS Soil: none HIS Type:

Gr

Depth Ap - 0-10"Bw - 10-22"

Obs. Water:

Color 10YR3/3 10YR4/4

Texture Structure SL Gr

Consistence Fr

Fr

Redox None None

Bedrock - 22"

Test Pit No.

6

Lot No.:

ESHWT:

None Observed 2"

CBSL

WSPCD Group: Roots to:

Termination @ Refusal: Obs. Water:

Yes none

SCS Soil: HIS Type:

Depth A - 0 - 2"

Color 10YR3/2

Texture **CBSL**

Structure Gr

Consistence Fr

Redox None

Bedrock 2"

Test Pit No.

ESHWT:

None Observed

Lot No.:

WSPCD Group:

Termination @ Refusal:

21" Yes Roots to: SCS Soil:

Obs. Water:

none

HIS Type:

Depth A - 0-21"

Color 10YR3/3

Texture CBSL

Structure Gr

Consistence Fr

Redox None

Bedrock - 21"

Test Pit No.

8

None Observed

Lot No.:

ESHWT:

31"

WSPCD Group:

Termination @ Refusal:

Yes

Roots to:

Obs. Water:

none

SCS Soil:

Depth

Color

HIS Type:

Ap - 0-10" Bw - 10-31"

10YR3/2 10YR4/6 Texture SL, CBSL Structure Gr Gr Consistence Fr

Fr

Redox None None

Bedrock - 31"

Legend:

GRLS = gravelly loamy sand

CBSL = cobbly sandy loam

SL= sandy loam

Gr = granular

Fr = friable

Om = massive

Ap = top soil

Bw = subsoil

Apb = buried topsoil

Bwb = buried subsoil



GOVE ENVIRONMENTAL SERVICES, INC. TEST PIT DATA

Project1169 Sagamore Avenue, Portsmouth

Client Garrepy Planning Consultants, LLC

GES Project No. 2021039

MM/DD/YY Staff 11-10-2021 JP Gove

Test Pit No. B1

ESHWT: 54 Termination @ 84

Refusal: 84

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-29"	10YR 4/4	GRS	OM	FR	NONE, Fill
29-33"	10YR 3/2	FSL	GR	FR	NONE, buried A
33-54"	10YR 5/6	FSL	GR	FR	NONE, buried B
54-84"	2.5Y 5/3	FSL	OM	FR	30%, C

Test Pit No. B2

ESHWT: 50 Termination @ 65

Refusal: 65

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-31"	10YR 4/4	GRS	OM	FR	NONE, Fill
31–35"	10YR 3/2	FSL	GR	FR	NONE, buried A
35-50"	10YR 5/6	FSL	GR	FR	NONE, buried B
50-65"	2.5Y 4/3	FSL	OM	FR	30%, C

Test Pit No. B3

ESHWT: 33

Termination @ 47

Refusal: 47

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-33"	10YR 4/4	GRS	OM	FR	NONE, Fill
33-47"	10YR 4/3	FSL	OM	FR	20%, buried A/B

Test Pit No. B4

ESHWT: 42 Termination @ 60 Refusal: 60 Obs. Water: 50

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-21"	10YR 4/4	GRS	OM	FR	NONE, Fill
21–29"	10YR 3/2	FSL	GR	FR	NONE, buried A
29–42"	10YR 5/6	FSL	GR	FR	NONE, buried B
42–60"	2.5Y 5/3	FSL	OM	FR	30%, C

Test Pit No. B5

ESHWT: 47 Termination @ 62 Refusal: 62 Obs. Water: 60

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-25"	10YR 4/4	GRS	OM	FR	NONE, Fill
25-36"	10YR 3/2	FSL	GR	FR	NONE, buried A
36-47"	10YR 4/6	FSL	GR	FR	NONE, buried B
47–62"	2.5Y 5/3	FSL	OM	FR	30%, C

Test Pit No. B6

ESHWT: none Termination @ 38 Refusal: 38 Obs. Water: none

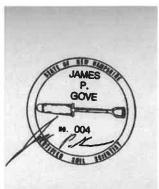
Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-20"	10YR 4/4	FSL	OM	FR	NONE, A/Fill
20-38"	10YR 5/6	FSL	GR	FR	NONE, B

Test Pit No. B7

ESHWT: none Termination @ 49 Refusal: 49

Obs. Water: none

Depth	Color	Texture	Structure	Consistence
0-36"	10YR 3/3 - Fill	FSL	OM	FR
20-38"	10YR 5/6 - buried	FSL	GR	FR
	В			



11-11-2021



GOVE ENVIRONMENTAL SERVICES, INC. TEST PIT DATA

Project – 1169 &1171 Sagamore Ave., Portsmouth, NH – TM 224, Lots 14 & 15.

Client - Jones & Beach Engineers, Inc.

GES Project No. 2021039

MM/DD/YY Staff

1-25-2022 JPG

Test Pit No. X1

ESHWT: n/a

Termination @ 20"

Refusal: 20"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-12"	10YR 3/2	FSL	GR	FR	NONE, Ap
12-20"	10YR 4/4	FSL	GR	FR	NONE, Bw
20"	Bedrock				

Test Pit No. X2

ESHWT: n/a

Termination @ 36"

Refusal: 36"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0–6"	10YR 3/2	FSL	GR	FR	NONE, Ap
6-36"	10YR 4/6	FSL	GR	FR	NONE, Bw
36"	Bedrock				

Test Pit No. X3

ESHWT: n/a

Termination @ 57"

Refusal: 57"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-12"	10YR 3/2	FSL	GR	FR	NONE, Ap
12-57"	10YR 4/6	FSL	GR	FR	NONE, Bw
57"	Bedrock				

Test Pit No. X4	Test	Pit	No.	X4
-----------------	-------------	-----	-----	-----------

ESHWT: n/a

Termination @ 75"

Refusal: n/a

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-70"	10YR 3/3	FSL	OM	FR	NONE, Fill
70-75"	10YR 4/6	FSL	GR	FR	NONE, Bw

Test Pit No. X5

ESHWT: 51"

Termination @ 66"

Refusal: 66"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0–6"	10YR 3/3	LS	GR	FR	NONE, Fill
6-39"	10YR 5/6	LS	OM	FR	NONE, Fill
39–51"	10YR3/2	FSL	GR	FR	Buried Ap
51-66"	7.5YR4/6	FSL	GR	FR	5%, Bw
66"	Bedrock				

Test Pit No. X6

ESHWT: 51"

Termination @ 65"

Refusal: 65"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-5"	10YR 3/3	LS	GR	FR	NONE, Fill
5-51"	10YR 4/6	LS	OM	FR	NONE, Fill
51-65"	10YR3/2	FSL	GR	FR	5%, Buried Ap
65"	Bedrock				

Test Pit No. X7

ESHWT: 49"

Termination @ 65"

Refusal: 65"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-10"	10YR 3/2	LS	GR	FR	NONE, Fill
10-49"	10YR 4/4	LS	OM	FR	NONE, Fill
49-65"	10YR3/2	FSL	GR	FR	5%, Buried Ap
65"	Bedrock				

Test Pit No. X8

ESHWT: n/a Termination @ 58" Refusal: 58"

Obs. Water: None

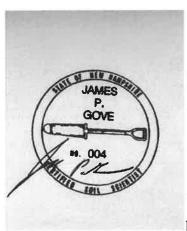
Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-25"	10YR 3/3	LS	GR	FR	NONE, Fill
25-37"	10YR 3/2	FSL	GR	FR	NONE, Buried Ap
37-58"	10YR4/6	FSL	GR	FR	NONE, Bw
58"	Bedrock				

Test Pit No. X9

ESHWT: n/a Termination @ 20" Refusal: 20"

Obs. Water: None

Depth	Color	Texture	Structure	Consistence	Redox %, Layer
0-16"	10YR 3/2	FSL	GR	FR	NONE, Ap
16-20"	10YR 4/6	FSL	GR	FR	NONE, Bw
20"	Bedrock				



1-26-2022

APPENDIX IV

HISS Soil Note and Map

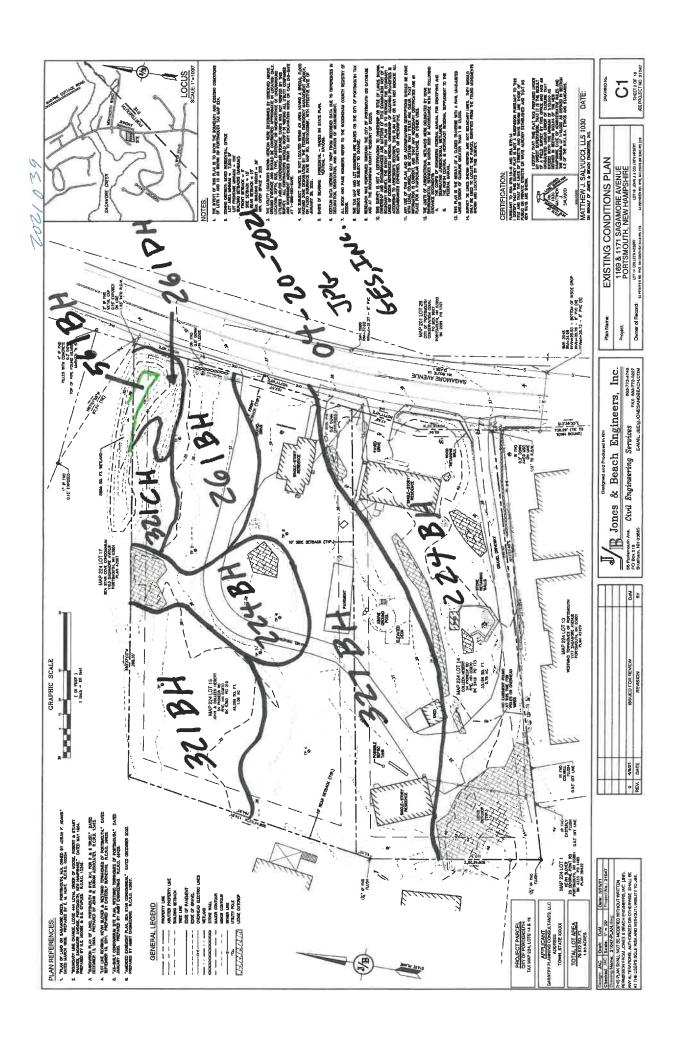
This soil map was prepared by a professional soil scientist and meets the technical standards of the SSSNNE Publication No. 1, High Intensity Soil Maps for NH, December 2017. Soil map was prepared on 4 April 2021. Soil map site was 1169 &1171 Sagamore Avenue, Portsmouth, NH.

Soil Map Units were identified using the Key to Soil Types. The conversion of High Intensity Soil Map Unit to NRCS Soil Map Unit Name was based upon the observed soil profiles, as was hydrologic soil group, as taken from SSSNNE Special Publication No. 5.

Soil mapping was performed by James Gove, CSS # 004.

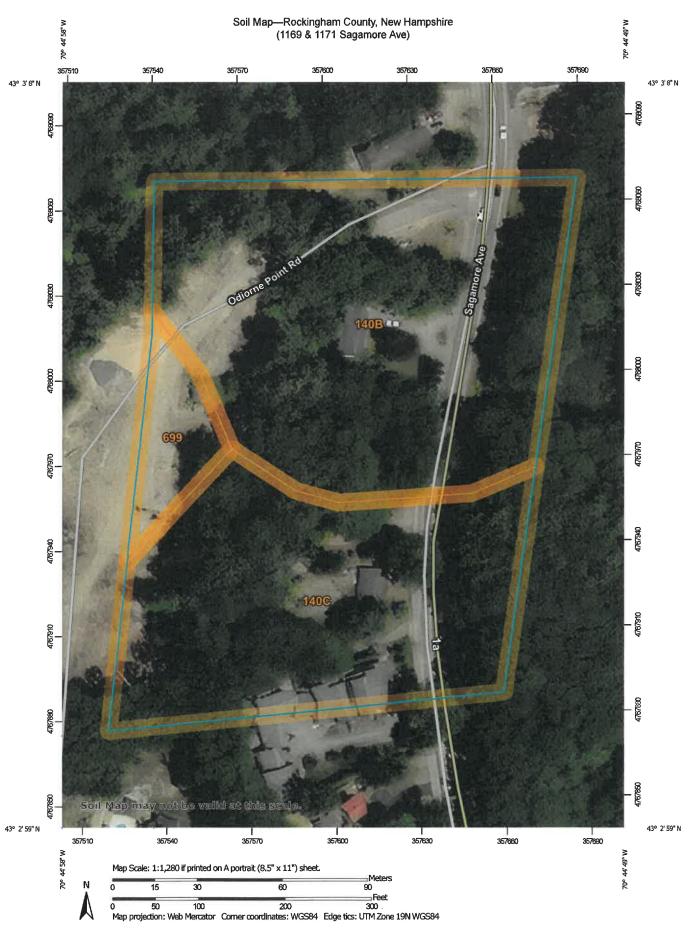
HISS Soil Map Unit	Soil Map Unit Name	Hydrologic Soil Group
224 (slope) H	Hollis-Rock Outcrop Complex	D
261 (slope) H	Made land – similar to Canton	В
321 (slope) H	Newfields	В
327 (slope) H	Chatfield Variant	В
561 (slope) H	Made land- similar to Walpole	С

B slope = 0-8%, C slope = 8-15%, D slope = 15-25%



APPENDIX V

NRCS Soil Map



MAP LEGEND

M 8 < O Soil Map Unit Polygons Area of Interest (AOI) Soil Map Unit Points Soil Map Unit Lines Special Point Features Area of Interest (AOI) Blowout 9 Soils

Very Stony Spot

Wet Spot

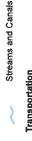
Stony Spot

Spoil Area









Borrow Pit

 \boxtimes 莱 \Diamond

Clay Spot



Closed Depression



Gravelly Spot

۰.

Gravel Pit

X







Marsh or swamp

Lava Flow

Landfill

Mine or Quarry

Miscellaneous Water

Perennial Water

Rock Outcrop

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000

Warning: Soil Map may not be valid at this scale

contrasting soils that could have been shown at a more detailed misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of Enlargement of maps beyond the scale of mapping can cause scale.

Please rely on the bar scale on each map sheet for map measurements. Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

distance and area. A projection that preserves area, such as the Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Rockingham County, New Hampshire Survey Area Data: Version 22, May 29, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger. Date(s) aerial images were photographed: Dec 31, 2009—Jun 14, 2017

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shiffing of map unit boundaries may be evident.

Severely Eroded Spot

1

Slide or Slip

Sinkhole

Sodic Spot

Sandy Spot

Saline Spot

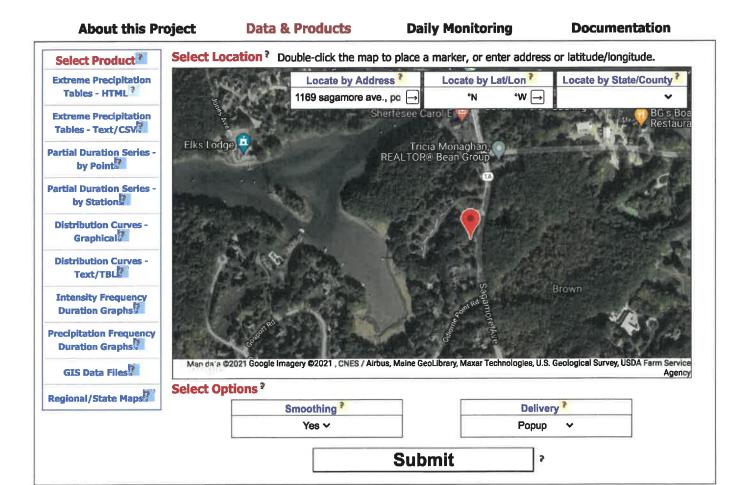
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Map Unit Legend

Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
140B	Chatfield-Hollis-Canton complex, 0 to 8 percent slopes, rocky	3.5	53.7%
140C	Chatfield-Hollis-Canton complex, 8 to 15 percent slopes, rocky	2.7	40.6%
699	Urban land	0.4	5.7%
Totals for Area of Interest	1	6.6	100.0%

APPENDIX VI

Extreme Precipitation Estimates



Version 1.12 Copyright 2010-2021. This project is a joint collaboration between:

Northeast Regional Climate Center (NRCC)



Natural Resources Conservation Service (NRCS)

Contact: precip@cornell.edu

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Smoothing

State Location

Longitude 70.748 degrees West Latitude 43.051 degrees North

Elevation 0 feet

Date/Time Wed, 16 Jun 2021 12:03:11 -0400

Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.26	0.40	0.50	0.65	0.82	1.04	1yr	0.70	0.98	1.21	1.56	2.03	2.67	2.94	1yr	2.36	2.82	3.24	3.96	4.57	1yr
2yr	0.32	0.50	0.62	0.82	1.03	1.30	2yr	0.89	1.18	1.52	1.94	2.49	3.22	3.58	2yr	2.85	3.45	3.95	4.70	5.35	2yr
5yr	0.37	0.58	0.73	0.98	1.25	1.61	5уг	1.08	1.47	1.89	2.44	3.15	4.08	4.60	5yr	3.61	4.42	5.07	5.96	6.73	5yr
10yr	0.41	0.65	0.82	1.12	1.46	1.90	10yr	1.26	1.73	2.24	2.91	3.76	4.88	5.55	10yr	4.32	5.34	6.12	7.14	8.01	10yr
25yr	0.48	0.77	0.97	1.34	1.78	2.35	25yr	1.54	2.15	2.79	3.65	4.76	6.19	7.13	25yr	5.48	6.85	7.85	9.07	10.09	25yr
50yr	0.54	0.87	1.11	1.55	2.09	2.78	50yr	1.80	2.54	3.31	4.35	5.69	7.42	8.62	50yr	6.56	8.29	9.48	10.87	12.02	50yr
100yr	0.60	0.97	1.26	1.79	2.44	3.28	100yr	2.10	3.00	3.93	5.19	6.80	8.88	10.42	100yr	7.86	10.02	11.46	13.03	14.33	100yr
200yr	0.68	1.11	1.44	2.07	2.85	3.87	200yr	2.46	3.54	4.65	6.17	8.12	10.65	12.60	200yr	9.42	12.11	13.85	15.63	17.08	200yr
500yr	0.81	1.33	1.73	2.51	3.52	4.81	500yr	3.03	4.42	5.82	7.76	10.28	13.53	16.20	500yr	11.97	15.58	17.81	19.89	21.57	500yr

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.23	0.36	0.44	0.59	0.72	0.88	1yr	0.62	0.86	0.93	1.34	1.69	2.26	2.50	1yr	2.00	2.41	2.88	3.21	3.94	1yr
2yr	0.31	0.49	0.60	0.81	1.00	1.19	2yr	0.86	1.16	1.37	1.81	2.33	3.07	3.47	2yr	2.72	3.33	3.84	4.56	5.11	2yr
5yr	0.35	0.54	0.67	0.92	1.17	1.40	5yr	1.01	1.37	1.61	2.11	2.72	3.80	4.20	5yr	3.36	4.04	4.74	5.56	6.26	5yr
10yr	0.39	0.59	0.74	1.03	1.33	1.60	10yr	1.15	1.57	1.80	2.38	3.05	4.38	4.88	10yr	3.88	4.69	5.47	6.44	7.22	10yr
25yr	0.44	0.67	0.83	1.19	1.56	1.90	25yr	1.35	1.86	2.10	2.74	3.52	4.78	5.91	25yr	4.23	5.68	6.69	7.83	8.72	25yr
50yr	0.48	0.73	0.91	1.31	1.77	2.17	50yr	1.53	2.12	2.35	3.05	3.91	5.41	6.82	50yr	4.79	6.56	7.77	9.10	10.06	50yr
100yr	0.54	0.81	1.02	1.47	2.02	2.47	100yr	1.74	2.41	2.63	3.39	4.31	6.10	7.87	100yr	5.40	7.57	9.04	10.58	11.63	100yr
200yr	0.59	0.89	1.13	1.64	2.28	2.81	200yr	1.97	2.75	2.94	3.74	4.74	6.86	9.09	200yr	6.07	8.74	10.50	12.32	13.45	200yr
500yr	0.69	1.02	1.31	1.91	2.72	3.36	500yr	2.34	3.29	3.42	4.26	5.39	8.01	10.98	500уг	7.09	10.56	12.80	15.09	16.30	500yr

Upper Confidence Limits

	5min	10min	15min	30min	60min	120min		1hr	2hr	3hr	6hr	12hr	24hr	48hr		1day	2day	4day	7day	10day	
1yr	0.29	0.44	0.54	0.72	0.89	1.09	1yr	0.77	1.06	1.26	1.74	2.20	2.98	3.18	1yr	2.64	3.06	3.59	4.38	5.05	1yr
2yr	0.34	0.52	0.64	0.87	1.07	1.27	2yr	0.92	1.24	1.48	1.96	2.52	3.43	3.72	2yr	3.03	3.58	4.11	4.86	5.64	2yr
5yr	0.40	0.62	0.77	1.05	1.34	1.63	5yr	1.16	1.59	1.89	2.54	3.26	4.36	4.98	5yr	3.85	4.79	5.40	6.40	7.18	5yr
10yr	0.47	0.72	0.89	1.25	1.62	1.99	10yr	1.39	1.94	2.29	3.11	3.97	5.36	6.23	10yr	4.74	5.99	6.85	7.87	8.79	10yr
25yr	0.58	0.88	1.10	1.57	2.06	2.59	25yr	1.78	2.53	2.97	4.08	5.18	7.75	8.38	25yr	6.86	8.05	9.20	10.38	11.45	25yr
50yr	0.68	1.03	1.28	1.84	2.48	3.15	50yr	2.14	3.08	3.61	5.02	6.36	9.69	10.50	50yr	8.57	10.10	11.51	12.78	14.01	50yr
100yr	0.80	1.20	1.51	2.18	2.99	3.84	100yr	2.58	3.76	4.40	6.19	7.83	12.11	13.16	100yr	10.71	12.65	14.40	15.76	17.15	100yr
200yr	0.93	1.41	1.78	2.58	3.60	4.70	200yr	3.10	4.59	5.37	7.63	9.63	15.17	16.51	200yr	13.43	15.87	18.04	19.43	20.98	200yr
500yr	1.16	1.73	2.22	3.23	4.59	6.11	500yr	3.96	5.97	6.97	10.10	12.71	20.46	22.28	500yr	18.11	21.43	24.31	25.62	27.41	500yr



5,61 7.12

8.93

APPENDIX VII

Rip Rap Calculations

RIP RAP CALCULATIONS

Sagamore Avenue Condominiums 1169 & 1171 Sagamore Avenue Portsmouth, NH 03801

Jones & Beach Engineers, Inc.

P.O. Box 219 Stratham, NH 03885

8/11/2021, Rev 9/20/2021, Rev 12/22/2021, Rev 1/28/2022, Rev 3/21/22, Rev 4/18/22, Rev 5/10/22

Rip Rap equations were obtained from the Stormwater Management and Erosion Control Handbook for Urban and Developing Areas in New Hampshire. Aprons are sized for the 25-Year storm event.

TAILWATER < HALF THE Do

 $L_a = (1.8 \text{ x Q}) / D_0^{3/2} + (7 \text{ x D}_o)$ W = $L_a + (3 \text{ x D}_o)$ or defined channel width

 $d_{50} = (0.02 \times Q^{4/3}) / (T_w \times D_0)$

Culvert or	Tailwater	Discharge	Diameter	Length of	Width of	d ₅₀ -Median Stone
Catch Basin	(Feet)	(C.F.S.)	of Pipe	Rip Rap	Rip Rap	Rip Rap
(Sta. No.)	$T_{\mathbf{w}}$	Q	\mathbf{D}_{o}	L _a (feet)	W (feet)	d50 (feet)
15" HDPE (Pond 20P)	0.47	1.5	1.25	10.7	14	0.06

TAILWATER > HALF THE D_o

 $L_a = (3.0 \times Q) / D_0^{3/2} + (7 \times D_o)$

 $W = (0.4 \times L_a) + (3 \times D_o)$ or defined channel width

 $d_{50} = (0.02 \times Q^{4/3}) / (T_w \times D_0)$

Culvert or Catch Basin	Tailwater (Feet)	Discharge (C.F.S.)	Diameter of Pipe	Length of Rip Rap	Width of Rip Rap	d ₅₀ -Median Stone Rip Rap
(Sta. No.)	$T_{\mathbf{w}}$	Q	\mathbf{D}_{o}	L _a (feet)	W (feet)	d50 (feet)
12" HDPE (Pond 10P)	0.63	1.59	1	11.8	8	0.06

d ₅₀ Size =	0.25	Feet	3	Inches
% of Weight Smaller	ight Smaller Size of Stone (Inches)			
Than the Given d ₅₀ Size		From		То
100%		5		6
85%		4		5
50%		3		5
15%	1			2

d ₅₀ Size =	0.5	Feet	6	Inches
% of Weight Smaller	Size of Stone (Inches)			
Γhan the Given d ₅₀ Size		From		То
100%		9		12
85%		8 6		11
50%				9
15%	2			3

APPENDIX VIII

BMP Worksheets



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name:	Bioretention #1 (1	P)

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

	Yes/No	Access grate provided?	← yes
Sheet		Note what sheet in the plan set contains the filter course specification.	4 voc
	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
YES	ac	Drainage Area check.	< 10 ac
a surface	sand filter	or underground sand filter is proposed:	
5 328	E-37	50 peak elevation ≤ Elevation of the top of the practice	← yes
	ft	Elevation of the top of the practice	
	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
BATT	feet	D _{FC to SHWT} = Depth to SHWT from the bottom of the filter course	≥ 1'
	feet	D _{FC to ROCk} = Depth to bedrock from the bottom of the filter course	≥1'
	feet	D _{FC to UD} = Depth to UD from the bottom of the filter course	≥ 1'
	feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
	feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
	feet	E_{UD} = Invert elevation of the underdrain (UD), if applicable	
	feet	E_{FC} = Elevation of the bottom of the filter course material ²	
	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	≤ 72-hrs
	cfs	Q _{WQV} = Discharge at the E _{WQV} (attach stage-discharge table)	. = 6.1
	ft	E _{WQV} = Elevation of WQV (attach stage-storage table)	
lculate ti		if system IS underdrained:	
	hours	T _{DRAIN} = Drain time = V / (A _{SA} * I _{DESIGN})	< 72-hrs
A PORT	Yes/No	(Use the calculations below)	∠ 72_b
		If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	iph	Ksat _{DESIGN} = Design infiltration rate ¹	
	sf ·	A _{SA} = Surface area of the practice	
iculate ti		if system IS NOT underdrained:	
laulata ti	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	2 23/04FQ4
	-£	Method of Pretreatment? (not required for clean or roof runoff)	≥ 25%WQV
320	cf	75% x WQV (check calc for surface sand filter volume)	
107		25% x WQV (check calc for sediment forebay volume)	
427	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
	ac-in	WQV= 1" x Rv x A	
	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.12	4	A _I = Impervious area draining to the practice	
0.16	ac	A = Area draining to the practice	

If a biorete	ntion ar	ea	is proposed:	
YES	ac	x Fi	Drainage Area no larger than 5 ac?	← yes
430	cf		V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
18.0	inches		D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet		D5	Note what sheet in the plan set contains the filter course specification	
3.0	:1		Pond side slopes	<u>> 3</u> :1
Sheet	2	L1	Note what sheet in the plan set contains the planting plans and surface cover	
If porous pa	avemen	t is	proposed:	
			Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres		A _{SA} = Surface area of the pervious pavement	
	:1	18	Ratio of the contributing area to the pervious surface area	≤5:1
	inches		D _{FC} = Filter course thickness	12", or 18" if within GPA
	7.2			mod. 304.1 (see
Sheet			Note what sheet in the plan set contains the filter course spec.	spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat_{design} includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:		

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Last Revised: January 2019

Prepared by Jones and Beach Engineers, Inc.
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Page 1

Stage-Area-Storage for Pond 1P: Bioretention #1

			er		Ξ.
Elevation	Surface	Storage	Elevation	Surface	Storage
(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)
33.99	315	0	36.64	362	247
34.04	315	6	36.69	379	266
34.09	315	13	36.74	396	285
34.14	315	19	36.79	413	306
34.19	315	25	36.84	430	327
34.24	315	32	36.89	447	349
34.29	315	38	36.94	464	371
34.34	315	44	36.99	481	395
34.39	315	50	37.04	499	419
34.44	315	57	37.09	517	445
34.49	315	63	37.14	536	471
34.54	315	69	37.19	554	498
34.59	315	76	37.24	572	527
34.64	315	82	37.29	591	556
34.69	315	88	37.34	609	586
	315	95	37.39	628	617
34.74			37.44	646	648
34.79	315	101			681
34.84	315	107	37.49	664	001
34.89	315	113			
Bottom of 34.94	315	120			
-21 44	315	126	WOV	Required = 427 cf	
filter course 35.04	315	128		Provided = 556-12	
= 35.0 35.09	315	131	"""	110VIGG	10 450 01 - 12
Storage 35.14	315	133			
35.19	315	135			
35.24	315	138			
126 cf 35.29	315	140			
35.34	315	143			
35.39	315	145			
35.44	315	147			
35.49	315	150			
35.54	315	152			
35.59	315	154			
35.64	315	157			
35.69	315	159			
35.74	315	161			
35.79	315	164			
35.84	315	166			
35.89	315	169			
35.94	315	171			
35.99	315	173			
36.04	315	176			
36.09	315	178			
36.14	315	180			
36.19	315	183			
36.24	315	185			
36.29	315	187			
36.34	315	190			
36.39	315	192			
36.44	315	195			
36.49	315	197			
36.54	329	213			
36.59	345	230			
			I .		

Riser Grate El. = 37.3 Storage below = 556 cf

6 = 430 cf > 427 cf



FILTRATION PRACTICE DESIGN CRITERIA (Env-Wq 1508.07)

Type/Node Name:	Bioretention #2 (2P)
i ibcling a manie	

Enter the type of filtration practice (e.g., bioretention system) and the node name in the drainage analysis, if applicable.

		Check if you reviewed the restrictions on unlined systems outlined in Env-Wq 1508.0	7(a).
0.24	-	A = Area draining to the practice	
0.15		A _I = Impervious area draining to the practice	
	decimal	I = Percent impervious area draining to the practice, in decimal form	
_	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
the same of the same of	ac-in	WQV= 1" x Rv x A	
533		WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
133		25% x WQV (check calc for sediment forebay volume)	
400	cf	75% x WQV (check calc for surface sand filter volume)	
	-£	Method of Pretreatment? (not required for clean or roof runoff)	≥ 25%WQV
0-11-4-4	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	<u> </u>
Calculate ti		if system IS NOT underdrained:	
	sf	A _{SA} = Surface area of the practice	
	iph -	Ksat _{DESIGN} = Design infiltration rate ¹	
		If Ksat (prior to factor of safety) is < 0.50 iph, has an underdrain been provided?	
	Yes/No	(Use the calculations below)	. 70 1
	hours	$T_{DRAIN} = Drain time = V / (A_{SA} * I_{DESIGN})$	≤ 72-hrs
Calculate ti		if system IS underdrained:	
	_ft	E _{wQV} = Elevation of WQV (attach stage-storage table)	
	cfs	Q_{WQV} = Discharge at the E_{WQV} (attach stage-discharge table)	
TO VINE	hours	$T_{DRAIN} = Drain time = 2WQV/Q_{WQV}$	≤ 72-hrs
	feet	E_{FC} = Elevation of the bottom of the filter course material ²	
	feet	E _{UD} = Invert elevation of the underdrain (UD), if applicable	
	feet	E _{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	it)
	feet	E _{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
300 45	feet	D _{FC to UD} = Depth to UD from the bottom of the filter course	≥ 1'
ide a sa	feet	D _{FC to ROCK} = Depth to bedrock from the bottom of the filter course	≥ 1'
WINESS !	feet	D _{FC to SHWT} = Depth to SHWT from the bottom of the filter course	≥ 1 ¹
	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
	ft	Elevation of the top of the practice	
1		50 peak elevation ≤ Elevation of the top of the practice	← yes
	sand filter	or underground sand filter is proposed:	
YES	ac	Drainage Area check.	< 10 ac
	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ 75%WQV
	inches	D _{FC} = Filter course thickness	18", or 24" if
	-		within GPA
Sheet		Note what sheet in the plan set contains the filter course specification.	← yes
	Yes/No	Access grate provided?	

COLUMN TWO IS NOT	1	a is proposed:	← yes
YES	36	Drainage Area no larger than 5 ac?	← yes
677	cf	V = Volume of storage ³ (attach a stage-storage table)	≥ WQV
18.0	inches	D _{FC} = Filter course thickness	18", or 24" if within GPA
Sheet	D	Note what sheet in the plan set contains the filter course specification	
3.0	:1	Pond side slopes	<u>> 3</u> :1
Sheet	L	1 Note what sheet in the plan set contains the planting plans and surface cover	
porous p	avement	is proposed:	
		Type of pavement proposed (Concrete? Asphalt? Pavers? Etc.)	
	acres	A _{SA} = Surface area of the pervious pavement	
	:1	Ratio of the contributing area to the pervious surface area	≤ 5:1
	inches	D _{FC} = Filter course thickness	12", or 18" if within GPA
Sheet		Note what sheet in the plan set contains the filter course spec.	mod. 304.1 (se spec)

- 1. Rate of the limiting layer (either the filter course or the underlying soil). Ksat_{design} includes factor of safey. See Env-Wq 1504.14 for guidance on determining the infiltration rate.
- 2. See lines 34, 40 and 48 for required depths of filter media.
- 3. Volume without depending on infiltration. The volume includes the storage above the filter (but below the invert of the outlet stucture, if any), the filter media voids, and the pretreatment area. The storage above the filter media shall not include the volume above the outlet structure, if any.

Designer's Notes:		
-		
*		

36.99

37.04 37.09

600

621

646

375

405

437

Page 2

Stage-Area-Storage for Pond 2P: Bioretention #2

			-	age for ronc			
Ele	vation	Surface	Storage	Elevation	Surface	Storage	
	(feet)	(sq-ft)	(cubic-feet)	(feet)	(sq-ft)	(cubic-feet)	
	34.49	600	0	37.14	672	470	
	34.54	600	12	37.19	697	504	
	34.59	600	24	37.24	723	540	
	34.64	600	36	37.29	749	577	
	34.69	600	48	37.34	774 800	615 654	
	34.74 34.79	600 600	60 72	37.39 37.44	826	695	
	34.84	600	84	37.49	851	737	
	34.89	600	96	37.54	877	780	
	34.94	600	108	37.59	903	824	
	34.99	600	120	37.64	928	870	
	35.04	600	132	37.69	954	917	Riser Grate El. = 37.7
	35.09	600	144	37.74	980	965	Storage below = 917 cf
	35.14	600	156	37.79	1,005	1,015	3
	35.19	600	168	37.84	1,031	1,066	
	35.24	600	180	37.89	1,057	1,118	
	35.29	600	192	37.94	1,082	1,172	
	35.34	600	204	37.99	1,108	1,226	
	35.39	600	216				
	35.44	600	228				
	35.49	600	240				
35.5	35.54	600	244	WOV Re	quired = 533 cf		
	35.59 35.64	600	249		ovided = 917-240	= 677 cf	
	35.69	600 600	253 258	110111	371d0d	071 01	
	35.74	600	263				
	35.79	600	267				
	35.84	600	272				
	35.89	600	276				
	35.94	600	281				
	35.99	600	285				
	36.04	600	289				
	36.09	600	294				
	36.14	600	298				
	36.19	600	303				
	36.24	600	308				
	36.29	600	312				
	36.34	600	317				
	36.39	600	321				
	36.44	600	326				
	36.49 36.54	600 600	330 334				
	36.59	600	339				
	36.64	600	343				
	36.69	600	348				
	36.74	600	353				
	36.79	600	357				
	36.84	600	362				
	36.89	600	366				
	36.94	600	371				



INFILTRATION PRACTICE CRITERIA (Env-Wq 1508.06)

Type/Node Name: Concrete Galley 8x14 (Subsurface infiltration basin, 5P)

Enter the type of infiltration practice (e.g., basin, trench) and the node name in the drainage analysis, if applicable.

Yes		Have you reviewed Env-Wq 1508.06(a) to ensure that infiltration is allowed?	← yes
0.77		A = Area draining to the practice	
0.44	ас	A _I = Impervious area draining to the practice	
0.57	decimal	I = Percent impervious area draining to the practice, in decimal form	
0.57	unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)	
0.43	ac-in	WQV= 1" x Rv x A	
1,577	cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")	
394	cf	25% x WQV (check calc for sediment forebay volume)	
		Method of pretreatment? (not required for clean or roof runoff)	
	cf	V _{SED} = Sediment forebay volume, if used for pretreatment	≥ 25%WQV
2,178	cf		≥ WQV
1,232	sf	A _{SA} = Surface area of the bottom of the pond	
0.30	iph	Ksat _{DESIGN} = Design infiltration rate ²	
51.2	hours	I DRAIN = Drain time = V / (A _{SA} * I _{DESIGN})	< 72-hrs
33.90		E _{BTM} = Elevation of the bottom of the basin	
30.82	feet	E_{SHWT} = Elevation of SHWT (if none found, enter the lowest elevation of the test p	
29.57	feet	E_{ROCK} = Elevation of bedrock (if none found, enter the lowest elevation of the test	pit)
3.08	feet	D _{SHWT} = Separation from SHWT	≥* ³
4.3	feet		≥* ³
	ft	D _{amend} = Depth of amended soil, if applicable due high infiltation rate	_ > 24"
	ft	D_T = Depth of trench, if trench proposed	4 - 10 ft
Yes	Yes/No	If a trench or underground system is proposed, has observation well been provid	ed? ←yes
		If a trench is proposed, does materialmeet Env-Wq 1508.06(k)(2) requirements.4	← yes
	Yes/No	If a basin is proposed, is the perimeter curvilinear, and basin floor flat?	← yes
	:1	If a basin is proposed, pond side slopes.	≥3:1
35.72	ft	Peak elevation of the 10-year storm event (infiltration can be used in analysis)	
36.86	ft	Peak elevation of the 50-year storm event (infiltration can be used in analysis)	
36.90	ft	Elevation of the top of the practice (if a basin, this is the elevation of the berm)	
YES	(1593.5	10 peak elevation ≤ Elevation of the top of the trench? ⁵	← yes
YES		If a basin is proposed, 50-year peak elevation ≤ Elevation of berm?	← yes

- 1. Volume below the lowest invert of the outlet structure and excludes forebay volume
- 2. Ksat_{DESIGN} includes a factor of safety. See Env-Wq 1504.14 for requirements for determining the infiltr. rate
- 3. 1' separation if treatment not required; 4' for treatment in GPAs & WSIPAs; & 3' in all other areas.
- 4. Clean, washed well graded diameter of 1.5 to 3 inches above the in-situ soil.
- 5. If 50-year peak elevation exceeds top of trench, the overflow must be routed in HydroCAD as secondary discharge.

-	

Prepared by Jones and Beach Engineers, Inc. HydroCAD® 10.10-4a s/n 10589 © 2020 HydroCAD Software Solutions LLC

Page 3

Stage-Area-Storage for Pond 5P: Concrete Galley 8x14 INFILTRATION

	Elevation	Surface	Storage	Elevation	Surface	Storage (acre-feet)	
-	(feet) 30.90	(acres) 0.035	(acre-feet) 0.000	(feet) 36.20	(acres) 0.071	0.107	
	31.00	0.035 0.035	0.000	36.20 36.30	0.071	0.110	
	31.10	0.035	0.003	36.40	0.071	0.112	
		0.035	0.003	36.50	0.071	0.115	
	31.20 31.30	0.035	0.004	36.60	0.071	0.118	
	31.40	0.035	0.007	36.70	0.071	0.121	
	31.50	0.035	0.009	36.80	0.071	0.124	
	31.60	0.035	0.010	36.90	0.071	0.126	
	31.70	0.035	0.011	37.00	0.071	0.127	
	31.80	0.035	0.013	37.10	0.071	0.127	
	31.90	0.035	0.014	37.20	0.071	0.127	
	32.00	0.035	0.016	37.30	0.071	0.128	
	32.10	0.035	0.017	37.40	0.071	0.128	
	32.20	0.035	0.018	37.50	0.071	0.128	
	32.30	0.035	0.020				
	32.40	0.035	0.021				
	32.50	0.035	0.023				
	32.60	0.035	0.024			- 2	
	32.70	0.035	0.026	_	equired $= 1,57$		
	32.80	0.035	0.027	WQV Pı	covided = 4,051	l cf - 1,873 cf = 2	1,178 cf > 1,577 cf
	32.90	0.035	0.028	(see belo	w calculations)	
	33.00	0.035	0.030			,	
	33.10	0.035	0.031				
	33.20	0.035	0.033				
	33.30	0.035	0.034				
	33.40	0.035	0.035				
	33.50	0.035	0.037				
	33.60	0.035	0.038				
	33.70	0.035 0.035	0.040 0.041				
Bottom of	33.80 33.90	0.035	0.043				
basin = 33.		0.071	0.045				
	04.40	0.071	0.048				
Storage bel	34.20	0.071	0.051				
= 0.043 ac	^{ft} 34.30	0.071	0.054				
= 1873 cf	34.40	0.071	0.057				
	34.50	0.071	0.059				
	34.60	0.071	0.062				
	34.70	0.071	0.065				
	34.80	0.071	0.068				
	34.90	0.071	0.071				
	35.00	0.071	0.073				
	35.10	0.071	0.076				
	35.20	0.071	0.079				
	35.30	0.071	0.082				
	35.40	0.071	0.084				
	35.50	0.071	0.087				
	35.60	0.071	0.090	Overflow invo			
	35.70	0.071	0.093	Storage below	v = 0.093 ac-ft	4051 cf	
	35.80	0.071	0.096				
	35.90	0.071 0.071	0.098 0.101				
	36.00 36.10	0.071	0.101				
	JO. 10	0.071	V. 104				

APPENDIX IX

Jellyfish Design Information



CONTECH Stormwater Solutions Inc. Engineer: JBS
Date Prepared: 5/4/2022

Site Information

Project Name
Project State
NH
Project City
Portsmouth
Site Designation
Total Drainage Area, Ad
Sagamore Avenue Condominiums
NH
Portsmouth
Jellyfish
0.19 ac

Total Drainage Area, Ad

Post Development Impervious Area, Ai

Pervious Area, Ap

Impervious

Runoff Coefficient, Rc

0.19 ac

0.19 ac

0.00 ac

100%

Mass Loading Calculations

Mean Annual Rainfall, P 50 in Agency Required % Removal 80%
Percent Runoff Capture 90%
Mean Annual Runoff, Vt 29,485 ft³
Event Mean Concentration of Pollutant, EMC 75 mg/l
Annual Mass Load, M total 138 lbs

Filter System

Filtration Brand

Cartridge Length

40 in

Jelly Fish Sizing Parameters

Mass to be Captured by Fitler Vault

Water Quality Flow to be treated by Filter Vault

0.18 cfs

Method to Use FLOW BASED

DANKE OF THE PARTY.	Summary	
Flance	Required Size	JF4-1-1
Flow	Treatment Flow Rate provided:	0.20 cfs



GENERAL CALCULATIONS - WQV and WQF (optional worksheet)

This worksheet may be useful when designing a BMP that does not fit into one of the specific worksheets already provided (i.e. for a technology which is not a stormwater wetland, infiltration practice, etc.)

Water Quality Volume (WQV)

0.19 ac	A = Area draining to the practice
0.19 ac	A _I = Impervious area draining to the practice
1.00 decimal	I = Percent impervious area draining to the practice, in decimal form
0.95 unitless	Rv = Runoff coefficient = 0.05 + (0.9 x I)
0.18 ac-in	WQV= 1" x Rv x A
655 cf	WQV conversion (ac-in x 43,560 sf/ac x 1ft/12")

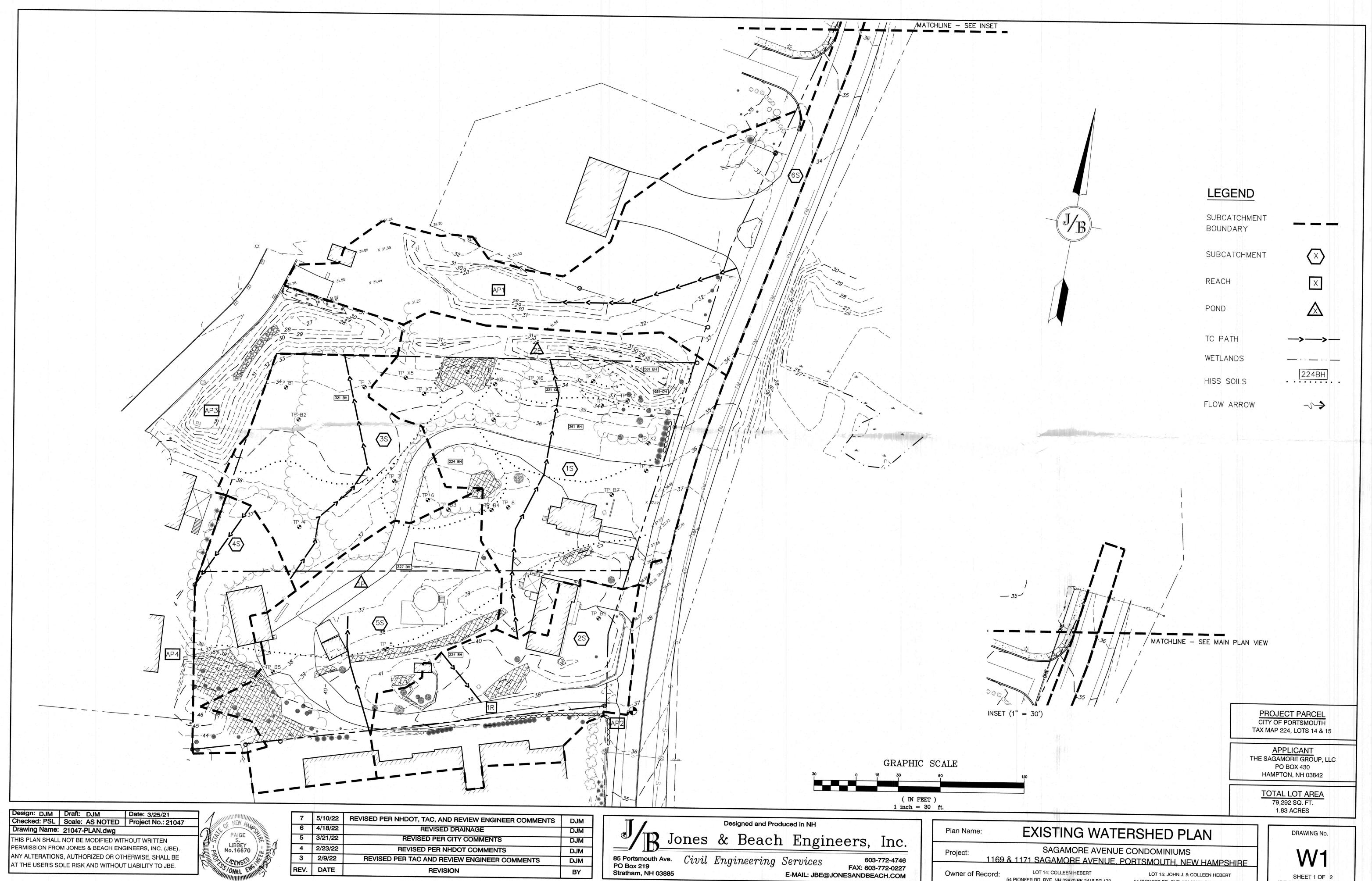
Water Quality Flow (WQF)

	11011 (11	
1	inches	P = Amount of rainfall. For WQF in NH, P = 1".
0.95	inches	Q = Water quality depth. Q = WQV/A
100	unitless	CN = Unit peak discharge curve number. CN = $1000/(10+5P+10Q-10*[Q^2+1.25*Q*P]^{0.5})$
0.0	inches	S = Potential maximum retention. S = (1000/CN) - 10
0.009	inches	la = Initial abstraction. la = 0.2S
	minutes	T _c = Time of Concentration
650.0	cfs/mi²/in	q _u is the unit peak discharge. Obtain this value from TR-55 exhibits 4-II and 4-III.
0.183	cfs	WQF = $q_u \times WQV$. Conversion: to convert "cfs/mi ² /in * ac-in" to "cfs" multiply by 1mi ² /640ac.

Designer's Notes:
This sheet is for the design of the Jellyfish filter system. System is designed to only treat runoff from
Sagamore Ave., as all other impervious runoff directed toward it is already treated.

APPENDIX X

Pre- and Post-Construction Watershed Plans



AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

REV. DATE

REVISION

BY

SHEET 1 OF 2 JBE PROJECT NO. **21047**

LOT 15: JOHN J. & COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173



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4 2/23/22 3 2/9/22 REV. DATE

DJM REVISED PER NHDOT COMMENTS DJM REVISED PER TAC AND REVIEW ENGINEER COMMENTS BY **REVISION**

85 Portsmouth Ave. Civil Engineering Services
PO Box 219
Stratham, NH 03885

Civil Engineering Services
E-MAIL: JBE@. 603-772-4746 FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

1169 & 1171 SAGAMORE AVENUE, PORTSMOUTH, NEW HAMPSHIRE

Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219 SHEET 2 OF 2 JBE PROJECT NO. **21047**

GENERAL LEGEND CONDOMINIUM SITE PLAN "SAGAMORE AVENUE CONDOMINIUMS" TAX MAP 224, LOTS 14 & 15 1169 & 1171 SAGAMORE AVENUE, PORTSMOUTH, NH CAPE COD BERM POURED CONCRETE CURB THRUST BLOCK IRON ROD/DRILL HOLE 100x0 100x0 SPOT GRADE SAGAMORE CREEK PAVEMENT SPOT GRADE CURB SPOT GRADE BENCHMARK (TBM) DOUBLE POST SIGN 0 0 0.0 SINGLE POST SIGN FAILED TEST PIT MONITORING WELL PERC TEST PHOTO LOCATION TREES AND BUSHES UTILITY POLE LIGHT POLES DRAIN MANHOLE SEWER MANHOLE HYDRANT LOCUS MAP WATER GATE SCALE 1" = 1000' SINGLE GRATE CATCH BASIN DOUBLE GRATE CATCH BASIN)—D— TRANSFORMER CULVERT W/WINGWALLS CIVIL ENGINEER / SURVEYOR LANDSCAPE DESIGNER **ELECTRIC** CULVERT W/FLARED END SECTION CULVERT W/STRAIGHT HEADWALL JONES & BEACH ENGINEERS, INC. LM LAND DESIGN, LLC **EVERSOURCE** STONE CHECK DAM ~~> ~~**>** DRAINAGE FLOW DIRECTION 85 PORTSMOUTH AVENUE 11 SOUTH ROAD PO BOX 219 BRENTWOOD, NH 03833 4K SEPTIC AREA STRATHAM, NH 03885 (603) 770-7728 WETLAND IMPACT (603) 772-4746 CONTACT: LISE MCNAUGHTON XXXXXVEGETATED FILTER STRIP **CONTACT: JOSEPH CORONATI** RIPRAP EMAIL: JCORONATI@JONESANDBEACH.COM WATER **TELEPHONE** OPEN WATER

LIGHTING CONSULTANT

CHARRON, INC. P.O BOX 4550 MANCHESTER, NH 03108 (603) 945-3500 **CONTACT: KEN SWEENEY** EMAIL: KSWEENEY@CHARRONINC.COM

WETLAND CONSULTANT GOVE ENVIRONMENTAL SERVICES, INC. 8 CONTINENTAL DR., BLDG 2, UNIT H EXETER, NH 03833-7507 (603) 418-7260 **CONTACT: JAMES GOVE** EMAIL: JGOVE@GESINC.BIZ

CITY OF PORTMOUTH DEPARTMENT OF PUBLIC WORKS WATER DIVISION 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 CONTACT: BRIAN GOETZ, P.E. (603) 427-1530

SEWER CITY OF PORTMOUTH DEPARTMENT OF PUBLIC WORKS **SEWER DIVISION** 680 PEVERLY HILL ROAD PORTSMOUTH, NH 03801 CONTACT: TERRY DESMARAIS, P.E. (603) 766-1421

PO Box 219

Stratham, NH 03885

74 OLD DOVER ROAD ROCHESTER, NH 03867 (800) 555-5334 CONTACT: NICHOLAI KOSKO

FAIRPOINT COMMUNICATIONS 1575 GREENLAND ROAD GREENLAND, NH 03840 (603) 427-5525 **CONTACT: JOE CONSIDINE**

CABLE TV COMCAST COMMUNICATION CORPORATION 334-B CALEF HIGHWAY EPPING, NH 03042-2325 (603) 679-5695

SHEET INDEX

COVER SHEET

EXISTING CONDITIONS PLAN

DEMOLITION PLAN

CONDOMINIUM SITE PLAN

GRADING AND DRAINAGE PLAN

OFFSITE IMPROVEMENTS PLAN

UTILITY PLAN

SEWER PLAN AND PROFILE

LANDSCAPE PLAN

LIGHTING PLAN

DETAIL SHEET

EROSION AND SEDIMENT CONTROL DETAILS

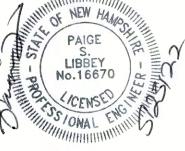
T1-T4 TRUCK TURNING PLAN

HIGHWAY ACCESS PLAN

APPROVED - PORTSMOUTH, NH PROJECT PARCEL PLANNING BOARD CITY OF PORTSMOUTH TAX MAP 224, LOTS 14 & 15 **APPLICANT** THE SAGAMORE GROUP, LLC PO BOX 430 HAMPTON, NH 03842 TOTAL LOT AREA 79,292 SQ. FT. DATE: 1.83 ACRES

Design: JAC Draft: DJM Date: 3/25/21 Checked: JAC | Scale: AS NOTED | Project No.: 21047 Drawing Name: 21047-PLAN.dwg THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE) ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE

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FRESHWATER WETLANDS

STABILIZED CONSTRUCTION

TIDAL WETLANDS

ENTRANCE

CONCRETE

SNOW STORAGE

RETAINING WALL

GRAVEL

14	5/10/22	REVISED PER NHDOT, TAC, AND REVIEW ENGINEER COMMENTS	DJM
13	4/18/22	DRAINAGE REVISIONS	DJM
12	4/6/22	REMOVED WALKWAYS	DJM
11	3/22/22	REVISED PER CITY COMMENTS	DJM
10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
REV.	DATE	REVISION	BY

Designed and Produced in NH Jones & Beach Engineers, Inc. 85 Portsmouth Ave. Civil Engineering Services

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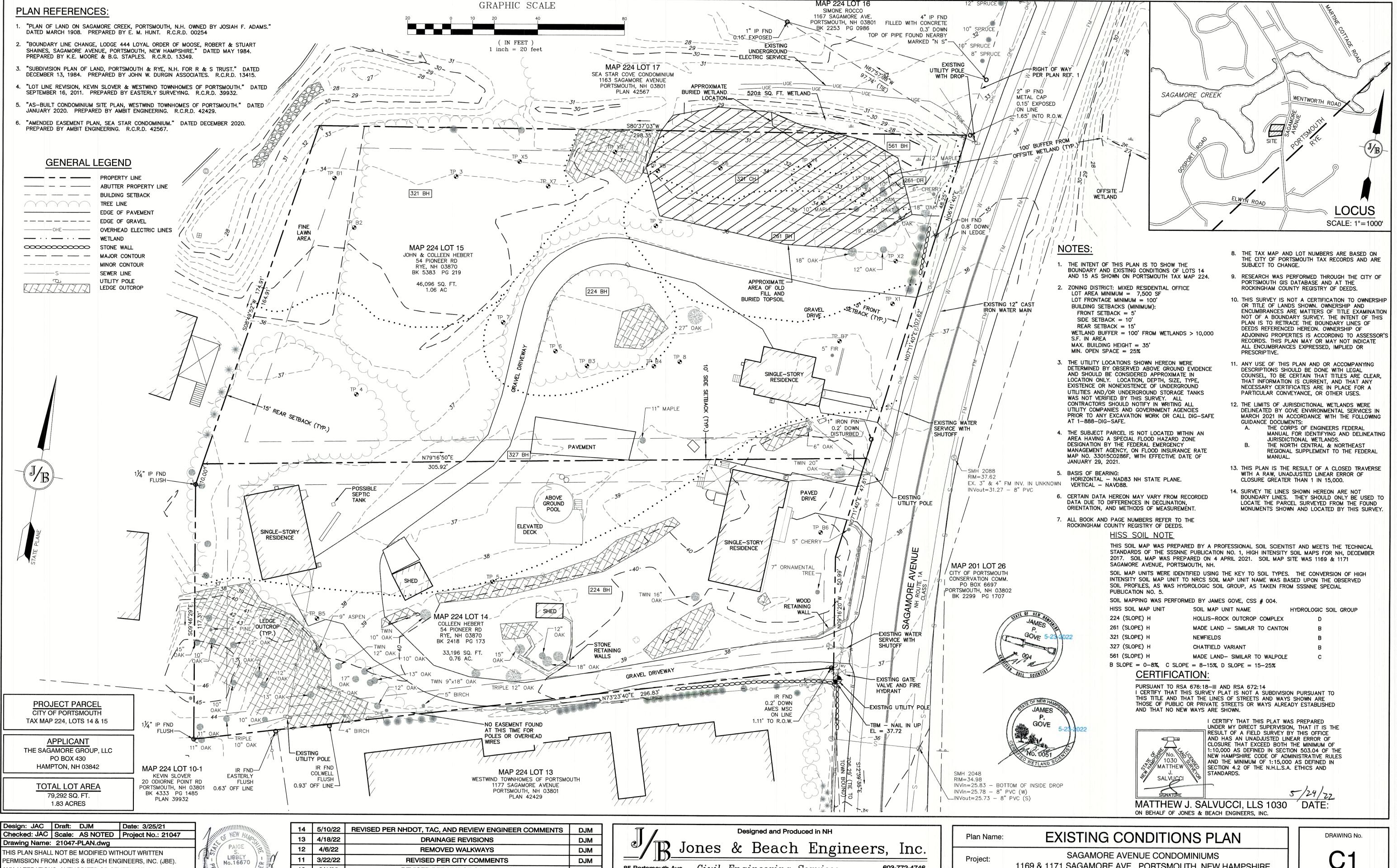
Plan Name:

COVER SHEET

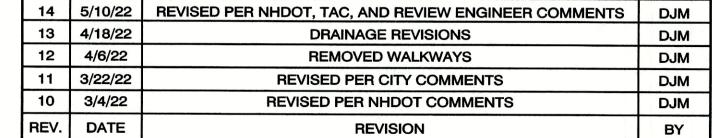
SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

DRAWING No. SHEET 1 OF 22 JBE PROJECT NO. 21047



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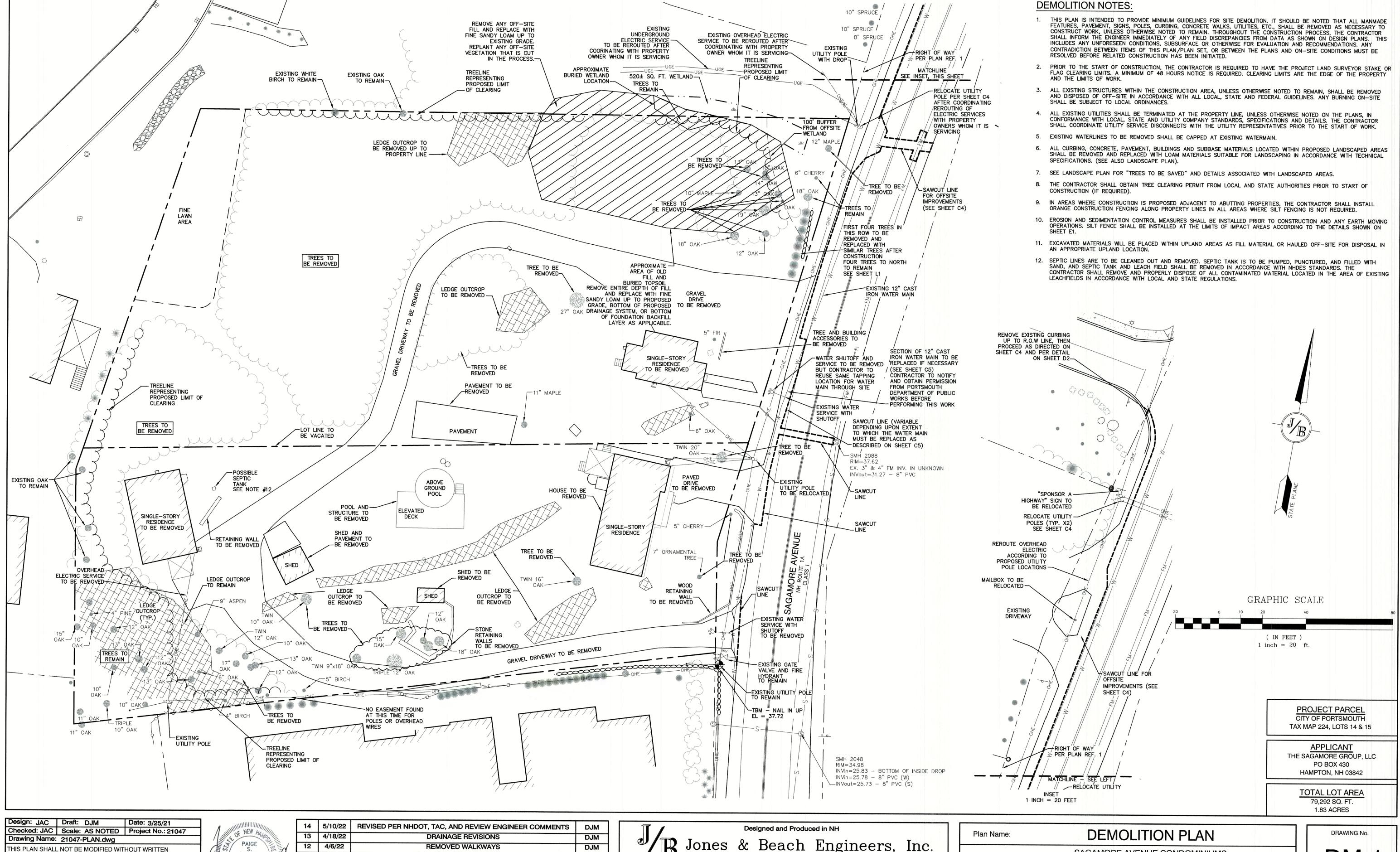
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SHEET 2 OF 22 JBE PROJECT NO. 21047



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12 4/6/22 **REMOVED WALKWAYS** 11 3/22/22 REVISED PER CITY COMMENTS DJM 10 3/4/22 REVISED PER NHDOT COMMENTS DJM DATE REVISION BY

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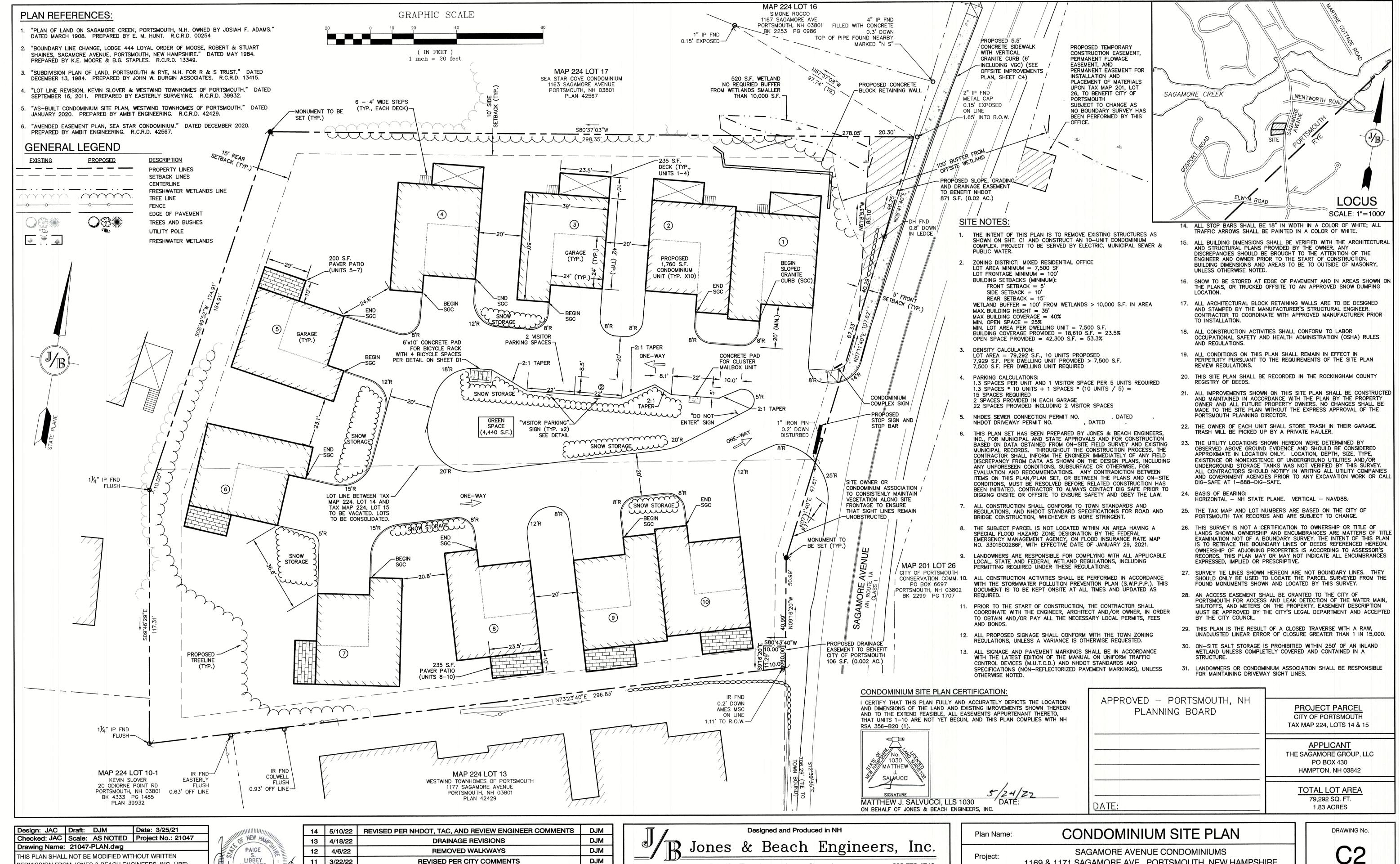
SAGAMORE AVENUE CONDOMINIUMS

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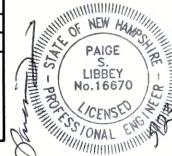
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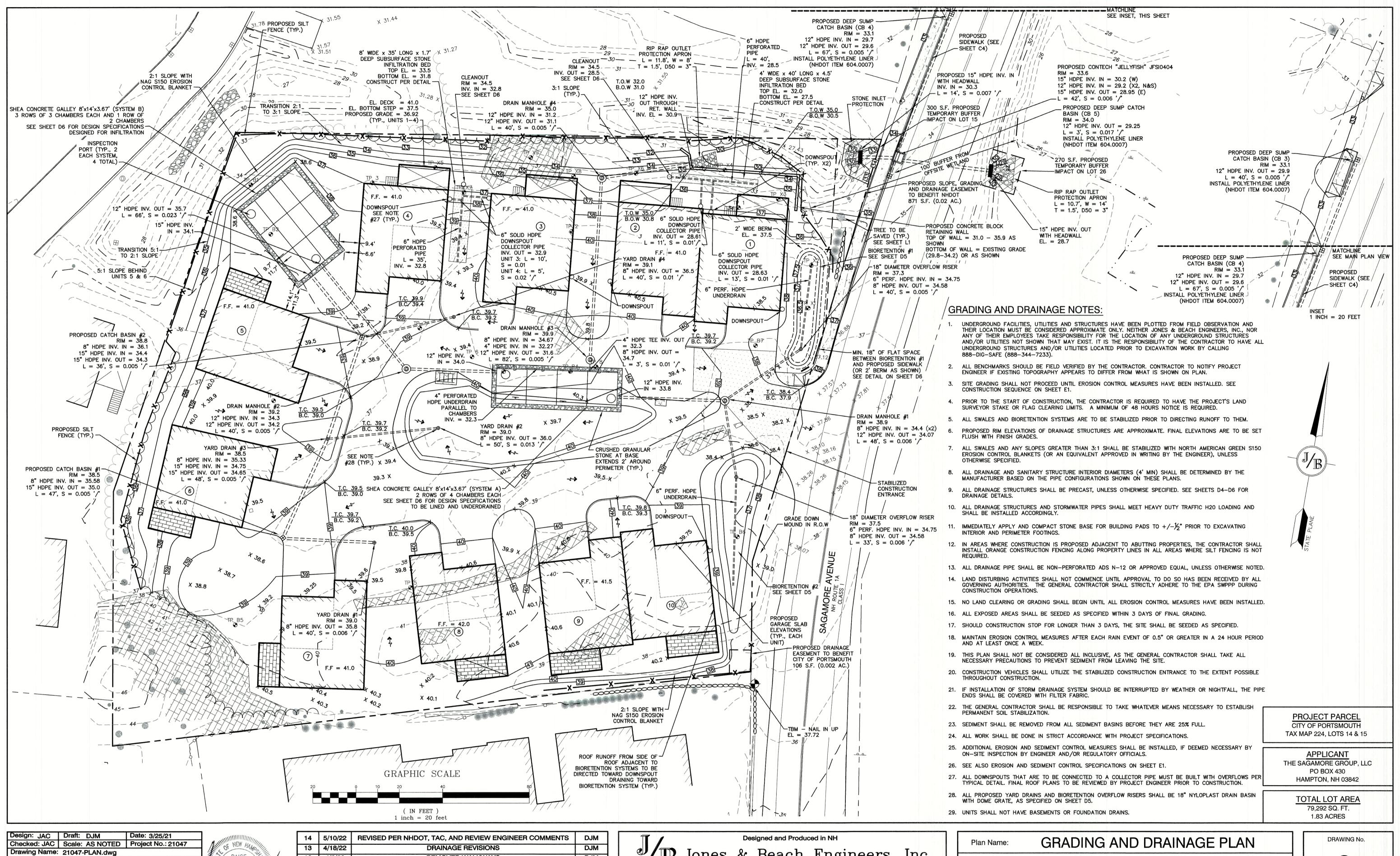
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LOT 14: COLLEEN HEBERT

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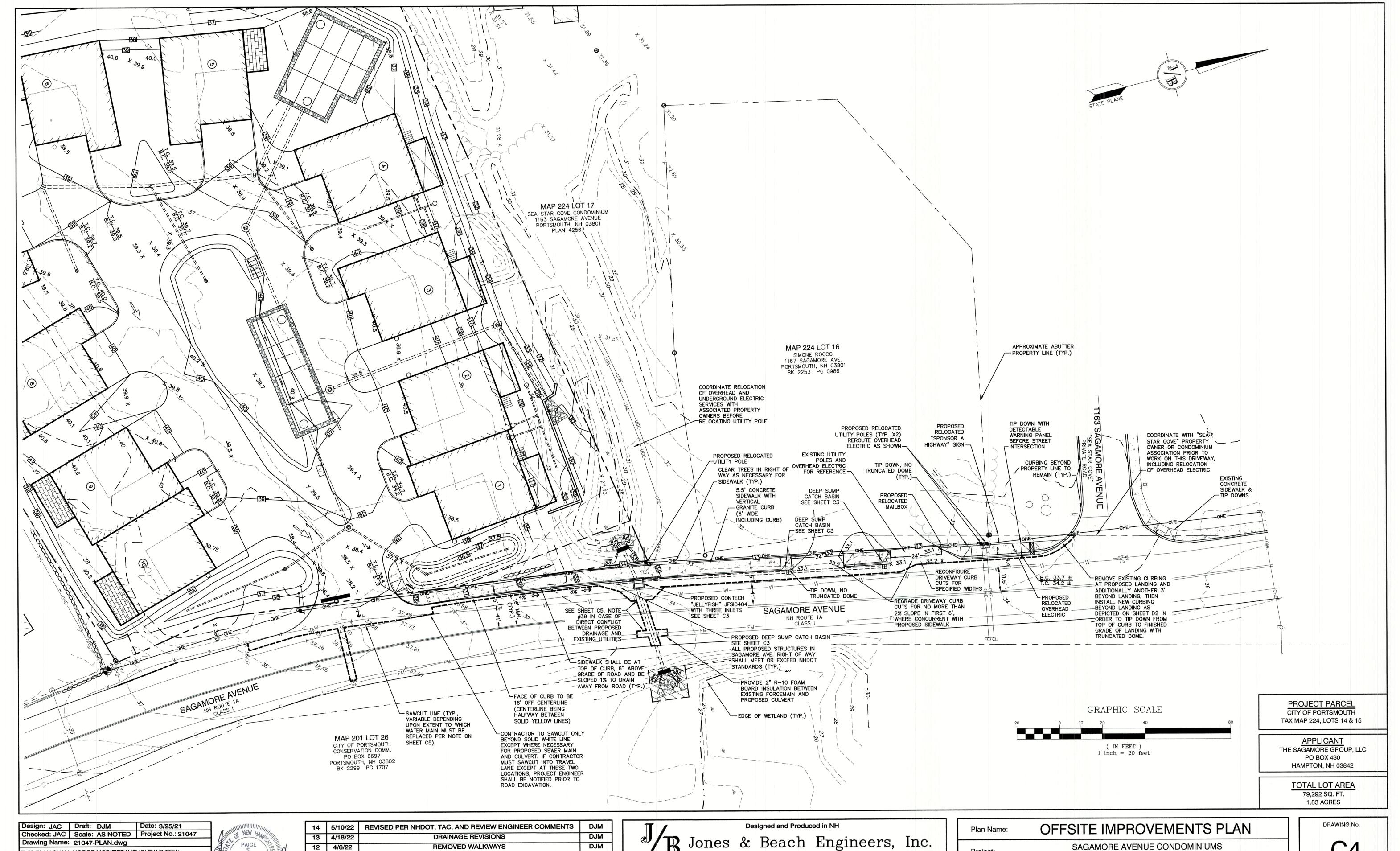
Project:

SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 15: JOHN J. & COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

SHEET 5 OF 22 JBE PROJECT NO. 21047



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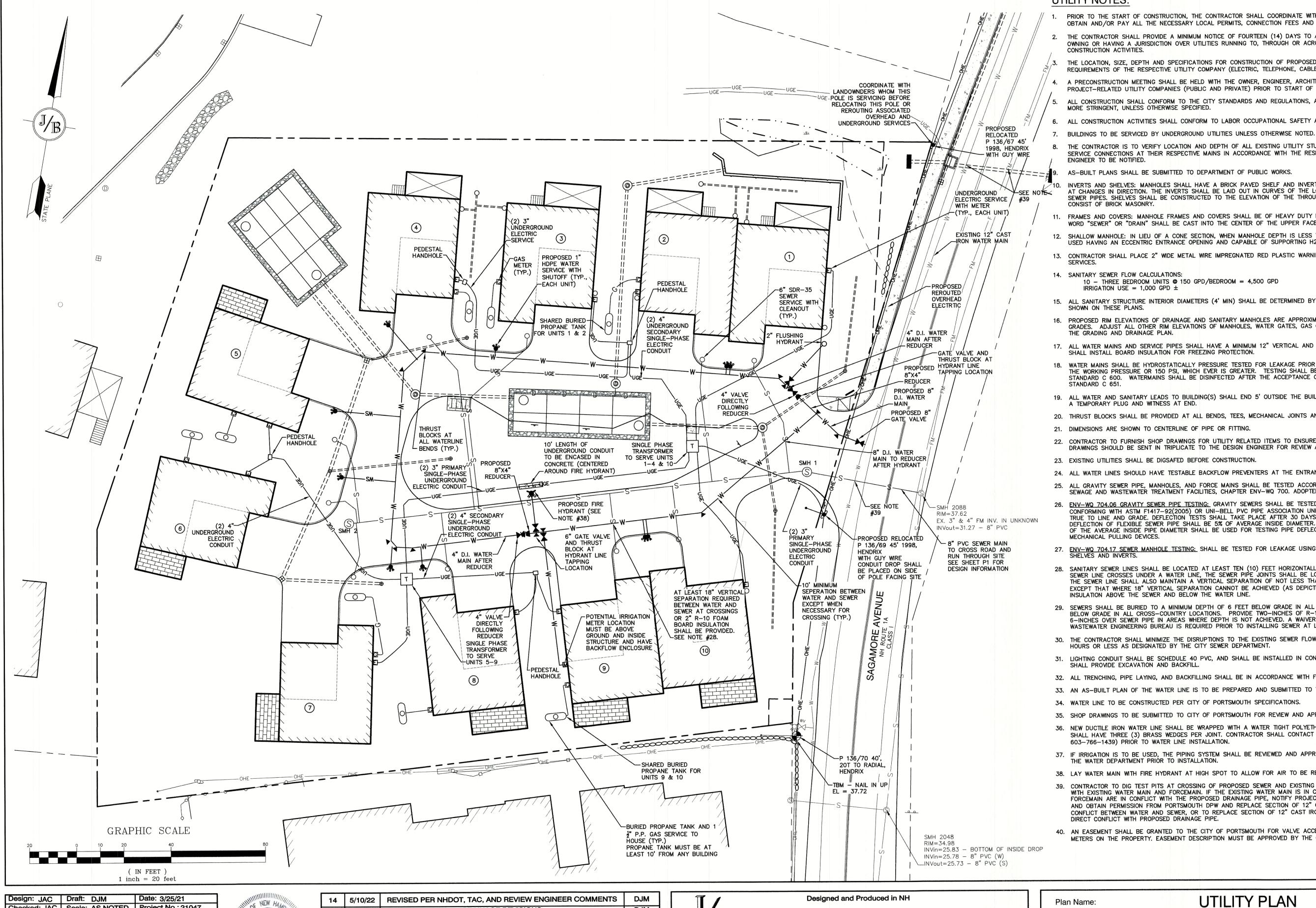
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SHEET 6 OF 22 JBE PROJECT NO. **21047**



UTILITY NOTES:

- PRIOR TO THE START OF CONSTRUCTION, THE CONTRACTOR SHALL COORDINATE WITH THE ENGINEER, ARCHITECT AND/OR OWNER, IN ORDER TO OBTAIN AND/OR PAY ALL THE NECESSARY LOCAL PERMITS, CONNECTION FEES AND BONDS.
- THE CONTRACTOR SHALL PROVIDE A MINIMUM NOTICE OF FOURTEEN (14) DAYS TO ALL CORPORATIONS, COMPANIES AND/OR LOCAL AUTHORITIES OWNING OR HAVING A JURISDICTION OVER UTILITIES RUNNING TO, THROUGH OR ACROSS PROJECT AREAS PRIOR TO DEMOLITION AND/OR
- THE LOCATION, SIZE, DEPTH AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE TO THE STANDARDS AND REQUIREMENTS OF THE RESPECTIVE UTILITY COMPANY (ELECTRIC, TELEPHONE, CABLE TELEVISION, FIRE ALARM, GAS, WATER, AND SEWER).
- A PRECONSTRUCTION MEETING SHALL BE HELD WITH THE OWNER, ENGINEER, ARCHITECT, CONTRACTOR, LOCAL OFFICIALS, AND ALL PROJECT-RELATED UTILITY COMPANIES (PUBLIC AND PRIVATE) PRIOR TO START OF CONSTRUCTION.
- ALL CONSTRUCTION SHALL CONFORM TO THE CITY STANDARDS AND REGULATIONS, AND NHDES STANDARDS AND SPECIFICATIONS, WHICHEVER ARE MORE STRINGENT, UNLESS OTHERWISE SPECIFIED.
- 6. ALL CONSTRUCTION ACTIVITIES SHALL CONFORM TO LABOR OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION (OSHA) RULES AND REGULATIONS.
- THE CONTRACTOR IS TO VERIFY LOCATION AND DEPTH OF ALL EXISTING UTILITY STUBS PRIOR TO CONSTRUCTION AND DISCONNECT ALL EXISTING SERVICE CONNECTIONS AT THEIR RESPECTIVE MAINS IN ACCORDANCE WITH THE RESPECTIVE UTILITY COMPANY'S STANDARDS AND SPECIFICATIONS.
- AS-BUILT PLANS SHALL BE SUBMITTED TO DEPARTMENT OF PUBLIC WORKS.
- NVERTS AND SHELVES: MANHOLES SHALL HAVE A BRICK PAVED SHELF AND INVERT, CONSTRUCTED TO CONFORM TO THE SIZE OF PIPE AND FLOW AT CHANGES IN DIRECTION. THE INVERTS SHALL BE LAID OUT IN CURVES OF THE LONGEST RADIUS POSSIBLE TANGENT TO THE CENTER LINE OF THE SEWER PIPES. SHELVES SHALL BE CONSTRUCTED TO THE ELEVATION OF THE THROUGH CHANNEL UNDERLAYMENT OF INVERT, AND SHELF SHALL
- 11. FRAMES AND COVERS: MANHOLE FRAMES AND COVERS SHALL BE OF HEAVY DUTY DESIGN AND PROVIDE A 30 INCH DIA, CLEAR OPENING. THE WORD "SEWER" OR "DRAIN" SHALL BE CAST INTO THE CENTER OF THE UPPER FACE OF EACH COVER WITH RAISED, 3" LETTERS.
- 12. SHALLOW MANHOLE: IN LIEU OF A CONE SECTION, WHEN MANHOLE DEPTH IS LESS THAN 6 FEET, A REINFORCED CONCRETE SLAB COVER MAY BE USED HAVING AN ECCENTRIC ENTRANCE OPENING AND CAPABLE OF SUPPORTING H20 LOADS.
- 13. CONTRACTOR SHALL PLACE 2" WIDE METAL WIRE IMPREGNATED RED PLASTIC WARNING TAPE OVER ENTIRE LENGTH OF ALL GRAVITY SEWERS AND
- 14. SANITARY SEWER FLOW CALCULATIONS: 10 - THREE BEDROOM UNITS @ 150 GPD/BEDROOM = 4,500 GPD
- IRRIGATION USE = 1,000 GPD ±
- 15. ALL SANITARY STRUCTURE INTERIOR DIAMETERS (4' MIN) SHALL BE DETERMINED BY THE MANUFACTURER BASED ON THE PIPE CONFIGURATIONS SHOWN ON THESE PLANS.
- 16. PROPOSED RIM ELEVATIONS OF DRAINAGE AND SANITARY MANHOLES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH WITH FINISH GRADES. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, GAS GATES AND OTHER UTILITIES TO FINISH GRADE AS SHOWN ON
- 17. ALL WATER MAINS AND SERVICE PIPES SHALL HAVE A MINIMUM 12" VERTICAL AND 24" HORIZONTAL SEPARATION TO MANHOLES, OR CONTRACTOR SHALL INSTALL BOARD INSULATION FOR FREEZING PROTECTION.
- 18. WATER MAINS SHALL BE HYDROSTATICALLY PRESSURE TESTED FOR LEAKAGE PRIOR TO ACCEPTANCE. WATERMAINS SHALL BE TESTED AT 1.5 TIMES THE WORKING PRESSURE OR 150 PSI, WHICH EVER IS GREATER. TESTING SHALL BE CONDUCTED IN ACCORDANCE WITH SECTION 4 OF AWWA STANDARD C 600. WATERMAINS SHALL BE DISINFECTED AFTER THE ACCEPTANCE OF THE PRESSURE AND LEAKAGE TESTS ACCORDING TO AWWA
- 19. ALL WATER AND SANITARY LEADS TO BUILDING(S) SHALL END 5' OUTSIDE THE BUILDING LIMITS AS SHOWN ON PLANS AND SHALL BE PROVIDED WITH A TEMPORARY PLUG AND WITNESS AT END.
- 20. THRUST BLOCKS SHALL BE PROVIDED AT ALL BENDS, TEES, MECHANICAL JOINTS AND HYDRANTS.
- 21. DIMENSIONS ARE SHOWN TO CENTERLINE OF PIPE OR FITTING.
- 22. CONTRACTOR TO FURNISH SHOP DRAWINGS FOR UTILITY RELATED ITEMS TO ENSURE CONFORMANCE WITH THE PLANS AND SPECIFICATIONS. SHOP DRAWINGS SHOULD BE SENT IN TRIPLICATE TO THE DESIGN ENGINEER FOR REVIEW AND APPROVAL PRIOR TO INSTALLATION.
- 23. EXISTING UTILITIES SHALL BE DIGSAFED BEFORE CONSTRUCTION.
- 24. ALL WATER LINES SHOULD HAVE TESTABLE BACKFLOW PREVENTERS AT THE ENTRANCE TO EACH BUILDING.
- 25. ALL GRAVITY SEWER PIPE, MANHOLES, AND FORCE MAINS SHALL BE TESTED ACCORDING TO NHDES STANDARDS OF DESIGN AND CONSTRUCTION FOR SEWAGE AND WASTEWATER TREATMENT FACILITIES, CHAPTER ENV-WQ 700. ADOPTED ON 10-15-14.
- 26. ENV-WQ 704.06 GRAVITY SEWER PIPE TESTING: GRAVITY SEWERS SHALL BE TESTED FOR WATER TIGHTNESS BY USE OF LOW-PRESSURE AIR TESTS CONFORMING WITH ASTM F1417-92(2005) OR UNI-BELL PVC PIPE ASSOCIATION UNI-B-6. LINES SHALL BE CLEANED AND VISUALLY INSPECTED AND TRUE TO LINE AND GRADE. DEFLECTION TESTS SHALL TAKE PLACE AFTER 30 DAYS FOLLOWING INSTALLATION AND THE MAXIMUM ALLOWABLE DEFLECTION OF FLEXIBLE SEWER PIPE SHALL BE 5% OF AVERAGE INSIDE DIAMETER. A RIGID BALL OR MANDREL WITH A DIAMETER OF AT LEAST 95% OF THE AVERAGE INSIDE PIPE DIAMETER SHALL BE USED FOR TESTING PIPE DEFLECTION. THE DEFLECTION TEST SHALL BE CONDUCTED WITHOUT
- 27. ENV-WQ 704.17 SEWER MANHOLE TESTING: SHALL BE TESTED FOR LEAKAGE USING A VACUUM TEST PRIOR TO BACKFILLING AND PLACEMENT OF SHELVES AND INVERTS.
- 28. SANITARY SEWER LINES SHALL BE LOCATED AT LEAST TEN (10) FEET HORIZONTALLY FROM AN EXISTING OR PROPOSED WATER LINE. WHEN A SEWER LINE CROSSES UNDER A WATER LINE, THE SEWER PIPE JOINTS SHALL BE LOCATED AT LEAST 6 FEET HORIZONTALLY FROM THE WATERMAIN. THE SEWER LINE SHALL ALSO MAINTAIN A VERTICAL SEPARATION OF NOT LESS THAN 18 INCHES FROM AN EXISTING OR PROPOSED WATER LINE, EXCEPT THAT WHERE 18" VERTICAL SEPARATION CANNOT BE ACHIEVED (AS DEPICTED ON SHEET P1), PROVIDE TWO INCHES R-10 FOAM BOARD INSULATION ABOVE THE SEWER AND BELOW THE WATER LINE.
- 29. SEWERS SHALL BE BURIED TO A MINIMUM DEPTH OF 6 FEET BELOW GRADE IN ALL ROADWAY LOCATIONS, AND TO A MINIMUM DEPTH OF 4 FEET BELOW GRADE IN ALL CROSS-COUNTRY LOCATIONS. PROVIDE TWO-INCHES OF R-10 FOAM BOARD INSULATION 2-FOOT WIDE TO BE INSTALLED 6-INCHES OVER SEWER PIPE IN AREAS WHERE DEPTH IS NOT ACHIEVED. A WAIVER FROM THE DEPARTMENT OF ENVIRONMENTAL SERVICES WASTEWATER ENGINEERING BUREAU IS REQUIRED PRIOR TO INSTALLING SEWER AT LESS THAN MINIMUM COVER.
- 30. THE CONTRACTOR SHALL MINIMIZE THE DISRUPTIONS TO THE EXISTING SEWER FLOWS AND THOSE INTERRUPTIONS SHALL BE LIMITED TO FOUR (4) HOURS OR LESS AS DESIGNATED BY THE CITY SEWER DEPARTMENT.
- 31. LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRIC CODE. CONTRACTOR
- SHALL PROVIDE EXCAVATION AND BACKFILL. 32. ALL TRENCHING, PIPE LAYING, AND BACKFILLING SHALL BE IN ACCORDANCE WITH FEDERAL OSHA REGULATIONS.
- 33. AN AS-BUILT PLAN OF THE WATER LINE IS TO BE PREPARED AND SUBMITTED TO THE CITY OF PORTSMOUTH WATER DEPARTMENT.
- 34. WATER LINE TO BE CONSTRUCTED PER CITY OF PORTSMOUTH SPECIFICATIONS.
- 35. SHOP DRAWINGS TO BE SUBMITTED TO CITY OF PORTSMOUTH FOR REVIEW AND APPROVAL
- 36. NEW DUCTILE IRON WATER LINE SHALL BE WRAPPED WITH A WATER TIGHT POLYETHYLENE WRAPPING FOR THE FULL LENGTH. ALL WATER LINE JOINTS SHALL HAVE THREE (3) BRASS WEDGES PER JOINT. CONTRACTOR SHALL CONTACT CITY OF PORTSMOUTH WATER DEPARTMENT (JIM TOW AT 603-766-1439) PRIOR TO WATER LINE INSTALLATION.
- 37. IF IRRIGATION IS TO BE USED, THE PIPING SYSTEM SHALL BE REVIEWED AND APPROVED BY THE PORTSMOUTH CITY PLANNER, CITY ENGINEER, AND THE WATER DEPARTMENT PRIOR TO INSTALLATION.
- 38. LAY WATER MAIN WITH FIRE HYDRANT AT HIGH SPOT TO ALLOW FOR AIR TO BE RELEASED DURING FILLING OF THE WATER MAIN.
- 39. CONTRACTOR TO DIG TEST PITS AT CROSSING OF PROPOSED SEWER AND EXISTING WATER MAIN, AND AT CROSSINGS OF PROPOSED DRAINAGE PIP WITH EXISTING WATER MAIN AND FORCEMAIN. IF THE EXISTING WATER MAIN IS IN CONFLICT WITH THE PROPOSED SEWER, OR IF EXISTING WATER OR FORCEMAIN ARE IN CONFLICT WITH THE PROPOSED DRAINAGE PIPE, NOTIFY PROJECT ENGINEER AND PORTSMOUTH DEPARTMENT OF PUBLIC WORKS AND OBTAIN PERMISSION FROM PORTSMOUTH DPW AND REPLACE SECTION OF 12" CAST IRON WATER MAIN AS NECESSARY TO AVOID DIRECT CONFLICT BETWEEN WATER AND SEWER, OR TO REPLACE SECTION OF 12" CAST IRON WATER MAIN OR 3" & 4" FORCEMAIN AS NECESSARY TO AVOID DIRECT CONFLICT WITH PROPOSED DRAINAGE PIPE.
- 40. AN EASEMENT SHALL BE GRANTED TO THE CITY OF PORTSMOUTH FOR VALVE ACCESS AND LEAK DETECTION OF THE WATER MAIN, SHUTOFFS, AND METERS ON THE PROPERTY. EASEMENT DESCRIPTION MUST BE APPROVED BY THE CITY'S LEGAL DEPARTMENT AND ACCEPTED BY THE CITY COUNCIL.

LOT 15: JOHN J. & COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

Checked: JAC | Scale: AS NOTED | Project No.: 21047 Drawing Name: 21047-PLAN.dwg

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	14	5/10/22	REVISED PER NHDOT, TAC, AND REVIEW ENGINEER COMMENTS	DJM
	13	4/18/22	DRAINAGE REVISIONS	DJM
/	12	4/6/22	REMOVED WALKWAYS	DJM
	11	3/22/22	REVISED PER CITY COMMENTS	DJM
	10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
	REV.	DATE	REVISION	BY

Jones & Beach Engineers, Inc.

603-772-4746 85 Portsmouth Ave. Civil Engineering Services FAX: 603-772-0227 PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

UTILITY PLAN

SAGAMORE AVENUE CONDOMINIUMS

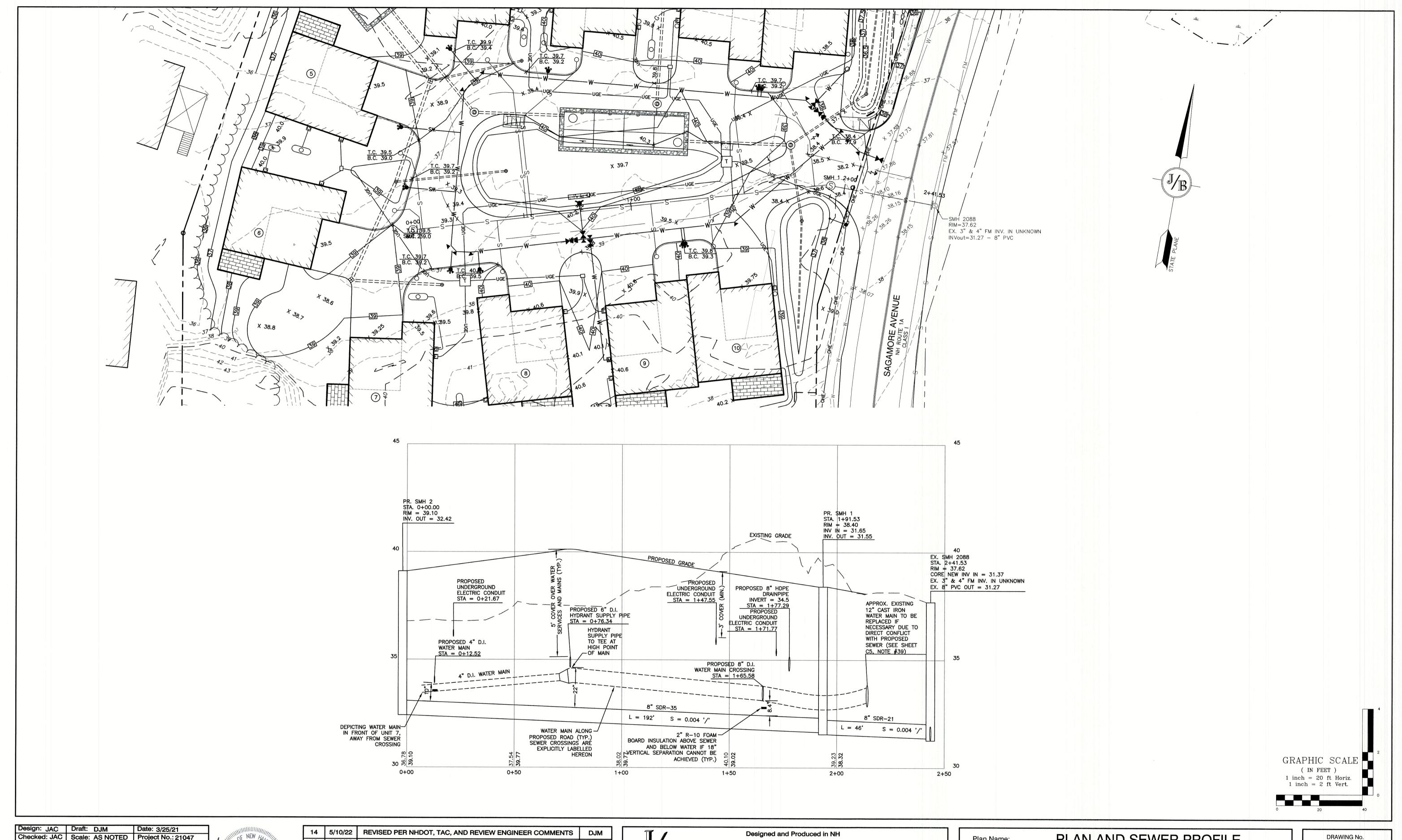
LOT 14: COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

SHEET 7 OF 22 JBE PROJECT NO. 21047

DRAWING No.



Design: JAC Draft: DJM Date: 3/25/21
Checked: JAC Scale: AS NOTED Project No.: 21047 OF NEW HAMO Drawing Name: 21047-PLAN.dwg PAIGE S. LIBBEY No.16670 THIS PLAN SHALL NOT BE MODIFIED WITHOUT WRITTEN PERMISSION FROM JONES & BEACH ENGINEERS, INC. (JBE). CENSED ENGLISH ANY ALTERATIONS, AUTHORIZED OR OTHERWISE, SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO JBE.

REVISED PER NHDOT, TAC, AND REVIEW ENGINEER COMMENTS 14 5/10/22 DJM 13 4/18/22 DRAINAGE REVISIONS DJM REMOVED WALKWAYS DJM 12 4/6/22 11 3/22/22 REVISED PER CITY COMMENTS DJM REVISED PER NHDOT COMMENTS 10 3/4/22 DJM DATE **REVISION** BY REV.

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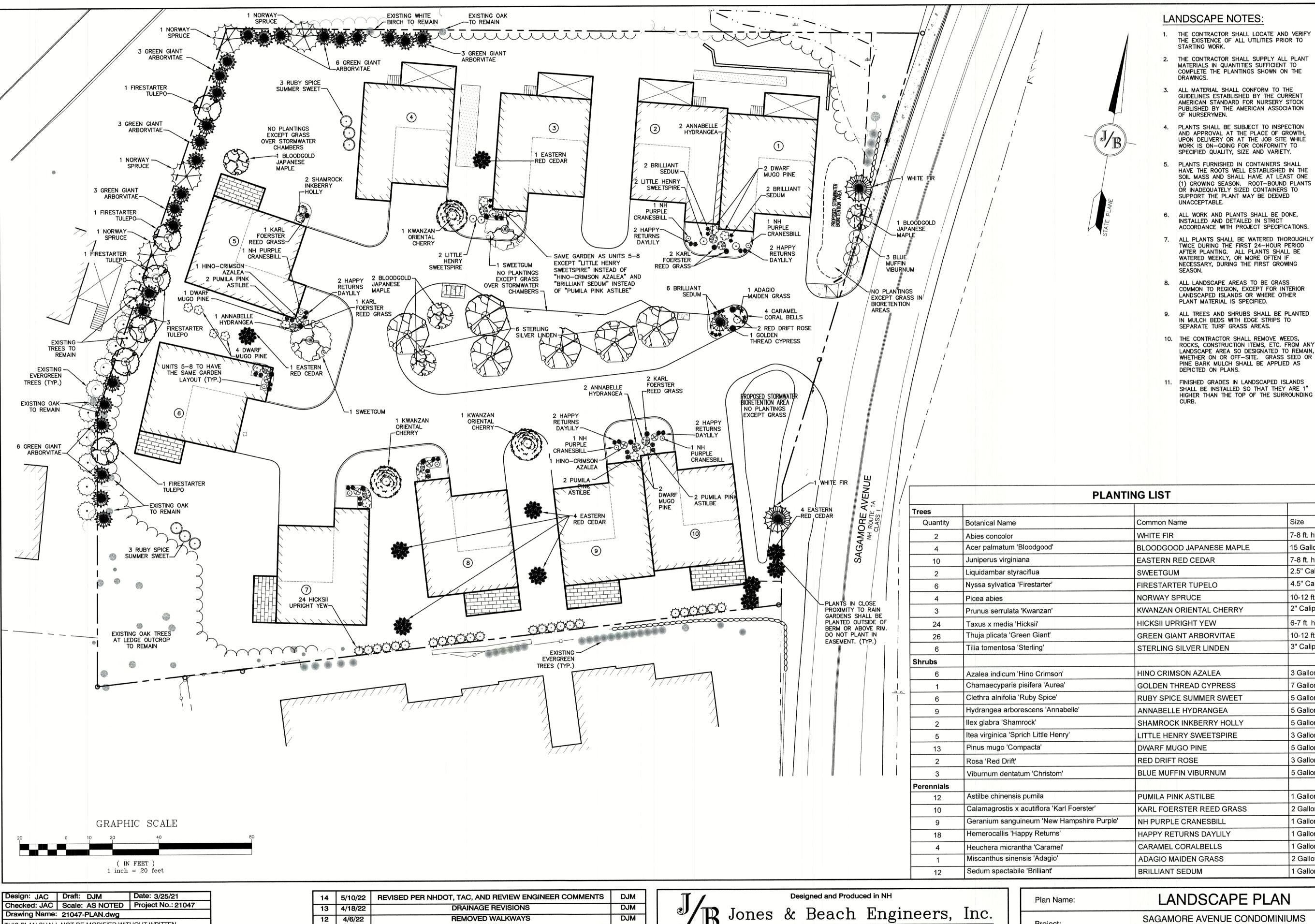
Stratham, NH 03885

PLAN AND SEWER PROFILE Plan Name:

SAGAMORE AVENUE CONDOMINIUMS Project: 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

P SHEET 8 OF 22 JBE PROJECT NO. 21047



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DJM

BY

PO Box 219

Stratham, NH 03885

85 Portsmouth Ave. Civil Engineering Services

REMOVED WALKWAYS

REVISED PER CITY COMMENTS

REVISED PER NHDOT COMMENTS

REVISION

12 4/6/22

11 3/22/22

10 3/4/22

REV. DATE

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LANDSCAPE PLAN SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

Project:

FAX: 603-772-0227

E-MAIL: JBE@JONESANDBEACH.COM

SHEET 9 OF 22

JBE PROJECT NO. 21047

DRAWING No.

PROJECT PARCEL CITY OF PORTSMOUTH

TAX MAP 224, LOTS 14 & 15

APPLICANT

THE SAGAMORE GROUP, LLC

PO BOX 430

HAMPTON, NH 03842

TOTAL LOT AREA

79,292 SQ. FT.

1.83 ACRES

12. ALL LANDSCAPING SHALL MEET THE CITY OF PORTSMOUTH STANDARDS AND REGULATIONS.

AT THE DRIPLINE OF THE TREE. THE

LAWN SHALL BE REPAIRED BY THE

14. ALL MULCH AREAS SHALL RECEIVE A 3"

PROTECTED WITH TEMPORARY SNOW FENCING

CONTRACTOR SHALL NOT STORE VEHICLES OF

MATERIALS WITHIN THE LANDSCAPED AREAS.

ANY DAMAGE TO EXISTING TREES, SHRUBS OF

CONTRACTOR AT NO ADDITIONAL COST TO TH

LAYER OF SHREDDED PINE BARK MULCH OVER

A 10 MIL WEED MAT EQUAL TO 'WEEDBLOCK' BY EASY GARDENER OR DEWITT WEED

ALL LANDSCAPED AREAS SHALL HAVE SELECT

MATERIALS REMOVED TO A DEPTH OF AT

RESULTING VOID IS TO BE FILLED WITH A

MINIMUM OF 9" HIGH-QUALITY SCREENED

LOAM AMENDED WITH 3" OF AGED ORGANIC

LEAST 9" BELOW FINISH GRADE. THE

16. THIS PLAN IS INTENDED FOR LANDSCAPING

IRRIGATION PIPING SYSTEM SHALL BE

ENGINEER PRIOR TO INSTALLATION.

INFORMATION.

PURPOSES ONLY. REFER TO CIVIL/SITE

DRAWINGS FOR OTHER SITE CONSTRUCTION

REVIEWED AND APPROVED BY OWNER AND

PROPERTY OWNERS SHALL BE RESPONSIBLE

ALL REQUIRED PLANT MATERIALS SHALL BE

NECESSARY, AND KEPT FREE OF REFUSE AND

RESPONSIBLE TO REMOVE AND REPLACE DEAD

OR DISEASED PLANT MATERIALS IMMEDIATELY

WITH THE SAME TYPE, SIZE, AND QUANTITY

INSTALLED, UNLESS ALTERNATIVE PLANTINGS

ARE REQUESTED, JUSTIFIED, AND APPROVED

SEE TYPICAL PLANTING DETAILS ON SHEET D4

BY THE PLANNING BOARD OR PLANNING

OF PLANT MATERIALS AS ORIGINALLY

DEBRIS. ALL REQUIRED FENCES AND WALLS

TENDED AND MAINTAINED IN A HEALTHY

SHALL BE MAINTAINED IN GOOD REPAIR.

GROWING CONDITION, REPLACED WHEN

REPLACEMENT OF ALL REQUIRED SCREENING

THE PROPERTY OWNER AND ALL FUTURE

FOR THE MAINTENANCE, REPAIR, AND

AND LANDSCAPE MATERIALS.

20. THE PROPERTY OWNER SHALL BE

7-8 ft. ht.

15 Gallon

7-8 ft. ht.

2.5" Caliper

4.5" Caliper

10-12 ft. ht.

2" Caliper

6-7 ft. ht.

10-12 ft. ht.

3" Caliper

3 Gallon

7 Gallon

5 Gallon

5 Gallon 5 Gallon

3 Gallon

5 Gallon

3 Gallon

5 Gallon

1 Gallon

2 Gallon

1 Gallon

1 Gallon

1 Gallon

2 Gallon

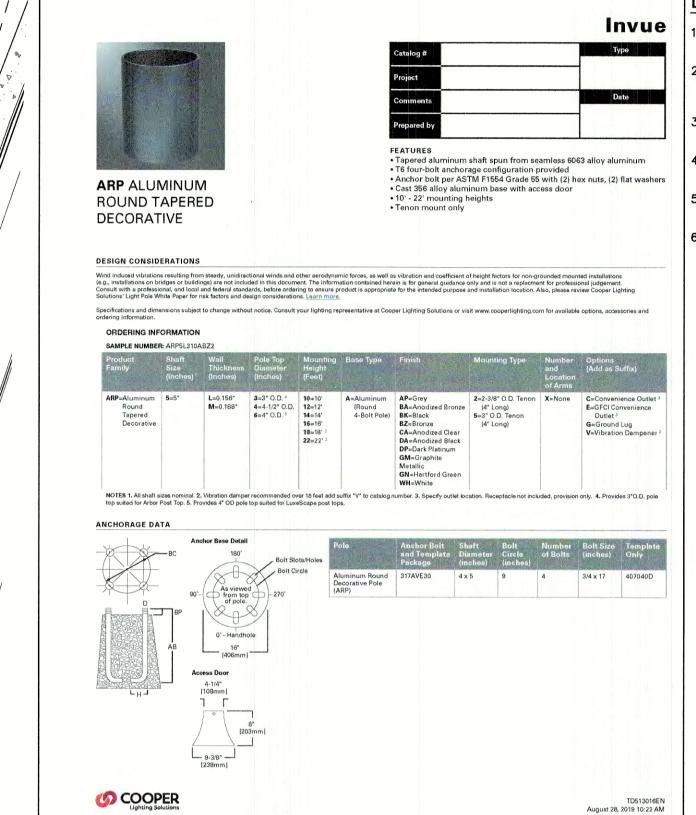
1 Gallon

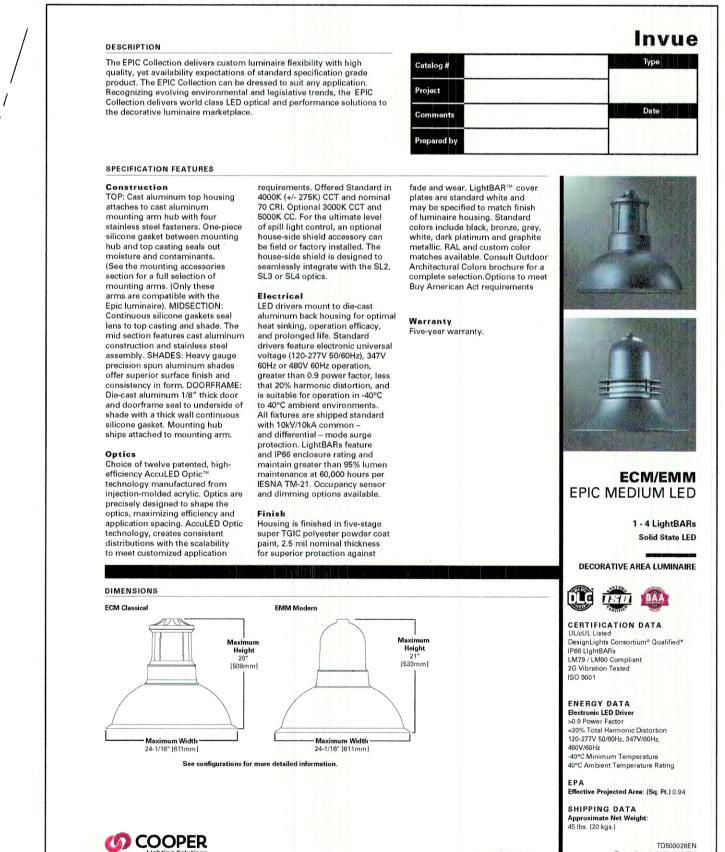
LOT 15: JOHN J. & COLLEEN HEBERT

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13. EXISTING TREES TO REMAIN SHALL BE

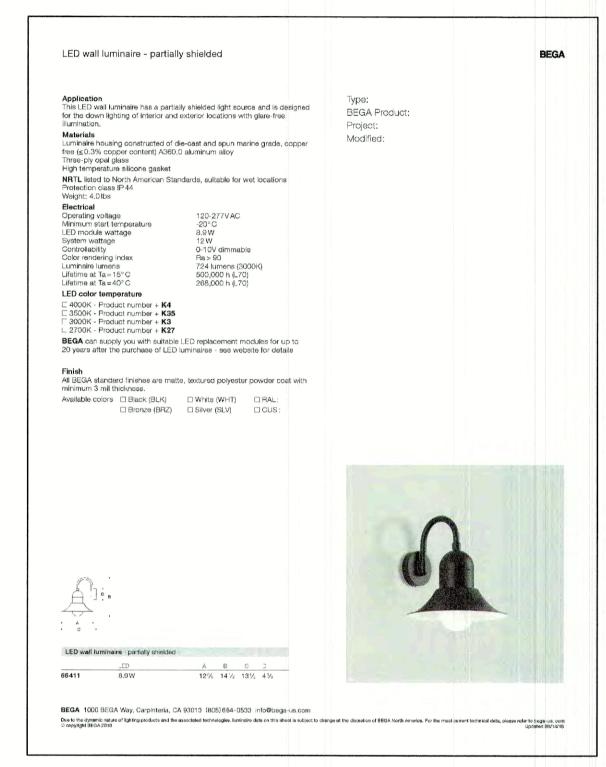


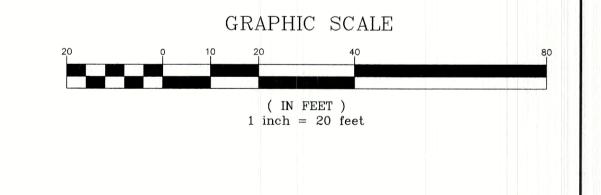




LIGHTING AND ELECTRICAL NOTES:

- 1. ALL OUTDOOR LIGHTING SYSTEMS SHALL BE EQUIPPED WITH TIMERS TO REDUCE ILLUMINATION LEVELS TO NON-OPERATIONAL VALUES PER TOWN REGULATIONS.
- 2. LIGHTING CONDUIT SHALL BE SCHEDULE 40 PVC, AND SHALL BE INSTALLED IN CONFORMANCE WITH THE NATIONAL ELECTRICAL CODE. CONTRACTOR SHALL PROVIDE EXCAVATION AND BACKFILL.
- ILLUMINATION READINGS SHOWN ARE BASED ON A TOTAL LLF OF 0.75 AT GRADE.
 ILLUMINATION READINGS SHOWN ARE IN UNITS OF FOOT—CANDLES.
- LIGHTING CALCULATIONS SHOWN ARE NOT A SUBSTITUTE FOR INDEPENDENT ENGINEERING ANALYSIS OF LIGHTING SYSTEM AND SAFETY.
- ALL LIGHTING FIXTURES SHALL BE FULL CUT-OFF DARK-SKY COMPLIANT, UNLESS
- THE PROPOSED LIGHTING CALCULATIONS AND DESIGN WAS PERFORMED BY CHARRON, INC., P.O. BOX 4550, MANCHESTER, NH 03108, ATTENTION KEN SWEENEY. ALL LIGHTS SHOULD BE PURCHASED FROM THIS COMPANY, OR AN EQUAL LIGHTING DESIGN SHOULD BE SUBMITTED FOR REVIEW IF EQUAL SUBSTITUTIONS ARE PROPOSED BY THE CONTRACTOR OR OWNER.





PROJECT PARCEL
CITY OF PORTSMOUTH
TAX MAP 224, LOTS 14 & 15

APPLICANT
THE SAGAMORE GROUP, LLC
PO BOX 430
HAMPTON, NH 03842

TOTAL LOT AREA 79,292 SQ. FT. 1.83 ACRES

Design: JAC Draft: DJM Date: 3/25/21
Checked: JAC Scale: AS NOTED Project No.: 21047
Drawing Name: 21047-PLAN.dwg

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皇	11	3/22/22	REVISED PER CITY COMMENTS	DJM
	10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
8	REV.	DATE	REVISION	BY

Designed and Produced in NH

Jones & Beach Engir

Jones & Beach Engineers, Inc.

85 Portsmouth Ave. Civil Engineering Services 603-772-4746
PO Box 219
Stratham, NH 03885

Civil Engineering Services FAX: 603-772-0227
E-MAIL: JBE@JONESANDBEACH.COM

Plan Name:

LIGHTING PLAN

54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

SAGAMORE AVENUE CONDOMINIUMS

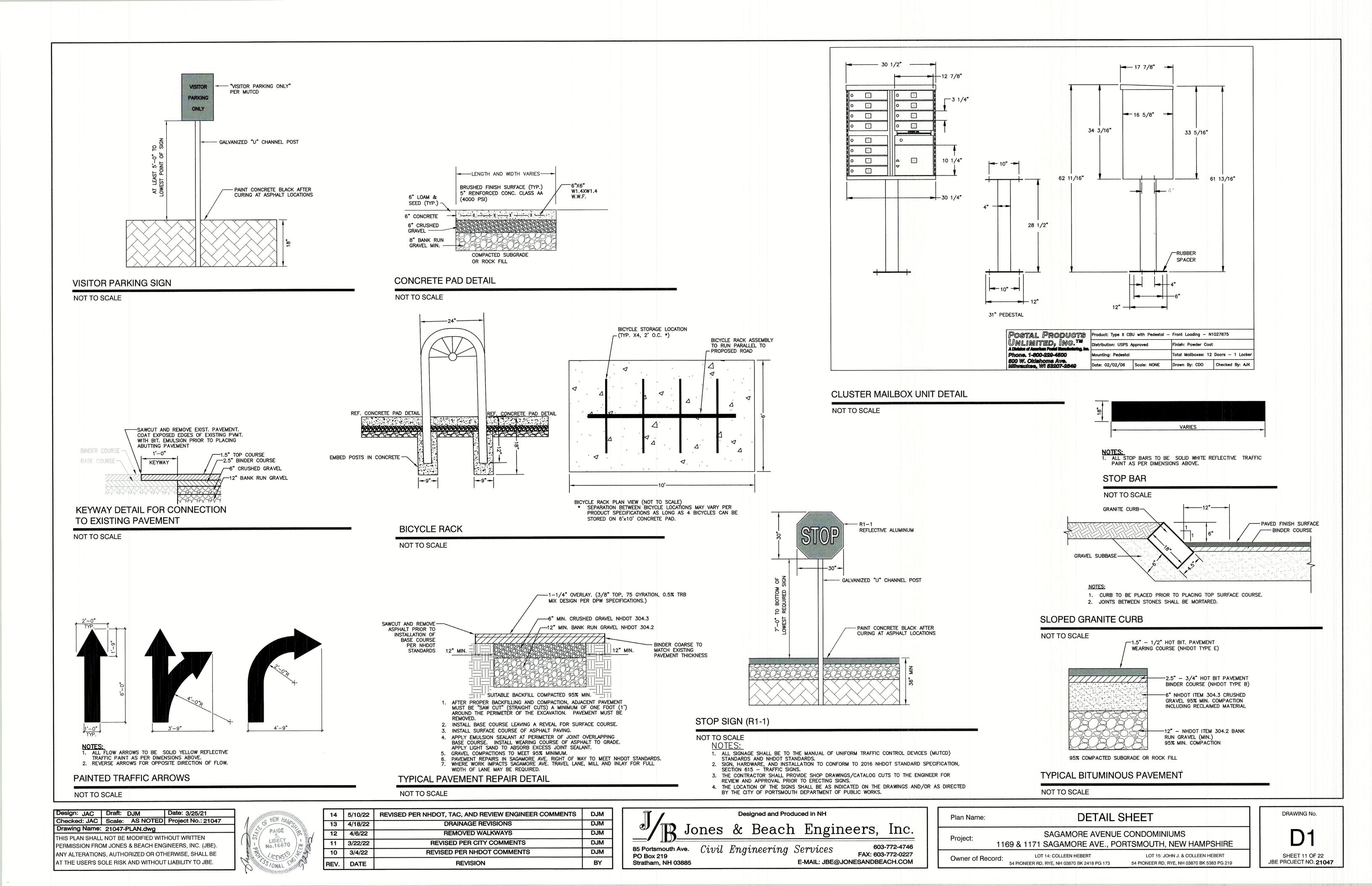
1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

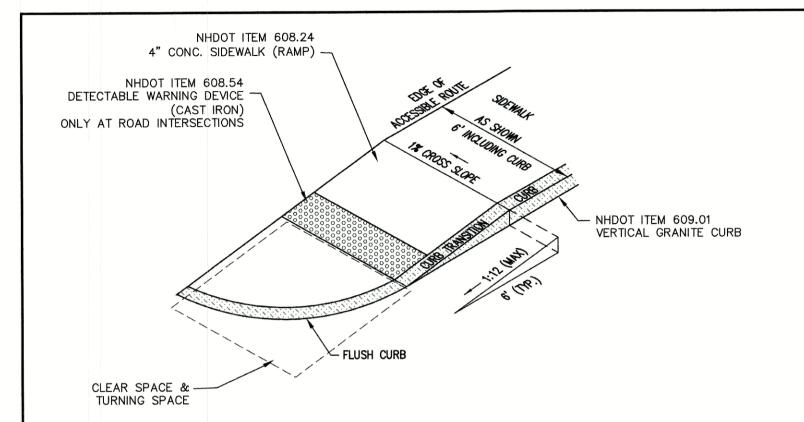
Owner of Record: LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

SHEET 10 OF 22
JBE PROJECT NO. **21047**

DRAWING No.



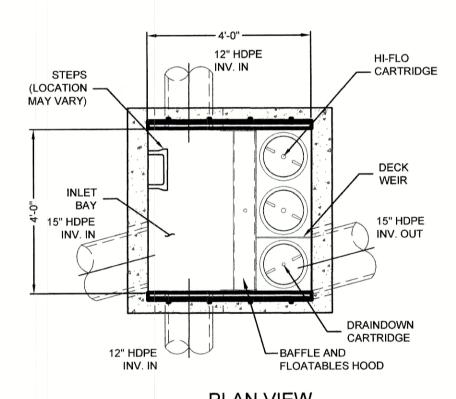


- 1. THE MAXIMUM ALLOWABLE CROSS SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) AND
- CURB SHALL BE 1.5% 2. THE MAXIMUM ALLOWABLE SLOPE OF ACCESSIBLE ROUTE EXCLUDING CURB RAMPS SHALL BE 5%.
- THE MAXIMUM ALLOWABLE SLOPE OF ACCESSIBLE ROUTE (SIDEWALK) CURB RAMPS
- SHALL BE 8.3% 4. A MINIMUM OF 4 FEET CLEAR SHALL BE MAINTAINED AT ANY PERMANENT OBSTACLE IN ACCESSIBLE ROUTE (i.e., HYDRANTS, UTILITY POLES, TREE WELLS,
- CURB TREATMENT VARIES, SEE PLANS FOR CURB TYPE. BASE OF RAMP SHALL BE GRADED TO PREVENT PONDING SEE TYPICAL SECTION FOR RAMP CONSTRUCTION.
- WHERE A CHANGE IN DIRECTION IS REQUIRED TO UTILIZE A CURB RAMP. A TURNING SPACE SHALL BE PROVIDED AT THE BASE AND/OR THE TOP OF THE CURB RAMP. TURNING SPACES SHALL BE PERMITTED TO OVERLAP CLEAR SPACES.
- 9. TURNING SPACE MAXIMUM CROSS SLOPE IS 2% IN ANY DIRECTION. 10. BEYOND THE BOTTOM GRADE BREAK, A CLEAR SPACE OF 4'X4' MINIMUM SHALL BE PROVIDED WITHIN THE WIDTH OF THE PEDESTRIAN CROSSWALK, AND OUTSIDE THE PARALLEL VEHICLE TRAVEL LANE. THE CLEAR SPACE MAY OVERLAP TURNING SPACES, DETECTABLE WARNING SURFACES AND DROP CURBS.

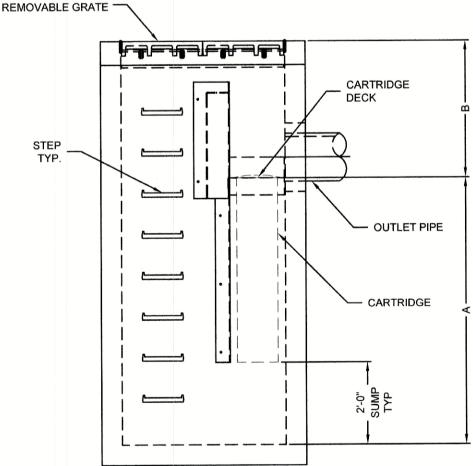
ACCESSIBLE CURB RAMP (NHDOT TYPE 1)

NOT TO SCALE

TRENCH FRAME AND



PLAN VIEW (TOP SLAB NOT SHOWN FOR CLARITY)



GENERAL NOTES:

1. CONTECH TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE

DETERMINED BY ENGINEER OF RECORD.

MAX. TREATMENT (CFS)

OUTLET INVERT TO RIM (MIN) (B)

TRENCH COVER

TLET INVERT TO STRUCTURE INVERT (A)

OW RATE HIGH-FLO / DRAINDOWN (CFS) (PER CART)

- 2. FOR SITE SPECIFIC DRAWINGS WITH DETAILED STRUCTURE DIMENSIONS AND WEIGHT, PLEASE CONTACT YOUR CONTECH ENGINEERED SOLUTIONS REPRESENTATIVE. www.ContechES.com
- 3. JELLYFISH WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS DRAWING. CONTRACTOR TO CONFIRM STRUCTURE MEETS REQUIREMENTS OF PROJECT. 4. STRUCTURE SHALL MEET AASHTO HS-20 OR PER APPROVING JURISDICTION REQUIREMENTS, WHICHEVER IS MORE STRINGENT, ASSUMING EARTH COVER OF 0', AND GROUNDWATER ELEVATION AT, OR BELOW, THE OUTLET

PIPE INVERT ELEVATION. ENGINEER OF RECORD TO CONFIRM ACTUAL GROUNDWATER ELEVATION. CASTINGS

TRENCH GRATE

DO NOT USE FOR THIS

APPLICATION

- SHALL MEET AASHTO M306 LOAD RATING AND BE CAST WITH THE CONTECH LOGO 5. STRUCTURE SHALL BE PRECAST CONCRETE CONFORMING TO ASTM C-857, ASTM C-918, AND AASHTO LOAD
- FACTOR DESIGN METHOD. 6. OUTLET PIPE INVERT IS EQUAL TO THE CARTRIDGE DECK ELEVATION.
- 7. THE OUTLET PIPE DIAMETER FOR NEW INSTALLATIONS IS RECOMMENDED TO BE ONE PIPE SIZE LARGER THAN THE INLET PIPE (WHERE APPLICABLE) AT EQUAL OR GREATER SLOPE.
- 8. NO PRODUCT SUBSTITUTIONS SHALL BE ACCEPTED UNLESS SUBMITTED 10 DAYS PRIOR TO PROJECT BID DATE, OR AS DIRECTED BY THE ENGINEER OF RECORD.
- INSTALLATION NOTES

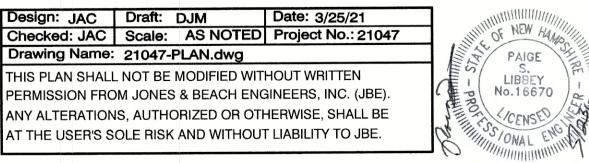
 A. ANY SUB-BASE, BACKFILL DEPTH, AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. CONTRACTOR TO PROVIDE EQUIPMENT WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE
- C. CONTRACTOR WILL INSTALL AND LEVEL THE STRUCTURE, SEALING THE JOINTS, LINE ENTRY AND EXIT POINTS (NON-SHRINK GROUT WITH APPROVED WATERSTOP OR FLEXIBLE BOOT).
- D. CARTRIDGE INSTALLATION, BY CONTECH, SHALL OCCUR ONLY AFTER SITE HAS BEEN STABILIZED AND THE JELLYFISH UNIT IS CLEAN AND FREE OF DEBRIS. CONTACT CONTECH TO COORDINATE CARTRIDGE INSTALLATION

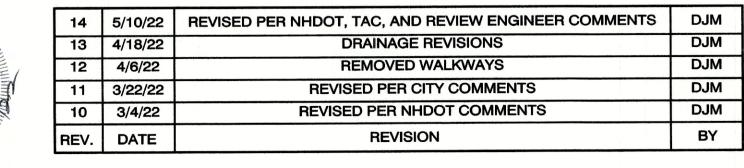
- PROJECT SPECIFIC NOTES

 1. 24" TRENCH GRATE SHALL NOT BE UTILIZED. UTILIZE TWO SOLID TRENCH COVERS INSTEAD. THREE PIPE INLETS SHALL BE CORED PER GRADING AND DRAINAGE PLAN. 2. SURFACE INLET CONFIGURATION WITH NO GRATE SHALL BE UTILIZED. DO NOT UTILIZE IN-LINE CONFIGURATION,
- 3. 12" INLETS SHALL ENTER AT EACH OPPOSING WALL OF INLET CHAMBER AND 15" INLET SHALL ENTER AT CORNER. INLET BAY SHALL BE CLOSEST TO SIDEWALK AND ALL THREE INLETS MUST ENTER DIRECTLY INTO THIS SECTION.

4' JELLYFISH FILTER - JF4

NOT TO SCALE





--FULL WIDTH OF SIDEWALK-

000000000

000000000

000000000

000000000

000000000

00000000

DETECTABLE WARNINGS SHALL CONSIST OF A SURFACE OF TRUNCATED DOMES AND SHALL COMPLY WITH THE FOLLOWING:

THE DETAIL PROVIDED IS NOT DRAWIN TO SCALE. THE QUANTITY OF DOMES

DEPICTED ON THE DETECTABLE WARNING DEVICE DETAIL IS FOR ILLUSTRATION

DETECTABLE WARNING FIELD INCLUDES A CONCRETE BORDER, IF PROVIDED.

PROPER INSTALLATION. IF REQUIRED, THE BORDER SHALL NOT EXCEED 2" IN

WIDTH OR 6" ALONG ROADWAY EDGE/CURB. THE BORDER DIMENSION SHALL BE

ON SLOPES OF 5% OR GREATER, THE ROWS OF DOMES SHALL BE ALIGNED TO BE

PERPENDICULAR OR RADIAL TO THE LOWER GRADE BREAK ON THE RAMP RUN. WHERE DOMES ARE ARRAYED RADIALLY, THEY MAY DIFFER IN DOME DIAMETER AND CENTER-TO-CENTER SPACING. ON SLOPES LESS THAN 5%, DOME

MINIMUM AND 2.4" MAXIMUM, AND A BASE-TO-BASE SPACING OF .65" MINIMUM,

ORIENTATION IS LESS CRITICAL AND MAY DIFFER FROM PERPENDICULAR OR

DETECTABLE WARNING SURFACES SHALL CONTRAST VISUALLY WITH ADJACENT

GUTTER, STREET, HIGHWAY, OR PEDESTRIAN ACCESS ROUTE SURFACE, EITHER

DETECTABLE WARNING PANELS SHALL BE CAST IRON WITH NO SURFACE COATING

DETECTABLE WARNING PANEL WITH TRUNCATED DOMES

0.089 / 0.045

TRUNCATED DOMES SHALL HAVE A CENTER-TO-CENTER SPACING OF 1.6"

MEASURED BETWEEN THE MOST ADJACENT DOMES ON A SQUARE GRID.

AND SHALL BE ALLOWED TO TRANSITION TO THEIR NATURAL PATINA.

TRUNCATED DOMES TO BE PLACED IN SIDEWALK BASE IN PUBLIC TRAFFIC AREAS.

C. SOME DETECTABLE WARNING PRODUCTS REQUIRE A CONCRETE BORDER FOR

ONLY. THE SIZE OF THE DETECTABLE WARNING FIELD SHALL BE 2' MINIMUM IN THE DIRECTION OF TRAVEL AND SHALL EXTEND THE FULL WIDTH OF THE CURB RAMP OR FLUSH SURFACE, EXCLUDING ANY FLARED SIDES. THE WIDTH OF THE

PLACEMENT AND ORIENTATION SHALL BE IN COMPLIANCE WITH THE PLANS AND

(MAX.), A TOP DIAMETER OF 50% OF THE BASE DIAMETER MINIMUM TO 65% OF

A. TRUNCATED DOMES SHALL HAVE A BASE DIAMETER OF 0.9" (MIN.) AND 1.4"

THE BASE DIAMETER MAXIMUM, AND A HEIGHT OF 0.2".

MEASURED FROM THE INSIDE EDGE OF THE RADIUS.

RADIAL ALIGNMENT TO THE GRADE BREAK.

0.133 / 0.067

LIGHT-ON-DARK OR DARK-ON-LIGHT

NOT TO SCALE

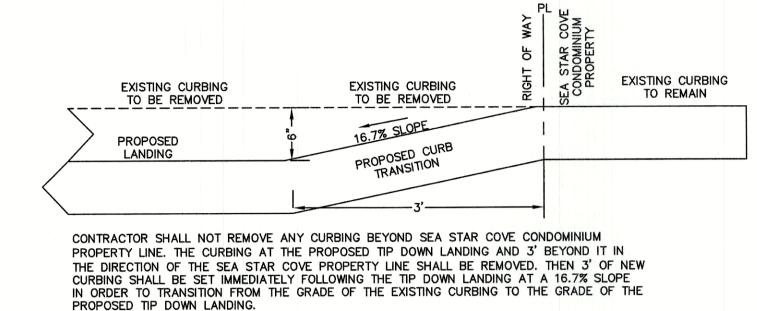
0.178 / 0.089

3'-4"

JELLYFISH DESIGN NOTES

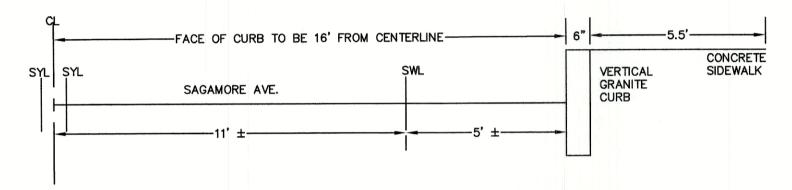
JELLYFISH TREATMENT CAPACITY IS A FUNCTION OF THE CARTRIDGE LENGTH AND THE NUMBER OF CARTRIDGES. THE STANDARD SURFACE INLET

STYLE WITH TRENCH COVER IS SHOWN. ALTERNATE CURB INLET OR PIPE INLET OPTIONS ARE AVAILABLE. PEAK CONVEYANCE CAPACITY TO BE



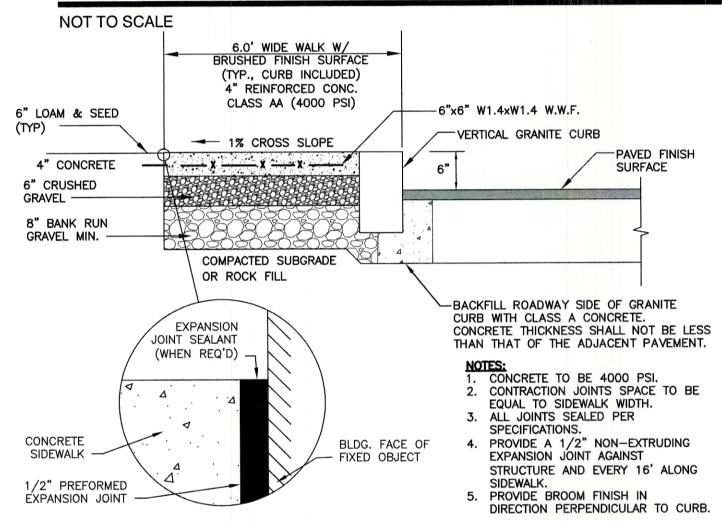
CURB TRANSITION AT SEA STAR COVE R.O.W LINE

NOT TO SCALE



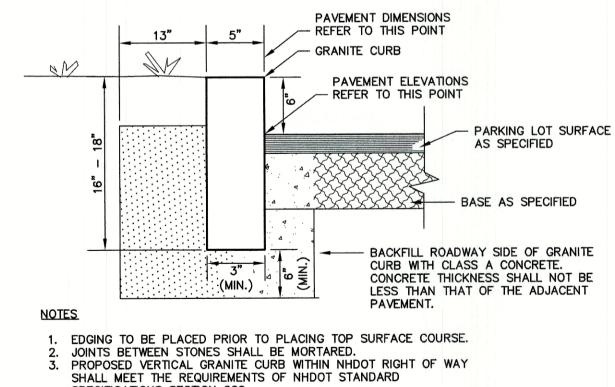
THE INTENT OF THIS DETAIL IS TO ILLUSTRATE THE LOCATION OF THE PROPOSED SIDEWALK IN RELATION TO THE CROSS SECTION OF SAGAMORE AVE. SEE BELOW CONCRETE SIDEWALK WITH VERTICAL GRANITE CURB DETAIL AS WELL

SAGAMORE AVE AND CONCRETE SIDEWALK CROSS SECTION



CONCRETE SIDEWALK W/ VERTICAL GRANITE CURB

NOT TO SCALE



SPECIFICATIONS SECTION 609.

VERTICAL GRANITE CURB

Designed and Produced in NH

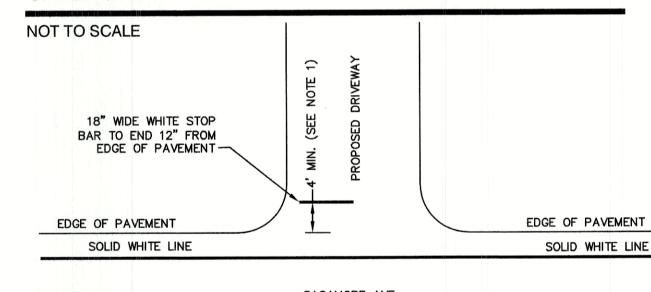
NOT TO SCALE

ALT. SLAB TOP REINFORCED TO MEET OR EXCEED REQUIREMENTS OF H20 LOADING -- AS REQUIRED -CAST IRON FRAME AND GRATE WITH H20 LOADING (TYPE B NEEENAH MODEL R-3570) -FINISH GRADE -FRAME TO BE SET IN FULL MORTAR BED ADJUST TO GRADE WITH BRICK OR PRE-CAST SQUARE * CONCRETE RINGS (12" MAX.) KENT SEAL ALL 5" MIN----FLEXIBLE BOOT CONFORMING ASTM SPEC. C-443 CAST-IN-PLACE OR FIELD INSTALLED -MIN .12 SQ. IN. STEEL PER VERTICAL FOOT PLACED ACCORDING TO AASHTO DESIGNATION M199 -6" OF 3/4" CRUSHED STONE COMPACTED SUBGRADE -COMPACTED TO 95% OF ASTM -1557 (NHDOT ITEM 304.3)

1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.

- 2. ALL SECTIONS SHALL BE DESIGNED FOR H20 LOADING.
- 3. CONCRETE SHALL BE COMPRESSIVE STRENGTH 4000 PSI, TYPE II CEMENT.
- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING
- 5. PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE CONNECTIONS SO AS TO BE WATERTIGHT.
- 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- 7. ALL CATCH BASIN FRAMES AND GRATES SHALL BE NHDOT CATCH BASIN TYPE ALTERNATE 1 OR NEENAH R-3570 OR APPROVED EQUAL (24"x24" TYPICAL). CATCH BASIN FRAME AND GRATE IN NHDOT RIGHT OF WAY MUST BE TYPE B.
- 8. STANDARD CATCH BASIN FRAME AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE 'DONUTS'.
- 9. CATCH BASINS CALLED OUT AS A "DEEP SUMP CATCH BASIN" SHALL HAVE A 48" SUMP; ALL OTHER CATCH BASINS SHALL HAVE A 36" SUMP.
- 10. INSTALL POLYETHYLENE LINER (NHDOT ITEM 604.0007) IN PROPOSED CATCH BASINS IN SAGAMORE AVE. RIGHT OF WAY.
- 11. PROPOSED CATCH BASINS WITHIN SAGAMORE AVE. RIGHT OF WAY SHALL MEET THE REQUIREMENTS OF NHDOT STANDARD SPECIFICATIONS SECTION 604.

CATCH BASIN



SAGAMORE AVE.

DOUBLE SOLID YELLOW LINE

DOUBLE SOLID YELLOW LINE

SOLID WHITE LINE EDGE OF PAVEMENT

- 1. LOCATION OF STOP BAR MAY VARY DUE TO INTERSECTION SIGHT DISTANCE AND VEHICLE TURNING RADIUS AND MAY NOT ALWAYS COINCIDE WITH THE LOCATION OF
- 2. END STOP BAR 12" FROM EDGE OF PAVEMENT.
- 3. STOP BARS, WORDS, LANE LINES, SYMBOLS AND ARROWS SHALL BE THERMOPLASTIC.
- 4. SOLID WHITE LINE AND DOUBLE SOLID YELLOW LINE SHALL NOT BREAK AT THE PROPOSED DRIVEWAY.

NHDOT PAVEMENT MARKINGS

NOT TO SCALE

DETAIL SHEET Plan Name: SAGAMORE AVENUE CONDOMINIUMS Project: 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

DRAWING No.

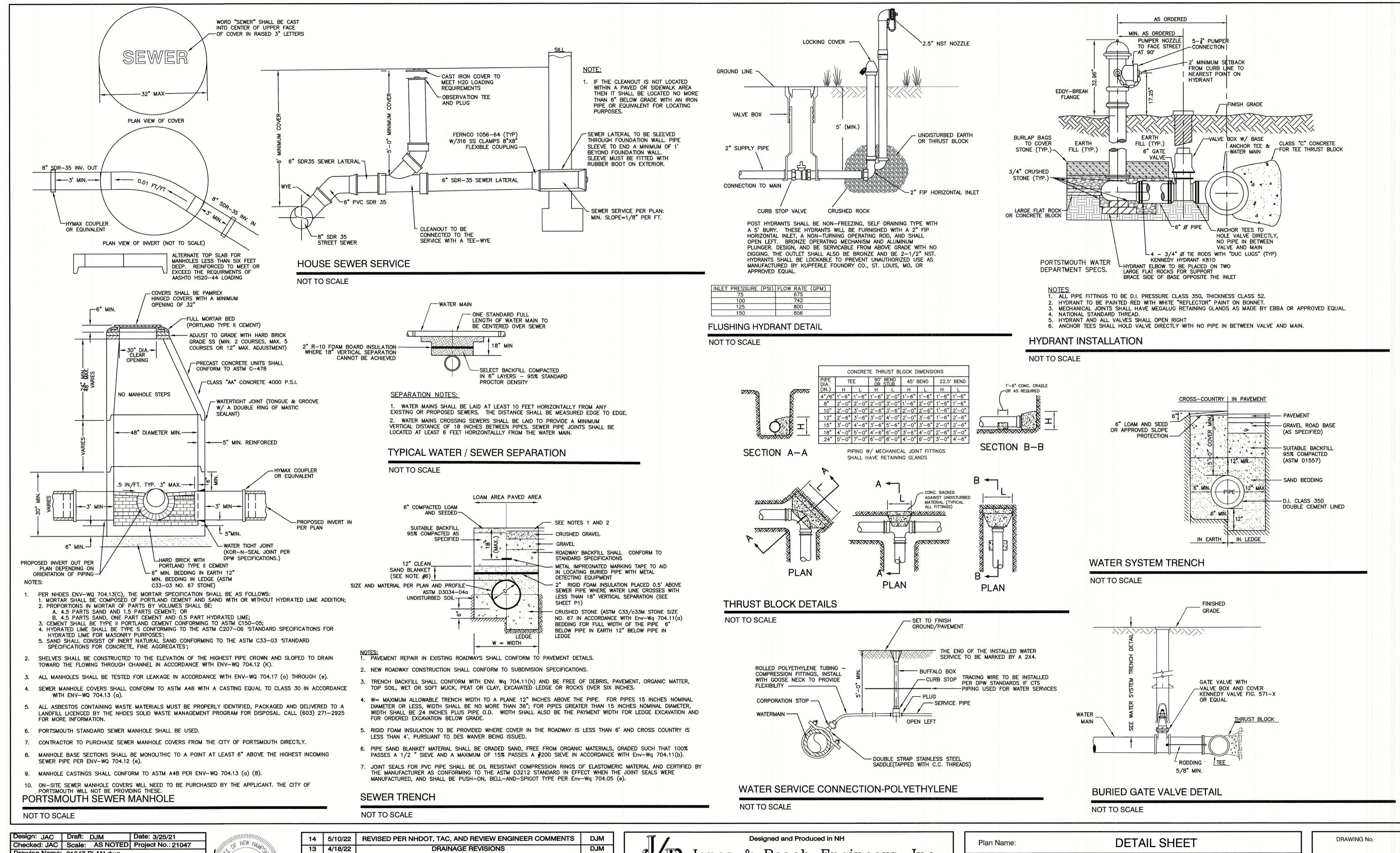
85 Portsmouth Ave. Civil Engineering Services 603-772-4746 FAX: 603-772-0227 PO Box 219 E-MAIL: JBE@JONESANDBEACH.COM Stratham, NH 03885

Jones & Beach Engineers, Inc.

LOT 14: COLLEEN HEBERT 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

LOT 15: JOHN J. & COLLEEN HEBERT 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

SHEET 12 OF 22 JBE PROJECT NO. 21047



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13	4/18/22	DRAINAGE REVISIONS	DJM
12	4/6/22	REMOVED WALKWAYS	DJM
11	3/22/22	REVISED PER CITY COMMENTS	DJM
10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
REV.	DATE	REVISION	BY

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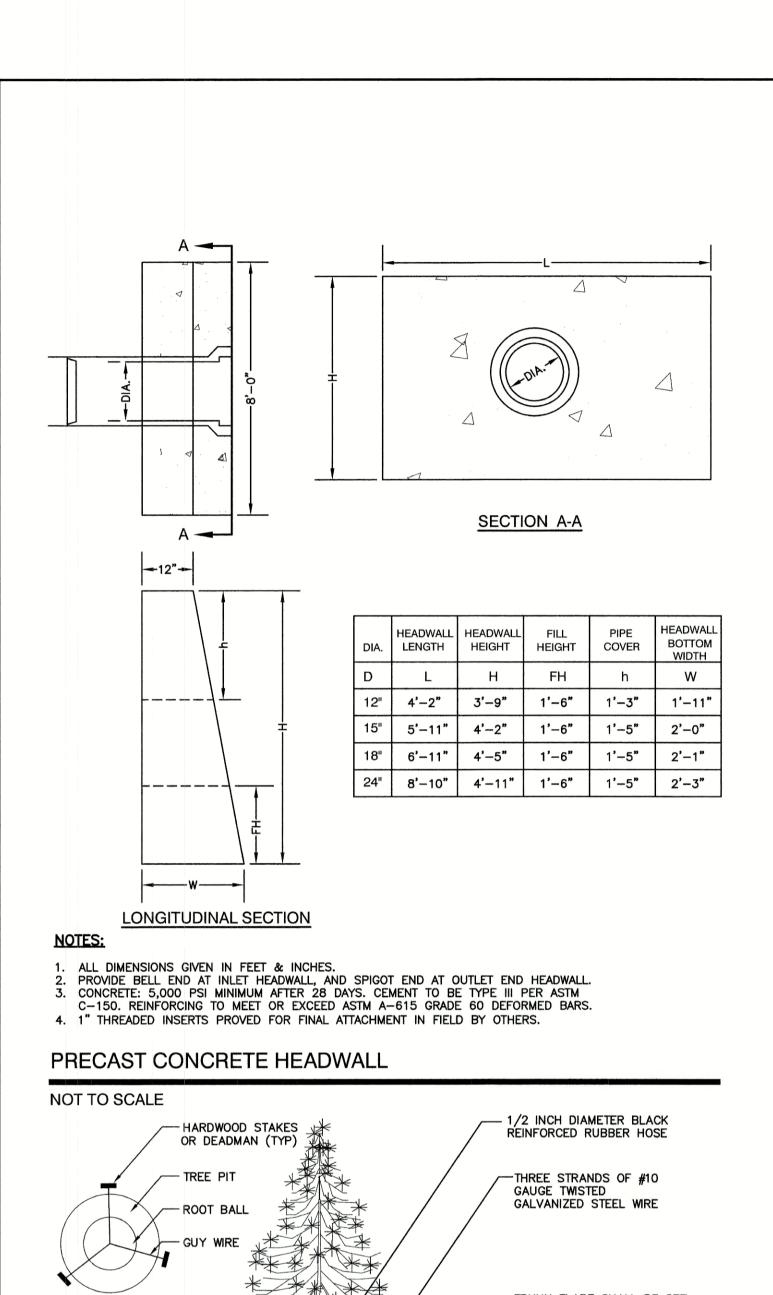
Plan Name:	DETAIL SH	HEET
Project:	SAGAMORE AVENUE C	
	169 & 1171 SAGAMORE AVE., POR	15MOUTH, NEW HAMPSHIRE
Owner of Rec	LOT 14: COLLEEN HEBERT	LOT 15: JOHN J. & COLLEEN HEBERT

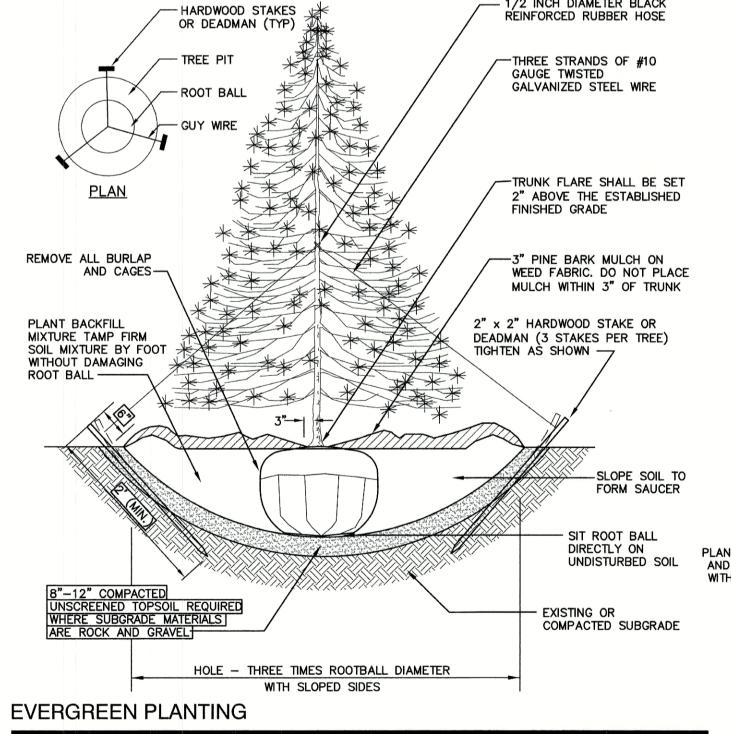
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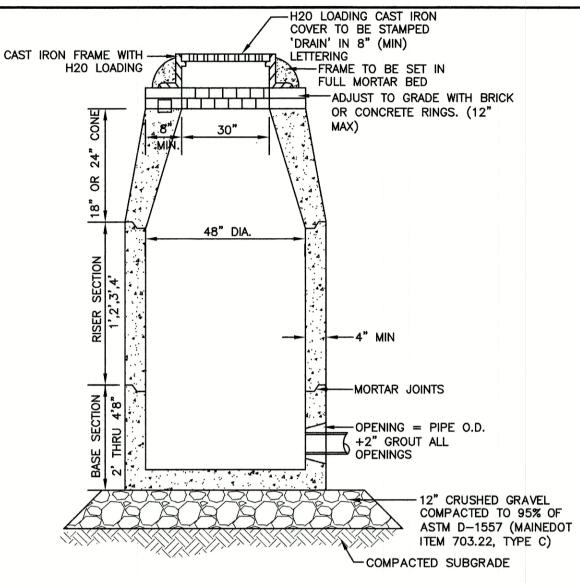
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Owner of Record:

SHEET 13 OF 22 JBE PROJECT NO. 21047



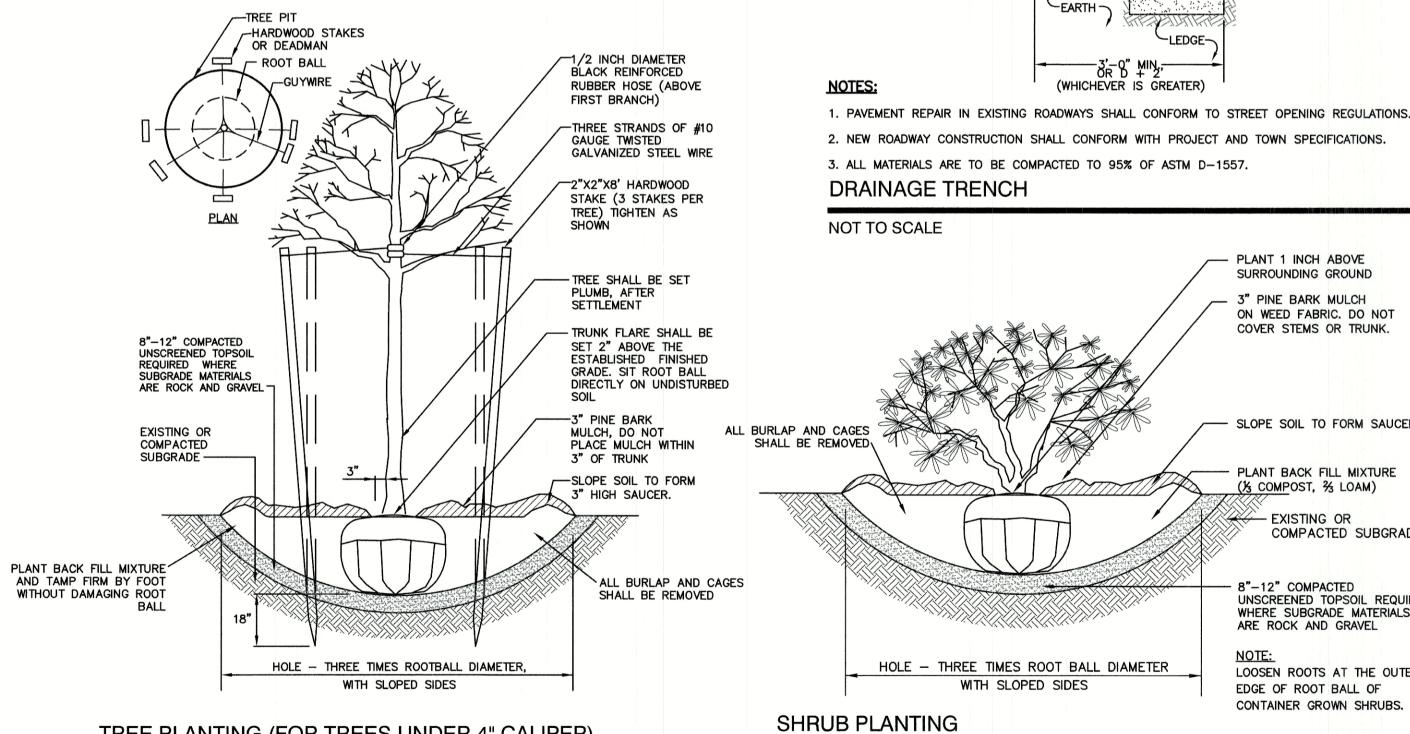




- 1. BASE SECTION SHALL BE MONOLITHIC WITH 48" INSIDE DIAMETER.
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- 4. FRAMES AND GRATES SHALL BE HEAVY DUTY AND DESIGNED FOR H20 LOADING.
- 5. PROVIDE "V" KNOCKOUTS FOR PIPES WITH 2" MAX. CLEARANCE TO OUTSIDE OF PIPE. MORTAR ALL PIPE
- CONNECTIONS SO AS TO BE WATERTIGHT. 6. JOINT SEALANT BETWEEN PRECAST SECTIONS SHALL BE BUTYL RUBBER.
- 7. ALL DRAIN MANHOLE FRAMES AND GRATES SHALL BE NEENAH R-1798 OR APPROVED EQUAL (30" DIA.
- 8. STANDARD FRAME(S) AND GRATE(S) SHALL BE SET IN FULL MORTAR BED. ADJUST TO GRADE WITH CLAY BRICK AND MORTAR (2 BRICK COURSES TYPICALLY, 5 BRICK COURSES MAXIMUM, BUT NO MORE THAN 12"), OR PRECAST CONCRETE 'DONUTS'.

DRAIN MANHOLE (4' DIAM.)

NOT TO SCALE



TREE PLANTING (FOR TREES UNDER 4" CALIPER)

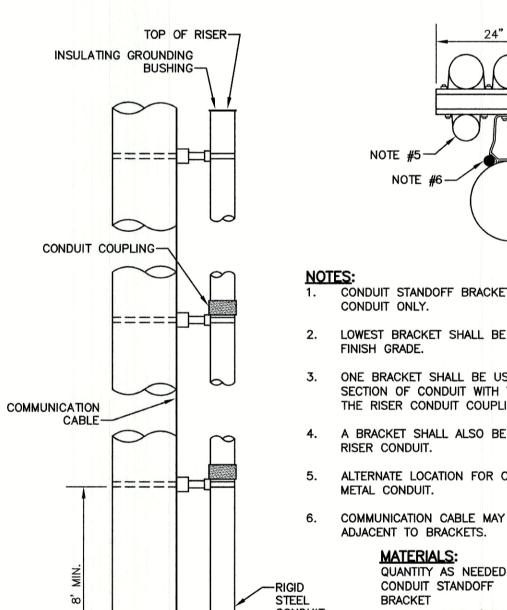
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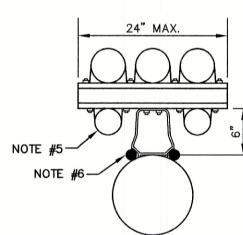
(12" MIN.) - EXCAVATION AND BACKFILL IN ACCORDANCE WITH UTILITY PLASTIC MARKER COMPANY STANDARDS TAPE ABOVE CABLES -ELECTRIC SERVICE CABLES 250 VAC OR LESS PVC-SCH 40 ---- CATV CABLE (PVC-SCH 2-SPARE 4" PVC - PRIMARY POWER 5" SCH. 80 PVC CABLE 7,200 VAC. OTHER POWER, TELEPHONE CATV. ETC., CABLES ARE NO CLOSER THAN 12"

NOTE: ALL UTILITIES SHALL BE REVIEWED AND APPROVED BY APPROPRIATE UTILITY COMPANY.

UTILITY TRENCH

NOT TO SCALE





- NOTES:
 1. CONDUIT STANDOFF BRACKETS TO BE USED WITH METAL
- 2. LOWEST BRACKET SHALL BE A MINIMUM OF 8 FEET ABOVE
- ONE BRACKET SHALL BE USED TO SUPPORT EACH 10 FT. SECTION OF CONDUIT WITH THE BRACKET PLACED JUST BELOW THE RISER CONDUIT COUPLING.
- 4. A BRACKET SHALL ALSO BE PLACED TO HOLD THE ROD OF THE
- ALTERNATE LOCATION FOR COMMUNICATION CABLE IF RUN IN
- 6. COMMUNICATION CABLE MAY BE ATTACHED DIRECTLY TO POLE

ADJACENT TO BRACKETS. ALUMA-FORM

CONDUIT STANDOFF 4-WAY T-SLOT (CUT TO REQUIRED LENGTH)

2" STK-2

CONDUIT STRAP KITS

2.5" STK-2.5 3" STK-3 3.5" STK-3.5 4" STK-4 5" STL-5 6" STK-6

6-CSO

UTILITY POLE RISER DETAIL

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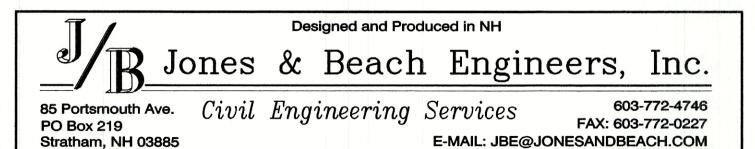
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	11	3/22/22	REVISED PER CITY COMMENTS	DJM
	10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
	REV.	DATE	REVISION	BY

NOT TO SCALE



LOAM AREA | PAVED AREA

EARTH -

6" COMPACTED LOAM ----

SUITABLE BACKFILL MATERIAL

SEE NOTES 1 AND 2

- CRUSHED GRAVEL

(NHDOT 304.3)

(NHDOT 304.2)

SPECIFICATIONS

BELOW PIPE IN LEDGE

PLANT 1 INCH ABOVE SURROUNDING GROUND

3" PINE BARK MULCH

ON WEED FABRIC. DO NOT

- SLOPE SOIL TO FORM SAUCER

- PLANT BACK FILL MIXTURE

(为 COMPOST, % LOAM)

COMPACTED SUBGRADE

UNSCREENED TOPSOIL REQUIRED WHERE SUBGRADE MATERIALS

LOOSEN ROOTS AT THE OUTER

EXISTING OR

8"-12" COMPACTED

ARE ROCK AND GRAVEL

EDGE OF ROOT BALL OF

CONTAINER GROWN SHRUBS.

COVER STEMS OR TRUNK.

- ROADWAY BACKFILL SHALL

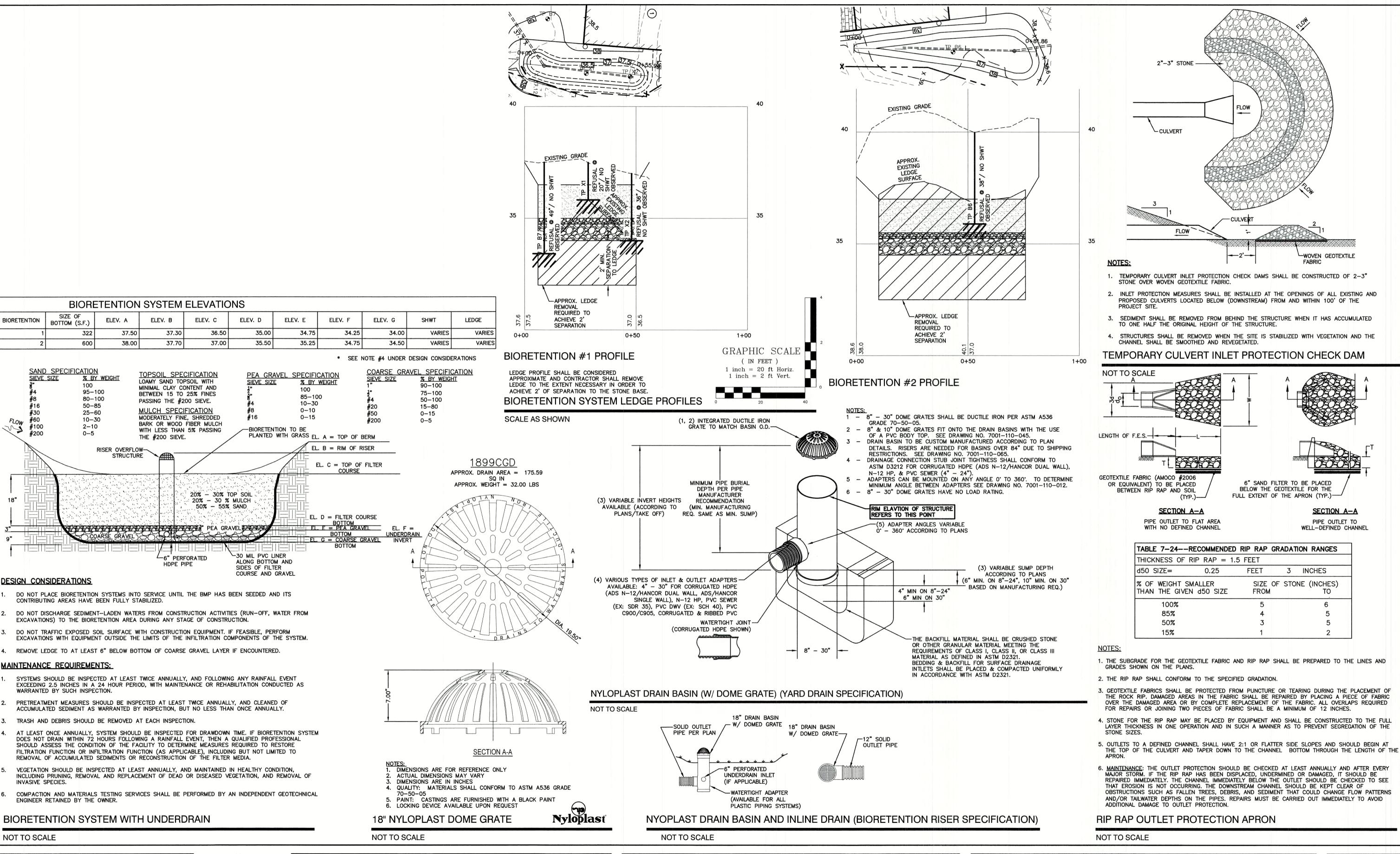
CONFORM TO STANDARD

-3/4" CRUSHED STONE BEDDING 6" BELOW PIPE IN EARTH 12"

> **DETAIL SHEET** Plan Name: SAGAMORE AVENUE CONDOMINIUMS Project: 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

SHEET 14 OF 22 JBE PROJECT NO. 21047

DRAWING No.



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Stratham, NH 03885

DETAIL SHEET Plan Name: SAGAMORE AVENUE CONDOMINIUMS Project: 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT

54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

Owner of Record:

2"-3" STONE -

- CULVERT

SECTION A-A

PIPE OUTLET TO FLAT AREA

WITH NO DEFINED CHANNEL

% OF WEIGHT SMALLER

85%

50%

THAN THE GIVEN d50 SIZE

d50 SIZE=

THICKNESS OF RIP RAP = 1.5 FEET

0.25

FLOW

-WOVEN GEOTEXTILE

6" SAND FILTER TO BE PLACED

BELOW THE GEOTEXTILE FOR THE

3 INCHES

SIZE OF STONE (INCHES)

SECTION A-A

PIPE OUTLET TO

WELL-DEFINED CHANNEL

FULL EXTENT OF THE APRON (TYP.)-

TABLE 7-24--RECOMMENDED RIP RAP GRADATION RANGES

LOT 15: JOHN J. & COLLEEN HEBERT

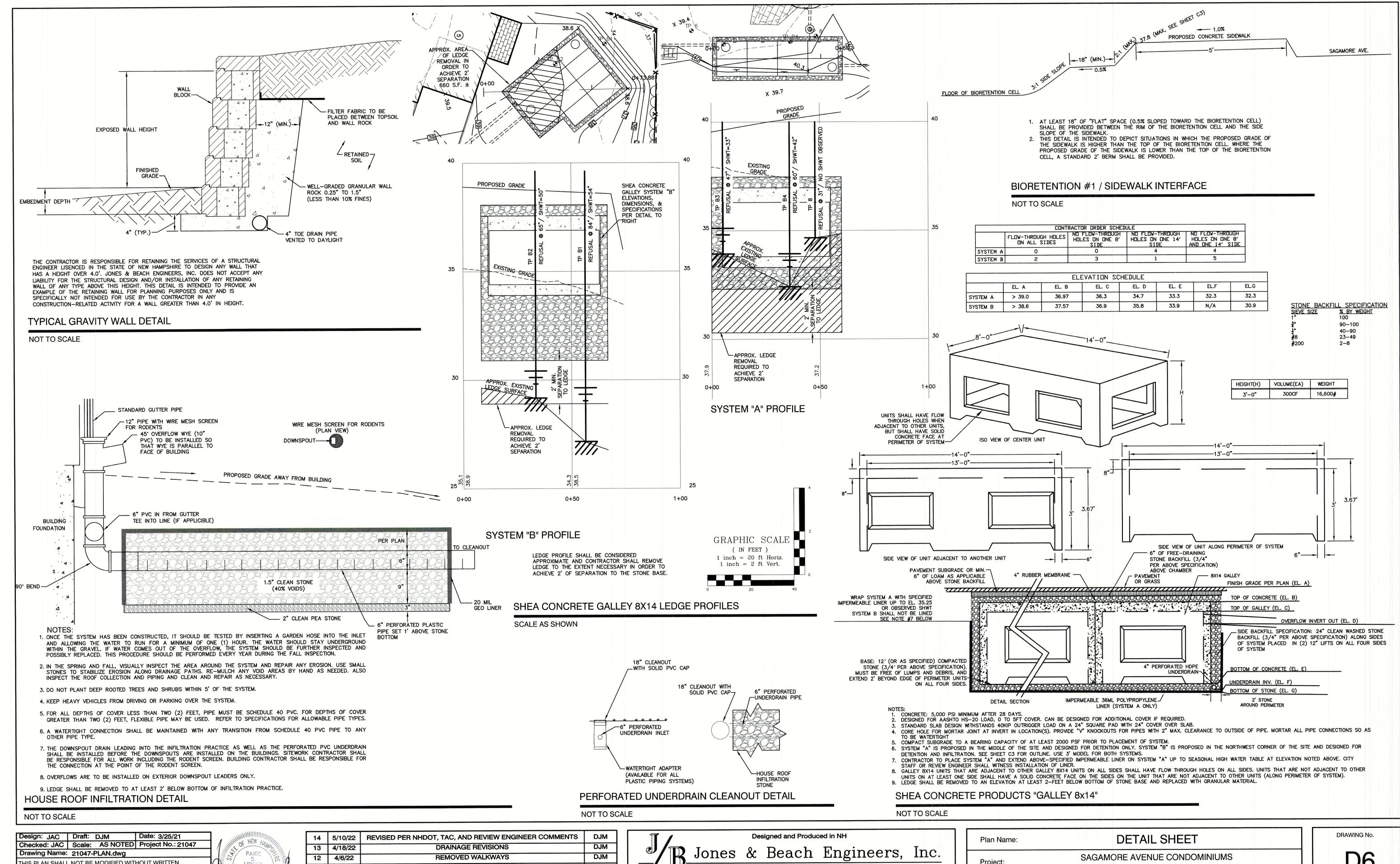
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FEET

FROM

DRAWING No. SHEET 15 OF 22

JBE PROJECT NO. 21047



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12	4/6/22	REMOVED WALKWAYS	DJM
13	4/18/22	DRAINAGE REVISIONS	DJM
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PO Box 219 Stratham, NH 03885			E-MAIL: JBE@J	ONESANDBEACH.COM

Plan Name:	DETAIL SHEET	
Project:	SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSH	HIRE
Owner of Dec	LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBE	RT

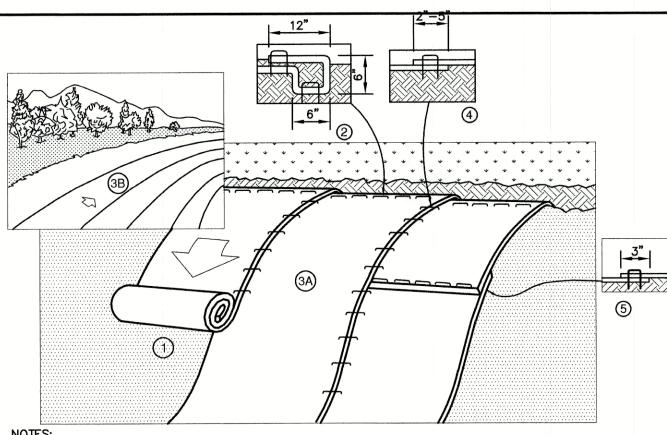
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SHEET 16 OF 22 JBE PROJECT NO. 21047

FEMPORARY EROSION CONTROL NOTES

- THE SMALLEST PRACTICAL AREA OF LAND SHALL BE EXPOSED AT ANY ONE TIME. AT NO TIME SHALL AN AREA IN EXCESS OF 5 ACRES BE EXPOSED AT ANY ONE TIME BEFORE DISTURBED AREAS ARE STABILIZED.
- EROSION, SEDIMENT AND DETENTION MEASURES SHALL BE INSTALLED AS SHOWN ON THE PLANS AND AT LOCATIONS AS REQUIRED, DIRECTED BY THE ENGINEER.
- ALL DISTURBED AREAS (INCLUDING POND AREAS BELOW THE PROPOSED WATERLINE) SHALL BE RETURNED TO PROPOSED GRADES AND ELEVATIONS. DISTURBED AREAS SHALL BE LOAMED WITH A MINIMUM OF 6" OF SCREENED ORGANIC LOAM AND SEEDED WITH SEED MIXTURE 'C' AT A RATE NOT LESS THAN 1.10 POUNDS OF SEED PER 1,000 S.F. OF AREA (48 LBS. /
- SILT FENCES AND OTHER BARRIERS SHALL BE INSPECTED EVERY SEVEN CALENDAR DAYS AND WITHIN 24 HOURS OF A RAINFALL OF 0.5" OR GREATER. ALL DAMAGED AREAS SHALL BE REPAIRED, AND SEDIMENT DEPOSITS SHALL PERIODICALLY BE
- AFTER ALL DISTURBED AREAS HAVE BEEN STABILIZED, THE TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED AND THE AREA DISTURBED BY THE REMOVAL SMOOTHED AND RE-VEGETATED.
- AREAS MUST BE SEEDED AND MULCHED OR OTHERWISE PERMANENTLY STABILIZED WITHIN 3 DAYS OF FINAL GRADING, OR TEMPORARILY STABILIZED WITHIN 14 DAYS OF THE INITIAL DISTURBANCE OF SOIL. ALL AREAS SHALL BE STABILIZED WITHIN 45
- ALL PROPOSED VEGETATED AREAS THAT DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED BY SEEDING AND INSTALLING NORTH AMERICAN GREEN S150 EROSION CONTROL BLANKETS (OR AN EQUIVALENT APPROVED IN WRITING BY THE ENGINEER) ON SLOPES GREATER THAN 3:1, AND SEEDING AND PLACING 3 TO 4 TONS OF MULCH PER ACRE, SECURED WITH ANCHORED NETTING, ELSEWHERE. THE INSTALLATION OF EROSION CONTROL BLANKETS OR MULCH AND NETTING SHALL NOT OCCUR OVER ACCUMULATED SNOW OR ON FROZEN GROUND AND SHALL BE COMPLETED IN ADVANCE OF THAW OR SPRING MELT EVENTS.
- ALL DITCHES OR SWALES WHICH DO NOT EXHIBIT A MINIMUM OF 85 PERCENT VEGETATIVE GROWTH BY OCTOBER 15, OR WHICH ARE DISTURBED AFTER OCTOBER 15, SHALL BE STABILIZED TEMPORARILY WITH STONE OR EROSION CONTROL BLANKETS APPROPRIATE FOR THE DESIGN FLOW CONDITIONS.
- AFTER OCTOBER 15th, INCOMPLETE ROAD OR PARKING SURFACES, WHERE WORK HAS STOPPED FOR THE WINTER SEASON, SHALL BE PROTECTED WITH A MINIMUM OF 3" OF CRUSHED GRAVEL PER NHDOT ITEM 304.3.
- AN AREA SHALL BE CONSIDERED STABLE IF ONE OF THE FOLLOWING HAS OCCURRED:
 - BASE COURSE GRAVELS HAVE BEEN INSTALLED IN AREAS TO BE PAVED;
 - b. A MINIMUM OF 85% VEGETATED GROWTH HAS BEEN ESTABLISHED;
 - c. A MINIMUM OF 3" OF NON-EROSIVE MATERIAL SUCH STONE OR RIPRAP HAS BEEN INSTALLED; OR
 - d. EROSION CONTROL BLANKETS HAVE BEEN PROPERLY INSTALLED.
- FUGITIVE DUST CONTROL IS REQUIRED TO BE CONTROLLED IN ACCORDANCE WITH ENV-A 1000, AND THE PROJECT IS TO MEET THE REQUIREMENTS AND INTENT OF RSA 430:53 AND AGR 3800 RELATIVE TO INVASIVE SPECIES.



- PREPARE SOIL BEFORE INSTALLING BLANKETS, INCLUDING ANY NECESSARY APPLICATION OF LIME, FERTILIZER, AND SEED. NOTE: WHEN USING CELL-O-SEED DO NOT SEED PREPARED AREA. CELL-O-SEED MUST BE INSTALLED WITH PAPER SIDE DOWN.
- 2. BEGIN AT THE TOP OF THE SLOPE BY ANCHORING THE BLANKET IN A 6" DEEP BY 6" WIDE TRENCH WITH APPROXIMATELY 12" OF BLANKET EXTENDED BEYOND THE UP-SLOPE PORTION OF THE TRENCH. ANCHOR THE BLANKET WITH A ROW OF STAPLES/STAKES APPROXIMATELY 12" APART IN THE BOTTOM OF THE TRENCH, BACKFILL AND COMPACT THE TRENCH AFTER STAPLING. APPLY SEED TO COMPACTED SOIL AND FOLD REMAINING 12" PORTION OF BLANKET BACK OVER SEED AND COMPACTED SOIL. | SECURE BLANKET OVER COMPACTED SOIL WITH A ROW OF STAPLES/STAKES SPACED APPROXIMATELY 12" APART ACROSS THE WIDTH OF THE BLANKET.
- 3. ROLL THE BLANKETS (A) DOWN OR (B) HORIZONTALLY ACROSS THE SLOPE. BLANKETS WILL UNROLL WITH APPROPRIATE SIDE AGAINST THE SOIL SURFACE. ALL BLANKETS MUST BE SECURELY FASTENED TO SOIL SURFACE BY PLACING STAPLES/STAKES IN APPROPRIATE LOCATIONS AS SHOWN IN THE STAPLE PATTERN GUIDE. WHEN USING OPTIONAL DOT SYSTEMTM, STAPLES/STAKES SHOULD BE PLACED THROUGH EACH OF THE COLORED DOTS CORRESPONDING TO THE APPROPRIATE STAPLE PATTERN.
- 4. THE EDGES OF PARALLEL BLANKETS MUST BE STAPLED WITH APPROXIMATELY 2"-5" OVERLAP DEPENDING ON BLANKET TYPE. TO ENSURE PROPER SEAM ALIGNMENT, PLACE THE EDGE OF THE OVERLAPPING BLANKET (BLANKET BEING INSTALLED ON TOP) EVEN WITH THE COLORED SEAM STITCH ON THE PREVIOUSLY INSTALLED BLANKET.
- 5. CONSECUTIVE BLANKETS SPLICED DOWN THE SLOPE MUST BE PLACED END OVER END (SHINGLE STYLE) WITH AN APPROXIMATE 3" OVERLAP. STAPLE THROUGH OVERLAPPED AREA, APPROXIMATELY 12" APART ACROSS ENTIRE BLANKET WIDTH. NOTE: IN LOOSE SOIL CONDITIONS, THE USE OF STAPLE OR STAKE LENGTHS GREATER THAN 6" MAY BE NECESSARY TO PROPERLY SECURE THE BLANKETS.



NORTH AMERICAN GREEN

14649 HIGHWAY 41 NORTH EVANSVILLE, INDIANA 47725 1-800-772-2040

EROSION CONTROL BLANKET SLOPE INSTALLATION NORTH AMERICAN GREEN (800) 772-2040

-MAXIMUM RECOMMENDED

CONTOUR LINES___

600' RECOMMENDED MAXIMUM

-FLARE ENDS UPHILL TO PROVIDE

7. SILT FENCES SHALL BE REMOVED WHEN NO LONGER NEEDED AND THE SEDIMENT COLLECTED SHALL BE DISPOSED AS DIRECTED BY THE ENGINEER. THE AREA DISTURBED BY THE REMOVAL SHALL BE

1. SILT FENCES SHALL BE INSPECTED IMMEDIATELY AFTER EACH RAINFALL AND AT LEAST DAILY DURING

2. IF THE FABRIC ON A SILT FENCE SHOULD DECOMPOSE OR BECOME INEFFECTIVE DURING THE EXPECTED

3. SEDIMENT DEPOSITS SHOULD BE INSPECTED AFTER EVERY STORM EVENT. THE DEPOSITS SHOULD BE

4. SEDIMENT DEPOSITS THAT ARE REMOVED, OR LEFT IN PLACE AFTER THE FABRIC HAS BEEN REMOVED,

PROLONGED RAINFALL. ANY REPAIRS THAT ARE REQUIRED SHALL BE DONE IMMEDIATELY.

REMOVED WHEN THEY REACH APPROXIMATELY ONE HALF THE HEIGHT OF THE BARRIER.

SHALL BE GRADED TO CONFORM WITH THE EXISTING TOPOGRAPHY AND VEGETATED.

LIFE OF THE FENCE, THE FABRIC SHALL BE REPLACED PROMPTLY.

TRAPPING CAPABILITY AND SEDIMENT

UNCONTROLLED SLOPE LENGTH

-FENCING IS TO RUN WITH THE

CONTOURS ACROSS A SLOPE

NOT TO SCALE

► DISTURBED AREA

(UPHILL) -

SMOOTHED AND REVEGETATED.

MAINTENANCE:

AREA OF EMBANKMEN CONSTRUCTION OR ANY DISTURBED AREA TO BE STABILIZED (UPHILL)-GEOTEXTILE FENCE WITH PROPEX-SILT STOP SEDIMENT CONTROL FABRIC OR APPROVED EQUAL 48" HARDWOOD 16" POST DEPTH (MIN)

CONSTRUCTION SPECIFICATIONS:

- WOVEN FABRIC FENCE TO BE FASTENED SECURELY TO FENCE POSTS WITH WIRE TIES OR STAPLES. FILTER CLOTH SHALL BE FASTENED TO WOVEN WIRE EVERY 24" AT TOP, MID AND BOTTOM AND EMBEDDED IN THE GROUND A MINIMUM OF 8" AND THEN COVERED WITH SOIL.
- 2. THE FENCE POSTS SHALL BE A MINIMUM OF 48" LONG, SPACED A MAXIMUM 10' APART, AND DRIVEN A MINIMUM OF 16" INTO THE GROUND.
- 3. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER, THE ENDS OF THE FABRIC SHALL BE OVERLAPPED 6", FOLDED AND STAPLED TO PREVENT SEDIMENT FROM BY-PASSING. 4. MAINTENANCE SHALL BE PERFORMED AS NEEDED AND SEDIMENT REMOVED AND PROPERLY DISPOSED OF
- 5. PLACE THE ENDS OF THE SILT FENCE UP CONTOUR TO PROVIDE FOR SEDIMENT STORAGE.

Date: 3/25/21

6. SILT FENCE SHALL REMAIN IN PLACE FOR 24 MONTHS

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WHEN IT IS 6" DEEP OR VISIBLE 'BULGES' DEVELOP IN THE SILT FENCE.

SILT FENCE

NOT TO SCALE

Design: JAC | Draft: DJM

Drawing Name: 21047-PLAN.dwg



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)	11	3/22/22	REVISED PER CITY COMMENTS	DJM
	10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
	REV.	DATE	REVISION	BY

SEEDING SPECIFICATIONS

- . GRADING AND SHAPING A. SLOPES SHALL NOT BE STEEPER THAN 2:1 WITHOUT APPROPRIATE EROSION CONTROL MEASURES AS
- SPECIFIED ON THE PLANS (3:1 SLOPES OR FLATTER ARE PREFERRED). B. WHERE MOWING WILL BE DONE, 3:1 SLOPES OR FLATTER ARE RECOMMENDED.

2. SEEDBED PREPARATION

- A. SURFACE AND SEEPAGE WATER SHOULD BE DRAINED OR DIVERTED FROM THE SITE TO PREVENT DROWNING OR WINTER KILLING OF THE PLANTS.
- B. STONES LARGER THAN 4 INCHES AND TRASH SHOULD BE REMOVED BECAUSE THEY INTERFERE WITH SEEDING AND FUTURE MAINTENANCE OF THE AREA. WHERE FEASIBLE, THE SOIL SHOULD BE TILLED TO A DEPTH OF ABOUT 4 INCHES TO PREPARE A SEEDBED AND FERTILIZER AND LIME MIXED INTO THE SOIL. THE SEEDBED SHOULD BE LEFT IN A REASONABLY FIRM AND SMOOTH CONDITION. THE LAST TILLAGE OPERATION SHOULD BE PERFORMED ACROSS THE SLOPE WHEREVER PRACTICAL.

- A. LIME AND FERTILIZER SHOULD BE APPLIED PRIOR TO OR AT THE TIME OF SEEDING AND INCORPORATED INTO THE SOIL. TYPES AND AMOUNTS OF LIME AND FERTILIZER SHOULD BE BASED ON AN EVALUATION OF SOIL TESTS. WHEN A SOIL TEST IS NOT AVAILABLE, THE FOLLOWING MINIMUM AMOUNTS SHOULD BE
- AGRICULTURAL LIMESTONE, 2 TONS PER ACRE OR 100 LBS. PER 1,000 SQ.FT. NITROGEN(N), 50 LBS. PER ACRE OR 1.1 LBS. PER 1,000 SQ.FT. PHOSPHATE(P205), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT.
- POTASH(K2O), 100 LBS. PER ACRE OR 2.2 LBS. PER 1,000 SQ.FT. (NOTE: THIS IS THE EQUIVALENT OF 500 LBS. PER ACRE OF 10-20-20 FERTILIZER OR 1,000 LBS. PER ACRE OF 5-10-10.)
- SEED SHOULD BE SPREAD UNIFORMLY BY THE METHOD MOST APPROPRIATE FOR THE SITE. METHODS INCLUDE BROADCASTING, DRILLING AND HYDROSEEDING. WHERE BROADCASTING IS USED, COVER SEED WITH .25 INCH OF SOIL OR LESS, BY CULTIPACKING OR RAKING.
- C. REFER TO THE 'SEEDING GUIDE' AND 'SEEDING RATES' TABLES ON THIS SHEET FOR APPROPRIATE SEED MIXTURES AND RATES OF SEEDING. ALL LEGUMES (CROWNVETCH, BIRDSFOOT, TREFOIL AND FLATPEA) MUST BE INOCULATED WITH THEIR SPECIFIC INOCULANT PRIOR TO THEIR INTRODUCTION TO THE SITE.
- WHEN SEEDED AREAS ARE MULCHED, PLANTINGS MAY BE MADE FROM EARLY SPRING TO EARLY OCTOBER. WHEN SEEDED AREAS ARE NOT MULCHED, PLANTINGS SHOULD BE MADE FROM EARLY SPRING TO MAY 20th OR FROM AUGUST 10th TO SEPTEMBER 1st.

YET COMPLETE.

A. HAY, STRAW, OR OTHER MULCH, WHEN NEEDED, SHOULD BE APPLIED IMMEDIATELY AFTER SEEDING. B. MULCH WILL BE HELD IN PLACE USING APPROPRIATE TECHNIQUES FROM THE BEST MANAGEMENT PRACTICE FOR MULCHING. HAY OR STRAW MULCH SHALL BE PLACED AT A RATE OF 90 LBS PER 1000 S.F.

5. MAINTENANCE TO ESTABLISH A STAND

- A. PLANTED AREAS SHOULD BE PROTECTED FROM DAMAGE BY FIRE, GRAZING, TRAFFIC, AND DENSE WEED
- FERTILIZATION NEEDS SHOULD BE DETERMINED BY ONSITE INSPECTIONS. SUPPLEMENTAL FERTILIZER IS USUALLY THE KEY TO FULLY COMPLETE THE ESTABLISHMENT OF THE STAND BECAUSE MOST PERENNIALS TAKE 2 TO 3 YEARS TO BECOME FULLY ESTABLISHED.
- C. IN WATERWAYS, CHANNELS, OR SWALES WHERE UNIFORM FLOW CONDITIONS ARE ANTICIPATED, ANNUAL MOWING MAY BE NECESSARY TO CONTROL GROWTH OF WOODY VEGETATION.

USE	SEEDING MIXTURE 1/	DROUGHTY	WELL DRAINED	MODERATELY WELL DRAINED	POORLY DRAINED
STEEP CUTS AND FILLS, BORROW AND DISPOSAL AREAS	A B C	FAIR POOR POOR	GOOD GOOD GOOD	GOOD FAIR EXCELLENT	FAIR FAIR GOOD
AREAS	D	FAIR	EXCELLENT	EXCELLENT	POOR
WATERWAYS, EMERGENC' SPILLWAYS, AND OTHER CHANNELS WITH FLOWING WATER.	Y A C	GOOD GOOD	GOOD EXCELLENT	GOOD EXCELLENT	FAIR FAIR
LIGHTLY USED PARKING LOTS, ODD AREAS, UNUSED LANDS, AND LOW INTENSITY USE RECREATION SITES.	A B C	GOOD GOOD GOOD	GOOD GOOD EXCELLENT	GOOD FAIR EXCELLENT	FAIR POOR FAIR
PLAY AREAS AND ATHLETIC FIELDS. (TOPSOIL IS ESSENTIAL FOR GOOD TURF.)	E F	FAIR FAIR	EXCELLENT EXCELLENT	EXCELLENT EXCELLENT	<u>2/</u> 2/

GRAVEL PIT, SEE NH-PM-24 IN APPENDIX FOR RECOMMENDATION REGARDING RECLAMATION OF SAND

/ REFER TO SEEDING MIXTURES AND RATES IN TABLE BELOW. 27 POORLY DRAINED SOILS ARE NOT DESIRABLE FOR USE AS PLAYING AREA AND ATHLETIC FIELDS. NOTE: TEMPORARY SEED MIX FOR STABILIZATION OF TURF SHALL BE WINTER RYE OR OATS AT A RATE OF 2.5 LBS. PER 1000 S.F. AND SHALL BE PLACED PRIOR TO OCTOBER 15th, IF PERMANENT SEEDING NOT

SEEDING GUIDE

MIXTURE	POUNDS PER ACRE	POUNDS F 1.000 Sq.
A. TALL FESCUE	20	0.45
CREEPING RED FESCUE	20	0.45
RED TOP	2	0.05
TOTAL	42	0.95
B. TALL FESCUE CREEPING RED FESCUE CROWN VETCH OR	15 10 15	0.35 0.25 0.35
FLAT PEA	30	0.75
TOTAL	40 OR 55	0.95 OR 1.3
C. TALL FESCUE CREEPING RED FESCUE BIRDS FOOT TREFOIL TOTAL	20 20 <u>8</u> 48	0.45 0.45 <u>0.20</u> 1.10
D. TALL FESCUE	20	0.45
FLAT PEA	30	<u>0.75</u>
TOTAL	50	1.20
E. CREEPING RED FESCUE 1/	50	1.15
KENTUCKY BLUEGRASS 1/	50	1.15
TOTAL	100	2.30
F. TALL FESCUE 1	150	3.60

SEEDING RATES

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EXISTING PAVEMENT -MOUNTABLE BERM EXISTING GROUND (OPTIONAL) WOVEN GEOTEXTILE **PROFILE** FILTER FABRIC -50' MINIMUM-PAVEMENT : PLAN VIEW RECYCLED CONCRETE EQUIVALENT.

- 1. STONE FOR STABILIZED CONSTRUCTION ENTRANCE SHALL BE 1 TO 2 INCH STONE, RECLAIMED STONE, OR
- 2. THE LENGTH OF THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 50 FEET, EXCEPT FOR A SINGLE
- RESIDENTIAL LOT WHERE A 30 FOOT MINIMUM LENGTH WOULD APPLY. 3. THICKNESS OF THE STONE FOR THE STABILIZED ENTRANCE SHALL NOT BE LESS THAN 6 INCHES.
- 4. THE WIDTH OF THE ENTRANCE SHALL NOT BE LESS THAN THE FULL WIDTH OF THE ENTRANCE WHERE INGRESS OR EGRESS OCCURS, OR 10 FEET, WHICHEVER IS GREATER.
- 5. GEOTEXTILE FILTER FABRIC SHALL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING THE STONE. FILTER FABRIC IS NOT REQUIRED FOR A SINGLE FAMILY RESIDENTIAL LOT.
- 6. ALL SURFACE WATER THAT IS FLOWING TO OR DIVERTED TOWARD THE CONSTRUCTION ENTRANCE SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A STONE BERM WITH 5:1 SLOPES THAT CAN BE CROSSED BY VEHICLES MAY BE SUBSTITUTED FOR THE PIPE.
- 7. THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION THAT WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO THE PUBLIC RIGHT-OF-WAY. THIS MAY REQUIRE PERIODIC TOP DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEAN OUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, WASHED, OR TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE

STABILIZED CONSTRUCTION ENTRANCE

NOT TO SCALE

CONSTRUCTION SEQUENCE

- PRIOR TO THE START OF ANY ACTIVITY, IT IS THE RESPONSIBILITY OF THE SITE'S SITE DEVELOPER (OR OWNER) TO FILE A NOTICE OF INTENT (NOI) FORM WITH THE ENVIRONMENTAL PROTECTION AGENCY (EPA) IN ORDER TO GAIN COVERAGE UNDER THE NPDES GENERAL PERMIT FOR STORM WATER DISCHARGES FROM CONSTRUCTION ACTIVITIES. A PRE CONSTRUCTION MEETING IS TO BE HELD WITH ALL DEPARTMENT HEADS PRIOR TO THE START OF CONSTRUCTION.
- 2. WETLAND BOUNDARIES ARE TO BE CLEARLY MARKED PRIOR TO THE START OF CONSTRUCTION.
- CUT AND REMOVE TREES IN CONSTRUCTION AREA AS REQUIRED OR DIRECTED.
- 4. INSTALL SILT FENCING, HAY BALES AND CONSTRUCTION ENTRANCES PRIOR TO THE START OF CONSTRUCTION. THESE ARE TO BE MAINTAINED UNTIL THE FINAL PAVEMENT SURFACING AND LANDSCAPING AREAS ARE ESTABLISHED.
- 5. CLEAR, CUT, GRUB AND DISPOSE OF DEBRIS IN APPROVED FACILITIES. THIS INCLUDES ANY REQUIRED DEMOLITION OF EXISTING STRUCTURES, UTILITIES, ETC.
- 6. CONSTRUCT AND/OR INSTALL TEMPORARY OR PERMANENT SEDIMENT AND/OR DETENTION BASIN(S) (INCLUDING RAIN GARDENS AND UNDERGROUND DETENTION SYSTEM) AS REQUIRED. THESE FACILITIES SHALL BE INSTALLED AND STABILIZED PRIOR TO DIRECTING
- STRIP LOAM AND PAVEMENT PER THE RECOMMENDATIONS OF THE PROJECT ENGINEER AND STOCKPILE EXCESS MATERIAL. STABILIZE STOCKPILE AS NECESSARY.
- 8. PERFORM PRELIMINARY SITE GRADING IN ACCORDANCE WITH THE PLANS.
- PREPARE BUILDING PADS TO ENABLE BUILDING CONSTRUCTION TO BEGIN.
- 10. INSTALL THE SEWER AND DRAINAGE SYSTEMS FIRST, THEN ANY OTHER UTILITIES IN ACCORDANCE WITH THE PLAN AND DETAILS. ANY CONFLICTS BETWEEN UTILITIES ARE TO BE RESOLVED WITH THE INVOLVEMENT AND APPROVAL OF THE ENGINEER.
- 11. ALL SWALES AND DRAINAGE STRUCTURES ARE TO BE CONSTRUCTED AND STABILIZED PRIOR TO HAVING RUN-OFF DIRECTED TO THEM.
- 12. DAILY, OR AS REQUIRED, CONSTRUCT TEMPORARY BERMS, DRAINAGE DITCHES, CHECK DAMS, SEDIMENT TRAPS, ETC., TO PREVENT EROSION ON THE SITE AND PREVENT ANY SILTATION OF ABUTTING WATERS AND/OR PROPERTY.
- 13. PERFORM FINAL FINE GRADING, INCLUDING PLACEMENT OF 'SELECT' SUBGRADE MATERIALS.
- 14. PAVE DRIVEWAYS AND ROADWAY WITH INITIAL 'BASE COURSE'.
- 15. PERFORM ALL REMAINING SITE CONSTRUCTION (i.e. BUILDING, CURBING, UTILITY CONNECTIONS, ETC.).
- 16. LOAM AND SEED ALL DISTURBED AREAS AND INSTALL ANY REQUIRED SEDIMENT AND EROSION CONTROL FACILITIES (i.e. RIP RAP, EROSION CONTROL BLANKETS, ETC.).
- 17. FINISH PAVING ALL DRIVEWAYS AND ROADWAY WITH 'FINISH' COURSE.
- 18. DRIVEWAYS AND ROADWAY SHALL BE STABILIZED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 19. ALL CUT AND FILL SLOPES SHALL BE SEEDED/LOAMED WITHIN 72 HOURS OF ACHIEVING FINISHED GRADE.
- 20. COMPLETE PERMANENT SEEDING AND LANDSCAPING.
- REMOVE TEMPORARY EROSION CONTROL MEASURES AFTER SEEDING AREAS HAVE BEEN 75%-85% ESTABLISHED AND SITE IMPROVEMENTS ARE COMPLETE. SMOOTH AND RE-VEGETATE ALL DISTURBED AREAS.
- 22. CLEAN SITE AND ALL DRAINAGE STRUCTURES, PIPES AND SUMPS OF ALL SILT AND DEBRIS.
- 23. INSTALL ALL PAINTED PAVEMENT MARKINGS AND SIGNAGE PER THE PLANS AND DETAILS.
- 24. ALL EROSION CONTROLS SHALL BE INSPECTED WEEKLY AND AFTER EVERY HALF-INCH OF RAINFALL.

SAGAMORE AVENUE CONDOMINIUMS

- 25. UPON COMPLETION OF CONSTRUCTION, IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO NOTIFY ANY RELEVANT PERMITTING
- AGENCIES THAT THE CONSTRUCTION HAS BEEN FINISHED IN A SATISFACTORY MANNER.

EROSION AND SEDIMENT CONTROL DETAILS

Project: 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE LOT 15: JOHN J. & COLLEEN HEBERT Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

SHEET 17 OF 22 JBE PROJECT NO. 21047

DRAWING No.



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10	3/4/22	REVISED PER NHDOT COMMENTS	DJM
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E-MAIL: JBE@. Services 603-772-4746 FAX: 603-772-0227 E-MAIL: JBE@JONESANDBEACH.COM

Name:	TRUCK TU	

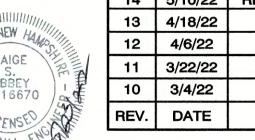
JRNING PLAN

1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE Owner of Record:

SAGAMORE AVENUE CONDOMINIUMS SHEET 18 OF 22 JBE PROJECT NO. **21047** LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219



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n Name:	TRUCK TURNING PLAN	
	THOOK TOTHING LAND	,

SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT Owner of Record: 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219 SHEET 19 OF 22 JBE PROJECT NO. **21047**



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Name:	TRUCK
	OACAMODE

TRUCK TURNING PLAN

Project: SAGAMORE AVENUE CONDOMINIUMS

Owner of Record:

1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT
54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

LOT 15: JOHN J. & COLLEEN HEBERT
54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173

LOT 15: JOHN J. & COLLEEN HEBERT
54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

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SHEET 20 OF 22 JBE PROJECT NO. **21047**



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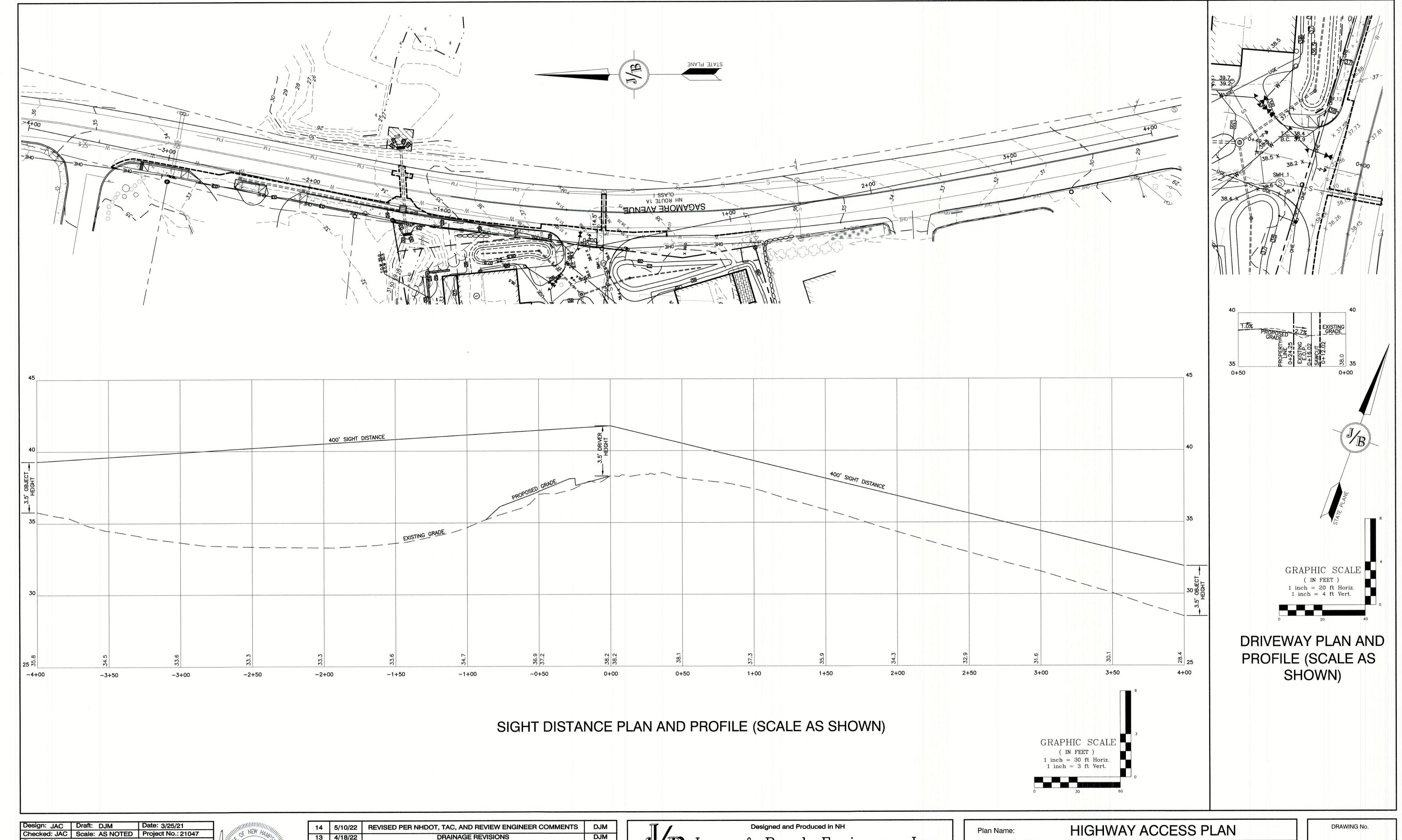
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TRUCK TURNING PLAN

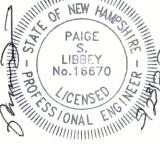
SAGAMORE AVENUE CONDOMINIUMS 1169 & 1171 SAGAMORE AVE., PORTSMOUTH, NEW HAMPSHIRE

LOT 14: COLLEEN HEBERT LOT 15: JOHN J. & COLLEEN HEBERT 54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173 54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

DRAWING No. SHEET 21 OF 22 JBE PROJECT NO. **21047**



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E-MAIL: JBE@JO	NESANDBEACH.COM	Owner of Necol	54 PIONEER RD, RYE, NH 03870 BK 2418 PG 173		

HIGHWAY ACCESS PLAN				
	SAGAMORE AVENU	E CONDOMINIUMS		
1169	& 1171 SAGAMORE AVE., PO	ORTSMOUTH, NEW HAMPSHIRE		
ord:	LOT 14: COLLEEN HEBERT	LOT 15: JOHN J. & COLLEEN HEBERT		

54 PIONEER RD, RYE, NH 03870 BK 5383 PG 219

